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An Energy Stable Monolithic Eulerian Fluid-Structure Numerical Scheme *

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Abstract

The conservation laws of continuum mechanics, written in an Eulerian frame, do not distinguish fluids and solids, except in the expression of the stress tensors, usually with Newton's hypothesis for the fluids and Helmholtz potentials of energy for hyperelastic solids. By taking the velocities as unknown monolithic methods for fluid structure interactions (FSI) are built. In this article such a formulation is analysed when the fluid is compressible and the fluid is incompressible. The idea is not new but the progress of mesh generators and numerical schemes like the Characteristics-Galerkin method render this approach feasible and reasonably robust. In this article the method and its discretisation are presented, stability is discussed through an energy estimate. A numerical section discusses implementation issues and presents a few simple tests.

AMS classification 65M60 (74F10 74S30 76D05 76M25).

Introduction

Currently two methods dominate FSI (Fluid-Structure-Interaction) science: Arbitrary Lagrangian Eulerian (ALE) methods especially for thin structures [30][34] and immersed boundary methods (IBM)[31][12], for which the mathematical analysis is more advanced[6] but the numerical implementations lag behind. ALE for large displacements have meshing difficulties [27] and to a lesser extent with the matching conditions at the fluid-solid interface[25]. Furthermore, iterative solvers for ALE-based FSI methods which rely on alternative solutions of the fluid and the structure parts are subject to the added mass effect and require special solvers[17][8].

Alternatives to ALE and IBM are few. One old method [2][3] has resurfaced recently, the so-called *actualized Lagrangian methods* for computing structures [24] [28] (see also [11] although different from the present study because it deals mostly with membranes).

^{*}Written in honour of Philippe Ciarlet for his 80th birthday.

Continuum mechanics doesn't distinguish between solids and fluids till it comes to the constitutive equations. This has been exploited numerically in several studies but most often in the context of ALE[26][22][36].

In the present study, which is a follow-up of [33] and [20], we investigate what Stephan Turek [22] Heil [21] and Wang [38] call a monolithic formulation but here in an Eulerian framework, as in [14] [15] [35] [16], following the displaced geometry of the fluid and the solid. In [14], the authors obtained excellent results with the fully Eulerian formulation adopted here but at the cost of meshing difficulties to handle the Lagrangian derivatives. Here we advocated the Characteristic-Galerkin method and obtain an energy estimate, which is not a proof of stability but a prerequisite for it.

1 Conservation Laws

Let the time dependent computational domain Ω_t be made of a fluid region Ω_t^f and a solid region Ω_t^s with no overlap: $\overline{\Omega}_t = \overline{\Omega}_t^f \cup \overline{\Omega}_t^s$, $\Omega_t^f \cap \Omega_t^s = \emptyset$ at any times $t \in (0, T)$. At initial time Ω_0^f and Ω_0^s are prescribed.

Let the fluid-structure interface be $\Sigma_t = \overline{\Omega}_t^f \cap \overline{\Omega}_t^s$ and the boundary of Ω_t be $\partial \Omega_t$. The part of $\partial \Omega_t$ on which either the structure is clamped or on which there is a no slip condition on the fluid, that part is denoted by Γ and assumed to be independent of time.

The following standard notations are used. For more details see one of a textbook: [10],[29],[2],[1], or the following article: ,[22],[26]. For clarity we use bold characters for vectors and tensors/matrices, with some exceptions, like $x, x^0 \in \mathbb{R}^d, d = 2$ or 3.

- $\mathbf{X}: \Omega_0 \times (0,T) \mapsto \Omega_t: \mathbf{X}(x^0,t)$, the Lagrangian position at t of x^0 .
- $\mathbf{u} = \partial_t \mathbf{X}$, the velocity of the deformation,
- $\mathbf{F} = \nabla^T \mathbf{X} = ((\partial_{x_i} \mathbf{X}_j))$, the Jacobian of the deformation,

•
$$J = \det_{\mathbf{H}}$$

We denote by tr_A and det_A the trace and determinant of A. To describe the fluid structure system we need the following:

- $\rho = \mathbf{1}_{\Omega_t^f} \rho^f + \mathbf{1}_{\Omega_t^s} \rho^s$, the density,
- $\sigma = \mathbf{1}_{\Omega^f} \sigma^f + \mathbf{1}_{\Omega^s_t} \sigma^s$, the stress tensor,
- $\mathbf{f}(x,t)$ the density of volumic forces at x, t.
- $\mathbf{d} = \mathbf{X}(x^0, t) x^0$, the displacement.

Finally and unless specified all spatial derivatives are with respect to $x \in \Omega_t$ and not with respect to $x^0 \in \Omega_0$. Let ϕ a function of x, t; as $x = \mathbf{X}(x^0, t), x^0 \in \Omega_0, \phi$ is also a function of x^0 and we have:

$$abla_{x^0}\phi = [\partial_{x^0_j}\phi] = [\partial_{x^0_j}\mathbf{X}_j\partial_{x_j}\phi] = \mathbf{F}^T
abla \phi.$$

When **X** is one-to-one and invertible, **d** and **F** can be seen as functions of (x, t) instead of (x^0, t) . They are related by

$$\mathbf{F}^{T} = \nabla_{x^{0}} \mathbf{X} = \nabla_{x^{0}} (\mathbf{d} + x^{0}) = \nabla_{x^{0}} \mathbf{d} + \mathbf{I} = \mathbf{F}^{T} \nabla \mathbf{d} + \mathbf{I}, \quad \Rightarrow \quad \mathbf{F} = (\mathbf{I} - \nabla \mathbf{d})^{-T}$$

Time derivatives are related by (note the notation \mathbb{D}_t)

$$\mathbb{D}_t \phi := \frac{d}{dt} \phi(\mathbf{X}(x_0, t), t)|_{x = \mathbf{X}(x_0, t)} = \partial_t \phi(x, t) + \mathbf{u} \cdot \nabla \phi(x, t)$$

