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Vortex coronagraphy from self-engineered liquid crystal spin-orbit masks

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We report on a soft route toward optical vortex coronagraphy based on self-engineered electrically tunable vortex masks made of liquid crystal topological defects. These results suggest that a nature-assisted technological approach to the fabrication of complex phase masks could be useful in optical imaging whenever optical phase singularities are at play.

OCIS codes: (260.6042) Singular optics; (160.3710) Liquid crystals; (050.4865) Optical vortices.

The observation of faint objects near a bright source of light is a basic challenge of high contrast imaging techniques such as the quest for extrasolar planets in astronomical imaging. This has led to the development of instruments called coronagraphs, which combine the high extinction of stellar light and the high transmission of a low level signal at small angular separation. Stellar coronagraphy was initiated more than 80 years ago when Lyot studied solar corona without an eclipse by selective occul tation of sunlight, placing an opaque disk in the focal plane of a telescope [1]. On the other hand, phase mask coronagraphs offer good performance for the observation of point like sources. An early version consisted of using a disk π phase mask [2] whose chromatic drawback arising from discrete radial phase step was solved a few years later by incorporating discrete radial [3] or azimuthal [4] phase modulation to the original design. Later on, continuous azimuthal phase ramps improved the approach [5,6] and led to the advent of optical vortex coronagraphy.

Vortex coronagraphs rely on the selective peripheral redis tribution of on axis light outside an area of null intensity at the exit pupil plane of the instrument, which is done by placing a spiraling phase mask in the Fourier plane characterized by a complex transmittance of the form $\exp(i\ell\phi)$, where the charge ℓ is an even integer and ϕ is the usual azimuthal angle in the transverse plane. This enables optimal on axis rejection of light by placing an iris (called Lyot stop) at the exit pupil plane, while the off axis weak signal is almost unaffected for an angular separation larger than the diffraction limit [7]. There are two families of optical vortex phase masks that rely on the scalar (phase) and vectorial (polarization degree of freedom) proper ties of light. The former case refers to the helical shaping of the wavefront from a refractive phase mask, whereas the latter one exploits the polarization properties of space variant birefringent optical elements. Indeed, inhomogeneous anisotropic phase masks endowed with azimuthal optical axis orientation of the form $\psi(\phi) = m\phi$ with *m* half integer and associated with half wave birefringent phase retardation lead to a vortex mask of charge $\ell = 2\sigma m$ for an incident on axis circularly polarized beam with helicity $\sigma = \pm 1$, as originally shown in [8] using form birefringence and, in [9], using true birefringence.

The achromatic features of the vectorial option versus its scalar counterpart [10,11] have eventually led to equip state of the art large instruments such as Keck, Subaru, Hale, Large Binocular Telescope, and Very Large Telescope with vectorial vortex coronagraphs. In practice, all these installations exploit vortex masks obtained either from brute force nanofabrication, where form birefringence arises from subwavelength material structuring [8], or liquid crystal polymers technology, where true birefringence is patterned on demand [12]. Still, these high tech "writing" processes ultimately suffer from fabrication constraints and finite resolution, preventing the creation of ideal material singularity, which implies various trade offs. One can mention the preferential use of natural, rather than a form birefringence option at shorter wavelengths [10], and the use of an opaque disk to reduce the detrimental influence of central misorientation of the engineered optical axis pattern [13,14]. The realization of higher order masks with even topological charges $\ell > 2$ [5] that are desirable for future extremely large telescopes [15] is another manufacturing challenge. Since the basic technological bottleneck can be identified as the man made technology itself, a nature assisted approach would likely open a novel generation of vortex masks.

Various kinds of spontaneously formed nematic liquid crys tal topological defects have been previously demonstrated to behave as natural [16,17] or field induced [18 20] vectorial optical vortex generators with even charge $|\ell| = 2$ and optimal beam shaping characteristics. Optical vortex masks realized with out the need for a machining technique have also been obtained from other mesophases such as cholesteric [21] and smectic [22] liquid crystals, but at the expense of efficiency. Here, we propose exploring the potential of self engineered liquid crystal vortex phase masks for high contrast imaging applications, in particular, in the case of optical vortex coronagraphy.

