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# CO<sub>2</sub> and CH<sub>4</sub> Separation by Adsorption Using Cu-BTC Metal–Organic Framework

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Molecular simulations have shown that the metal–organic framework Cu-BTC (Cu<sub>3</sub>(BTC)<sub>2</sub>) is an interesting candidate for the separation of CO<sub>2</sub> by adsorption. In this work, the first experimental binary and ternary adsorption data of CO<sub>2</sub>, CH<sub>4</sub>, and CO on the Cu-BTC are reported. These data are analyzed and compared with coadsorption models that are built from pure component isotherm data. Cu-BTC has a CO<sub>2</sub>/CH<sub>4</sub> selectivity of ~8 and a high delta loading (=difference between adsorption capacity under conditions of adsorption and desorption) and therefore appears to be a good compromise between zeolites, with high selectivity for CO<sub>2</sub>, but low delta loadings, and activated carbons, with high delta loadings, but low selectivity, for pressure swing adsorption applications.

## Introduction

Hydrogen is mainly produced by steam reforming of natural gas, a process which generates a synthesis gas mixture containing H<sub>2</sub>, CO<sub>2</sub>, CO, and CH<sub>4</sub> (and eventually some other impurities). Pure H<sub>2</sub> is obtained from this synthesis gas mixture by pressure swing adsorption (PSA). A series of different adsorbents remove the impurities (CO<sub>2</sub>, CO, and CH<sub>4</sub>), and H<sub>2</sub> of very high purity leaves the adsorber column at high pressure. The adsorbed impurities are then recovered from the column by desorption during a low-pressure purge (which explains the name pressure swing). The CO<sub>2</sub>–CH<sub>4</sub>–CO purge gas is normally used as combustible for the steam reformer, but in view of the current concerns about CO<sub>2</sub> emissions this is not the ideal solution. Methods would be needed to produce a separate waste stream of pure CO<sub>2</sub>, which could then be sequestered, and recycle only CH<sub>4</sub> and CO as fuels to the steam reformer. For that purpose, adsorbents have to be developed that selectively adsorb CO<sub>2</sub>, i.e., that separate CO<sub>2</sub> from CO and CH<sub>4</sub>.

CO<sub>2</sub> selective adsorbents are also needed in the purification of biogas, which is essentially a mixture of CO<sub>2</sub> and CH<sub>4</sub>. The objective is to produce pure CH<sub>4</sub> as a fuel and to lose as little CH<sub>4</sub> as possible in the CO<sub>2</sub> waste stream.

Recently metal–organic frameworks (MOFs) have attracted attention as adsorbents for the separation of CO<sub>2</sub> and CH<sub>4</sub>.<sup>1–4</sup> These new microporous materials, which are formed by the combination of metallic clusters with organic ligands, present high adsorption capacities and could potentially be used for the separation of CO<sub>2</sub>, CH<sub>4</sub>, and CO.<sup>5,6</sup> In this study, we focus on the Cu<sub>3</sub>(BTC)<sub>2</sub> or Cu-BTC or HKUST-1.<sup>7</sup> This MOF is easily synthesized from nonexpensive primary compounds and is also commercially available. This microporous material is made of copper clusters linked to each other via trimesic acid (Figure 1). It forms a structure presenting a large pore surrounded by eight small pores called side pockets. The window between large pore and side pocket exhibits a triangular shape limited by trimesic acid with a window size of 4.6 Å. Recent papers compared the experimental adsorption of pure CH<sub>4</sub><sup>8–10</sup> and pure CO<sub>2</sub>,<sup>8,11–17</sup> and several studies presented molecular simulations of the adsorption of the CO<sub>2</sub>–CH<sub>4</sub> binary mixtures, predicting

a high selectivity of Cu-BTC for CO<sub>2</sub>.<sup>9,18–22</sup> Surprisingly, no experimental data of the mixture adsorption are yet available, but such data are needed if we want to develop new adsorption processes based on Cu-BTC.

In this paper, we therefore focus on coadsorption measurements of binary and ternary mixtures of CO<sub>2</sub>, CH<sub>4</sub>, and CO on Cu-BTC. The experimental coadsorption results are compared to predictions from coadsorption models that rely on pure component isotherms only. Finally, we compare the performance of Cu-BTC in the separation of synthesis gas mixtures by PSA to conventional adsorbents, i.e., activated carbons and zeolite Na–X.

