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Paraxial Gaussian beam shooting algorithm for 3D propagation simulation in built environments

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Abstract — Frame-based Gaussian Beam Shooting is presented as an alternative to ray-based methods, when reliable and accessible knowledge of propagated electromagnetic fields is required at all points in built-up environments.

This communication presents a general Gaussian Beam Shooting algorithm based on paraxial beam tracking complemented with the use of "image" frames and with frame redecomposition on reflecting surfaces, to account for the presence of ground and buildings.

Numerical results obtained in the case of a "single wall" and of a "parallelepipedic building" are compared to Parabolic Equation and FEKO software results.

1 INTRODUCTION

Reliable and accessible knowledge of propagated electromagnetic fields at all points in built-up environments is a prerequisite to control emission levels and optimize spectrum management in communication systems, as well as to optimize the design of ground-based Radar systems taking advantage of multipath propagation.

Gaussian Beam Shooting (GBS) is well suited for 3D field simulations in multi-reflecting contexts, thanks to spectral localization of Gaussian beams (GB), allowing for paraxial approximations of reflected fields, and subsequent tracking algorithms, similar to ray-based ones. In the millimetric range, a "paraxial tracking" GBS algorithm was validated by comparison with experimental results, in indoor environments [1]. As compared to ray launching or ray tracing methods, GBS does not rely on any far field assumption, and in the millimetric range paraxial tracking appears to be accurate enough regarding diffraction, thus limiting the number of launched beams with respect to launched or traced rays in ray algorithms.

At frequencies of conventional communication or ground based Radar systems, however, paraxial GB tracking does not account for diffraction ef-

fects with reasonable accuracy. Some recent studies have proposed "beam to beam" formulations to discretize radiated and scattered fields into sets of GBs: empirical sampling and normalisation at arrival [2], empirical sampling in the angular domain and frame decomposition along the edge [3], frame decomposition and frame based truncation of fields on obstacle surface [4]. None of these formulations is used in this study: frame decomposition is favored, and direct frame decomposition of incident fields on reflecting or equivalence surfaces is performed when needed.

Section 2 is devoted to an outline of the frame based GBS algorithm used in this work, which combines free space GBS with:

- frame decompositions of source and incident field distributions,
- the use of image frames to perform paraxial GB tracking in the presence of reflecting surfaces,
- "beam selection" to determine which beams are incident on a given obstacle and on its edges.

Section 3 presents results obtained by GBS over a reflecting ground, in the presence of a screen and of a single building. Comparisons with Parabolic Equation simulations [5], and Method of Moments or PTD results are shown.

2 FRAME BASED GAUSSIAN BEAM SHOOTING ALGORITHM

In order to represent fields radiated into a half-space as superpositions of Gaussian beams (GB), complete sets of Gaussian windows defined in the source plane are used to discretize source field distributions. Such sets belong to the class of "frames" in $L_2(\mathbb{R}^2)$.

2.1 Frame of Gaussian windows

The frame windows $\Psi_{\boldsymbol{\mu}}(y, z)$ used to describe a planar source distribution in the yOz plane are constructed as the product of frame windows $\psi_{m,n}^y(y)$ and $\psi_{p,q}^z(z)$ in $L_2(\mathbb{R})$:

$$\Psi_{\boldsymbol{\mu}}(y, z) = \psi_{m,n}^y(y)\psi_{p,q}^z(z) \quad (1)$$

where $\boldsymbol{\mu} = (m, n, p, q)$ is a composite translation index in \mathbb{Z}^4 , and $\psi_{m,n}^u$, $(m, n) \in \mathbb{Z}^2$, is obtained by translating a Gaussian function ψ along the spatial

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coordinate u and along its spectral counterpart k_u :

$$\psi_{m,n}^u(u) = \psi(u - m\bar{u})e^{in\bar{k}_u u}$$

with $\psi(u) = \left(\frac{\sqrt{2}}{L}\right)^{\frac{1}{2}} \exp\left(-\pi\frac{u^2}{L^2}\right)$; \bar{u} and m are the spatial translation step and index, \bar{k}_u and n their spectral counterparts.

The set $\{\psi_\mu, \mu \in \mathbb{Z}^2\}$ is a frame if and only if $\bar{u}\bar{k}_u = 2\pi\nu$, with $\nu < 1$ (ν : oversampling factor), and the favorite choice for the translation steps is: $\bar{u} = \sqrt{\nu}L$, $\bar{k}_u = \sqrt{\nu}(2\pi/L)$ ("balanced" frame).

An α -polarized electric field distribution $E^\alpha(y, z)$ is discretized by "frame decomposition" as:

$$E^\alpha(y, z) = \sum_{\mu \in \mathbb{Z}^4} A_\mu^\alpha \Psi_\mu(y, z) \quad (2)$$

with the A_μ complex coefficients called "frame coefficients". These coefficients are not unique, but can be calculated by projecting the function on a "dual frame" of functions [6, 7]. This calculation is performed by Discrete Fourier Transform, and for high enough oversampling ($\nu \leq 0.25$), approximating the dual functions by Gaussian windows provides accurate enough results [7].