We choose the so called umbilical defects that appear in ho meotropic nematic liquid crystal films and negative dielectric anisotropy under a quasi static electric field and above a thresh old voltage $U = U^*$ of a few volts [23]. These defects are associated with optical axis orientation angle of the form $\psi(\phi) = m\phi + \psi_0$ with $m = \pm 1$ and ψ_0 a constant; see Figs. 1(a) and 1(b) for imaging between crossed linear polar izers. It has been shown previously that such defects behave as spin orbit optical vortex generators [19]. This can be de scribed by neglecting the diffraction inside the optical element itself given the circularly polarized incident field in the plane of the sample, $E(r)\mathbf{c}_{\sigma}$, where r = 0 refers to the defect location and $\mathbf{c}_{\sigma} = (\mathbf{x} + i\sigma \mathbf{y})/\sqrt{2}$ refers to the circular polarization basis. In the case of transparent media as is our case, the output light field can be expressed as [24]

$$\mathbf{E}_{\text{out}}(r,\phi) \propto E(r) \exp[i\Delta(r)/2] \{\cos[\Delta(r)/2] \mathbf{c}_{\sigma} + i \sin[\Delta(r)/2] \exp[i2\sigma\psi(\phi)] \mathbf{c}_{-\sigma} \}, \quad (1)$$

where $\Delta(r)$ is the *r* dependent birefringent phase retardation modeled following the work of Rapini [23]. Within such a description, one has $\Delta(r) = \delta(r/r_c)\Delta_{\infty}$, where $r_c = (L/\pi)(\mathcal{K}/\mathcal{K}_3)^{1/2}[(U/U^*)^2 \quad 1]^{-1/2}$ is the voltage dependent defect core radius with *L* being the nematic film thickness; $\mathcal{K} = K_2$ for m = +1, and $\psi_0 = \pi/2$ (our case) and $\mathcal{K} = (K_1 + K_2)/2$ for m = 1 whatever ψ_0 , with $K_{i=1,2,3}$ being the Frank elastic constant of splay, twist, and bend director dis tortions [25]; and Δ_{∞} is the voltage dependent asymptotic value of Δ at large *r*. The calculated voltage independent func tion $\delta(r/r_c)$, which describes how the retardance depends on the distance to the defect core, and reduced core radius r_c/L versus reduced voltage U/U^* are shown in Figs. 1(c) and 1(d).

From Eq. (1), the spin orbit generation of a spiraling optical phase with charge ± 2 for the helicity flipped output field com ponent is never ideal due to the space variant retardance, which is quantitatively evaluated by the purity

$$\eta = \int_0^\infty |E(r)|^2 \sin^2[\Delta(r)/2] r dr / \int_0^\infty |E(r)|^2 r dr,$$
 (2)

 $0 < \eta < 1$, while the spin orbit mask is described up to an un important phase factor by the complex amplitude transmittance

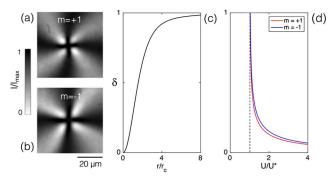


Fig. 1. (a) and (b) Typical images of nematic umbilical defects with a topological charge $m = \pm 1$ observed between crossed linear polar izers. (c) Calculated radial dependence of the function δ from Rapini's model. (d) Calculated reduced core radius r_c/L versus reduced voltage U/U^* for $m = \pm 1$ (red/blue curves).

$$\tau(r,\phi) = \sin[\Delta(r)/2] \exp[i\Delta(r)/2 + 2i\sigma\psi(\phi)].$$
 (3)

Looking for a complex transmittance of the form $\exp(i\ell\phi)$, one should ideally target an umbilic with $\Delta_{\infty} = \pi$ (that defines the voltage $U = U_{\pi}$ and a core radius r_c smaller than the char acteristic beam spot size w in the plane of the sample. Here, we choose a $L = 10 \ \mu m$ thick nematic film made from a glass cell (from EHC Ltd.) whose inner surface is provided with trans parent electrodes. The liquid crystal film is prepared from the nematic MLC 2079 (from Licristal) having a dielectric relative permittivity of $\epsilon_{\parallel} = 4.1$ along the molecular alignment and $\epsilon_{\perp} = 10.2$ perpendicular to it (tabulated data at 1 kHz fre quency) and refractive indices $n_{\parallel} = 1.64$ and $n_{\perp} = 1.49$ at a 589 nm wavelength. The Frank elastic constant of splay, twist, and bend director distortions [25] are $K_1 = 15.9$ pN (tabulated), $K_2 = 9.5$ pN (measured), and $K_3 = 18.3$ pN (tabulated), respectively. This gives $U^* = 1.83 \text{ V}_{\text{rms}}$ and $U_{\pi} =$ 2.52 V_{rms} [23], and $r_c = (2.4, 2.8) \ \mu m$ for $m = \pm 1$.

