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Miniature and Wide-Band ILA Antenna with Non-Foster Matching

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Abstract—In this paper, we present a miniature, wide-band, Inverted L Antenna (ILA) with non-Foster matching. The antenna size is $9.5 \times 19.5 \text{ mm}^2$ and it is integrated on a Printed Circuit Board (PCB) of $100 \times 60 \text{ mm}^2$. The antenna covers the whole frequency band of $(0.76 - 2.17) \text{ GHz}$ and the circuit is stable throughout this band.

Keywords—Electrically small antenna, miniaturization, non-Foster

I. INTRODUCTION

Antenna miniaturization is the key for a compact wireless technology. The main drawbacks of Electrically Small Antennas (ESAs) are their low efficiencies and narrow bandwidths even when a passive matching circuit is used. The maximum achievable bandwidth with passive matching is limited by the theoretical limits of Bode-Fano [1] and Chu-Harrington [2], [3]. A possible solution is the use of non-Foster matching that surpasses these limits [4] and enhances miniature antenna performance in reception [5]. A.J. Bahr showed that using an active coupling network with a receiving antenna (a short monopole) can significantly improve its Noise Figure (NF) [6]. Sussman-Fort experimentally showed that using a negative capacitor for matching a 152.4-mm monopole for $(20 - 110) \text{ MHz}$ frequency band presents a significant improvement in the Signal to Noise Ratio (SNR) compared to the same antenna without matching [7]. Koulouridis and Volakis demonstrated that using a non-Foster circuit to match a 152.4-mm loop can highly increase its bandwidth and decrease its resonance frequency [8]. G. Mishra et al presented a Bowtie antenna covering $(0.6 - 1.1) \text{ GHz}$ frequency band using a non-Foster circuit [9]. The design of non-Foster circuits becomes more challenging when targeting at higher frequencies (due to the active components non-Linearity) and when targeting high impedance values (due to the parasitic elements).

In this paper, we present a broadband miniature Inverted L Antenna (ILA) with a non-Foster matching. In particular, we focus our attention on exploiting the parasitic capacitance of the transistors in order to match this antenna requiring a high reactance value. By using the proposed non-Foster circuit, we demonstrate three times improvement in the antenna -10 dB bandwidth compared to the passive antenna. The realistic implementation and stability issues are discussed throughout the paper.

II. ANTENNA STRUCTURE AND NON-FOSTER CIRCUIT

The proposed antenna is an ILA of $9.5 \times 19.5 \text{ mm}^2$ integrated on a Printed Circuit Board (PCB) $100 \times 60 \text{ mm}^2$

as shown in Fig. 1(a). This antenna, printed on a 0.8mm-thick Rogers Duroid 5880 substrate, has a measured resonance frequency of 2.39 GHz (1(b)).

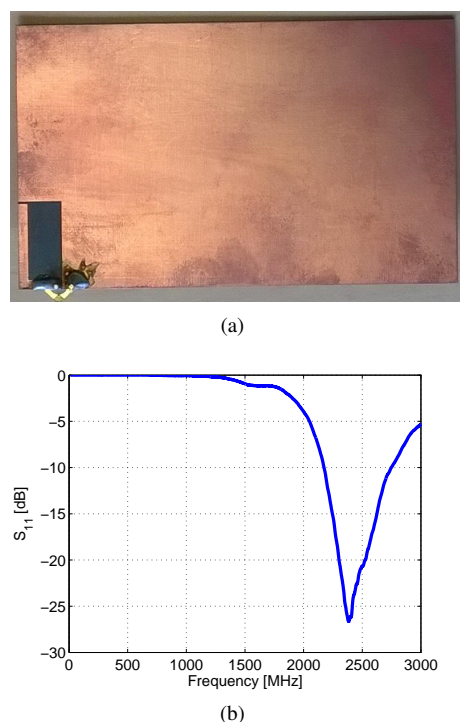


Fig. 1. Passive ILA. (a) The realized prototype, (b) measured input reflection coefficient magnitude in dB.

To eliminate the reactance of the antenna at 910 MHz , a negative capacitor of 0.7 pF is required. We optimized a Linvill floating type [10] Negative Impedance Converter (NIC) circuit to realize this capacitance as shown in Fig. 2. The active components in the circuit are BFR93A transistors [11]. The circuit is supplied by 4 V_{DC} , it consumes a current of 24 mA or equivalently a DC power of 96 mW . The measured reactance of this circuit is shown in Fig. 3(a). As it can be noticed, the circuit reactance decreases with frequency which means that the circuit has a non-Foster behavior (negative capacitance). The value of the equivalent capacitance is given in Fig. 3(b).

