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Measurements and time-domain simulations of multiphonics in the trombone.

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Abstract

Multiphonic sounds of brass instruments are studied in this article. They are produced by playing a note on a brass instrument while simultaneously singing another note in the mouthpiece. This results in a peculiar sound, heard as a chord or a cluster of more than two notes in most cases. This effect is used in different artistic contexts.

Measurements of the mouth pressure, the pressure inside the mouthpiece and the radiated sound are recorded while a trombone player performs a multiphonic, firstly by playing an F_3 and singing a C_4 , then playing an F_3 and singing a note with a decreasing pitch. Results highlight the quasi-periodic nature of the multiphonic sound and the appearance of combination tones due to intermodulation between the played and the sung sound.

To assess the ability of a brass instrument physical model to reproduce the measured phenomenon, time-domain simulations of multiphonics are carried out. A trombone model consisting in an exciter and a resonator non-linearly coupled is forced while self-oscillating to reproduce simultaneous singing and playing. Comparison between simulated and measured signals is discussed. Spectral content of the simulated pressure match very well with the measured one, at the cost of a high forcing pressures.

I INTRODUCTION

A "monodic instrument", by its etymological meaning, is an instrument designed to play "monophonic" sounds, that is sounds with a single pitch. However, most monodic instruments of the orchestra can also produce unusual sounds, called "multiphonic sounds". This term means that the listener perceives multiple notes in the sound.

A range of wind instruments can produce sounds called multiphonics [Castellengo, 1981]. Actually, this word designates two distinct phenomena. On the one hand, the term "multiphonic" can refer to a multiple-pitched sound generated with an extension of the conventional playing techniques: woodwind multiphonics, where quasi-periodic regimes are generated through specific embouchures and/or fingerings [Backus, 1978, Keefe and Laden, 1991, Dalmont et al., 1995, Gibiat and Castellengo, 2000, Doc et al., 2014], belong to this category. A quasi-periodic oscillation is a deterministic oscillation whose energy is located at frequencies which are integer combinations of base frequencies. The ratios between the base frequencies are irrational

numbers. Flute-like instrument multiphonics are also based on an extended playing technique: the oscillation of the air jet becomes quasi-periodic with no need to introduce another oscillator [Campbell and Greated, 1994, Blanc et al., 2010, Terrien et al., 2013]. Brass instrument multiphonics can be based on two distinct mechanisms: a spontaneous quasi-periodic self-oscillation, similar to those in flutes and in reed instruments, can be involved [Castellengo et al., 1983]. But on the other hand, the brass instrument player can also produce a multiphonic sound by singing while he plays [Campbell and Greated, 1994, Sluchin, 1995]: two oscillators are then involved, the lips and the vocal folds. This paper only focuses on this latter kind of multiphonic sound on the trombone. In this situation, an intermodulation is observed, making non-harmonic frequencies appear in the resulting sound.

According to the musical context, a multiphonic sound can be considered as a mistake made by the musician or due to a defect of the instrument: in occidental art-music, a "rolling sound" is generally considered to be a mistake the musician makes and a bowed instrument with "wolf notes" [Iniacio et al., 2008] is considered to be of poor quality. However, multiphonic sounds can also be intentional. This applies to extra-European traditional instruments such as pre-Columbian *flautas de chinos* producing *sonidos rajados* [Wright and Campbell, 1998, Blanc et al., 2010, Terrien et al., 2013], or the Australian aboriginal *didjeridu* [Wolfe and Smith, 2008] where the musician has several options for modifying the sound by singing or tuning of vocal tract resonance while he plays. But European classical music also includes examples of multiphonics: an example of cadenza of a French horn concertino is displayed in the score in Figure 1. The technique is mentioned in teaching methods of the 19th century, as reported in [Sluchin, 1995]. Jazz and avant-garde music have popularized this musical effect with artists like James Morrison, Nils Landgren, Nat McIntosh and many others.



Figure 1: Cadenza from C.M. von Weber's concertino for horn, including multiphonic sounds.

Multiphonics produced by a musician simultaneously singing and playing a brass instrument have been documented in [Campbell and Greated, 1994, Sluchin, 1995] but, to the author's knowledge, simulations of this phenomenon have never been carried out. This paper examines the ability of a simple instrument physical model to simulate trombone multiphonics. This helps a better understanding of the multiphonic phenomenon and defines the abilities of the considered model. Comparisons between results of this model and measurements on trombone players are proposed on both multiphonic sounds studied: namely, playing an F_3 while singing a C_4 (referred to hereafter as $F_3 - C_4$ multiphonic), and playing an F_3 while singing a note whose pitch decreases from C_4 to slightly above C_3 (referred to later as "decreasing playing frequency multiphonic"). The measurement and simulation tools are first presented in Section 2; then, measurements and simulations of a selection of multiphonic sounds are compared in Section 3 to evaluate the ability of the model to reproduce multiphonics.

II TOOLS

II.A Experimental setup

An experimental device has been developed to measure some characteristic variables during a trombone multiphonic performance. The acoustic pressure inside the instrument mouthpiece $p(t)$, characteristic of the response of the instrument, is measured. Another sensor measures the blowing pressure as well as the acoustic pressure inside the mouth $p_m(t)$. The radiated sound, $p_{ext}(t)$, is also recorded. The measurements room has a short reverberation time, similar to that of a rehearsal studio, for the musician's convenience.

- The mouth pressure $p_m(t)$ is measured with an Endevco 8510B-5 miniature pressure sensor, through a capillary tube (1.5 mm inner diameter) inserted in the mouth of the musician. The capillary tube is glued to a short piece of silicone tubing (4 mm diameter) connected to the pressure sensor. The assembly of tubes forms a Helmholtz resonator which bandpass-filters the signal. An *ad hoc* convolution filter is applied to the measured signal in order to compensate for the transfer function of the tube.
- The pressure inside the mouthpiece $p(t)$ is measured through the same sensor model. The sensor is screwed into the mouthpiece wall. The microphone is small enough for the shape of the mouthpiece cup not to be significantly altered.
- The radiated sound $p_{ext}(t)$ is recorded with a *B&K* 1/4" microphone, placed about 40 cm downstream from the center of the trombone's bell. The vicinity with the bell limits the influence of the reflections in the room.

These sensors are connected to their respective conditioners/amplifiers. The signals are simultaneously recorded by a computer through NI-9234 and 9215 acquisition modules. The sampling frequency is 51200 Hz.

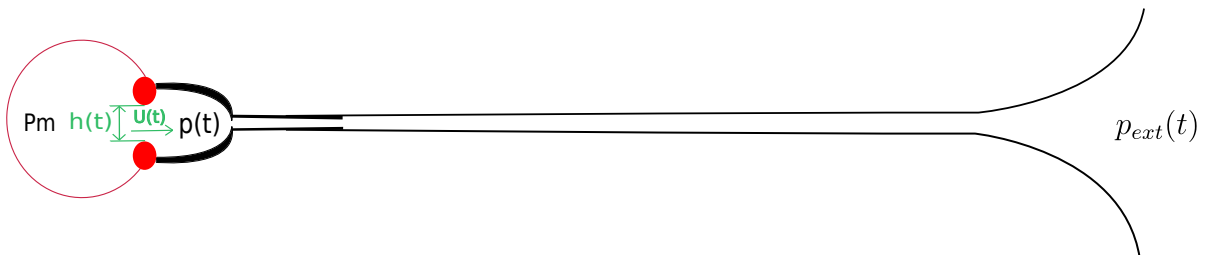


Figure 2: (color online) Sketch of the trombone positioning $p_m(t)$, $p(t)$ and $p_{ext}(t)$. Some variables of the model defined in Section II.B are written in green.

II.B Time-domain simulation of a trombone's physical model

All along this article, measurements are compared with time-domain simulations from a trombone physical model. The retained self-sustained model relies on a linear exciter which is non-linearly coupled with a linear resonator. Each of these three elements is described below. This kind of model has been widely used for wind instruments [Fletcher, 1993] including brass instruments [Elliott and Bowsher, 1982, Yoshikawa, 1995, Cullen et al., 2000], since the seminal work of von Helmholtz [von Helmholtz, 1877].

For brass instruments, the exciter consists of the lips of the musician, represented by a linear, oscillator-like valve, linking the height between the lips $h(t)$ and the pressure difference across the

lips $\delta p(t) = p_m(t) - p(t)$. A one degree of freedom valve (referred to hereafter as "1-DOF valve" [Fletcher, 1993] is enough to model the lips for common playing situations [Yoshikawa, 1995] with a tractable number of parameters. Two kinds of 1-DOF valves can be considered : "striking outward", which tends to open when δp grows, and "striking inward" which presents the opposite behavior. For the reasons detailed in [Velut et al., 2016] we chose a "striking outward" valve to model the lips of the trombonist. This model relies on the following equation:

$$\frac{d^2h}{dt^2} + \frac{\omega_l}{Q_l} \frac{dh}{dt} + \omega_l^2(h - h_0) = \frac{1}{\mu}(p_m - p(t)), \quad (1)$$

where $\omega_l = 2\pi f_l$ (rad/s) is the lip resonance angular frequency; Q_l the (dimensionless) quality factor of the lips; h_0 the value of $h(t)$ at rest (m); μ an equivalent surface mass of the lips (kg.m^{-2}).