In practice, once U is set above U^* , a few defects remain at a fixed location in the sample after the annihilation dynamics between nearby topological defects with the opposite topologi cal charges has taken place. Typically, experiments are per formed a couple of hours or more after the voltage, whose steady value is set at U_{π} , has been switched on. Then, a defect is placed on axis in the focal plane (P_F) of a telescope, as de picted in Fig. 2(a), which sketches the main part of the optical arrangement used to simulate a vortex coronagraph in the lab oratory where starlight is mimicked by an on axis incident quasi plane wave. Experiments are performed using point like sources generated from He Ne lasers at a wavelength $\lambda =$ 633 nm and located in the focal plane of the microscope ob jectives (10×, NA = 0.25) with an overfilled entrance pupil. The obtained light beams are collimated by lenses with a 20 cm focal length, apertured by an iris with 25 mm diameter, and remotely redirected at an angle α from the optical axis z by mirrors. Lenses L_1 and L_2 [see Fig. 2(a)] are identical microscope objectives ($4\times$, NA = 0.1, entrance pupil radius R = 4.42 mm); the radii of I_1 and I_2 are $R_1 = 1$ and $R_2 = 0.75$ mm, respectively. This gives $w = 0.61\lambda/$ $(0.1R_1/R) = 17 \ \mu m$. The imaging of the sources is made by lens L₃ with a focal length of $f_3 = 30$ cm. The input circular polarization is ensured by the polarizer and quarter wave plate, whereas the contra circularly polarized field component after the optical vortex mask OVM is selected by another set of

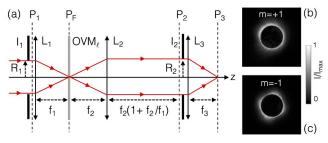


Fig. 2. (a) Optical setup. It consists of a set of irises $I_{1,2}$ and lenses $L_{1,2,3}$ with focal lengths $f_{1,2,3}$, and an optical vortex mask of the topo logical charge ℓ , OVM $_{\ell}$, placed in the Fourier plane P_F of the tele scope formed by lenses $L_{1,2}$. The planes $P_{1,2}$ refer to the entrance and exit pupil planes, respectively, while the plane P_3 refers to the imaging plane. The red lines refer to the ray optics tracing. (b) and (c) Rings of fire observed in the exit pupil plane P_2 for $m = \pm 1$.

quarter wave plates and polarizers (not shown in Fig. 2). Finally, all images are recorded by a 12 bit room temperature camera.

The coronagraphic behavior of our self engineered spin orbit masks is illustrated in Figs. 2(b) and 2(c) which show the so called "rings of fire" surrounding a dark area with a diameter $2R_1f_2/f_1$ in the exit pupil plane P_2 . The four fold rotational symmetry for m = 1 is reminiscent of the elastic anisotropy of the liquid crys tal. Indeed, while only the twist distortions are involved for m = +1, when $K_2 < K_1$, both chiral and splay distortions at play for m = 1 [23] break the axisymmetry; see [26] for recent numerical investigations. Ensuing starlight rejection is demon strated in Figs. 3(a) and 3(b) which refer to the image of the on axis source that is collected in the plane P_3 when the corona graph is "on" (i.e., presence of Lyot stop I_2) or "off" (i.e., I_2 is removed), while the azimuth averaged radial intensity profiles in the plane P_2 are shown as solid curves in Fig. 3(c).