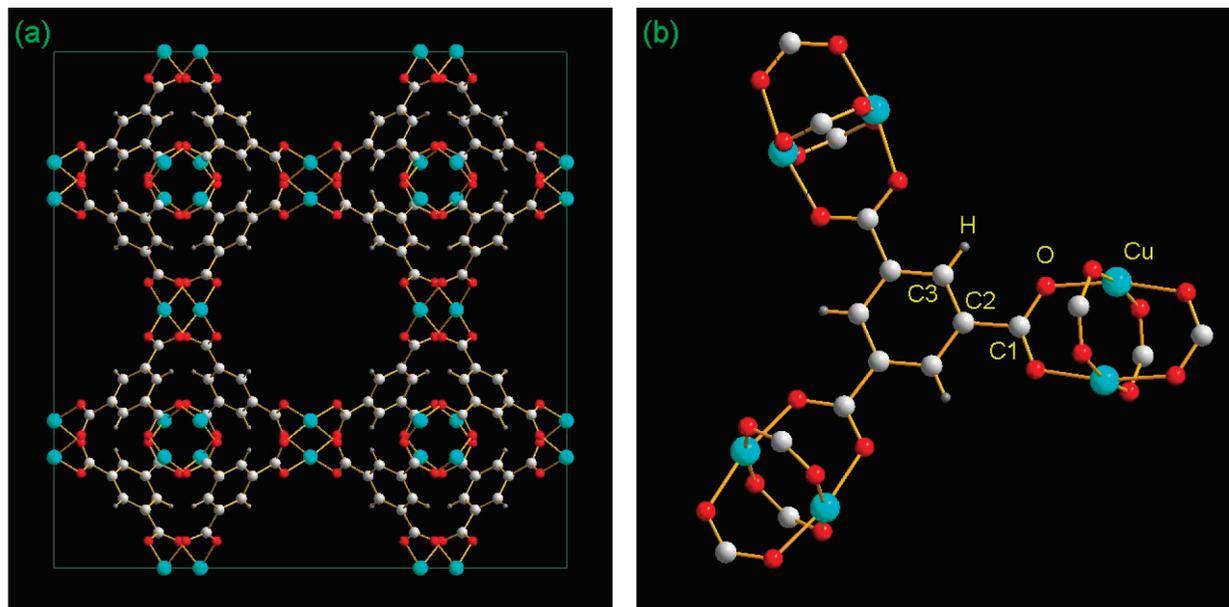
## Experimental Section

**Synthesis.** Cu-BTC has been synthesized according to the modus operandi of Bordiga et al.<sup>23</sup> A 30.51 g amount of CuNO<sub>3</sub>·3H<sub>2</sub>O was dissolved in a 500 mL 50/50 (v/v) water–ethanol mixture. After adding 17.84 g of trimesic acid, the solution was filled in a 1 L Teflon liner placed in an autoclave. It was heated to 393 K for 24 h and then filtered and washed with ethanol.

**Characterization.** A Brunauer–Emmett–Teller (BET) surface area determination was carried out using a Micromeritics ASAP 2000 instrument. Before measurement, the sample was outgassed under secondary vacuum at 423 K overnight. X-ray diffraction (XRD) patterns were recorded with a Bruker AXS D4 Endeavor diffractometer (2θ values between 2 and 60° with a step of 60 s; 1 step, 0.02°; Cu Kα radiation with a wavelength of 1.5406 Å) on a dried sample of Cu-BTC as powder. Thermogravimetric (TG) analysis was carried out with a Netzsch TG 209 F1 apparatus under a helium atmosphere at 100 kPa controlled by a flow meter with a flow rate of 3 NL·h<sup>-1</sup>. A first measurement was performed from 296 K up to 773 K with a temperature rate of 5 K·min<sup>-1</sup> to record a complete TG analysis. In the aim to check the thermal stability of the Cu-BTC sample, a second TG analysis was recorded, cycling the temperature with a rate of 3 K·min<sup>-1</sup> from 298 to 473 K, and a 15 min hold; cycles were repeated 5 times.

**Gravimetric Measurements.** Pure CO<sub>2</sub>, CH<sub>4</sub>, and CO adsorption measurements were carried out using a high-pressure magnetic suspension balance marketed by Rubotherm (Rubotherm Präzisionsmesstechnik GmbH).<sup>24,25</sup> Approximately 1 g of sample was used for the experiments. The material was

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**Figure 1.** (a) Unit cell crystal structure of the Cu-BTC along the [100] direction. (b) Cluster of the Cu-BTC. (Cu, green; O, red; C, white; H, gray).

activated and outgassed between each experiment under secondary vacuum at 448 K with a temperature ramp of  $1 \text{ K} \cdot \text{min}^{-1}$ . The buoyancy effect of the gas phase on the adsorbent volume and on the volume of the adsorbed phase, which is supposed to be equal to the micropore volume of the solid, is corrected for, so as to determine the absolute adsorbed mass.<sup>26</sup> We prefer here to work with absolute adsorbed amounts instead of excess adsorbed amounts, to facilitate the comparison with the results of breakthrough experiments. The gas density is determined using an appropriate equation of state (EoS).<sup>27,28</sup> The adsorbent volume is evaluated by measuring the buoyancy effect of helium, supposing that helium does not adsorb. Helium density is determined using a modified Benedict–Webb–Rubin EoS.<sup>29</sup>

**Breakthrough Curve Measurements.**  $\text{CO}_2$ – $\text{CH}_4$  binary and  $\text{CO}_2$ – $\text{CH}_4$ – $\text{CO}$  ternary mixture adsorption measurements were carried out using a homemade breakthrough curve apparatus, allowing one to perform measurements from atmospheric pressure up to 5.0 MPa (see the Supporting Information for more details). Gas mixtures were generated in situ. The sample (2.89 g) was packed into the column as powder (not pelletized) and was activated and outgassed at 448 K (rate of  $1 \text{ K} \cdot \text{min}^{-1}$ ) under a helium flow of  $1 \text{ N} \cdot \text{L} \cdot \text{h}^{-1}$ . Breakthrough curve measurements were carried out in two steps: The feed gas mixture (total gas flow rate is  $4 \text{ N} \cdot \text{L} \cdot \text{h}^{-1}$ ) is first injected in the column, which is under helium atmosphere at the pressure of the experiment. This method allows one to evaluate the adsorbed amount of  $\text{CO}_2$ , but uncertainties on the determination of  $\text{CH}_4$  are large due to the roll-up effect (vide infra). Therefore, a second experiment is carried out. The  $\text{CO}_2$ – $\text{CH}_4$  mixture is injected on a  $\text{CO}_2$ -presaturated column at the pressure of the experiment. This method yields a  $\text{CH}_4$  breakthrough curve without roll-up and, thus, reduces the uncertainty of the evaluation of the first moment of the  $\text{CH}_4$  breakthrough curve. The breakthrough experiments were carried out between 0.1 and 1.0 MPa. The pressure drop over the column was always less than 0.005 MPa.