2.2 Gaussian beam shooting

Let us denote $B_\mu^\alpha(\mathbf{r})$ the field radiated at point \mathbf{r} by an α -polarized electric field distribution $E^\alpha = \Psi_\mu(y, z)$ ($\alpha = y$ or z). The paraxial expression of $B_\mu^\alpha(\mathbf{r})$, obtained by paraxial asymptotic evaluation of a plane wave spectrum integral, writes as:

$$B_\mu^\alpha(\mathbf{r}) = \mathbf{b}_\mu^\alpha \sqrt{\frac{\det \mathbf{\Gamma}^{-1}(0)}{\det \mathbf{\Gamma}^{-1}(x_\mu)}} \exp ik \left[x_\mu + \frac{1}{2} \mathbf{y}_\mu^t \mathbf{\Gamma}(x_\mu) \mathbf{y}_\mu \right]$$

with \mathbf{b}_μ^α a vector depending on the source polarization. This expression is that of a GB with its axis along the x_μ direction determined by the spectral translation vector $(n\bar{k}_y, q\bar{k}_z)$. $\mathbf{y}_\mu = (y_\mu, z_\mu)$ is the position vector of the point \mathbf{r} in a plane transverse to the x_μ axis, and $\mathbf{\Gamma}$ is a complex curvature matrix yielding transverse field decay.

The expression of the radiated field at point \mathbf{r} in the $x > 0$ half-space is then easily derived using (2), in the form of a GBS formula:

$$\mathbf{E}(\mathbf{r}) = \sum_{\mu \in \mathbb{Z}^4} [A_\mu^y \mathbf{B}_\mu^y(\mathbf{r}) + A_\mu^z \mathbf{B}_\mu^z(\mathbf{r})]$$

2.3 Reflexion and diffraction by planar obstacles

GBS algorithms have to take advantage of the transverse localization of beams to limit the number of beams to shoot. A selection algorithm determines which beams contribute to the field in a

given zone or on a given surface [8]. In the presence of an obstacle, the same algorithm is used to determine which of the beams impinging on the obstacle surface are impinging on the edge or corners of this surface. This information leads to different processing of beams, either paraxially reflected if they do not "touch" edges, or else "diffracted".

In our algorithm, paraxial reflexion is accounted for by introducing image frame windows, with their vector part transformed by reflexion operators (Fresnel or derived from surface impedance models) [8]. Diffraction is accounted for by considering the fields incident on a given surface as being truncated at the edge of the surface. Contrary to Physical Optics however, where equivalent currents radiate into all directions of space, GBS involves plane wave spectrum representations of fields, radiating into one half-space only, and spectrally narrow GB fields can be transformed by reflexion operators applied to plane waves.

In the special case of obstacles with perfectly conducting "walls", equivalence theorems are specially easy to implement for a zero order approximation of diffraction effects. The surface of the obstacle is considered as an equivalent surface where the null tangent electric field boundary condition must be enforced, in the presence of source fields propagating in free space. This approach leads to frame decomposition of incident fields on all the virtual surfaces replacing the walls of the obstacle. The radiated field obtained by GBS from these walls is then subtracted from the source field propagating in free space. Next section will illustrate the application of this algorithm.

3 NUMERICAL RESULTS

Test cases are designed to compare results obtained by GBS, with those of a Parabolic Wave Equation algorithm developed at NOVELTIS (3DPWE), and with those obtained with the FEKO code.

The source is given as a field distribution in the xOz plane, with linear polarization along y (horizontal) or z (vertical). The distribution is of the form of a Gaussian frame window $\Psi_\mu(y, z)$, defined by: $L = 7.5\lambda$, $\nu = 0.16$, centered at $z = 12.5m$, $y = 0$, without any spectral shift. In the following, the frequency is taken equal to 430MHz, a classical frequency used for UHF ground Radar applications, and the source polarization is horizontal. The frame used to decompose the source distribution in the yOz plane, as well as incident fields on reflecting planes, is defined by $L = 10\lambda$ and $\nu = 0.16$.

3.1 Test case with screen

The first test case addresses the problem of diffraction by a perfectly conducting (PEC) screen, in the presence of a plane PEC ground, as shown in figure 1. The screen is 5 meter wide and 20 meter high, in the plane $x = 200\text{m}$, centered with respect to the vertical plane $y = 0$.

In such a case, the GBS algorithm computes propagated fields by summing up six different fields, each of them obtained by GB summation:

- the source beam field and its image field with respect to the ground, both radiated in free space (without screen) into the half-space $x > 0$.
- the field reflected by the screen, obtained by GBS from the frame decomposition of the field incident on the screen, which is radiated by the source and by its image by the ground.
- the image of this reflected field by the ground; both reflected fields are present in the half-space $x < 200\text{m}$.
- the “shadow” field, radiated into the half-space $x > 200\text{m}$ by the opposite of the field incident on the screen; the image of this “shadow” field by the ground.