Lip parameters very similar to those chosen in [Velut et al., 2016] after a thorough bibliographical review are used. These parameters are given in Table I. The only difference is the quality factor Q_l lessened from 7 to 5. Results previously obtained in [Velut et al., 2016] were satisfactory, with reasonable threshold blowing pressures in the [1kPa : 15kPa] range for commonly played notes. The refining of the Q_l value results in periodic playing on a larger range of f_l on the Jupiter JSL 2321 trombone used in the experiment.

$h_0(\text{m})$	$L(\text{m})$	$1/\mu(\text{m}^2\text{kg}^{-1})$	Q_l
5.10^{-4}	12.10^{-3}	0.11	5

Table I: Lip parameters retained for this article.

In most studies about brasswinds, p_m is assumed to be constant in usual playing, corresponding to the blowing pressure. However, in order to simulate a multiphonic, a forcing component is added to the static value of p_m , corresponding to the acoustic pressure produced by the vibrating vocal folds. For multiphonic simulations with a constant singing frequency, the p_m signal takes the following form:

$$p_m(t) = p_m^0 + p_m^1 \cdot \sin(2\pi t f_s), \quad (2)$$

where p_m^0 and p_m^1 are respectively the constant blowing pressure and the amplitude of the singing signal, and f_s the singing frequency.

For simulations with a decreasing frequency, the signal is divided into 3 parts: first, the mouth pressure is a constant blowing pressure for 6 seconds: this gives time to reach a steady-state oscillating regime. Then, the p_m signal is similar to Eq. (2) for 6 seconds with $f_s = f_1$. Then, the frequency decreases from f_1 to f_2 taking this form:

$$p_m(t) = p_m^0 + p_m^1 \cdot \sin \left[2\pi t \left(f_s + \frac{(f_2 - f_s) \cdot t}{2d} \right) \right], \quad (3)$$

where d is the duration of the frequency decrease (s).

In the measurements, the p_m^1/p_m^0 ratio is about 0.02, but higher values are used in simulations, to get computed spectra as close as possible to experimental ones. A value of $p_m^1 = 0.3p_m^0$ is used all along this paper. This difference in p_m^1 values between simulation and measurement is a limitation of our model.

This exciter is non-linearly coupled to a resonator: the bore of the trombone. Propagation in brass instruments, particularly the trombone, is known to be nonlinear for loud tones. This causes nonlinear distortion of the waveform, possibly leading to shockwaves [Hirschberg et al., 1996,

Myers et al., 2012]. In musical terms, the sound becomes "brassy" at louder playing dynamics. However, since this study focuses on low and moderate playing dynamics, a linear model of propagation is sufficient. Thus, the resonator is modeled by its input impedance Z . By definition, Z is the ratio, in the frequency domain, of the pressure at the input of the resonator $P(\omega)$ to the acoustic flow $U(\omega)$ taken at this same point :

$$Z(\omega) = \frac{P(\omega)}{U(\omega)}. \quad (4)$$

The input impedance of the Jupiter JSL 232l tenor trombone used for experiments (with the slide fully pulled in) is measured with the impedance sensor described in [Macaluso and Dalmont, 2011], then fitted by a sum of 13 Lorentzian functions -representing the 13 first modes of the trombone- using a least squares method similar to that in [Silva, 2009].

The coupling between this resonator and the aforementioned exciter is non linear. It is provided by the airflow through the lip channel. The air jet is assumed to be laminar in the lip channel, then turbulent in the mouthpiece, all its kinetic energy being dissipated without pressure recovery. Applying the Bernoulli law and the mass conservation law between the mouth and the lip channel gives the following expression of the flow between the lips, depending on the pressure difference and the height of the lip channel [Elliott and Bowsher, 1982, Hirschberg et al., 1995]:

$$u(t) = \sqrt{\frac{2}{\rho}} \cdot L \cdot h(t) \cdot \text{sign}(p_m - p(t)) \cdot \sqrt{|p_m - p(t)|} \cdot \theta(h), \quad (5)$$

where $u(t)$ is the airflow rate ($\text{m}^3 \cdot \text{s}^{-1}$), $\rho = 1.19 \text{ kg} \cdot \text{m}^{-3}$ the air density at $20 \text{ }^\circ\text{C}$, $\theta(h)$ the Heaviside step function related to $h(t)$ and L the width of the lip channel (m).

Simulations based on this model are carried out with MoReeSC [Silva, 2013]. This open-access Python library solves the equations of the model numerically, based on the modal decomposition of the pressure signal in the instrument. This provides values of p , the lip opening h and the airflow between the lips u at each time sample. It features the possibility of modifying input parameters during the simulation, which is particularly useful in this study for defining time-varying mouth pressure signals. In order to get a simulated pressure, a measurement of the transfer function of the trombone, between p and p_{ext} is made. Filtering the simulated p with the given transfer function results in a simulated p_{ext} .

II.C Preliminary measurement on vocal folds

A preliminary experiment is carried out to assess the choice of a forcing term to model the singing like in Eq. (2) and (3). The production of a multiphonic sound requires two exciters: the lips of the musician and his vocal folds. In order to evaluate the independence of the vocal fold oscillation with respect to the lip oscillation, an estimation of the vocal fold oscillation is carried out by measuring the electrical conductivity of the glottis, similarly to what was done in the experimental campaign conducted on the didjeridu [Wolfe and Smith, 2008]. The glottis conductivity is assumed to be approximatively proportional to the contact area of the lips [Hezard et al., 2014]. Since we are interested in comparing orders of magnitude, this approximative proportionality is sufficient. An electroglottograph from VoceVista is used to measure the conductivity of the vocal folds while the musician plays an $F_3 - C_4$ multiphonic. The spectrum of the resulting signal is shown in Fig. 3.

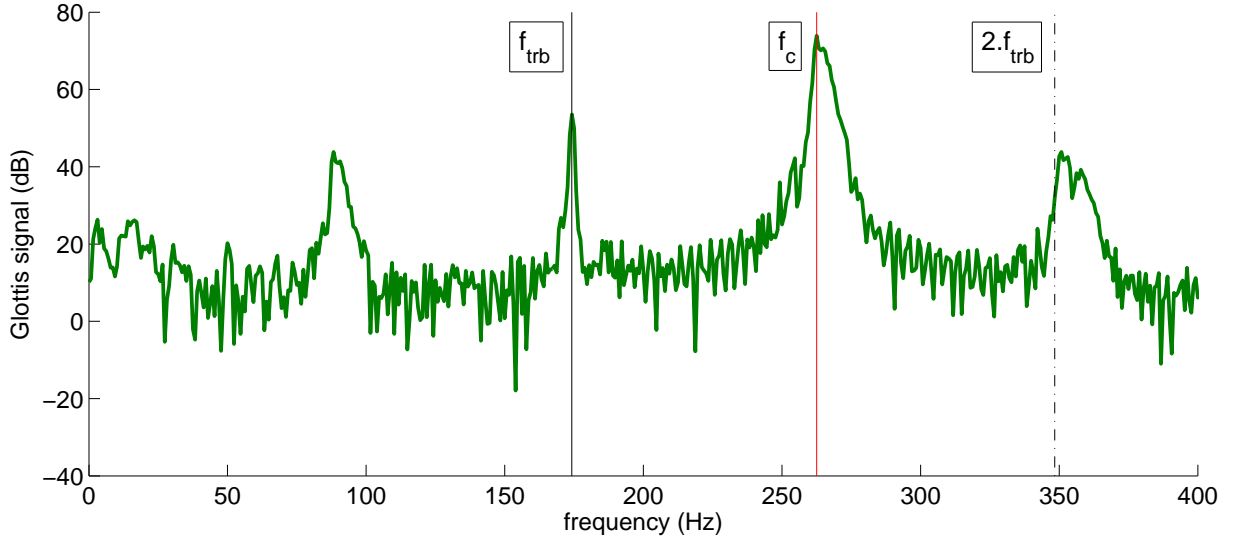


Figure 3: (color online) Spectrum of glottis signal when playing an $F_3 - C_4$ multiphonic. Vertical lines indicate the playing frequency f_{trb} (black), the singing frequency f_s (red) and f_{trb} first harmonic (black, dash-dotted). Hanning window of width 0.2 s, zero-padding of the signal until frequency precision is under 1 Hz.

Spectral components can be observed at the singing frequency $f_s = 262.5$ Hz but also at the playing frequency $f_{trb} = 174.2$ Hz, showing a coupling between the lips and the vocal folds. However, the amplitude of the f_{trb} component is 20 dB lower than the amplitude of the f_s one: this indicates that the oscillation of the vocal folds is not much altered by the acoustic feedback. Thus, since we are interested in identifying the simplest model simulating multiphonic sounds, modeling the contribution of vocal folds through a forcing term seems to be a decent approximation, much simpler than a model that would take into account the vocal folds, the vocal tract and the lips. However, a time-domain simulation tool which would simulate the coupling with the impedance of the vocal tract would probably be of some interest. The implementation of such a model could be realized with the tools presented here.