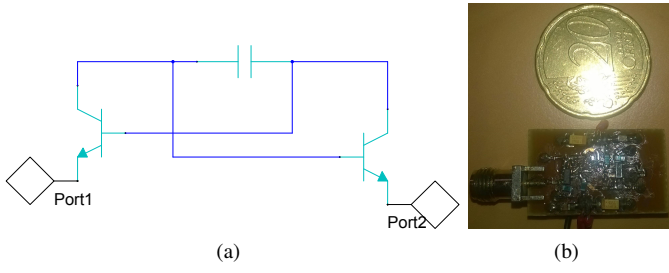


Fig. 2. Proposed NIC circuit. (a) General schematic of Linvill floating circuit and (b) photograph of the prototype.

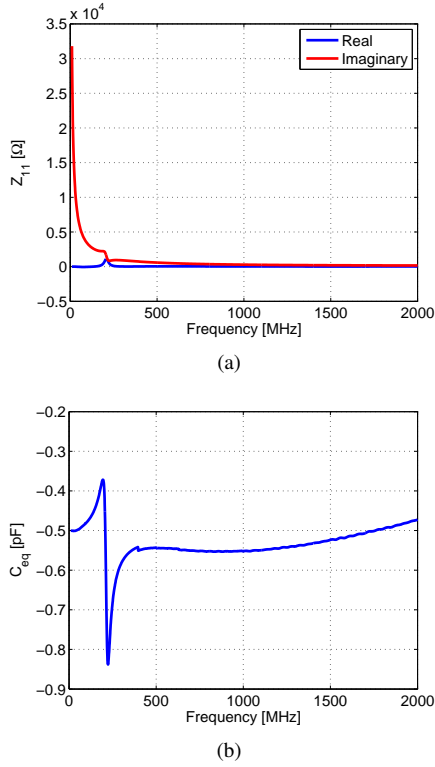


Fig. 3. Measured parameters of NIC circuit. (a) Input reactance and (b) equivalent capacitance.

III. ACTIVE ANTENNA PERFORMANCE

A prototype of the antenna with the non-Foster circuit was realized and measured. Fig. 4 shows a photograph of the active antenna with the NIC circuit on the bottom side. Fig. 5 shows the antenna measured input reflection coefficient magnitude in dB. It can be noticed that antenna has an impedance bandwidth of 100 % (matched throughout (0.76 – 2.17) GHz frequency band). The antenna was also tested for transistors non-linearity effect by increasing the input power level from -35 dB to 10 dBm. The measurement results given in Fig. 6 shows that the antenna is well suited for RF power levels less than 5 dBm. Finally, the antenna stability has been underlined using a spectrum analyzer (RIGOL DSA1030 [12]) with a Power Spectral Density (PSD) of -134 dBm/Hz. Fig. 7 shows the noise floor of the spectrum analyzer. It can be noticed that no visible additive noise affect the bandwidth of interest. To investigate the added noise by the non-Foster circuit, we compare the output of the spectrum analyzer when connected

to the non-Foster antenna and when connected to a 50Ω load. The measurement conditions are the same as before, however, the results are averaged on 10 cycles for fair comparison. The obtained results given in Fig. 8 shows that the added noise by the non-Foster circuit is negligible.

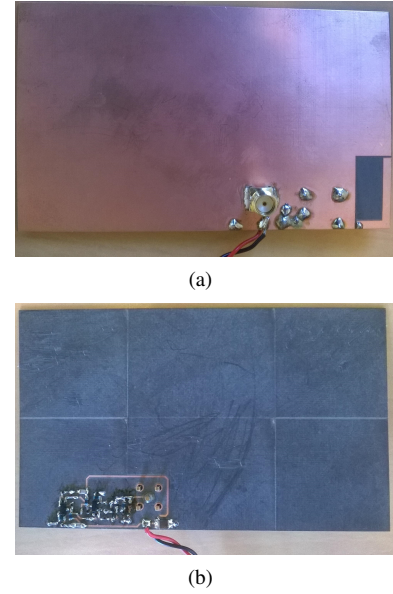


Fig. 4. A photograph of the fabricated active antenna. (a) Top view and (b) bottom view.

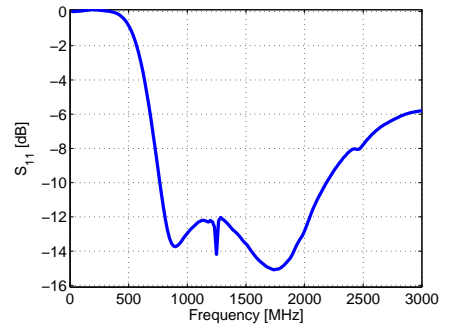


Fig. 5. The measured input reflection coefficient magnitude in dB of the active antenna.