Quantitatively, the coronagraphic performances are gauged from the rejection of on axis illumination. A peak to peak star light rejection ratio of $\mathcal{R}_{\text{peak,exp}} \approx 1000$ is obtained and is as sociated with a typical power rejection rate $\mathcal{R}_{\text{power,exp}} \approx 50$ defined as the ratio between the power outside and inside the Lyot stop:

$$\mathcal{R}_{\text{power}} = \int_{R_2}^{\infty} I_2(r) r \mathrm{d}r \Big/ \int_0^{R_2} I_2(r) r \mathrm{d}r, \qquad (4)$$

where $I_2(r)$ is the intensity profile in the plane P_2 . Statistics from 10 defects for $m = \pm 1$ are summarized in Fig. 4. The purity η shown in Fig. 4(a) is evaluated as the ratio between the power of the generated vortex beam (post selection circular polarizer is present) and the total output power (post selection circular polarizer is removed). The experimental data are $\eta_{exp} \simeq (0.55 \pm 0.02, 0.46 \pm 0.02)$ for $m = \pm 1$. Statistics of measured power rejection rates are shown in Fig. 4(b) which gives $\mathcal{R}_{power,exp} \simeq (46 \pm 9, 43 \pm 7)$ for $m = \pm 1$.

Simulations are carried out under the assumption of a para xial on axis plane wave impinging on the iris I_1 , namely by considering $E_1 \propto \operatorname{circ}(r/R_1)$ as the entrance pupil field in the plane P_1 , where $\operatorname{circ}(r/\rho) = 0$ for $r > \rho$ and $\operatorname{circ}(r/\rho) =$ 1 for $r < \rho$. Then, η is calculated by inserting the expression of starlight intensity profile in the plane P_F , namely $I_F = |\mathcal{F}[E_1]|^2$, in Eq. (2), where \mathcal{F} refers to the Fourier trans form. This gives $\eta_{\text{model}} = (0.80, 0.75)$ for $m = \pm 1$. On the

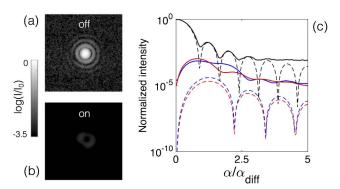


Fig. 3. (a) and (b) Typical on axis point like source images in the plane P_3 when the coronagraph is off/on, I_0 : maximal intensity in the off state, while the intensity range refers to the 4096 levels of the 12 bit camera. (c) Azimuth averaged angular intensity profile in off (black curve) and on (color curves) states. Solid curves, experimental data; dashed curves, simulations; red curves, m = +1; blue curves, m = 1.

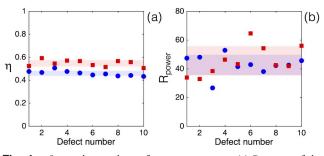


Fig. 4. Spin orbit masks performance statistics. (a) Purity η of the optical vortex generation process. (b) Power rejection rate \mathcal{R}_{power} . The colored area refers to the standard deviation region. Red square mark ers, m = +1; blue circle markers, m = -1.

other hand, $I_2(r) = |\mathcal{F}^{-1}[\tau(r, \phi)\mathcal{F}[E_1]]|^2$, where \mathcal{F}^{-1} refers to the Fourier transform, and gives $\mathcal{R}_{\text{peak,model}} \simeq (5 \times 10^4, 2 \times 10^4)$ for $m = \pm 1$. Finally, inserting the latter expression of $I_2(r)$ in Eq. (4) gives $\mathcal{R}_{\text{power,model}} \approx (3000, 1500)$ for $m = \pm 1$. As usual, in vortex coronagraphy, simulations predict better performances than experiments. Indeed, any source of material and optical imperfections is not taken into account. Still, our experimental values are rather promising for a first at tempt, noting that early [10,27] and recent [28] laboratory and on sky astronomical observations with an artificial vectorial vor tex mask reported a peak to peak stellar rejection ratio <100.

Next, we implement the coronagraphic observation of a "star/ planet" system. This is done by adding a faint off axis illumina tion (the "planet") at an angle $2\alpha_{\text{diff}}$ ($\alpha_{\text{diff}} = 0.61\lambda/R_1$ is the diffraction limit) from the on axis light (the "star") obtained from a distinct laser source. The experimental situation without a coronagraph is shown in Fig. 5(a), where the peak to peak in tensity ratio between the star and the planet in the imaging plane P_3 is $I_{\text{star}}/I_{\text{planet}} = 20$ for the purpose of demonstration. The latter ratio is drastically reduced to 0.15 when the vortex mask is electrically turned on; see Fig. 5(b). Data are compared with simulations taking the same conditions as in experiments.