The (absolute) adsorbed amount is calculated from the first moment of the breakthrough curve (after correction for the dead time) by the equation

$$q_i = \frac{C_i}{m_{\text{ads}}} \left( Q\mu - V_{\text{col}} + \frac{m_{\text{ads}}}{\rho_{\text{grain}}} \right) \quad (1)$$

The selectivity is calculated as

$$S_{1,2} = \frac{q_1/y_1}{q_2/y_2} \quad (2)$$

where  $q_i$  is the adsorbed amount of compound  $i$  and  $y_i$  is the mole fraction of compound  $i$  in the gas phase. On the basis of reproducibility measurements as well as theoretical calculations of the error margin, we estimate that the error of our selectivity values is approximately 20%.

**Breakthrough Curves Model.** The main assumptions of the model are as follows: (1) The flow pattern is described by the axially dispersed plug-flow model. (2) The column is isothermal. (3) Frictional pressure drop through the column is negligible. (4) The variation of fluid velocity along the column length, as determined by the global mass balance, is accounted for. (5) An external film resistance between the fluid and the crystal surface is assumed (in practice, this resistance was found to be negligible in our experimental conditions; it was nevertheless kept in the model, for numerical considerations). (6) Diffusion in the crystal follows Fick's law. The driving force is the gradient of adsorbed phase concentration, and the diffusion coefficient is constant. Using the above hypotheses, a set of well-known equations can be established (see Table 1).

Equations were written in the collocation form, thus reducing the set of partial differential equations to a set of algebraic and ordinary differential equations. These equations were then numerically integrated using the IMSL DASPG routine, based on Petzold–Gear's integration method.

## Results

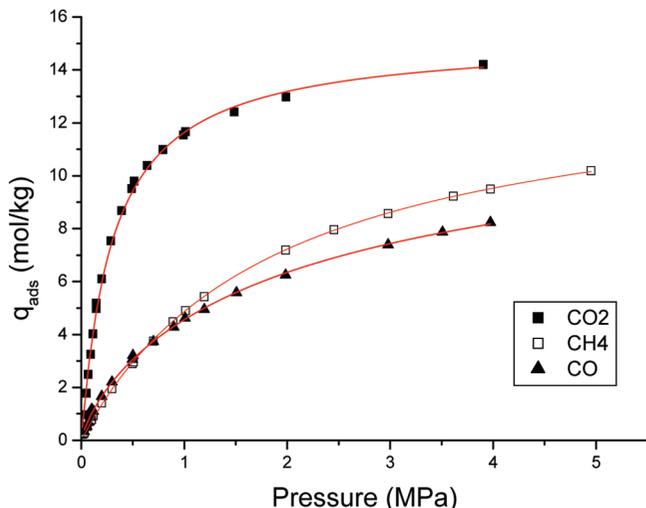
**Characterization of the Materials.** The XRD pattern of our Cu-BTC sample is similar to the theoretical one. The material was stable up to 500 K. The  $\text{N}_2$  isotherm at 77 K exhibits a kink, which can be attributed to the presence of the side pockets and the large pores.<sup>30–33</sup> The BET surface area is  $2211 \text{ m}^2 \cdot \text{g}^{-1}$ , and the micropore volume is  $0.813 \text{ cm}^3 \cdot \text{g}^{-1}$  (see the Supporting Information for more details).

**Single Component Adsorption Measurements.** Adsorption isotherms of pure  $\text{CO}_2$ ,  $\text{CO}$ , and  $\text{CH}_4$  have type I shapes (see Figure 2) according to the IUPAC classification.<sup>34</sup> A hysteresis

**Table 1. Equations of the Breakthrough Curve Model**

fluid phase	$\frac{\partial C_i}{\partial t} = D_L \frac{\partial^2 C_i}{\partial z^2} - \frac{\partial v C_i}{\partial z} - \left( \frac{1 - \varepsilon_i}{\varepsilon_i} \right) \frac{3}{R_c} k_i (n_i^* - n_i _{r=R_c})$ $\frac{\partial v C_i}{\partial z} = v \frac{\partial C_i}{\partial z} + C_i \frac{\partial v}{\partial z}$ $\frac{\partial C_i}{\partial z} \Big _{z=L} = 0$ $D_L \frac{\partial C_i}{\partial z} \Big _{z=0} = -v_0 (C_i _{z=0-} - C_i _{z=0+})$
velocity variation	$C_T \frac{\partial v}{\partial z} = - \frac{1 - \varepsilon_i 3k_i}{\varepsilon_i R_c} \sum_{j=1}^N (n_i^* - n_j _{r=R_c})$
crystal	$\frac{\partial n_i}{\partial t} = \frac{D_c}{r^2} \frac{\partial}{\partial r} \left( r^2 \frac{\partial n_i}{\partial r} \right)$ $\frac{\partial n_i}{\partial r} \Big _{r=0} = 0$ $D_c \frac{\partial n_i}{\partial r} \Big _{r=R_c} = k_i (n_i^* - n_i _{r=R_c})$
thermodynamic equilibrium conditions	$n_i^* = n_{i,\text{sat}} \frac{B_i C_i}{1 + \sum_j B_j C_j}$