III RESULTS

III.A $F_3 - C_4$ multiphonic

III.A.1 Experiment

The study firstly focuses on the $F_3 - C_4$ multiphonic, which is one of the most commonly played by trombonists and proposed as a first exercise in [Sluchin, 1995]. Producing an $F_3 - C_4$ multiphonic consists in playing an F_3 while singing a C_4 , i.e. a fifth above. In physical terms, this means playing on the third register of the trombone, while simultaneously singing the note whose frequency is 1.5 times higher ($f_s/f_{trb} = 1.5$). The musician is asked to successively sing a C_4 , then play an F_3 , then perform an $F_3 - C_4$ multiphonic.

Figure 4 shows the spectrograms corresponding to this experiment and calculated for the time-domain signals of p_m in Fig. 4 (a), p in Fig.4 (b) and p_{ext} in Fig.4 (c). The successive tasks - singing, playing, multiphonic - successively appear on the spectrograms. During the singing, a component appears at $f_s = 259.8$ Hz with its harmonics. Similarly, $f_{trb} = 173.6$ Hz and its

harmonics appear while the musician is playing an F_3 . A component at f_{trb} can be observed in Fig. 4 (b) and (c) but also in the p_m spectrogram, because of the coupling with the vocal tract of the musician [Chen et al., 2012, Fréour and Scavone, 2013]. When the multiphonic is played, $p(t)$ and $p_{ext}(t)$ contain the fundamental and harmonics of both f_s and f_{trb} . In addition, other frequency components also appear, which do not belong to either the harmonic series of f_s or that of f_{trb} . These components are shown by arrows in Fig. 4 (b). Note that one of these components has its frequency under f_{trb} . Figure 5 superimposes the spectra of $p(t)$ during the three phases of the performance: singing, playing, multiphonic. This highlights that some peaks of the multiphonics spectrum clearly do not belong to the played signal or to the sung signal.

III.A.2 Simulation

This experiment (playing an F_3 on a trombone while singing a C_4) is simulated, using the method described in Section II.B with the parameters given in Table I: the physical model of trombone is set to play an F_3 , on its 3^d register, with a lip resonance frequency $f_l = 140$ Hz and a steady blowing pressure set to $p_m^0 = 4500$ Pa. This value is slightly above the threshold pressure calculated by linear stability analysis, as in [Velut et al., 2016]. Then, the "sung" note is included to simulate the multiphonic: a forcing sinusoidal component is added to the static blowing pressure, at a frequency f_s corresponding to the upper fifth, as written in Eq. (2). The amplitude of the forcing sinusoidal component is set to 30% of p_m^0 so that $p_m^1 = 1350$ Pa. This forcing component starts 3 seconds after the blowing pressure, once the self-oscillation of the instrument model has reached its steady state. This avoids interferences between the forcing component and the transitory phase of the self-sustained oscillation.

Spectrograms of the simulation results for p_m , p and p_{ext} are displayed in Fig. 6 (a), (b) and (c), respectively. First, the model auto-oscillates on its own until $t = 3s$; then the forcing component is added. Fig. 6 (a) does not display any spectral component at f_{trb} , because the retained model does not take the coupling with the vocal tract into account. Before $t = 3s$, Fig. 6 (b) and (c) only display spectral components at $f_{trb} = 189$ Hz and its harmonics. The oscillation frequency of the simulation is higher than the experimentally recorded playing frequency in Fig. 4. This is consistent with a well-known limitation of this brass model, known to oscillate at sharper frequencies than the tempered scale notes [Campbell, 2004, Silva et al., 2007, Chaigne and Kergomard, 2016, p.547]. Then, at $t = 3$ s, the forcing component at $f_s = 282.7$ Hz appears. As in the experiment, $p(t)$ and $p_{ext}(t)$ show frequency components which are neither f_s , nor f_{trb} , nor their harmonics. This is also to be seen in the p spectra displayed in Fig. 7: some peaks of the multiphonic signal do not match f_s , f_{trb} (solid lines) or their harmonics (dashed lines).

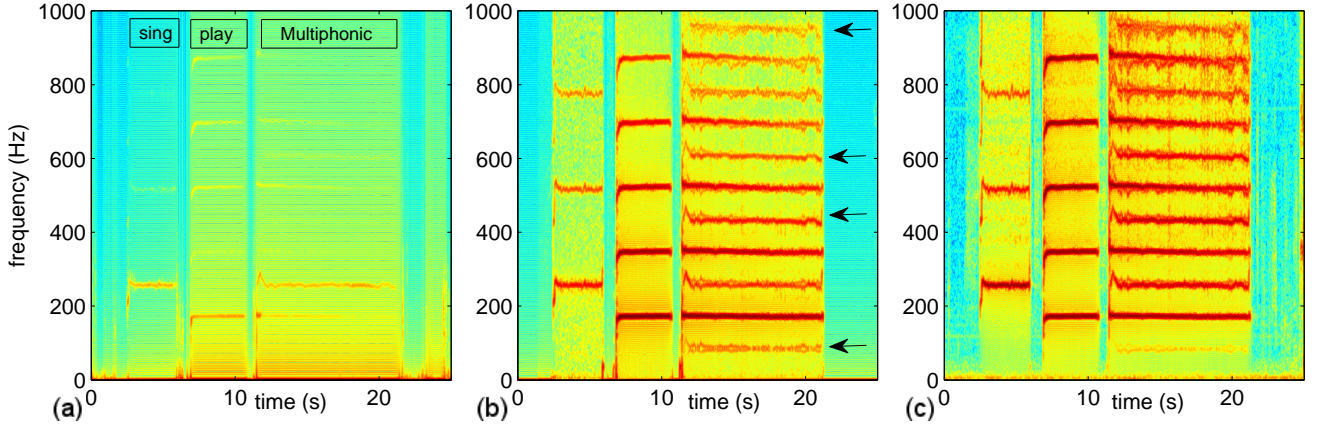


Figure 4: (color online) Experiment: spectrograms of the pressures in the mouth p_m (a), in the mouthpiece p (b) and radiated p_{ext} (c) measured *in vivo*. Hanning window of width 0.2 s, 95% overlap, zero-padding of the signal until frequency precision is under 1 Hz. The musician successively sings C_4 (2.5 – 6.5s), plays F_3 (7 – 11s), then performs an $F_3 - C_4$ multiphonic (12 – 21s). During multiphonic, the p and p_{ext} spectrograms exhibit spectral components which do not belong to either the sung or the played note: they are designated with arrows in (b).