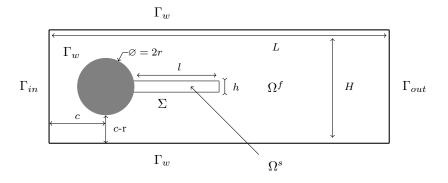


Figure 1.1: The geometry of the FLUSTRUK test[16]. The cylinder (in black) is fixed but the flag is a thick compressible Mooney-Rivlin material clamped to the cylinder by its left boundary; the outer rectangle is filled with a fluid which enters from the left Γ_{in} and leaves on the right Γ_{out} ; the horizontal boundaries of the outer rectangle are walls, so they form together with the cylinder the boundary Γ_w . The flag is at time zero a rectangle of size $l \times h$. The outer rectangle has size $L \times H$. The center of the circle representing the cylinder is at (c, c) in a frame of reference which has the lower left corner at (0,0); the cylinder has radius r and is fixed.

It is convenient to introduce (note the difference between \mathbb{D}_t above and D here):

$$D\mathbf{u} = \nabla \mathbf{u} + \nabla^T \mathbf{u}$$

Conservation of momentum and conservation of mass take the same form for the fluid and the solid:

$$\rho \mathbb{D}_t \mathbf{u} = \mathbf{f} + \nabla \cdot \sigma, \quad \mathbb{D}_t \rho + \rho \nabla \cdot \mathbf{u} = \mathbb{D}_t (J\rho) = 0.$$

So $J\rho = \rho_0$ at all times and

$$J^{-1}\rho_0 \mathbb{D}_t \mathbf{u} = f + \nabla \cdot \sigma \text{ in } \Omega_t, \ \forall t \in (0,T),$$
(1.1)

with continuity of **u** and of $\sigma \cdot \mathbf{n}$ at the fluid-structure interface Σ in absence of interface constraint like surface tension. There are also unwritten constraints pertaining to the realisability of the map **X** (see [10],[29]).

1.1 Constitutive Equations

We consider a bi-diemsional geometry. For the 3d case, see [9].

- For a Newtonian incompressible fluid : $\sigma^f = -p^f \mathbf{I} + \mu^f \mathbf{D} \mathbf{u}$
- For an hyperelastic material : $\sigma^s = \rho^s \partial_{\mathbf{F}} \Psi \mathbf{F}^T$

where Ψ is the Helmholtz potential which, in the case of a S^t-Venant-Kirchhoff material, is [10]

$$\Psi(\mathbf{F}) = \frac{\lambda^s}{2} \operatorname{tr}_{\mathbf{E}}^2 + \mu^s \operatorname{tr}_{\mathbf{E}^2}, \quad \mathbf{E} = \frac{1}{2} (\mathbf{F}^T \mathbf{F} - \mathbf{I})$$
(1.2)

It is easy to see that $tr_{\mathbf{E}} = \frac{1}{2} tr_{\mathbf{F}^T \mathbf{F}} - 1$ and

$$\partial_{\mathbf{F}} \mathrm{tr}_{\mathbf{F}^T\mathbf{F}^-} = ((\partial_{\mathbf{F}_{ij}}\sum_{m,n}F_{m,n}^2)) = 2\mathbf{F} \ \ \Rightarrow \ \partial_{\mathbf{F}} \mathrm{tr}_{\mathbf{E}} = \mathbf{F}$$

$$\partial_{\mathbf{F}} \operatorname{tr}_{(\mathbf{F}^T \mathbf{F})^2} = \left(\left(\partial_{\mathbf{F}_{ij}} \sum_{n,m,p,k} F_{n,k} F_{n,m} F_{p,m} F_{p,k} \right) \right) = 4 \mathbf{F} \mathbf{F}^T \mathbf{F}$$
(1.3)

which implies that $\partial_{\mathbf{F}} \operatorname{tr}_{\mathbf{E}^2} = 2\mathbf{F}\mathbf{E}$. Therefore

$$\partial_{\mathbf{F}} \Psi(\mathbf{F}) \mathbf{F}^{T} = (\lambda^{s} \operatorname{tr}_{\mathbf{E}} \mathbf{F} + 2\mu^{s} \mathbf{F} \mathbf{E}) \mathbf{F}^{T}$$

which in turn implies that

$$\sigma^{s} = \rho^{s} \mathbf{F} (\lambda^{s} \operatorname{tr}_{\mathbf{E}} + 2\mu^{s} \mathbf{E}) \mathbf{F}^{T} = J^{-1} \rho_{0}^{s} \mathbf{F} (\lambda^{s} \operatorname{tr}_{\mathbf{E}} + 2\mu^{s} \mathbf{E}) \mathbf{F}^{T}$$

For a tensor **A** define $|\mathbf{A}| = \sum_{ij} A_{ij}^2$.

Remark 1. Some authors have a different definition for the Lamé coefficient $\lambda \rho_0^s \to \lambda, \ \mu \rho_0^s \to \mu$ which define σ^s .