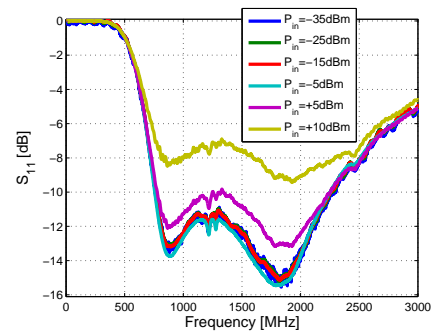
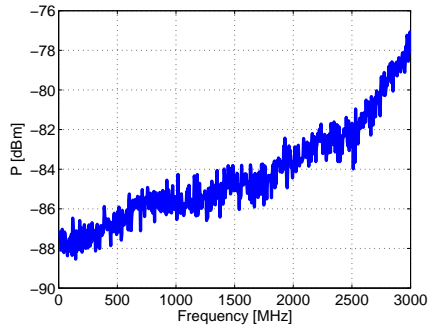
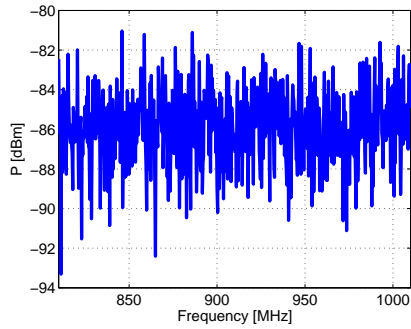


Fig. 6. The measured input reflection coefficient magnitude in dB of the active antenna for different input power levels.



(a)



(b)

Fig. 7. The noise floor level of the spectrum analyzer terminated at the input with the non-Foster matched antenna. (a) On $(0.01 - 3)$ GHz frequency band and (b) on $(0.81 - 1.01)$ GHz frequency band.

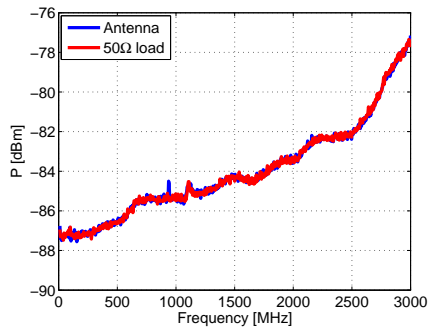


Fig. 8. A comparison between the noise floor levels of the spectrum analyzer terminated at the input with a matched load and non-Foster matched antenna.

IV. CONCLUSION

In this paper, we presented a miniature broadband ILA. The passive antenna resonant at 2.39 GHz was matched in the $(0.76 - 2.17)$ GHz band using a Linvill floating-type non-Foster circuit. The measurement results show that the antenna is stable and demonstrates a good behavior across the band of interest.

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REFERENCES

- [1] R. M. Fano, "Theoretical Limitations on the Broadband Matching of Arbitrary Impedances", J. Franklin Institution, vol. 249, pp. 57-83 and 139-155, January and February 1950.
- [2] L. J. Chu, "Physical Limitations of OmniDirectional Antennas", Journal of Applied Physics, vol. 19, no. 12, pp. 1163-1175, 1948.
- [3] R. F. Harrington, "On the Gain and Beamwidth of Directional Antennas", IRE Transactions on Antennas and Propagation, pp. 219-225, July 1958.
- [4] M. Hirvonen, A. Hujanen, J. Holmberg, and J.C.-E. Sten, "Bandwidth Limitations of Dipoles Matched with Non-Foster Impedances", The Second European Conference on Antennas and Propagation (EuCAP 2007), pp. 1,5, 11-16 November 2007.
- [5] J. T. Aberle, "Two-Port Representation of an Antenna with Application to Non-Foster Matching Networks", IEEE Transactions on Antennas and Propagation, vol. 56, no. 5, pp. 1218,1222, May 2008.
- [6] A. Bahr, "On The Use of Active Coupling Networks with Electrically Small Receiving Antennas", IEEE Transactions on Antennas and Propagation, vol. 25, no. 6, pp. 841,845, November 1977.
- [7] S. E. Sussman-Fort, "Matching Network Design Using NonFoster Impedances", International Journal of RF and Microwave ComputerAided Engineering, vol. 16, no. 2, p.p. 135-142, 2006.
- [8] S. Koulouridis, and J. L. Volakis, "Non-Foster Circuits for Small Broadband Antennas", IEEE Antennas and Propagation Society International Symposium (APSURSI 2009), pp.1,4, 1-5 June 2009.
- [9] G. Mishra, S. K. Sharma, and G. Rebeiz, "Non-Foster Matching of Eclectically Small Bowtie Antenna Covering 600MHz to 1100MHz", 2015 IEEE Symposium on Antennas and Propagation (APS 2015), 19-25 July, 2015.
- [10] J. G. Linvill, "Transistor Negative-Impedance Converters", Proceedings of the IRE, vol. 41, no. 6, pp. 725-729, June 1953.
- [11] [Online]. Available: <http://pdf1.alldatasheet.com/datasheet-pdf/view/16347/PHILIPS/BFR93A.html>
- [12] [Online]. Available: <http://beyondmeasure.rigoltech.com/acton/attachment/1579/f-0025/0/-/-/-/file.pdf>