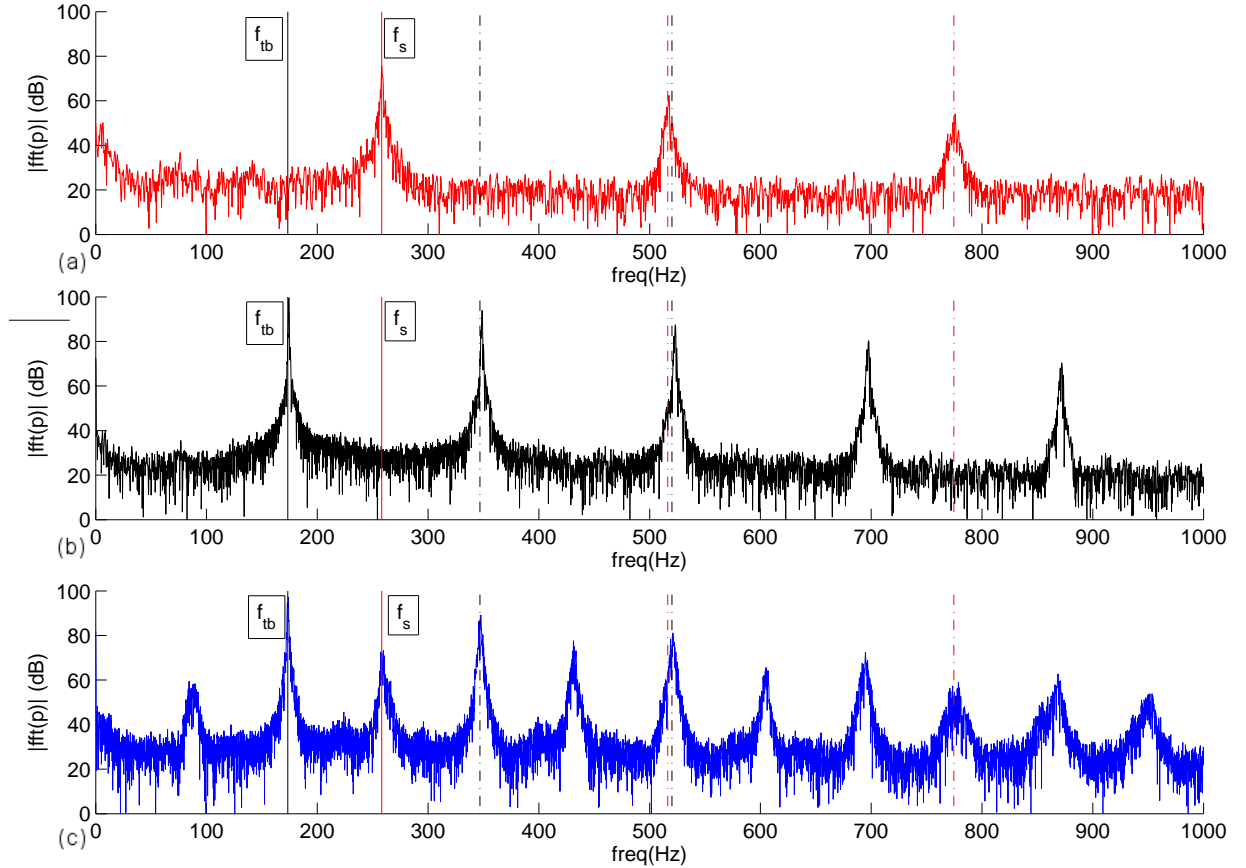


Figure 5: (color online) Experiment: spectra of the mouthpiece pressure $p(t)$ from the same performance: playing (a), singing (b), multiphonic (c). Spectra taken from the spectrograms in Fig. 4b). Peaks appear in the multiphonic spectrum, whose frequencies match neither the oscillation frequency $f_{trb} = 173.6Hz$ nor the singing frequency $f_s = 259.8Hz$ nor their harmonics. f_{trb} and f_s are represented as vertical plain lines (fundamentals) and dash-dotted lines (harmonics).

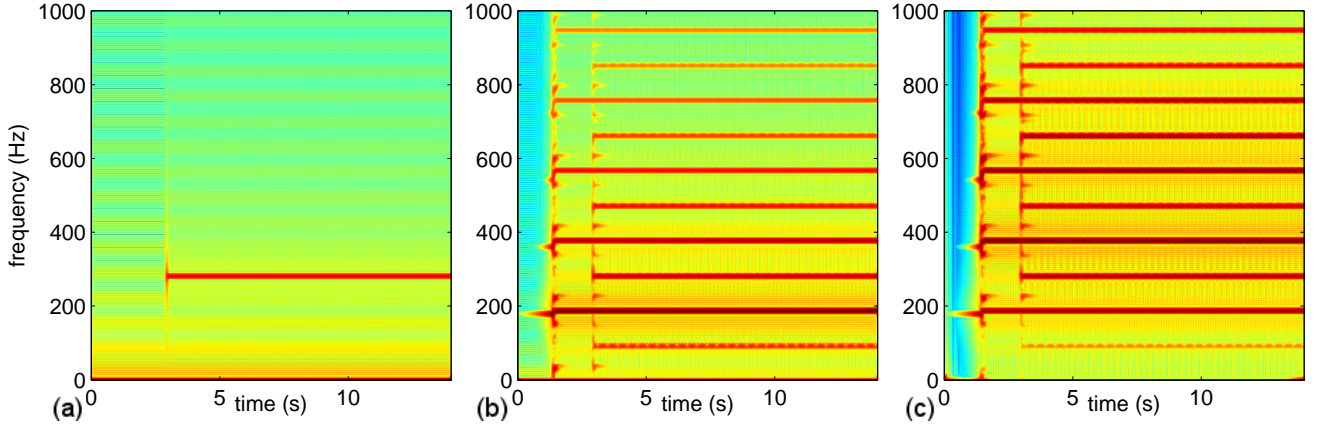


Figure 6: (color online) Simulation: spectrograms of the simulated pressures in the mouth p_m (a), in the mouthpiece p (b) and radiated p_{ext} (c). Hanning window of width 0.2 s, overlapping of 95%, zero-padding of the signal until frequency precision is under 1 Hz. The blowing pressure p_m has a stationary component ($p_m^0 = 4500$ Pa) and, after $t = 3$ s, an oscillating component (amplitude $p_m^1 = 1350$ Pa, frequency $f_s = 282.7$ Hz). The transient occurs at $t = 1.3$ s, the forcing signal is added after $t = 3$ s. As in the experiment, spectral components other than harmonics of the playing and the singing frequencies appear.

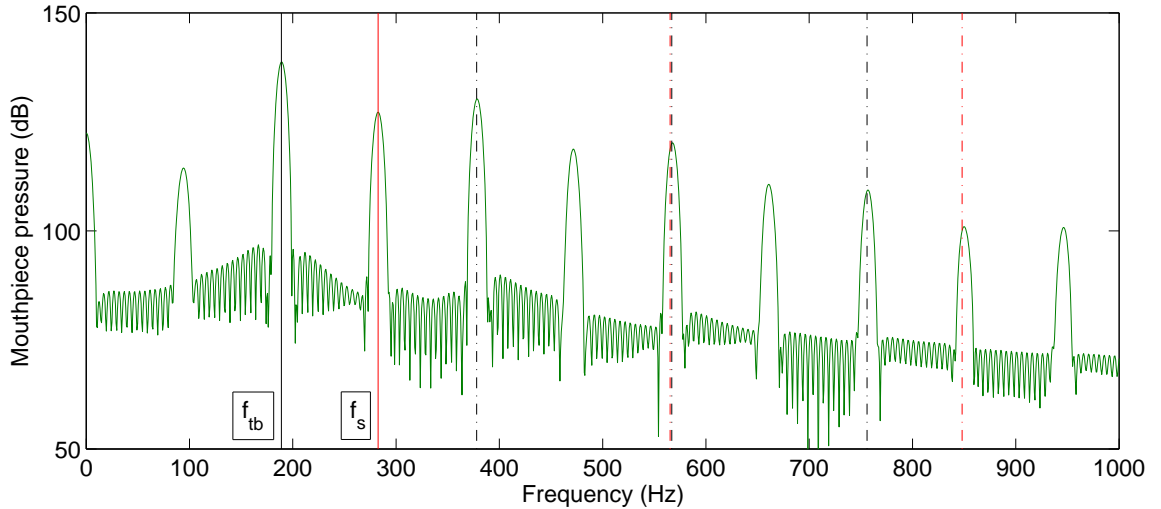


Figure 7: (color online) Simulation: spectrum of the mouthpiece pressure $p(t)$ from the simulation of the multiphonics. Spectrum is taken from spectrogram in Fig. 6b). $f_{trb} = 189$ Hz, $f_s = 282.7$ Hz and their harmonics are shown. Some frequencies are neither harmonic of f_s nor of f_{trb} but are integer combinations of those.

III.A.3 Discussion

Frequencies of the peaks appearing in the spectra of multiphonics, either simulated (Fig. 6 and 7) or measured (Fig. 4 and 5), match very well integer combinations of f_s and f_{trb} : the relative error is less than 3% for the measured frequencies and less than 0.5% for the simulated frequencies. Table II reports the frequencies appearing in the simulation and in the measurement, and proposes one or two integer combinations giving the same frequency. A given integer combination matches the peak of the same rank in the experiment and in the simulation. These frequency components at integer combinations of f_{trb} and f_s are hereafter called combination tones (CT),

as in [Campbell and Greated, 1994, p.64]. In terms of amplitude, the peaks in the spectra of the simulated and the measured multiphonics are not the same, even if the shapes of the spectral envelopes remain comparable.

Peak No.	1	2	3	4	5	6	7	8	9	10
$f_{exp}(Hz)$	86.1	176	259.8	347.3	433.4	521	605.1	694.8	778.7	868.7
$f_{sim}(Hz)$	94.15	189	282.7	377.9	471.4	567.6	661.1	756.6	850	946.2
lin. comb.	$f_s - f_{trb}$ $2f_{trb} - f_s$	f_{trb}	f_s $3f_{trb} - f_s$	$2f_{trb}$ $4f_{trb} - f_s$	$f_s + f_{trb}$	$3f_{trb}$ $2f_s$	$3f_s - f_{trb}$ $5f_{trb} - f_s$	$2f_s + f_{trb}$ $4f_{trb}$	$3f_s$	$5f_{trb}$ $4f_s - f_{trb}$

Table II: (color online) Frequencies of first peaks of spectrum of $p(t)$ measured (f_{exp}) and simulated (f_{sim}) during an $F_3 - C_4$ multiphonic. Integer combinations of f_s and f_{trb} corresponding to each combination tone are indicated.

Signals recorded during this multiphonic playing are periodic signals. However, the fundamental frequency of these signals is an octave below the played note, at $f_{trb}/2$.