Proposition 1. Let $\gamma = tr_{\mathbf{FF}^T}$; then

 γ

$$= tr_{\mathbf{F}\mathbf{F}^T} = (2 - 2\nabla \cdot \mathbf{d} + |\nabla \mathbf{d}|^2)J^2, \ \tilde{\gamma} = \gamma J^{-2}$$

and the following holds

$$\sigma^{s} = \rho^{s} \left(a \mathbf{I} + 2b (\mathbf{D} \mathbf{d} - \nabla \mathbf{d} \nabla^{T} \mathbf{d}) \right), \quad with$$

$$a = \lambda^{s} \left(\frac{1}{2} \gamma - 1 \right) (\tilde{\gamma} - 1) + \mu^{s} (\gamma - J^{2} - 1) \tilde{\gamma},$$

$$b = \frac{1}{2} \left(\frac{\lambda^{s}}{2} + \mu^{s} \right) (\gamma - 1) - \frac{\lambda^{s}}{4}$$
(1.4)

Proof

First note that if $\mathbf{B} = \mathbf{F}\mathbf{F}^T$ then

$$\sigma^{s} = \rho^{s} \left[\left[\lambda^{s} \left(\frac{1}{2} \gamma - 1 \right) - \mu^{s} \right] \mathbf{B} + \mu^{s} \mathbf{B}^{2} \right]$$
(1.5)

Now by the Cayley- Hamilton theorem in 2 dimensions, $\mathbf{B}^2 - \gamma \mathbf{B} + J^2 \mathbf{I} = 0$. As $\mathbf{B}^{-1} = I - \mathbf{D}\mathbf{d} + \nabla \mathbf{d}\nabla^T \mathbf{d}$ let $\mathbf{C} = \mathbf{I} - \mathbf{B}^{-1} = \mathbf{D}\mathbf{d} - \nabla \mathbf{d}\nabla^T \mathbf{d}$. Then

$$\mathbf{B} = \gamma \mathbf{I} - J^2 \mathbf{B}^{-1} = (\gamma - J^2) \mathbf{I} + J^2 \mathbf{C}, \ \mathbf{B}^2 = (\gamma^2 - (1 + \gamma)J^2) \mathbf{I} + \gamma J^2 \mathbf{C}.(1.6)$$

Therefore

$$\sigma^{s} = \rho^{s} \Big[[\lambda^{s} (\frac{1}{2}\gamma - 1) - \mu^{s}] [(\gamma - J^{2})\mathbf{I} + J^{2}\mathbf{C}] + \mu^{s} [(\gamma^{2} - (1 + \gamma)J^{2})\mathbf{I} + \gamma J^{2}\mathbf{C}] \Big]$$

= $\rho^{s} \Big[[(\lambda^{s} (\frac{1}{2}\gamma - 1))(\gamma - J^{2}) + \mu^{s} \gamma (\gamma - 1 - J^{2})]\mathbf{I} + [\lambda^{s} (\frac{1}{2}\gamma - 1) + \mu^{s} (\gamma - 1)]J^{2}\mathbf{C} \Big]$ (1.7)

1.2 Variational Monolithic Eulerian Formulation

From now on we limit our analysis to the case ρ_0^s, ρ_0^f constant.

One must find (\mathbf{u}, p) with $\mathbf{u}_{|\Gamma} = 0$, \mathbf{d} and Ω_t^s , Ω^f , solution for all $(\hat{\mathbf{u}}, \hat{p})$ with $\hat{\mathbf{u}}_{|\Gamma} = 0$ of

$$\begin{pmatrix}
\int_{\Omega_t^f} \left[\rho^f \mathbb{D}_t \mathbf{u} \cdot \hat{\mathbf{u}} - p \nabla \cdot \hat{\mathbf{u}} - \hat{p} \nabla \cdot \mathbf{u} + \frac{\mu^f}{2} \mathrm{D} \mathbf{u} : \mathrm{D} \hat{\mathbf{u}} \right] \\
+ \int_{\Omega_t^s} \rho^s \left[\mathbb{D}_t \mathbf{u} \cdot \hat{\mathbf{u}} + b (\mathrm{D} \mathbf{d} - \nabla \mathbf{d} \nabla^T \mathbf{d}) : \mathrm{D} \hat{\mathbf{u}} + a \nabla \cdot \hat{\mathbf{u}} \right] = \int_{\Omega_t} f \cdot \hat{\mathbf{u}} \quad (1.8) \\
\mathbb{D}_t \mathbf{d} = \mathbf{u}, \quad J^{-1} = \det_{\mathbf{I} - \nabla \mathbf{d}}, \quad \rho^r = J^{-1} \rho_0^r, \\
\langle \dot{x}(t) = \mathbf{u}(x(t), t), \quad x(0) = x_0 \in \Omega_0^r \Rightarrow x(t) \in \Omega_t^r \}, \quad r = s, f.
\end{cases}$$

For an existence result, up to time T^* , see [4] [13] (see also [37]), provided a regularization term is added to the formulation to insure that $\partial_t \mathbf{d}$ has H^1 regularity; T^* is such that the solid does not touch the boundary and Σ_t does not buckle.

4

2 Numerical Scheme

For the stability of the numerical scheme, the problem is that even for small displacements the Lamé terms $\mu^s \nabla \mathbf{u} : \nabla \hat{\mathbf{u}} + \lambda^s \nabla \cdot \mathbf{u} \nabla \cdot \hat{\mathbf{u}}$ are hidden in $b \mathrm{D} \mathbf{d} : \mathrm{D} \hat{\mathbf{u}}$ and $a \nabla \cdot \hat{\mathbf{u}}$ in the above variational formulation (1.8).

But notice that

$$J^{2} = 1 + 2\nabla \cdot \mathbf{d} - 2\det_{\nabla \mathbf{d}} + 3(\nabla \cdot \mathbf{d})^{2} + o(|\nabla \mathbf{d}|^{2})$$

$$\gamma = 2(1 + \nabla \cdot \mathbf{d} + (\nabla \cdot \mathbf{d})^{2} + \frac{1}{2}|\nabla \mathbf{d}|^{2} - 2\det\nabla \mathbf{d}) + o(|\nabla \mathbf{d}|^{2})$$

$$(\frac{\gamma}{2} - 1)(\tilde{\gamma} - 1) = \nabla \cdot \mathbf{d} - (\nabla \cdot \mathbf{d})^{2} - \frac{1}{2}|\nabla \mathbf{d}|^{2} - 2\det\nabla \mathbf{d} + o(|\nabla \mathbf{d}|^{2}) (2.1)$$