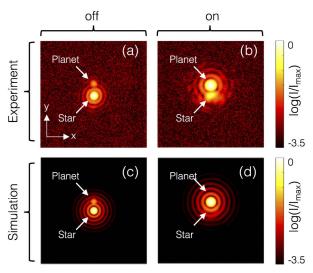


Fig. 5. Imaging a star/planet system when the coronagraph is off (without the Lyot stop, which gives a smaller point spread function than in the case when iris I_2 is present) and on. (a) and (b) Experimental data. (c) and (d) Simulations.

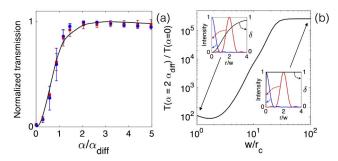


Fig. 6. (a) Transmitted power ratio $P_{\rm on}/P_{\rm off}$ as a function of the nor malized angular separation distance $\alpha/\alpha_{\rm diff}$ to the telescope axis for $m = \pm 1$. Markers, measurements with red/blue color for $m = \pm 1$. Solid curves, simulations. (b) Calculated ratio $T(2\alpha_{\rm diff})/T(0)$. Insets: normalized intensity profiles of on axis ($\alpha = 0$) and off axis ($\alpha = 2\alpha_{\rm diff}$) point sources and δ in the plane P_F for $w/r_c = 1$ and $w/r_c = 100$.

Namely, the images of the star and the planet are calculated from $I_i = |\mathcal{F}[E_i]|^2$ when the coronagraph is off (Lyot stop is removed) and $I_j = |\mathcal{F}[\operatorname{circ}(r/R_2)\mathcal{F}^{-1}[\tau(r,\phi)\mathcal{F}[E_j]]|^2$ when the coronagraph is on, with $E_{\text{star}} = \sqrt{20 \operatorname{circ}(r/R_1)}$ and $E_{\text{planet}} =$ $\operatorname{circ}(r/R_1) \exp(i2k\alpha_{\operatorname{diff}}y), k = 2\pi/\lambda$. More quantitatively, the coronagraphic throughput is experimentally assessed from the transmitted power ratio $P_{\rm on}/P_{\rm off}$ of the light field passing through the Lyot stop when the coronagraph is on and off as a function of $\alpha/\alpha_{\text{diff}}$. Figure 6(a) summarizes the data obtained for three independent defects for each *m*, where the markers refer to the experiment while the solid curve corresponds to simula tions, which exhibit good agreement. Moreover, the central apodization effect of the spin orbit vortex mask due to the r de pendent retardance profile [Fig. 1(a)] is illustrated in Fig. 6(b) which shows the ratio $T(2\alpha_{\text{diff}})/T(0)$ between the transmission of the two identical off axis ($\alpha = 2\alpha_{diff}$) and on axis ($\alpha = 0$) point sources as a function of the ratio w/r_c when the corona graph is on, taking $\Delta_{\infty} = \pi$, $R_1 = 1$ mm, and $R_2 = 0.75R_1$, whatever r_c . The apodization drawback manifests typically for $w < 10r_c$ whereas, for $w > 10r_c$, the asymptotic high contrast regime is reached. The cutoff ratio for w/r_c , of course, decreases with the separation between the sources. Finally, note that present self engineered liquid crystal spin orbit vortex masks are not restricted to operating at a predetermined central wave length since Δ_{∞} is electrically tunable as is the case of their ar tificial self engineered counterparts [29].

More broadly, the proposed nature assisted approach to the fabrication of singular phase masks goes beyond the possible use in optical vortex coronagraphy, and includes stimulated emis sion depletion microscopy [30] and spiral phase contrast micros copy [31]. Moreover, the proposed approach is not restricted to pure phase masks and opens the way to self engineered apod ization masks that are heavily used in coronagraphy [32], which may involve the use of either transparent or absorbing liquid crystal mesophases. Further work is needed, in particular regard ing large vortex mask size issues as usually requested in low numerical aperture telescopes.

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