The radiated pressure signals p_{ext} of the recorded [MM1,] and the simulated [MM2,] multiphonic are both heard as chords rather than as a single note. The playing and singing frequencies appear, along with other notes, notably the F_2 one octave below f_{trb} . Though, informal listening tests highlights some perceptive differences. First, the sung note is heard louder in the experimental recording than in the simulation. Then, while listening to the recording of the musical performance, a third note, namely an A_4 , can be heard, whose fundamental frequency is $f_s + f_{trb}$. This note cannot be clearly heard in the simulated p_{ext} signal, although its frequency components are present. One reason might be the differences in spectral balance between the experiment and the simulation, which could be related to the simplicity of the forcing signal: this latter hypothesis will be investigated later in the article.

As a conclusion, the $F_3 - C_4$ multiphonic studied here appears to be quite a peculiar periodic regime of oscillation. The spectral components are f_s , f_{trb} , their harmonics, and the combination tones of frequencies $f_{CT} = qf_{trb} \pm f_s$, $q \in \mathbb{N} \cup \{-1\}$ (except negative frequencies). The simulation model, based on a self-oscillating system, sinusoidally forced to model the contribution of the singing voice, reproduces the emergence of a regime which is very similar in terms of frequency content, but with some differences in the peak amplitudes.

Though it is periodic, this regime is not a usual self-sustained oscillation of a brass instrument: the fundamental frequency is not the trombone's oscillation frequency, but a combination tone. Several harmonics are also combination tones, each one matching with several integer combinations of f_s and f_{trb} . This fact is related to this specific situation where f_{trb}/f_s is a rational value. The system undergoes a 3:2 synchronization (also called an internal resonance in the dynamic system terminology) which makes combination tones integer multiples of $f_s - f_{trb}$. It is a particular behavior of a forced self-sustained oscillator. Academic case studies presenting this situation are developed in [Nayfeh and Balachandran, 1995, p.156] with forced Van Der Pol oscillators for instance. According to the oscillator theory, the system studied should generate a quasi-periodic oscillation when there is no internal resonance. The following part will investigate multiphonic situations with a variable singing frequency, leading to multiple situations where f_s/f_{trb} is irrational.

III.B Variable singing frequency

III.B.1 Experiment

The trombone player is now asked to play a multiphonic with f_{trb} as stable as possible, while decreasing his singing frequency. He starts playing the same $F_3 - C_4$ multiphonic as before. Then, he lowers its singing frequency f_s as linearly as possible, until he reaches a frequency just above f_{trb} , while he keeps playing an F_3 . He then holds these playing and singing frequencies for a few seconds.

Spectrograms of the resulting p_m , p and p_{ext} are shown in Fig. 8 (a), (b) and (c), respectively. Fig. 8 (a) exhibits the evolution of the f_s and f_{trb} components in the mouth. The f_{trb} component is fairly stable all along the measurement. The singing component remains stable between 0 and 5 seconds, then decreases between 5 and 10 seconds, and stays 152 musical cents above f_{trb} until the end ($f_s/f_{trb} = 1.09$). After $t = 6$ s, a new spectral component emerges in the mouth, at a frequency growing towards f_{trb} . The peak at f_s has the highest amplitude all along the measurement.

The phenomenon that appears during the first 6 seconds of the spectrogram in Fig. 8 (b) and (c) is very similar to the one appearing after 12s in Fig. 4. Then, when f_s decreases, some frequency peaks seem to "split" in two components, one with a decreasing frequency, the other one with an increasing frequency. While the frequencies get closer to one another, other components with increasing or decreasing frequencies become stronger in amplitude, collecting towards f_{trb} and its harmonics. This leads to a quite rich spectrum with several secondary peaks around f_{trb} and its harmonics, after $t = 8$ s when the singing frequency stabilizes.

To follow the evolution of the components more easily, spectra are computed at each second on the mouthpiece signal and plotted in Fig. 9. The splitting of certain frequency components is noticeable: for illustration, the first peak at $t = 3.12$ s at 85 Hz (Fig. 9 (a)) splits progressively into two distinct peaks of frequency 75 Hz and 100 Hz, respectively, at $t = 5.06$ s (Fig. 9 (c)). The last spectrum, at $t = 10.12$ s (Fig. 9 (h)), shows numerous peaks on either side of f_{trb} and its harmonics.

III.B.2 Simulation

The same simulation model as in Section III.A is used to reproduce this second experiment. Starting with the same parameter values as in the previous section ($f_l = 140$ Hz, $p_m^0 = 4500$ Pa, $p_m^1 = 1350$ Pa, $f_s = 282.7$ Hz i.e. a fifth above f_{trb}), the singing frequency is decreased linearly (sweep signal) between $t = 6$ s and $t = 12$ s, to 152 cents above the playing frequency: $p_b(t)$ follows Eq. (3) with $f_1 = 282.7$ Hz, $f_2 = 206$ Hz and $d = 6$ s. The final frequency is chosen to stick with the experiment, where the final singing frequency of the musician is also 152 cents above the playing frequency. During the last two seconds, $f_s = 206$ Hz. Just as above, spectrograms of p_m , p and p_{ext} are shown in Fig. 10 (a), (b) and (c), respectively. Fig. 11 represents the spectra of p computed each second. Fig. 10 and 11 for simulation are equivalent to Fig. 8 and 9 for experiment. According to Eq. (3), the mouth pressure only contains the forcing term, providing a convenient view on the evolution of f_s . The first seconds of the p and p_{ext} spectrograms of Fig. 10 (b) and (c) are very similar to the spectrograms of Fig. 6 with components of f_s and f_{trb} plus the combination tones. Then, when f_s starts decreasing, each component at f_s or its harmonics splits into two components moving away from one another, one having a decreasing frequency and the other having an increasing frequency. The amplitude of increasing-frequency components is weaker than that of decreasing-frequency components. Between $t = 7$ s and $t = 8$ s, a regime briefly emerges at $38,5 Hz = f_{trb}/5$ and its harmonics, while $f_s = 265 Hz$: it can be noticed under the form of evenly spaced lines (at 38.5 Hz, 77 Hz, 115.5 Hz, 154 Hz, 192.5 Hz, 231 Hz etc.) in Fig. 10 (b) (between the dash-dotted lines) and (c). This is a periodic regime due to a 5 : 1 internal resonance.

Indeed, at this point the f_s/f_{trb} ratio is rational and the resulting regime is periodic. The resulting frequency is very close to the first acoustic resonance frequency of the trombone (38.9 Hz) so the first mode may sustain this oscillation. This will be addressed in Section III.C. After $t = 10s$, the existing components strengthen and new ones appear, to end up with several secondary peaks on each side of the components of the auto-oscillation. These new peaks are particularly visible in the last spectra in Fig. 11.

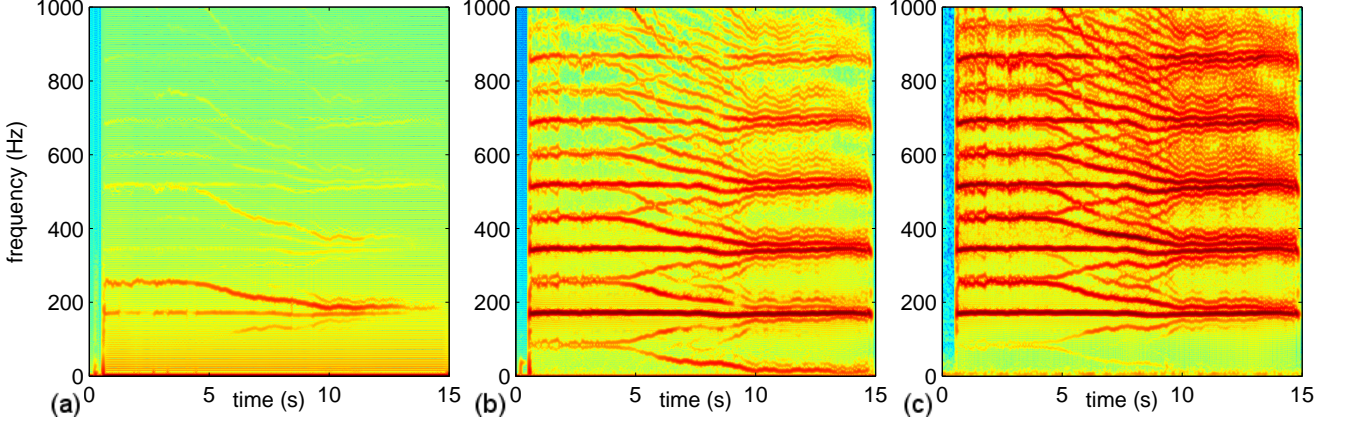


Figure 8: (color online) Experiment: Spectrograms of p_m (a), p (b) and p_{ext} (c) measured during a multiphonic. Hanning window of width 0.2 s, overlapping of 95%, zero-padding of the signal until frequency precision is under 1 Hz. The singing frequency is constant at $f_s = 255Hz$ (note C_4) for 5 seconds, then decreases towards $f_s = 185Hz$ (slightly above f_{trb} , note F_3) and remains at this value after $t = 10s$. The playing frequency remains as constant as possible, with $f_{trb} \in [167.2 : 173.4]$.