So it makes sense to define

$$c = a - \lambda^s \nabla \cdot \mathbf{d} \tag{2.2}$$

To prepare the time discretisation of (1.8) with a given time step δt , let

$$\bar{\mathbf{d}} = \mathbf{d} - \delta t \mathbf{u} \tag{2.3}$$

Then (1.8) becomes

$$\begin{cases} \int_{\Omega_t^f} \left[\rho \mathbb{D}_t \mathbf{u} \cdot \hat{\mathbf{u}} - p \nabla \cdot \hat{\mathbf{u}} - \hat{p} \nabla \cdot \mathbf{u} + \frac{\mu^f}{2} \mathbf{D} \mathbf{u} : \mathbf{D} \hat{\mathbf{u}} \right] \\ + \int_{\Omega_t^s} \rho \delta t \left[b (\mathbf{D} \mathbf{u} - \nabla \bar{\mathbf{d}} \nabla^T \mathbf{u} - \nabla \mathbf{u} \nabla^T \bar{\mathbf{d}} + \delta t \nabla \mathbf{u} \nabla^T \mathbf{u}) : \mathbf{D} \hat{\mathbf{u}} + \lambda^s \nabla \cdot \mathbf{u} \nabla \cdot \hat{\mathbf{u}} \right] \\ + \int_{\Omega_t^s} \rho \left[\mathbb{D}_t \mathbf{u} \cdot \hat{\mathbf{u}} + b (\mathbf{D} \bar{\mathbf{d}} - \nabla \bar{\mathbf{d}} \nabla^T \bar{\mathbf{d}}) : \mathbf{D} \hat{\mathbf{u}} + (c + \lambda^s \nabla \cdot \bar{\mathbf{d}}) \nabla \cdot \hat{\mathbf{u}} \right] = \int_{\Omega_t} f \cdot \hat{\mathbf{u}} \\ \mathbb{D}_t \mathbf{d} = \mathbf{u}, \quad \rho = \rho_0 \mathrm{det}_{\mathbf{I} - \nabla \mathbf{d}}. \end{cases}$$

Here linear elasticity is visible because the zero order term of b is $\frac{\mu^f}{2}$. From now on we do not use $\bar{\mathbf{d}}$ because the Characteristics-Galerkin discretisation of $\mathbb{D}_t \mathbf{d} = \mathbf{u}$ will give an analogue of (2.3).

2.1 Discretisation of Total Derivatives

Let $\Omega \subset \mathbb{R}^d$, $\mathbf{u} \in \mathbf{H}_0^1(\Omega) = (H_0^1(\Omega))^d$, (d = 2 here), $t \in (0,T)$ and $x \in \Omega$. Then let $\chi_{\mathbf{u},x}^t(\tau)$ be the solution at time τ of

$$\dot{\chi}(\tau) = \mathbf{u}(\chi(\tau), \tau)$$
 with $\chi(t) = x$.

If \mathbf{u} is Lipschitz in space and continuous in time the solution exists. The Characteristics-Galerkin method relies on the concept of total derivative:

$$\mathbb{D}_t \mathbf{v}(x,t) := \frac{d}{d\tau} \mathbf{v}(\chi(\tau),\tau)|_{\tau=t} = \partial_t \mathbf{v} + \mathbf{u} \cdot \nabla \mathbf{v}.$$

Given a time step δt , let us approximate

$$\chi_{\mathbf{u}^{n+1},x}^{(n+1)\delta t}(n\delta t) \approx \mathbb{Y}^{n+1}(x) := x - \mathbf{u}^{n+1}(x)\delta t$$

Remark 2. Note also that, as $J\rho$ is convected by **u**, that is $J\rho|_{\chi_{\mathbf{u},x}^t(\tau),\tau} = J\rho|_{x,t}$, so a consistent approximation is

$$(J^n \rho_n) \circ \mathbb{Y}^{n+1}(x) = J^{n+1}(x)\rho_{n+1}(x), \ x \in \Omega_{n+1}$$

Thus discretizing the total derivative of ${\bf u}$ or the one of $\rho_0 {\bf u}$ will give the same scheme.

$$\rho_{0}(x)\frac{\mathbf{u}^{n+1}(x) - \mathbf{u}^{n}(\mathbb{Y}^{n+1}(x))}{\delta t} = J^{n+1}\rho_{n+1}\frac{\mathbf{u}^{n+1} - \mathbf{u}^{n} \circ \mathbb{Y}^{n+1}}{\delta t}$$
$$= \frac{J^{n+1}\rho_{n+1}\mathbf{u}^{n+1} - (J^{n}\rho_{n}\mathbf{u}^{n}) \circ \mathbb{Y}^{n+1}}{\delta t} = \frac{\rho_{0}\mathbf{u}^{n+1} - (\rho_{0}\mathbf{u}^{n}) \circ \mathbb{Y}^{n+1}}{\delta t} (2.4)$$

2.2 Updating the fluid and solid domain

From the definition of \mathbb{Y} , notice that the only way to be consistent is to define Ω_{n+1} using \mathbf{u}^{n+1} , i.e. implicitly, since the later is defined also on Ω_{n+1} :

$$\Omega_{n+1} = (\mathbb{Y}^{n+1})^{-1}(\Omega_n) = \{x : \mathbb{Y}^{n+1}(x) := x - \mathbf{u}^{n+1}(x)\delta t \in \Omega_n\}$$

2.3 The Time Discretized Scheme

Let

$$\tilde{\mathbf{d}}^{n} := \mathbf{d}^{n} \circ \mathbb{Y}^{n+1}, \ \mathbf{d}^{n+1} = \tilde{\mathbf{d}}^{n} + \delta t \mathbf{u}^{n+1}, \ \rho_{n+1} = \rho_{0} \det_{\mathbf{I} - \nabla \mathbf{d}^{n+1}}.$$
 (2.5)