is not observed. The maximum adsorbed quantity of CO<sub>2</sub> is 14 mmol·g<sup>-1</sup> (135 molecules·(unit cell)<sup>-1</sup>), CO, and CH<sub>4</sub> did not reach saturation in our measurements. The CO<sub>2</sub> isotherm is similar to those already measured by several authors,<sup>8,11,14,16</sup> except for Cu-BTC prepared in a mixture of water–ethanol–DMF (DMF = dimethylformamide)<sup>11</sup> or prepared in a water–ethanol mixture but washed with methanol.<sup>16</sup> It is well-known that it is difficult to remove DMF entirely from the pores of Cu-BTC, which results in a reduced adsorption capacity.<sup>35</sup> Our results for the adsorption of CH<sub>4</sub> are also similar to previous measurements<sup>8,15</sup> except for Cavenati et al.<sup>14</sup> who obtained smaller adsorbed quantities on a pelletized sample.



**Figure 2.** Absolute adsorbed amounts of pure CO<sub>2</sub> (full squares), CH<sub>4</sub> (open squares), and CO (triangles) at 303 K and the corresponding Langmuir (for CO<sub>2</sub> and CH<sub>4</sub>) and Langmuir–Freundlich fits (for CO).

**Table 2. Parameters of the Langmuir and Langmuir–Freundlich Isotherms That Fit Best the Experimental Isotherms of Pure CO<sub>2</sub>, CO, and CH<sub>4</sub> at 303 K**

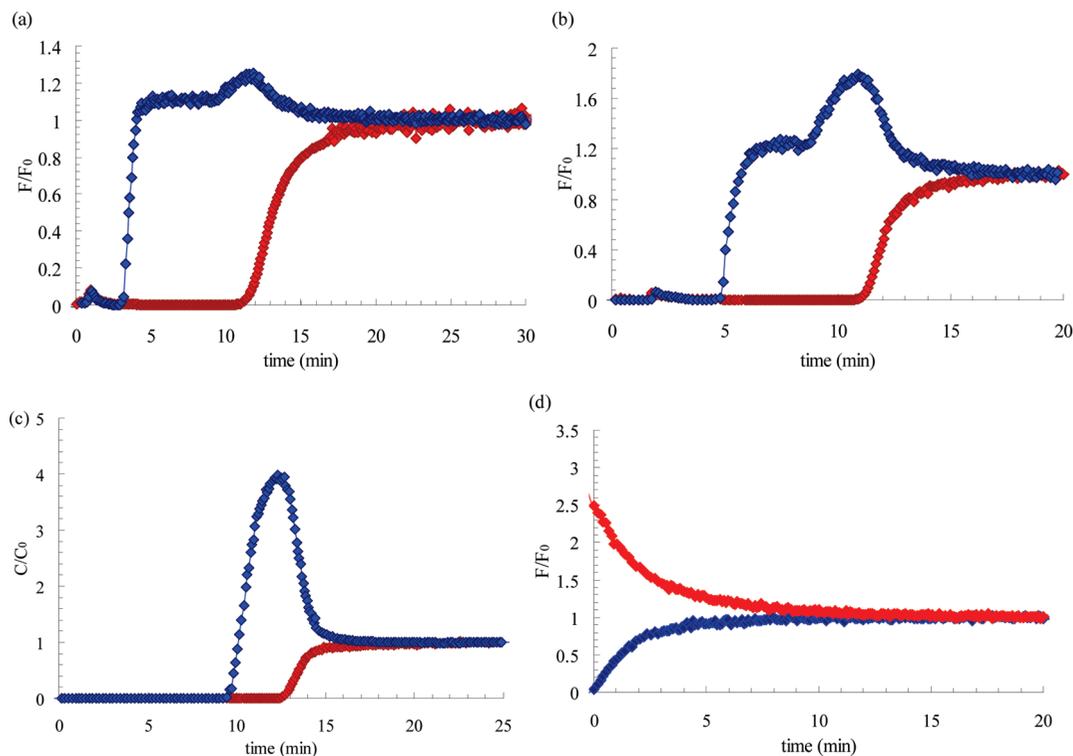
	CO			
	CO <sub>2</sub>	CH <sub>4</sub>	Langmuir	Langmuir–Freundlich
$q_{\text{sat}}$ (mmol·g <sup>-1</sup> )	15.21	14.00	10.44	13.45
$b$ (MPa <sup>-1</sup> )	3.25	0.533	0.818	0.512
$\xi$	1	1	1	0.801

In analogy to the N<sub>2</sub> isotherm at 77 K, we would have expected to find a step or a kink in the isotherms of CO<sub>2</sub> and CH<sub>4</sub>, due to the presence of two types of pores, i.e., the side pockets and the large pores. In practice such a kink cannot be distinguished in isotherms of Figure 2. When fitting the isotherms with a dual-site Langmuir model, using a minimization of the square residual, the fit converges to the equal values of the affinity coefficients of the two sites, i.e., to a single-site Langmuir isotherm. Hence, from a macroscopic point of view, the two types of pores are not sufficiently different to be distinguishable as two separate adsorption sites in the isotherms. Table 2 compiles the parameters of the Langmuir and Langmuir–Freundlich isotherms that fit best the experimental values. The Langmuir–Freundlich model allows one to fit the CO isotherm slightly better than a simple Langmuir equation.