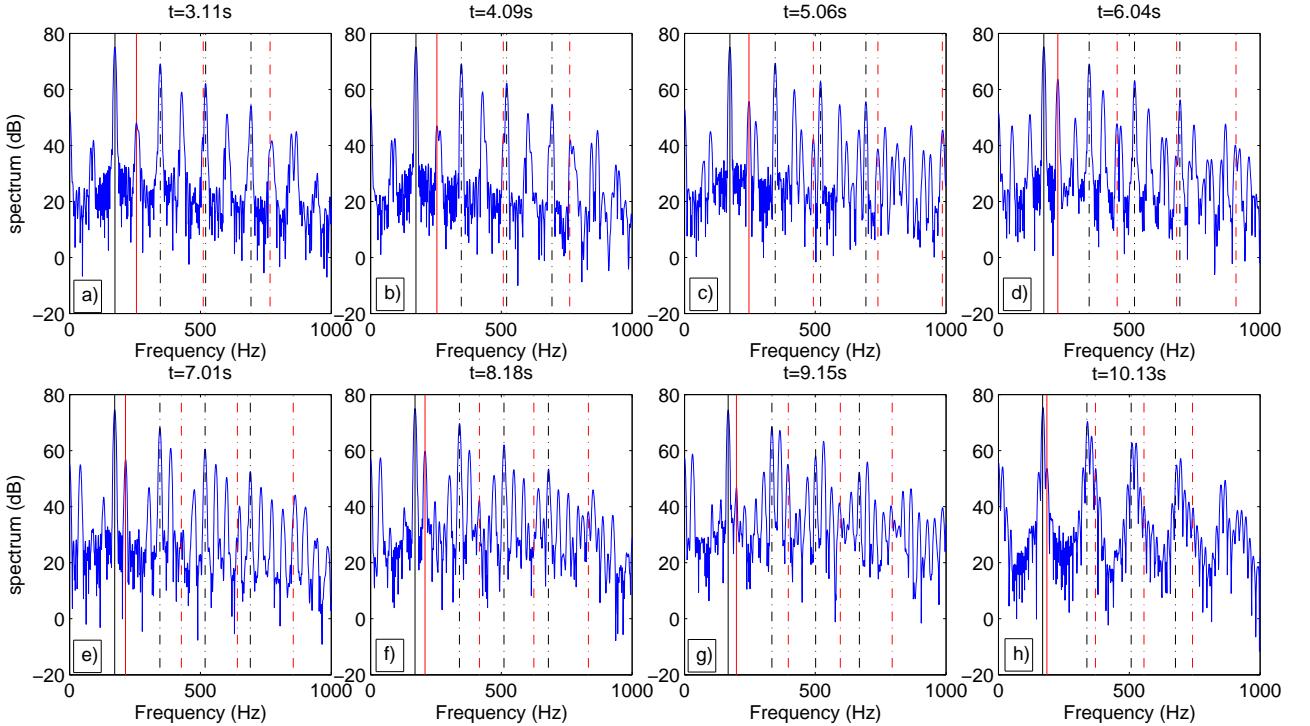


Figure 9: (color online) Experiment: Spectra taken from instants of Fig. 8b) each second between approximately $t = 3s$ and $t = 10s$, when f_s decreases. The plain lines represent f_{trb} (black) and f_s (red), the dash-dotted lines represent their respective harmonics.

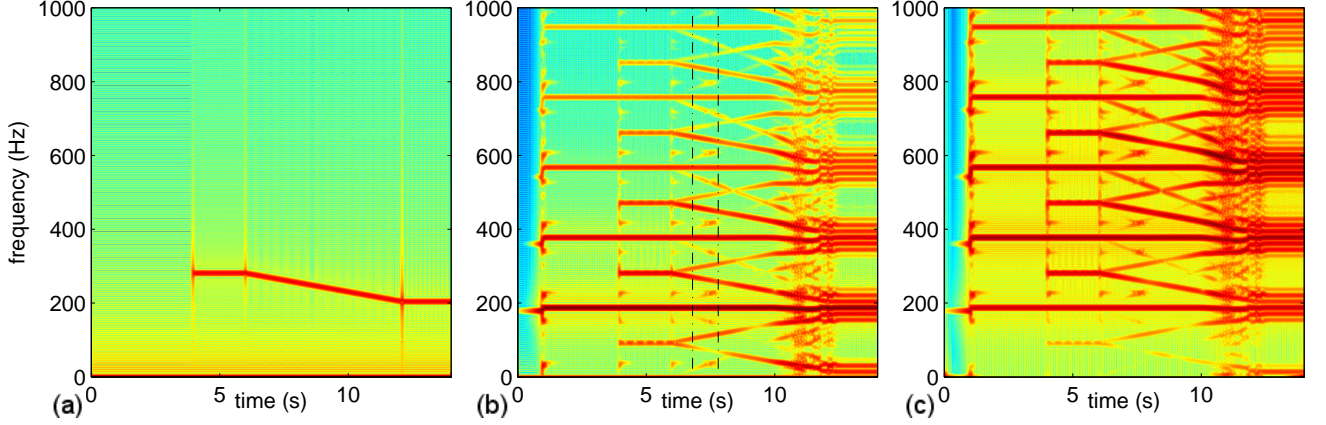


Figure 10: (color online) Simulation: Spectrograms of the simulated p_m (a), p (b) and p_{ext} (c). Hanning window of width 0.2 s, overlapping of 95%, zero-padding of the signal until frequency precision is under 1 Hz. The forcing term appears after $t = 4$ seconds at $f_s = 282.7 Hz$ (a fifth above f_{trb}), then is steady until $t = 6$ s; then decreases linearly towards $f_s = 206$ Hz (155 cents above f_{trb}) for 6 seconds: then it stays at this frequency for 2 seconds. The playing frequency remains stable at $f_{trb} = 188.7$ Hz all along the simulation. Vertical dash-dotted lines in (b) highlight the periodic oscillation regime at $38.5 Hz$.

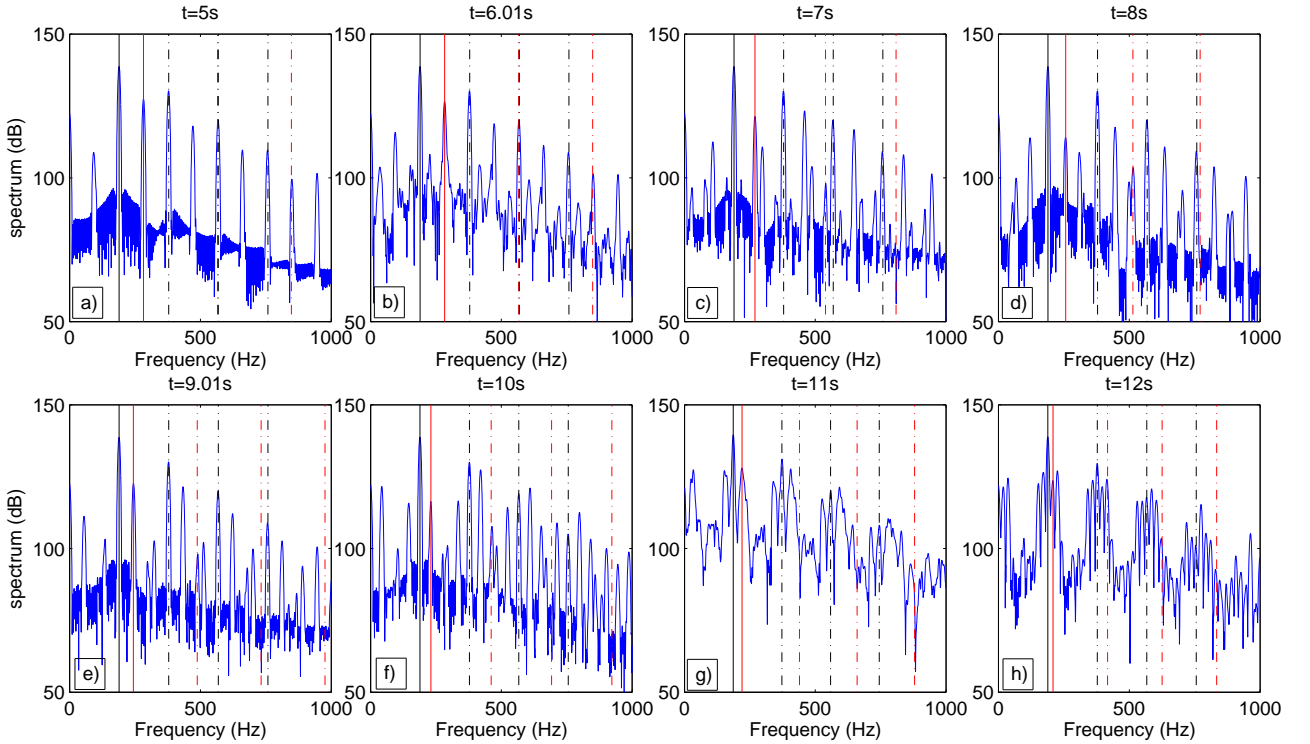


Figure 11: (color online) Simulation: Spectra of the simulated p , taken from the spectrogram in Fig. 10b) each second, between approximately $t = 5s$ and $t = 12s$ where f_s decreases. The plain vertical lines represent f_{trb} and f_s , the dash-dotted lines represent their respective harmonics.