Let \tilde{b}_n, \tilde{c}_n be given by (1.4,2.2) computed with \tilde{d}^n . The following defines $\mathbf{u}^{n+1}, p^{n+1}$ with $\mathbf{u}^{n+1}|_{\Gamma} = 0$: $\forall \hat{\mathbf{u}}, \hat{p}$, with $\hat{\mathbf{u}}|_{\Gamma} = 0$,

$$\begin{cases} \int_{\Omega_{n+1}} \rho_{n+1} \frac{\mathbf{u}^{n+1} - \mathbf{u}^n \circ \mathbb{Y}^{n+1}}{\delta t} \cdot \hat{\mathbf{u}} \\ + \int_{\Omega_{n+1}^f} \left[-p^{n+1} \nabla \cdot \hat{\mathbf{u}} - \hat{p} \nabla \cdot \mathbf{u}^{n+1} + \frac{\mu^f}{2} \mathbf{D} \mathbf{u}^{n+1} : \mathbf{D} \hat{\mathbf{u}} \right] \\ + \int_{\Omega_{n+1}^s} \rho_{n+1} \delta t \left[\tilde{b}_n (\mathbf{D} \mathbf{u}^{n+1} - \nabla \tilde{\mathbf{d}}^n \nabla^T \mathbf{u}^{n+1} - \nabla \mathbf{u}^{n+1} \nabla^T \tilde{\mathbf{d}}^n) : \mathbf{D} \hat{\mathbf{u}} \\ + \lambda^s \nabla \cdot \mathbf{u}^{n+1} \nabla \cdot \hat{\mathbf{u}} \right] \\ + \int_{\Omega_{n+1}^s} \left[\tilde{b}_n (\mathbf{D} \tilde{\mathbf{d}}^n - \nabla \tilde{\mathbf{d}}^n \nabla^T \tilde{\mathbf{d}}^n) : \mathbf{D} \hat{\mathbf{u}} + (\tilde{c}_n + \lambda^s \nabla \cdot \tilde{\mathbf{d}}^n) \nabla \cdot \hat{\mathbf{u}} \right] \\ = \int_{\Omega_{n+1}} f \cdot \hat{\mathbf{u}}. \end{cases}$$
(2.6)

2.4 Iterative Solution by Fixed Point

The most natural method to solve the above is to freeze some coefficients so as to obtain a well posed linear problem and iterate:

- 1. Start with $\mathbf{u} = \mathbf{u}^n$, $\mathbb{Y}(x) = x \mathbf{u}\delta t$, $\Omega^r = \mathbb{Y}^{-1}(\Omega_n^r)$, r = s, f.
- 2. Set $\tilde{\mathbf{d}}^n = \mathbf{d}^n \circ \mathbb{Y}$, $\tilde{\rho}_n = \rho_0 \det_{\mathbf{I} \nabla \tilde{\mathbf{d}}}$; compute \tilde{b}_n, \tilde{c}_n .
- 3. Find $\mathbf{u}^{n+1}, p^{n+1}$ by solving

$$\begin{cases} \int_{\Omega} \tilde{\rho}_{n} \frac{\mathbf{u}^{n+1} - \mathbf{u}^{n} \circ \mathbb{Y}}{\delta t} \cdot \hat{\mathbf{u}} \\ + \int_{\Omega^{f}} \left[-p^{n+1} \nabla \cdot \hat{\mathbf{u}} - \hat{p} \nabla \cdot \mathbf{u}^{n+1} + \frac{\mu^{f}}{2} \mathrm{D} \mathbf{u}^{n+1} : \mathrm{D} \hat{\mathbf{u}} \right] \\ + \int_{\Omega^{s}} \tilde{\rho}_{n} \delta t \left[\tilde{b}_{n} (\mathrm{D} \mathbf{u}^{n+1} - \nabla \tilde{\mathbf{d}}^{n} \nabla^{T} \mathbf{u}^{n+1} - \nabla \mathbf{u}^{n+1} \nabla^{T} \tilde{\mathbf{d}}^{n}) : \mathrm{D} \hat{\mathbf{u}} \\ + \lambda^{s} \nabla \cdot \mathbf{u}^{n+1} \nabla \cdot \hat{\mathbf{u}} \right] \\ + \int_{\Omega^{s}} \left[\tilde{b}_{n} (\mathrm{D} \tilde{\mathbf{d}}^{n} - \nabla \tilde{\mathbf{d}}^{n} \nabla^{T} \tilde{\mathbf{d}}^{n}) : \mathrm{D} \hat{\mathbf{u}} + (\tilde{c}_{n} + \lambda^{s} \nabla \cdot \tilde{\mathbf{d}}^{n}) \nabla \cdot \hat{\mathbf{u}} \right] \\ = \int_{\Omega} f \cdot \hat{\mathbf{u}} \end{cases}$$
(2.7)

Set u = uⁿ⁺¹, 𝒱(x) = x − uδt, Ω^r = 𝒱⁻¹(Ω^r_n), r = s, f.
 If not converged return to Step 2 else set dⁿ⁺¹ = dⁿ ∘ 𝒱 + δtuⁿ⁺¹.

 $\mathbf{6}$

Notice that (2.7) is a well posed linear problem whenever

$$A(\mathbf{u}, \hat{\mathbf{u}}) = \int_{\Omega^s} \left[\frac{\rho}{\delta t} \mathbf{u} \cdot \hat{\mathbf{u}} + \tilde{b} (\mathrm{D}\mathbf{u} - \nabla \tilde{\mathbf{d}}^n \nabla^T \mathbf{u} - \nabla \mathbf{u} \nabla^T \tilde{\mathbf{d}}^n) : \mathrm{D}\hat{\mathbf{u}} + \lambda^s \nabla \cdot \mathbf{u} \nabla \cdot \hat{\mathbf{u}} \right]$$

is coercive. Then (2.7) gives a solution bounded in $\mathbf{H}^{1}(\Omega)$ and converging subsequences can be extracted from $\rho_{n+1}, \mathbf{u}^{n+1}, \Omega_{n+1}^{r}$ when $\bar{\Omega} = \overline{\Omega_{n}^{f} \cup \Omega_{n}^{s}}$ is fixed. Then convergence would occur if we could prove that Ω_{n+1}^{r} converges.