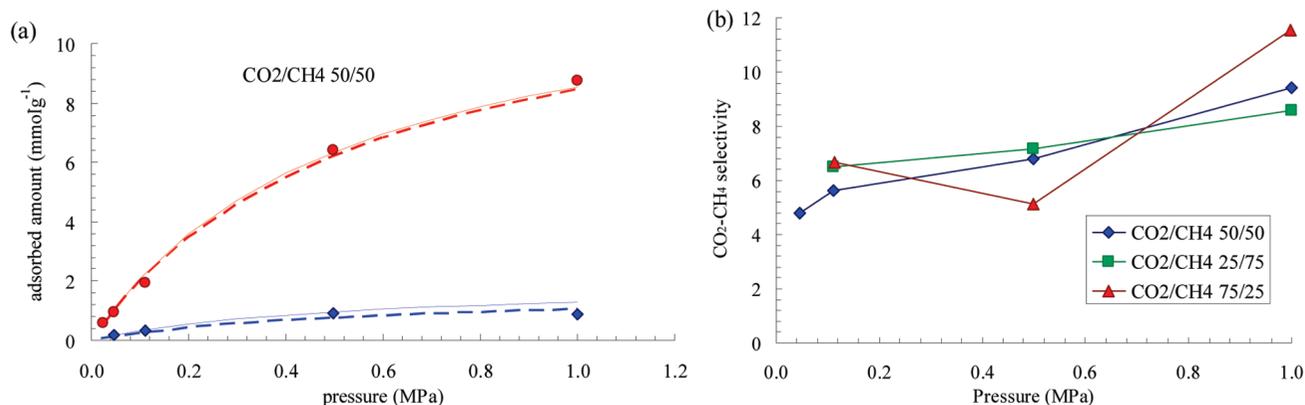
**Binary Mixture Adsorption.** Breakthrough curve experiments were carried out at 303 K to evaluate the separation performance of the Cu-BTC. Three mixtures (25–75, 50–50, and 75–25 CO<sub>2</sub>–CH<sub>4</sub>) were tested at three pressures (0.1, 0.5, and 1.0 MPa). Figure 3 shows the breakthrough curves of the three mixtures at 0.5 MPa (the complete set of breakthrough curves is given in the Supporting Information). For all of the mixtures, CH<sub>4</sub> breaks first, testifying that it adsorbs least. For the first mixture, i.e., 25–75 CO<sub>2</sub>–CH<sub>4</sub>, the breakthrough curve of CH<sub>4</sub> exhibits a double roll-up. The first part of the roll-up corresponds to the partial desorption of CH<sub>4</sub> due to the adsorption of CO<sub>2</sub> (the CH<sub>4</sub> flow rate temporarily exceeds the feed flow rate). An additional peak is observed just before CO<sub>2</sub> breaks through the column: this peak is attributed to a temperature wave that accompanies (slightly runs ahead of) the concentration front of CO<sub>2</sub>, due to the exothermic adsorption of CO<sub>2</sub>. This temperature wave causes a rapid desorption of CH<sub>4</sub>. The higher the concentration of CO<sub>2</sub> in the feed, the more this thermal effect becomes mixed with the classical roll-up (in particular for the 75–25 CO<sub>2</sub>–CH<sub>4</sub> mixture).

The roll-up increases the uncertainty in the determination of the first moment of the CH<sub>4</sub> breakthrough curve. To determine the adsorbed quantity of CH<sub>4</sub> more precisely, a second experiment is carried out: the Cu-BTC sample is initially saturated under CO<sub>2</sub> atmosphere at the pressure of the experiment, and the CO<sub>2</sub>–CH<sub>4</sub> mixture is then injected. In this case, the breakthrough curve of CH<sub>4</sub> has a classical shape; i.e., the roll-up is avoided (Figure 3d), but since there are no hysteresis effects, the adsorbed amount of CH<sub>4</sub> at the end of the experiment is the same as in the direct breakthrough (He → CO<sub>2</sub>/CH<sub>4</sub>).

Figure 4a shows the adsorbed amount of CH<sub>4</sub> and CO<sub>2</sub> for the equimolar mixture as a function of pressure (see the Supporting Information for other compositions). The CO<sub>2</sub>–CH<sub>4</sub> selectivity (Figure 4b) is between 4.8 and 11.5 and has the tendency to increase at higher pressure but does not depend much on the composition of the gas mixture. The deviating values for the 75–25 CO<sub>2</sub>–CH<sub>4</sub> mixture can be attributed to the higher uncertainty of the results when the mixture is poor in CH<sub>4</sub>. Cu-BTC is less selective than zeolite Na–X or Na–Y



**Figure 3.** Breakthrough curve of  $\text{CO}_2$  (red) and  $\text{CH}_4$  (blue) at 0.5 MPa and 303 K for the 25–75  $\text{CO}_2$ – $\text{CH}_4$  mixture (a), 50–50 mixture (b), and the 75–25 mixture (c) and the 50–50 mixture on a column presaturated with  $\text{CO}_2$  (d).