III.B.3 Discussion

As in the previous experiment, several frequency components appear to be harmonics of neither f_{trb} nor f_s . At the beginning, the frequencies are the same as in Section III.A. Certain integer

combinations result in the same combination tones, like for example $3f_{trb} = 2f_s$. Then, when f_s decreases, these integer combinations are no longer equal since f_s and f_{trb} are no longer in a 3 : 2 ratio: the combination tone frequencies either increase or decrease, depending on the sign in front of f_s in the integer combination. The frequencies contained in the signal are no longer integer multiples of the lowest frequency. The oscillation becomes quasi-periodic as soon as f_s/f_{trb} is no longer rational.

Frequencies of the components of p during the phase where f_s decreases are recorded, and plotted with marks in Fig. 12 (a) (experimental measurement) and (b) (simulation). Some integer combinations of f_s and f_{trb} , of positive frequency $qf_{trb} \pm f_s, q \in \mathbb{N} \cup \{-1\}$ are also plotted with plain lines on the same figures. The match between each peak frequency and one integer combination is remarkable, with a maximum relative error of 2.5%. Therefore, the emerging frequency components are integer combinations of f_s and f_{trb} , just as the $F_3 - C_4$ multiphonic. It can be concluded that this more complex multiphonic regime is due to the same phenomenon as in Section III.A, emerging from the coupling between a self-sustained oscillator and a forcing term. However, here the oscillation regime is quasi-periodic.

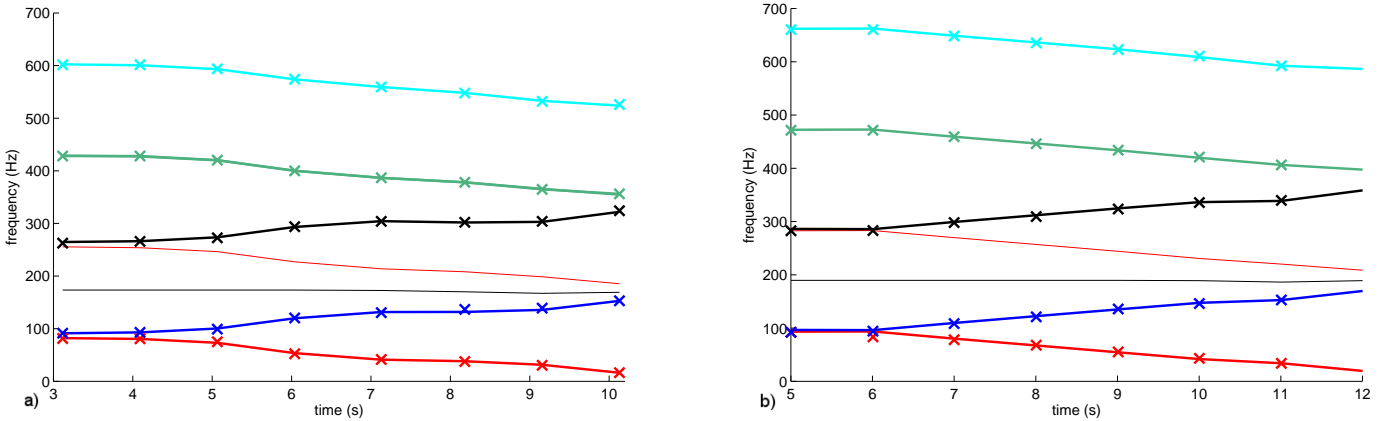


Figure 12: (color online) Plot of f_s (red), f_{trb} (black) and some integer combinations (plain lines) along with the frequencies of the five first components of experimental (a) and simulation (b) mouthpiece pressure (marks). These marks correspond to the peak frequencies in Fig. 9 and 11. The recorded values very closely match the integer combinations.

The simulated p_{ext} and the musical performance were heard as similar during the experiment, yet differences exist. In the recorded multiphonic [MM3,], an A_3 can be heard at the beginning. When f_s begins to change, this A_3 rapidly decreases in loudness. During the decrease in f_s , certain notes become audible while others disappear. These notes can also be heard in the simulated p_{ext} [MM4,] but their overall loudness is weaker. At the end of this multiphonic, f_s and f_{trb} are close to each other. There, a "rolling" or "beating" sound can be heard, both in the experimental and in the simulated p_{ext} signals. This could be explained by the very low $f_s - f_{trb} = 16\text{Hz}$ component (16.3 Hz in measurements, 17.3 Hz in simulation), perceived as a modulation of the sound.

These observations can be related to the spectral envelopes of the measured and the simulated p : comparatively with the peaks at f_{trb} , the combination tones and the harmonics of f_s have a smaller amplitude in simulation than in experimental measurements. The f_s component of p is an exception as it is weaker in measurement than in simulation. At the end of the multiphonic, the peaks at harmonics of f_{trb} are flanked by smaller peaks on both sides. These secondary peaks are significantly weaker in measurement than in simulations.

It can be assumed that these amplitude differences between experiment and simulation are related to the sinusoidal nature of the forcing whereas the singing is a more complex periodic signal. To

assess this hypothesis, another simulation is carried out, this time with a forcing signal reproducing the three first harmonics of the recorded singing signal. The oscillating component of p_m now consists of three sinusoids, with the same relative amplitudes and phases as the first components of the measured sung signal. Figure 13 compares spectra of p simulated with a forcing signal consisting of one or three harmonics (blue and red plots, respectively), at the beginning (Fig. 13 (a)) and the end (Fig. 13 (b)) of a simulation with decreasing f_s . All parameters of the three-harmonic forcing simulation are equal to those of the simulation presented in Fig. 10 and Fig. 11 except the p_m signal.

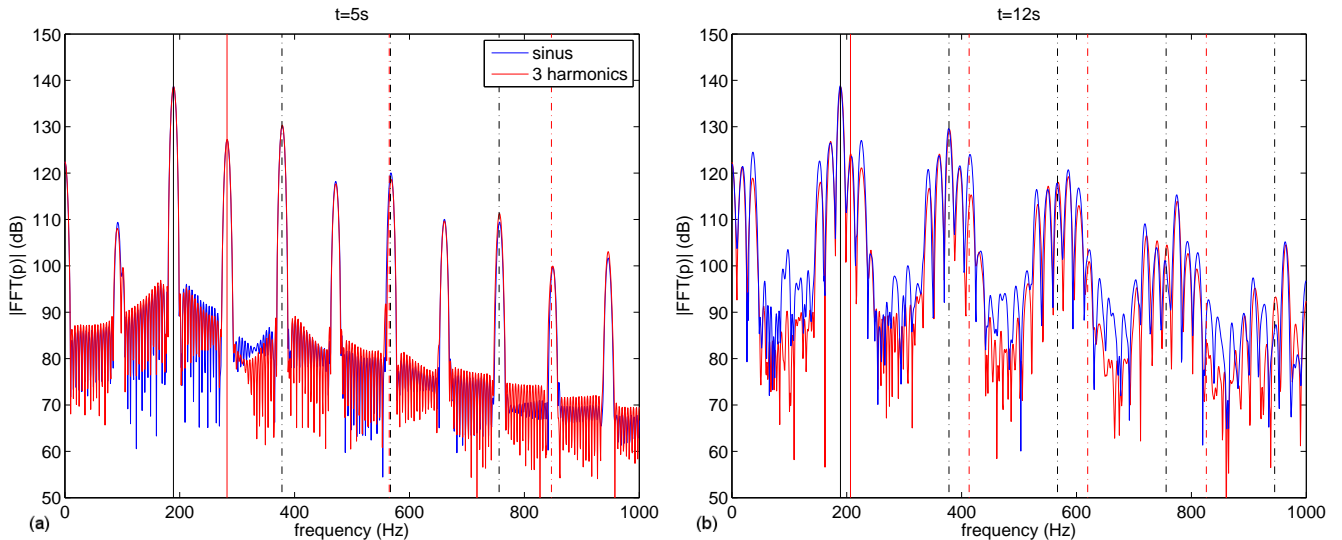


Figure 13: (color online) Comparison of spectra of internal pressures simulated either with a sinusoidal forcing component, or a 3-harmonic forcing component. Hanning window of width 0.2 s, zero-padding of the signal until frequency precision is under 1 Hz. Frequency decreases as in Fig. 10. Fig. (a) is the spectra of p at the beginning of the simulations, Fig. (b) at the end. Differences in terms of amplitude are small in (a) and reach 6 dB in (b). Vertical lines indicate f_{trb} and f_s (plain) and their harmonics (dash-dotted).