2.5 Spatial Discretisation with Finite Elements

Let \mathcal{T}_h^0 be a triangulation of the initial domain. Spatial discretisation can be done with the most popular finite element for fluids: the Lagrangian triangular elements of degree 2 for the space V_h of velocities and displacements and Lagrangian triangular elements of degree 1 for the pressure space Q_h ; later we will also discuss the stabilised $P^1 - P^1$ element; provision must be made for two pressure variables, one in the structure and one in the fluid because the pressure is discontinuous at the interface Σ ; therefore Q_h is the space of piecewise linear functions on the triangulation continuous in Ω_{n+1}^r , r = s, f. A small penalization with parameter ϵ must be added to impose uniqueness of the pressure.

This leads us to find $\mathbf{u}_h^{n+1} \in V_{h0_{\Gamma}}, p_h^{n+1} \in Q_h, \Omega_{n+1}$ such that for all $\hat{\mathbf{u}}_h, \hat{p}_h \in V_{h0_{\Gamma}} \times Q_h$ with

$$\tilde{\mathbf{d}}_h^n := \mathbf{d}_h^n \circ \mathbb{Y}^{n+1}, \text{ where } \mathbb{Y}^{n+1}(x) = x - \mathbf{u}_h^{n+1}(x)\delta t,$$

the following holds:

$$\begin{cases} \mathbf{a}(\tilde{\rho}_{n},\tilde{b}_{n},\tilde{c}_{n};\mathbf{u}^{n+1},\hat{\mathbf{u}}) := \int_{\Omega_{n+1}} \tilde{\rho}_{n} \frac{\mathbf{u}_{h}^{n+1} - \mathbf{u}_{h}^{n} \circ \mathbb{Y}^{n+1}}{\delta t} \cdot \hat{\mathbf{u}}_{h} \\ + \int_{\Omega_{n+1}^{f}} \left[-p^{n+1}\nabla \cdot \hat{\mathbf{u}}_{h} - \hat{p}\nabla \cdot \mathbf{u}_{h}^{n+1} + \frac{\mu^{f}}{2} \mathrm{D}\mathbf{u}_{h}^{n+1} : \mathrm{D}\hat{\mathbf{u}}_{h} \right] \\ + \int_{\Omega_{n+1}^{s}} \tilde{\rho}_{n}^{s} \delta t \left[\tilde{b}_{n}(\mathrm{D}\mathbf{u}_{h}^{n+1} - \nabla \tilde{\mathbf{d}}_{h}^{n} \nabla^{T} \mathbf{u}_{h}^{n+1} - \nabla \mathbf{u}_{h}^{n+1} \nabla^{T} \tilde{\mathbf{d}}_{h}^{n}) : \mathrm{D}\hat{\mathbf{u}}_{h} \\ + \lambda^{s} \nabla \cdot \mathbf{u}_{h}^{n+1} \nabla \cdot \hat{\mathbf{u}}_{h} \right] \\ + \int_{\Omega_{n+1}^{s}} \left[\tilde{b}_{n}(\mathrm{D}\tilde{\mathbf{d}}_{h}^{n} - \nabla \tilde{\mathbf{d}}_{h}^{n} \nabla^{T} \tilde{\mathbf{d}}_{h}^{n}) : \mathrm{D}\hat{\mathbf{u}}_{h} + (\tilde{c}_{n} + \lambda^{s} \nabla \cdot \tilde{\mathbf{d}}_{h}^{n}) \nabla \cdot \hat{\mathbf{u}}_{h} \right] \\ = \int_{\Omega_{n+1}} \mathbf{f} \cdot \hat{\mathbf{u}}_{h}, \qquad \Omega_{n+1} = (\mathbb{Y}^{n+1})^{-1}(\Omega_{n}) = \{x : \ \mathbb{Y}^{n+1}(x) \in \Omega_{n}\}. \end{cases}$$

Then \mathbf{d}

$$\mathbf{d}_h^{n+1} = \tilde{\mathbf{d}}_h^n + \delta t \mathbf{u}_h^{n+1}$$

2.6 Implementation

The various tests we made lead us to recommend the following:

• Move the vertices of the mesh in the structure with its own velocity:

$$q_i^{n+1} = q_i^n + \mathbf{u}_h^{n+1}(q_i^{n+1})\delta t$$
(2.9)

which, as explained above has to be implemented through an iterative process.

- Remesh the fluid part at each iteration with a Delaunay-Voronoi mesh generator from the boundary vertices (Σ_{n+1} included). This required the development of a specific module to identify computationally the vertices of the fluid-structure interface Σ , which are then input to the fluid mesh generator.
- In doing so, the discrete topological properties of the structural part are preserved and we have the important property that the value $\mathbf{d}[i]$ of \mathbf{d} at vertex q_i in the computer implementation of \mathbf{d} by an array of values at the nodes, satisfies

$$\mathbf{d}^{n+1}[i] = \mathbf{d}^n[i] + \delta t \mathbf{u}^{n+1}[i], \quad \forall i.$$

In other words $\mathbf{d}^n \circ \mathbb{Y}^{n+1}$ is $\mathbf{d}^n[i]$ after moving the vertices by (2.9).