**Figure 4.** (a) Co-adsorption isotherm of the equimolar mixture of  $\text{CO}_2$  (circles) and  $\text{CH}_4$  (diamonds) at 303 K. Full lines represent the Langmuir model based on single-component isotherms; dashed thick lines, ideal adsorbed solution theory (IAST); dashed thin lines, the Langmuir model based on binary breakthrough experiments. (b)  $\text{CO}_2$ – $\text{CH}_4$  selectivity as a function of pressure for the three gas mixtures.

in the same experimental conditions<sup>36</sup> but significantly more selective than activated carbons.<sup>37</sup>

We wanted to verify whether it is possible to predict the coadsorption of  $\text{CO}_2$  and  $\text{CH}_4$  from the single-component isotherms, using either a simple multicomponent Langmuir model (eq 3) or ideal adsorbed solution theory (IAST).<sup>38</sup>

$$q_i = q_{i,\text{sat}} \frac{b_i y_i}{1/p + b_{\text{CO}_2} y_{\text{CO}_2} + b_{\text{CH}_4} y_{\text{CH}_4}} \quad (3)$$

Figure 4 shows the coadsorption data calculated from eq 3 using the  $b$  and  $q_{\text{sat}}$  values of Table 1 (full lines). The selectivity in the Langmuir model is constant ( $S = b_{\text{CO}_2} q_{\text{sat},\text{CO}_2} / (b_{\text{CH}_4} q_{\text{sat},\text{CH}_4}) = 6.6$ ). Hence, the Langmuir model does not describe the small increase in selectivity with pressure that was observed experimentally. It therefore slightly underestimates the adsorbed amount of  $\text{CO}_2$  at high pressure and overestimates  $\text{CH}_4$ . When using IAST, the selectivity slightly increases with pressure (from

6.6 to 7.0), but the improvement is not significant. We have also observed that the IAST calculations are quite sensitive to the isotherm model that is used. For example, replacing a Langmuir isotherm by a Langmuir–Freundlich isotherm hardly changes the quality of the fit of the experimental pure component  $\text{CO}_2$  isotherm but leads to a much stronger evolution of selectivity with pressure in IAST. For the use in breakthrough curve or PSA simulations, IAST also has the disadvantage of strongly increasing the computation time compared to the Langmuir model (eq 3).

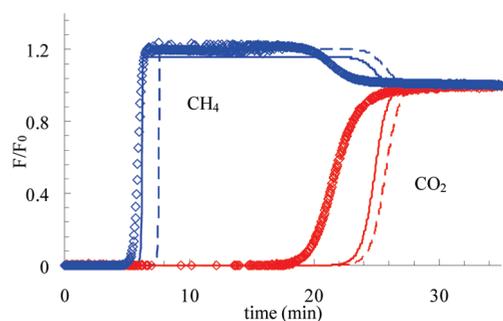
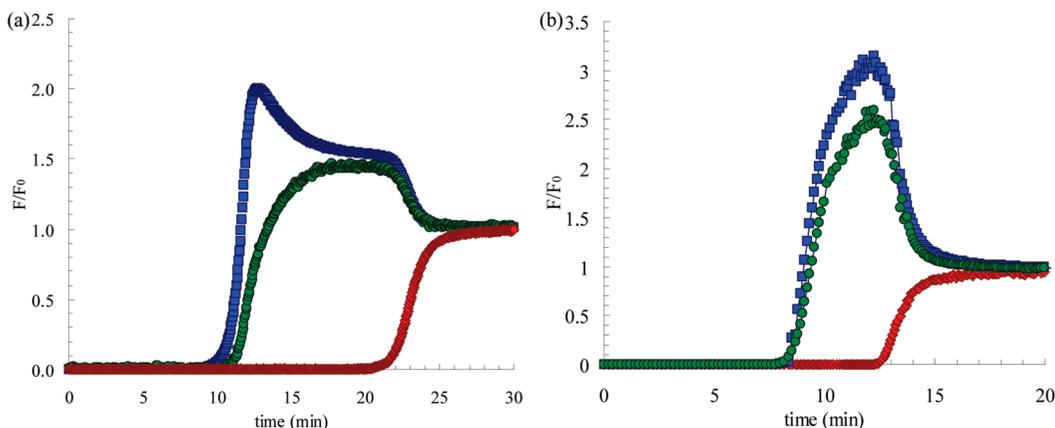
We therefore thought that the best match with the breakthrough results would be obtained by fitting the Langmuir eq 3 with our coadsorption data (nine points, i.e., three compositions at three pressures). The new parameters are given in Table 3. The average selectivity is now 8.1. The quality of the fit of the experimental data hardly changes for  $\text{CO}_2$  but improves for  $\text{CH}_4$  at high pressure (dashed line in Figure 4).