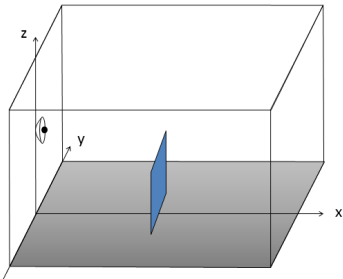


Figure 1: Test case with a vertical screen at $x = 200\text{m}$, on a flat ground.

A comparison with MoM results obtained with FEKO and with results obtained with 3DPWE is presented in Figures 2 and 3 along vertical lines at distances $x = 100\text{m}$ and 300m in the xOz plane (100 m in front of and 100 m behind the screen). Results visibly compare well, in spite of strong oscillations along the x axis in the region where reflected and incident fields superpose (cf Figure 6).

3.2 Test case with building

This case is derived from the previous one, the screen being replaced by a “building” modelled by a PEC parallelepiped, with $5 \times 5\text{m}^2$ basis and 20 meter height, with its first wall parallel to the yOz plane, at $x = 200\text{m}$ (Figure 4).

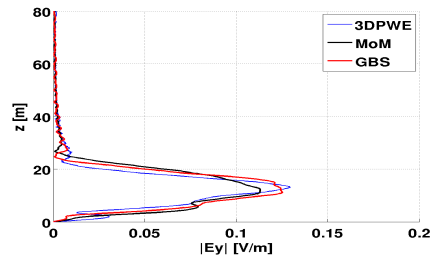


Figure 2: Horizontal field component along the line $y = 0$, $x = 100\text{m}$.

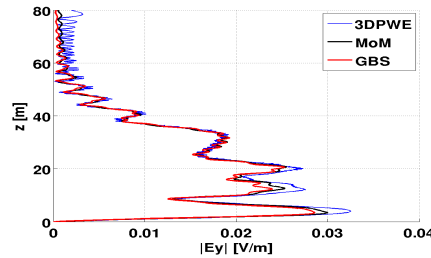


Figure 3: Horizontal field component along the vertical lines in xOz plane, at $x = 300\text{m}$.

Propagated fields are shown in Figure 5 on a horizontal map parallel to xOy at height $z = 12.5\text{m}$. Fields are sampled every 1 meter along x , 0.25 meter along y . The building is colored in black at the center of the map. Oscillations caused by interferences between incident and reflected waves ($x < 200\text{m}$), as well as shadowing for $x > 200\text{m}$ and diffraction effects are clearly visible.

A comparison with PTD results obtained with FEKO and with results obtained with 3DPWE is presented in Figure 6 along the horizontal line defined by $y = 0$ and $z = 12.5\text{m}$. Strong oscillations in front of the building do not allow for a clear comparison of the different results, which vary however in the same range of values. Behind the building, GBS and PTD results match very well.

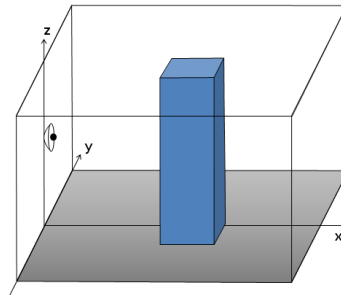


Figure 4: Test case with a parallelepipedic building at $x = 200\text{m}$, on a flat ground.

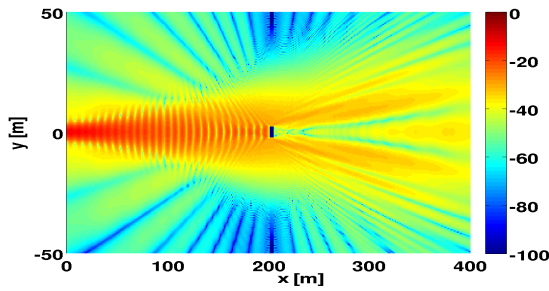


Figure 5: Horizontal field component in the horizontal plane $z = 12.5\text{m}$, in the presence of the building.

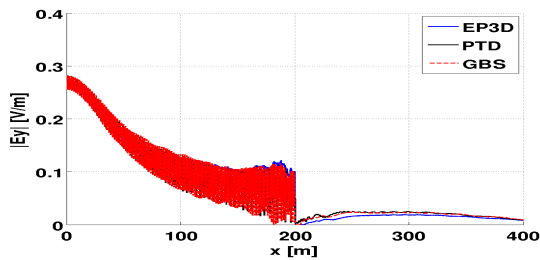


Figure 6: Horizontal field component along the beam axis: comparison between 3DPWE, PTD and GBS.

4 CONCLUSION

Computation of propagated fields by a frame-based Gaussian beam shooting algorithm has been performed in test case environments involving reflecting/diffracting obstacles. Diffraction is accounted for in an approximate way, through frame redecomposition on reflecting surfaces. Numerical results compare very well with results obtained with the FEKO code, through a Method of Moments in the case involving a single screen, through PTD in the case of a single building. Results involving both types of obstacles, as a model for a realistic non line of sight situation, will be presented at the conference.

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