3 Energy Estimate

3.1 Stability of the Scheme Discretized in Time

To conserve energy we need to change the scheme (2.8) slightly, from

$$\mathbf{a}(\tilde{\rho}_{n}, \tilde{b}_{n}, \tilde{c}_{n}; \mathbf{u}^{n+1}, \hat{\mathbf{u}}) = \int_{\Omega_{n+1}} \mathbf{f} \cdot \hat{\mathbf{u}}_{h} \text{ to}$$
$$\mathbf{a}(\rho_{n+1}, b_{n+1}, c_{n+1}; \mathbf{u}^{n+1}, \hat{\mathbf{u}}) + \delta t^{2} \int_{\Omega_{n+1}^{s}} \rho_{n+1}^{s} b_{n+1} \nabla \mathbf{u}_{h}^{n+1} \nabla^{T} \mathbf{u}_{h}^{n+1} : \mathbf{D} \hat{\mathbf{u}}_{h}$$
$$= \int_{\Omega_{n+1}} \mathbf{f} \cdot \hat{\mathbf{u}}_{h}$$
(3.1)

Lemma 3.1. The mapping $\mathbf{X}^n : \Omega_0 \mapsto \Omega_n$ is also $\mathbf{X}^{n+1} = (\mathbb{Y}^{n+1})^{-1} \circ \mathbf{X}^n$, $n \ge 1$ and the jacobian of the transformation is $\mathbf{F}^n := \nabla_{x_0}^T \mathbf{X}^n = (\mathbf{I} - \nabla \mathbf{d}^n)^{-T}$.

Proof

Notice that $\mathbb{Y}^1(\mathbb{Y}^2(..\mathbb{Y}^{n-1}(\mathbb{Y}^n(\Omega_n))..)) = \Omega_0$ Hence

$$\mathbf{X}^{n+1} = [\mathbb{Y}^{1}(\mathbb{Y}^{2}(..\mathbb{Y}^{n}(\mathbb{Y}^{n+1})))]^{-1} = (\mathbb{Y}^{n+1})^{-1} \circ \mathbf{X}^{n}.$$

By definition of \mathbf{d}^{n+1} in (2.5)

$$\mathbf{d}^{n+1}(\mathbf{X}^{n+1}(x_0)) = \mathbf{d}^n(\mathbb{Y}^{n+1}(\mathbf{X}^{n+1}(x_0))) + \mathbf{u}^{n+1}(\mathbf{X}^{n+1}(x_0))\delta t = \mathbf{d}^n(\mathbf{X}^n(x_0)) + \mathbf{u}^{n+1}(\mathbf{X}^{n+1}(x_0))\delta t, \qquad (3.2)$$

and since $\mathbf{X}^{n+1}(x_0) = \mathbf{d}^{n+1}(\mathbf{X}^{n+1}(x_0)) + x_0$ we have that

$$\mathbf{F}^{n+1} = \nabla_{x_0}^t (\mathbf{d}^{n+1}((\mathbf{X}^{n+1}(x_0))) + x_0),$$

= $\nabla \mathbf{d}^{n+1^T} \mathbf{F}^{n+1} + \mathbf{I} \Rightarrow \mathbf{F}^{n+1} = (\mathbf{I} - \nabla \mathbf{d}^{n+1})^{-T}$ (3.3)

 \diamond

Note that (3.2) shows also that

$$\mathbf{F}^{n+1} = \mathbf{F}^n + \delta t \nabla_{x_0}^T \mathbf{u}^{n+1} \tag{3.4}$$

Lemma 3.2. With Ψ defined by (1.2),

$$\int_{\Omega_{n+1}^s} \rho_{n+1}^s \left[b^{n+1} (\mathrm{D} \mathbf{d}^{n+1} - \nabla \mathbf{d}^{n+1} \nabla^T \mathbf{d}^{n+1}) : \mathrm{D} \hat{\mathbf{u}} + a^{n+1} \nabla \cdot \hat{\mathbf{u}} \right]$$
$$= \int_{\Omega_0^s} \partial_{\mathbf{F}} \Psi^{n+1} : \nabla_{x_0} \hat{\mathbf{u}}$$
(3.5)

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Proof By Proposition 1 and Lemma 3.1:

$$\int_{\Omega_{n+1}^{s}} \rho_{n+1}^{s} \left(a^{n+1} \mathbf{I} + 2b^{n+1} (\mathbf{D} \mathbf{d}^{n+1} - \nabla \mathbf{d}^{n+1} \nabla^{T} \mathbf{d}^{n+1}) \right) : \nabla \hat{\mathbf{u}}$$

$$= \int_{\Omega_{n+1}^{s}} \sigma_{n+1}^{s} : \nabla \hat{\mathbf{u}} = \int_{\Omega_{n+1}^{s}} \left[\rho_{n+1}^{s} \partial_{\mathbf{F}} \Psi \mathbf{F}^{T} \right] |_{n+1} : \nabla \hat{\mathbf{u}}$$

$$= \int_{\Omega_{n+1}^{s}} \left[J_{n+1}^{-1} \rho_{0}^{s} \partial_{\mathbf{F}} \Psi \mathbf{F}^{T} \right] |_{n+1} : \nabla \hat{\mathbf{u}} = \int_{\Omega_{0}^{s}} \rho_{0}^{s} \partial_{\mathbf{F}} \Psi^{n+1} : \nabla \hat{\mathbf{u}} \qquad (3.6)$$

Theorem 3.3. When f = 0 and ρ_0 is constant in each domain Ω_0^r , r = s, f, the numerical scheme (3.1) has the following property:

$$\int_{\Omega_n} \frac{\rho_n}{2} |\mathbf{u}^n|^2 + \delta t \sum_{k=1}^n \int_{\Omega_k^f} \frac{\mu^f}{2} |\mathbf{D}\mathbf{u}^k|^2 + \int_{\Omega_0^s} \Psi^n \le \int_{\Omega_0} \frac{\rho_0}{2} |\mathbf{u}^0|^2 + \int_{\Omega_0^s} \Psi^0(3.7)$$