**Table 3. Single-Site Langmuir Parameters Obtained by Fitting the Binary CO<sub>2</sub>–CH<sub>4</sub> Mixture Experimental Data**

	CO <sub>2</sub>	CH <sub>4</sub>
$q_{\text{sat}}$ (mmol·g <sup>-1</sup> )	15.67	10.18
$b$ (MPa <sup>-1</sup> )	3.02	0.577

**Breakthrough Curve Simulations.** The input parameters of the model are listed in Table S1 and Table S2 of the Supporting Information. The axial dispersion coefficient is calculated from well-known correlations.<sup>39</sup> We compare two coadsorption Langmuir isotherms (eq 3), based on the parameters of Tables 2 and 3, respectively, i.e., either based on the pure component isotherms or on the coadsorption data. The only unknown parameters are the values of the diffusion coefficients of CO<sub>2</sub> and CH<sub>4</sub>. For comparison with other MOFs, the CO<sub>2</sub> diffusion coefficient has been estimated (by uptake measurements) to be  $7.9 \times 10^{-13}$  and  $1.72 \times 10^{-8}$  m<sup>2</sup>·s<sup>-1</sup> for the MOF-5,<sup>40,41</sup> and QENS yields a value of  $10^{-8}$  m<sup>2</sup>·s<sup>-1</sup> for the MIL-47(V).<sup>42</sup> The range of diffusion coefficients of CO<sub>2</sub> in zeolite Na–X is between  $6.49 \times 10^{15}$  and  $3.4 \times 10^{-10}$  m<sup>2</sup>·s<sup>-1</sup>, depending on the measurement methods.<sup>43–49</sup> The discrepancies between these values have already been discussed by Kärger and Ruthven.<sup>50</sup> We chose, quite arbitrarily, an intermediate value of  $1 \times 10^{-10}$  m<sup>2</sup>·s<sup>-1</sup> for both CO<sub>2</sub> and CH<sub>4</sub>.

Figure 5 compares the simulated breakthrough curve obtained with the two coadsorption isotherms with the experimental curve. None of the two simulations fits the experimental curve of CO<sub>2</sub> well, because both isotherm models overestimate the equilibrium adsorption capacity by at least 10%. We have varied the isotherm parameters and the diffusion coefficients and have observed that the steepness of the breakthrough curve depends

**Figure 5.** Breakthrough curves of the CO<sub>2</sub>–CH<sub>4</sub> equimolar mixture at 303 K and 0.1 MPa on the Cu-BTC: experimental data (diamonds), simulated data based on pure component isotherms (dashed line), and simulated data based on coadsorption isotherms (full line).**Figure 6.** Breakthrough curve of CO<sub>2</sub> (red), CH<sub>4</sub> (blue), and CO (green) at 0.1 (a) and 1.0 MPa (b) at 303 K for the 70–15–15 CO<sub>2</sub>–CH<sub>4</sub>–CO mixture.

very sensibly on the isotherm parameters and on the order of magnitude of the diffusion coefficients. Since it is very difficult to reproduce the experimental isotherm with high precision, it follows that we cannot extract a reliable estimation of the diffusion coefficient from the breakthrough curve simulations.

**Ternary Mixture Adsorption.** Finally CO<sub>2</sub>–CH<sub>4</sub>–CO ternary experiments were carried out at 0.1 and 1.0 MPa (Figure 6). The breakthrough curves show that at 0.1 MPa CH<sub>4</sub> breaks through first, followed by CO. At 1.0 MPa CH<sub>4</sub> and CO break simultaneously through the column. Thus, at low pressure the CO<sub>2</sub>–CH<sub>4</sub> selectivity is higher than the CO<sub>2</sub>–CO selectivity, but at high pressures both values become equivalent. This corresponds to the observation that the pure component isotherms cross each other at ~0.7 MPa (Figure 2). The higher affinity for CO at low pressure is most probably due to the direct interaction of CO with the Cu sites.

Since the ternary mixture CO<sub>2</sub>–CH<sub>4</sub>–CO represents a typical synthesis gas composition, we have used these data to calculate an empirical parameter that is a very important criterion for adsorbent selection: the delta loading or working capacity. The delta loading is defined as the difference of adsorbed amounts of one compound of the mixture between high pressure, i.e., at the pressure of the production step in the PSA process, and low pressure, i.e., at the pressure of the regeneration step in the process. The delta loading is therefore an indication of the adsorbent capacity in cyclic conditions. With our ternary mixture, the delta loading of CO<sub>2</sub> between 1.0 and 0.1 MPa is evaluated to be 7.37 mmol·g<sup>-1</sup>. As an example, applying the IAST on previous published results,<sup>51</sup> the dynamic capacity of a BPL activated carbon is estimated to be 3.43 mmol·g<sup>-1</sup> in the same conditions. For a Na–X,<sup>52</sup> the dynamic capacity is 1.44 mmol·g<sup>-1</sup>. This comparison proves that Cu-BTC is a good adsorbent for CO<sub>2</sub> adsorption in synthesis gas mixtures.