Adding harmonics to the forcing signal only results in minor changes in the spectral envelope of the signal. Apart from the components at $2f_s$ and $3f_s$ being logically stronger, the major difference between these simulations is the relative height of the peaks as compared to the numerical noise. Between amplitude peaks, the minima are visibly weaker with a three-component forcing signal, particularly at the end of the simulation (Fig.13 (b)). The influence on the amplitude of combination tones is not significant. The lack of major difference could be explained by the weakness of the harmonics of the forcing, the second and third harmonics of f_s being respectively 17.5 dB and 27.5 dB weaker than the fundamental.

From the results on multiphonics with a sliding f_s described in this section the conclusions from the previous section can be generalized: the self-oscillating model with an additional forcing term is sufficient to simulate multiphonics, resulting in the same frequency components as the measured ones. The frequencies of the components of both the simulated and the measured p match very well with integer combinations of the instrument self-oscillation frequency and the singing or forcing frequency: these components are either harmonics of f_s and f_{trb} or combination tones. This consolidates the idea that multiphonic regimes of brass instruments are either quasi-periodic regimes or, when the f_{trb}/f_s ratio is rational, periodic regimes. Both behaviors come from the same phenomenon. The $F_3 - C_4$ multiphonic considered in III.A is a particular case, where all

frequencies in the signal are harmonic because of the 3:2 internal resonance.

The simulation model tested here reproduces this behavior accurately, in spite of the simplicity of the model. The main difference is the spectral envelope. A forcing signal closer to the singing signal does not significantly change this limitation.

III.C Simulations with one acoustic resonance

New simulations with an even simpler model are carried out. Not only the forcing is sinusoidal as seen in Fig. 14, but the resonator is reduced to one resonance, the third acoustic mode of the trombone - the one used for playing an F_3 .

A simulation with a decreasing sinusoidal forcing is carried out. The playing frequency with this resonator is $f_{trb} = 180.5$ Hz, so the playing frequency decreases from $f_s = 270$ Hz to $f_2 = 196.4$ Hz for 6 seconds to keep the same frequency ratios as in Section III.B.

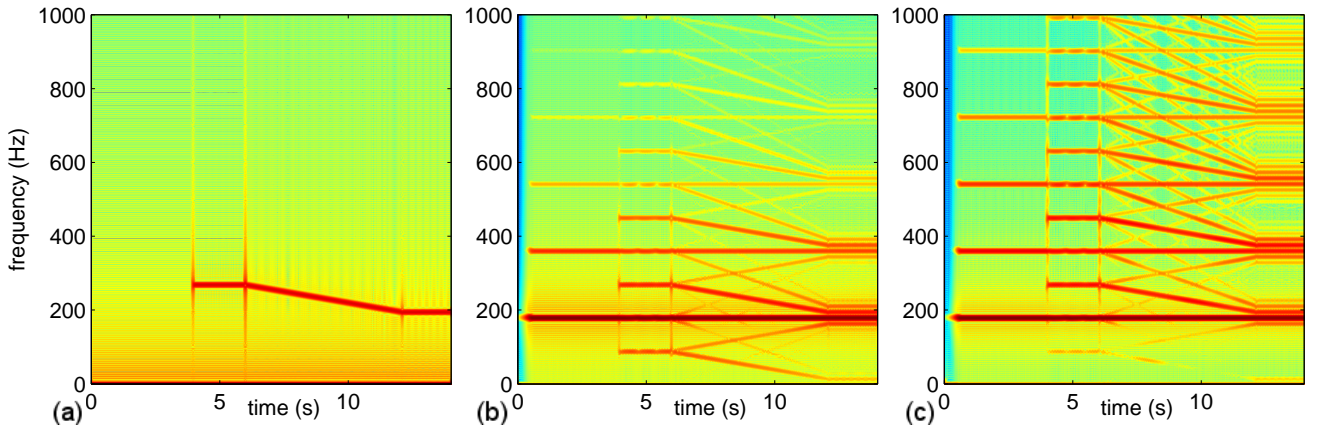


Figure 14: (color online) Simulation: Spectrograms of p_m , p and p_{ext} simulated with a one-mode resonator. Hanning window of width 0.2 s, 95% overlapping, zero-padding of the signal until frequency precision is under 1 Hz. $f_{trb} = 180.5$ Hz, f_s from 270 Hz to 196.4 Hz. The results are comparable with those presented in Fig. 10 with weaker components at high frequencies.

The frequency components of the internal pressure p are harmonics of f_{trb} and f_s or combination tones, as in the previous simulations and measurements, for all values of f_s tested. Thus, the multiphonic behavior appears with this model. However, the amplitude of most frequency components is weaker. This is illustrated by the amplitude differences reported in Table III: while the amplitude of the component at f_{trb} remains fairly constant, all other components are significantly weaker for the 1-mode simulation. Harmonics of f_{trb} are no longer supported by the modes 6, 9 and 12, which affects the amplitude of combination tones. The f_s component in $p(t)$ is weaker, even though the amplitude of the forcing is equal: the modulus of the resonator impedance is 13 times weaker at f_s with only one mode than with 13 modes, which reduces the amplitude of the f_s component in the mouthpiece. The lowest component $f_s - f_{trb} = 15.9$ Hz at the end of the simulation is also weaker, but it is perceived as a modulation of the sound, making a "rolling" sound just like in previous simulations and in measurement. The brief regime at fundamental frequency $f_{trb}/5$ which can be seen between $t = 7s$ and $t = 8s$ in Fig 10 does not occur here, because of the absence of the first mode. Another simulation with all acoustic modes except the first one does not make this regime appear, which strengthens this hypothesis. This simulation result is not shown here for the sake of brevity.

frequency	$f_s - f_{trb}$	f_{trb}	f_s	$2f_{trb}$	$f_s + f_{trb}$	$3f_{trb}$	$3f_s - f_{trb}$
difference (dB) at $t = 5$ s	0.6	0.3	10.7	27	11.7	23.2	16
difference (dB) at $t = 9$ s	7.6	0.5	4.8	27.4	14.2	27	8.7
difference (dB) at $t = 13$ s	26	1.2	4.5	17.9	12.7	25.1	17.4

Table III: Differences (in dB) in the amplitudes of the first peaks for one-mode and 13-mode simulations, measured on the data displayed in Fig. 14, at three time points: $t = 5$ s when $f_s = 270$ Hz, $t = 9$ s when $f_s = 233$ Hz and decreases, and $t = 13$ s when $f_s = 196.4$ Hz. While amplitudes of the peaks at f_{trb} are equivalent, other components are much weaker when the resonator has a single mode.

The quasi-periodic regime related to multiphonics therefore occurs even with a very simple instrument model: a one-DOF mechanical exciter non-linearly coupled with a one-mode acoustic resonator, self-oscillating and forced with a sinusoidal signal.

IV CONCLUSIONS

Both measurement and simulation results presented in this paper confirm the type of oscillating regime of the multiphonic sounds studied. When the musician sings and plays different notes simultaneously, the resulting pressure signal inside the instrument contains harmonics of the sung and played frequencies, as well as combination tones, whose frequencies are integer combinations of f_s and f_{trb} . This is verified not only in the particular case of an $F_3 - C_4$ multiphonic as in Section III.A but also in the case of a time-variable frequency. This generally corresponds to quasi-periodic oscillation, except when an internal resonance occurs and the ratio between playing and singing frequencies is rational. In this latter case, the oscillation is periodic, though it is different from the usual periodic self-oscillation of a brass instrument.

To some extent, the trombone physical model used in this paper is able to simulate this phenomenon. Even if the simulated and measured f_{trb} are not exactly the same (as usual with an outward-striking lip model), the frequency content of the simulated internal pressure of the instrument p is very similar to the probe microphone measurements inside the mouthpiece, with harmonics of both the sung and played signals along with combination tones. This similarity also applies when f_s decreases with time, and when the instrument model is simplified at most. The major difference between simulation and measurement consists in differences in the spectral envelopes: the amplitude of the peaks corresponding to combination tones is generally weaker in measurement than in simulation when the forcing is sinusoidal. This is particularly true when f_s and f_{trb} are close to each other, the secondary peaks being much weaker in measurement. A richer forcing signal with three harmonics, closer to the measured sung signal, does not dramatically change the results: changing the forcing signal does not seem the best way to improve the simulation.

While the simulated blowing pressure p_m^0 is of the same order of magnitude as blowing pressures usually measured on trombone players [Bouhuys, 1968, Fréour and Scavone, 2013], the amplitude of the forcing signal p_m^1 used in our simulations is about 15 times higher than the amplitude measured in the recorded mouth pressure signal p_m . This is the main limitation of this model for multiphonic simulation. Yet, these very different input parameters give comparable results in terms of internal pressure p , the difference in amplitude between the peaks at f_{trb} and f_s being of the same order of magnitude in the measured and simulated p spectra. This is the main limitation of our model. A more complex model, taking into consideration the couplings between the lips, the vocal folds, the resonances in the instrument and those in the vocal tract would possibly give

a better simulation of multiphonics in terms of amplitude of the frequency components, yet at the expense of a far greater complexity.

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