Proof Let r = s or f. Let us choose $\hat{\mathbf{u}} = \mathbf{u}^{n+1}$ in (3.1). By Schwartz inequality

$$\begin{split} &\int_{\Omega_{n+1}^{r}} \rho_{n+1}(\mathbf{u}^{n} \circ \mathbb{Y}^{n+1}) \cdot \mathbf{u}^{n+1} = \rho_{0} \int_{\Omega_{n+1}^{r}} (J^{n+1})^{-1}(\mathbf{u}^{n}) \circ \mathbb{Y}^{n+1}) \cdot \mathbf{u}^{n+1} \\ &\leq \rho_{0} \left(\int_{\Omega_{n+1}^{r}} (J^{n+1})^{-1} (\mathbf{u}^{n} \circ \mathbb{Y}^{n+1})^{2} \right)^{\frac{1}{2}} \left(\int_{\Omega_{n+1}^{r}} (J^{n+1})^{-1} (\mathbf{u}^{n+1})^{2} \right)^{\frac{1}{2}} \\ &= \left[\int_{\Omega_{n}^{r}} \rho_{n} (\mathbf{u}^{n})^{2} \int_{\Omega_{n+1}^{r}} \rho_{n+1} (\mathbf{u}^{n+1})^{2} \right]^{\frac{1}{2}} \leq \frac{1}{2} \int_{\Omega_{n}^{r}} \rho_{n}^{r} \mathbf{u}^{n2} + \frac{1}{2} \int_{\Omega_{n+1}^{r}} \rho_{n+1}^{r} \mathbf{u}^{n+12}, \end{split}$$

Plugging this estimate in (3.1) with $\hat{\mathbf{u}} = \mathbf{u}^{n+1}$ leads to

$$\int_{\Omega_{n+1}} \frac{\rho_{n+1}}{2} |\mathbf{u}^{n+1}|^2 + \delta t \int_{\Omega_{n+1}^f} \frac{\mu^f}{2} |\mathbf{D}\mathbf{u}^{n+1}|^2 + \int_{\Omega_0} \Psi^{n+1} \le \int_{\Omega_n} \frac{\rho_n}{2} |\mathbf{u}^n|^2 + \int_{\Omega_0} \Psi^n$$

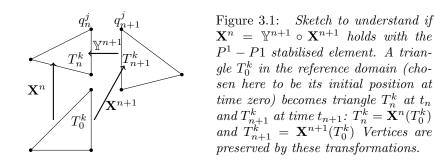
3.2 Energy Estimate for the Fully Discrete Scheme

The proof for the spatially continuous case will work for the discrete case if

$$\mathbf{X}^n = \mathbf{X}^{n+1} \circ \mathbb{Y}^{n+1}. \tag{3.8}$$

As discussed in [20] it may be possible to program an isoparametric $P^2 - P^1$ element for which (3.8) but it is certainly far from easy. On the other hand, consider the stabilised $P^1 - P^1$ element: the fluid pressure and the solid pressure are continuous and piecewise linear on the triangulation. The infsup condition for stability does not hold unless the incompressibility condition in the fluid, $\nabla \cdot \mathbf{u} = 0$, is changed to $-\epsilon \Delta p + \nabla \cdot \mathbf{u} = 0$, (see [5] for details). It amounts to adding $\epsilon \nabla p^{n+1} \nabla \hat{p}$ next to the term with μ^f in the variational formulations. Then (3.8) holds (see Figue 3.1) and the proof of the spatially continuous case can be adapted leading to (3.7) with an additional viscous term $\epsilon |\nabla p^{n+1}|^2$ next to the term with μ^f .

Remark 3. Because of energy preservation scheme (3.1), implemented via a fixed point algorithm as in (2.7), generates bounded sequences ρ , \mathbf{u} , q^i ; it seems safe to assess that out of these bounded subsequences will converge to a solution of the problem discretized in space but continuous in time when $\delta t \to 0$.



4 Numerical Tests

In our tests we have used the $P^2 - P^1$ element, confident that it will behave as well as the stabilised $P^1 - P_1$ element as indicated in [20].

4.1 The Cylinder-Flag Test

A compressible hyperelastic Mooney-Rivlin material, shaped as a rectangle of size $[0, l] \times [0, h]$, is attached behind a cylinder of radius r and beats in tune with the Karman vortices of the wake behind the cylinder; the fluid in the computational rectangular domain $[0, L] \times [0, H]$ enters from the left and is free to leave on the right. The center of the cylinder is at (c, c) (see figure 1.1). In [14] the following numerical values are suggested:

Geometry l = 0.35, h = 0.02, L = 2.5, H = 0.41, c = 0.2 which puts the cylinder slightly below the symmetry line.

Fluid density $\rho^f = 10^3 kg/m^3$ and a reduced viscosity $\nu^f = \frac{\mu^f}{\rho^f} = 10^{-3} m^2/s$; inflow horizontal velocity $\mathbf{u}(0, y) = \bar{U} \left(\frac{6}{H^2} y(H-y), 0\right)^T$ is a parabolic

profile with flux $\bar{U}H.$ Top and bottom boundaries are walls with no-slip conditions.

Solid
$$E = 2\mu(1+\sigma)/\rho^s$$
, $\sigma = 0.4$, $\lambda = \frac{E\sigma}{(1+\sigma)(1-2\sigma)}$

Initial velocities and displacements are zero. In all cases the same mesh is used initially with 2500 vertices. The time step is 0.005.

4.1.1 Free Fall of a Thick Flag

The gravity is g = 9.81 in Ω_t . When $\overline{U} = 0$, $\mu = 0.13510^6$ and $\rho^s = 20\rho^f$, the flag falls under its own weight; it comes to touch the lower boundary with zero velocity at time 0.49 and then moves up under its spring effect. This test is named FLUSTRUK-FSI-2^{*} in [14] but we have used a different value for μ because the one reported in [14] seems unlikely.

Figure 4.1 shows a zoom around the flag at the time when it has stopped to descend and started to move upward. Pressure lines are drawn in the flow region together with the mesh and the velocity vectors in the flag and drawn at each vertex. Figure 4.2 shows the coordinates of the upper right tip of the flag versus time.