## Conclusions

Cu-BTC contains two types of pores, the large pores and the side pockets. GCMC simulation studies have shown that adsorption in the side pockets increases the CO<sub>2</sub>–CH<sub>4</sub> selectivity of the material by 30–50%.<sup>53</sup> The simulations predict a strong increase of the CO<sub>2</sub>–CH<sub>4</sub> selectivity in the pressure range where the side pockets are filled, i.e., below ~0.02 MPa.<sup>18,19</sup> Experimentally, we did not find a significant influence of the side pockets, neither on the selectivity at low pressure nor on the shape of the pure component isotherms. It seems as if the two types of pores had, after all, similar affinities for CO<sub>2</sub> and CH<sub>4</sub>. The direct interaction with the accessible Cu sites in the large

pores holds the balance with the stronger confinement in the side pockets.

From an application point of view, Cu-BTC has very good selectivities and adsorption capacities with a measured CO<sub>2</sub> delta loading of the Cu-BTC of 7.37 mmol·g<sup>-1</sup> between the production step at 1.0 MPa and the regeneration step at 0.1 MPa for the 70–15–15 CO<sub>2</sub>–CH<sub>4</sub>–CO separation. It makes it an attractive material for PSA applications. Its delta loading between 0.1 and 1.0 MPa is significantly higher than that of zeolite Na–X (delta loading of CO<sub>2</sub> in the same conditions of 1.44 mmol·g<sup>-1</sup>) and of activated carbons (CO<sub>2</sub> delta loading of such an adsorbent is estimated to be 3.43 mmol·g<sup>-1</sup>). Zeolite Na–X is highly selective but has an almost rectangular CO<sub>2</sub> isotherm. Saturation is reached at moderate pressure; thus, the difference of adsorption capacities between high pressure and low pressure is small. On the contrary, with an activated carbon as BPL, the shape of the pure CO<sub>2</sub> adsorption isotherm shows a moderate slope in the Henry region and the saturation is reached at very high pressure. Thus, the adsorbent chosen for PSA processes should ideally be a compromise between these two extremes: the curvature of the CO<sub>2</sub> adsorption isotherm should be similar to that of an activated carbon but attain saturation at the pressure of the production step of the PSA process. The Cu-BTC comes close to this good compromise. A second important criterion for adsorbent selection for a PSA with recovery of CO<sub>2</sub> is the selectivity of the adsorbent. Na–X is a highly CO<sub>2</sub>-selective adsorbent, but the price to pay for the high selectivity is the difficult regeneration. Activated carbons are easily regenerable but not very selective (CO<sub>2</sub>–CH<sub>4</sub> selectivity of 3.5).<sup>37,51</sup> Cu-BTC has an intermediate CO<sub>2</sub>–CH<sub>4</sub> selectivity ranging from 4.8 to 11.5, which presents a significant gain compared to activated carbons.

Yet, before Cu-BTC can be used in separations on an industrial scale several remaining questions have to be resolved, in particular the issue of shaping of the material and its stability toward water vapor.<sup>9,54</sup>

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**Supporting Information Available:** Text describing the experimental details of the breakthrough curves measurements and Cu-BTC characterization results, figures showing the breakthrough curve apparatus, powder XRD patterns, thermogravimetric analysis, nitrogen adsorption isotherms, breakthrough curves of CO<sub>2</sub>–CH<sub>4</sub>, and adsorption isotherms, and a table showing the input and isotherm parameters of the model. This information is available free of charge via the Internet at <http://pubs.acs.org>.

## Notation

$b_i$  = affinity coefficient in the Langmuir model (MPa<sup>-1</sup>)  
 $B_i$  = affinity coefficient in the Langmuir model (m<sup>3</sup>·mol<sup>-1</sup>)  
 $C_i$  = concentration of component  $i$  in the gas phase (mol·m<sup>-3</sup>)  
 $C_T$  = total concentration in the gas phase (mol·m<sup>-3</sup>)  
 $D_L$  = axial dispersion coefficient (m<sup>2</sup>·s<sup>-1</sup>)  
 $D_c$  = diffusivity in the crystal (m<sup>2</sup>·s<sup>-1</sup>)  
 $k_t$  = film mass-transfer coefficient (m·s<sup>-1</sup>)  
 $m_{ads}$  = mass of adsorbent (kg)  
 $n_i$  = adsorbed phase concentration of component  $i$  (mol·m<sup>-3</sup> of adsorbent)

$n_i^*$  = adsorbed phase concentration in the equilibrium state of component  $i$  (mol·m<sup>-3</sup>)  
 $p$  = pressure (bar)  
 $Q$  = total volumetric gas flow rate (m<sup>3</sup>·min<sup>-1</sup>)  
 $q_i$  = adsorbed phase concentration of component  $i$  (mol·kg<sup>-1</sup>)  
 $q_{i,sat}$ ,  $n_{i,sat}$  = maximum adsorbed amount of component  $i$  in the multisite Langmuir model  
 $R_c$  = crystal radius (m)  
 $r$  = radial coordinate (m)  
 $t$  = time (s)  
 $V_{col}$  = volume of the column (m<sup>3</sup>)  
 $v$  = interstitial velocity (m·s<sup>-1</sup>)  
 $v_0$  = interstitial velocity at the inlet of the column (m·s<sup>-1</sup>)  
 $y_i$  = mole fraction of component  $i$  in the gas phase  
 $z$  = axial coordinate (m)

## Greek Letters

$\varepsilon_i$  = interstitial porosity of the column  
 $\mu$  = first moment of the breakthrough curve (min)  
 $\rho_{grain}$  = grain density of the adsorbent (kg·m<sup>-3</sup>)

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