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Rémi Manczak, Marc Fouet, Rémi Courson, Paul-Louis Fabre, Armelle Montrose, et al.. Improved on-chip impedimetric immuno-detection of subpopulations of cells toward single-cell resolution. *Sensors and Actuators B: Chemical*, 2016, 230, pp.825-831. 10.1016/j.snb.2016.02.070 . hal-01305407

HAL Id: hal-01305407

<https://hal.science/hal-01305407v1>

Submitted on 22 Apr 2016

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1 **IMPROVED ON-CHIP IMPEDIMETRIC IMMUNO-DETECTION OF**
2 **SUBPOPULATIONS OF CELLS TOWARD SINGLE-CELL RESOLUTION**

3
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15

1

2 **ABSTRACT**

3 Impedance spectroscopy has gained interest for the quantitative detection of specific cells mainly
4 due to a label-free detection and their miniaturization capability required for integration on chip and
5 development of point-of-care diagnostics. In this paper, we report the study of impedimetric
6 microfluidic devices with improved sensitivity targeting the immuno-detection of cells. The sensitivity
7 of our system was evaluated in terms of the capacity of the electrodes to trap monocytes by
8 immune-reaction with CD14 antibody immobilized on micro-electrode surface. All measurements
9 were performed in faradic mode using a redox probe. The sensitivity was evaluated as a function of
10 the impedance increase ΔZ recorded at 100 Hz caused by the insulating character of the cell trapped
11 on electrodes. Analyses first confirmed that the sensing performances were significantly improved by
12 using microfluidic. This increase could originate from an increase in the probability of cell trapping
13 and a better organization of cells on the electrode due to the laminar flow. The great sensitivity was
14 recorded with interdigitated electrodes for which the influence of the gap value was evaluated. The
15 maximum sensitivity was reached with the smallest inter-electrodes gap tested (50 μm). This
16 performance was in part attributed to the redox cycling taking place between neighboring fingers
17 that was strongly affected when cells were trapped on the electrodes edges. Furthermore we also
18 demonstrate that the slice of cell concentration for which the sensitivity is maximized is correlated to
19 the area of electrodes. Moreover, the smallest area of interdigitated electrode (0.1 mm length)
20 allowed the detection of as low as 5 cells per mL

21

22 **KEYWORDS:**

23 Impedance, interdigitated electrode, microfluidic, immune-detection, cell detection

24

1 1. INTRODUCTION

2 The quantitative detection of specific cells is usually carried out by flow cytometry due to its high
3 sensitivity and reliability. Fluorescence-activated cell sorting (FACS) analysis which combines fluidic
4 techniques and optics is the reference method used to count cells via fluorescently labeled antibody
5 conjugates. However, this technique is time-consuming, expensive and not suited to routine
6 screening and point-of-care diagnostics. The development of total analysis solutions in microfluidic or
7 lab on-chip devices for integrated cell-based detection increased considerably over last ten years [1].
8 Miniaturized cell detection devices have several advantages such as rapid detection, low cost, use of
9 small volumes of biological materials, portability and improved sterile conditions. The most widely
10 used techniques for cell counting are optical techniques [2,3] (fluorescence, surface plasmon
11 resonance, interferometric detection) or electrical methods [4,5]. Electrochemical methods have
12 gained interest mainly due to a label-free detection and their miniaturization capability required for
13 integration on a chip, but also for their low cost and short analyses times. Among electrochemical
14 methods, Impedance is a powerful electrochemical method that uses periodic small AC amplitudes
15 and responds to modifications caused by the target cells (coulter counter for single cell analysis) [6-
16 8]. Electrochemical impedance spectroscopy (EIS) is the method of choice in the case of cells trapped
17 on functionalized electrodes surface. In this latter case, the change in the electrode impedance is
18 measured and can be correlated to the amount of trapped cells [9]. Bio-impedance monitoring has
19 already been employed for example to study cellular kinetics [10], cancer drug screening [11], or
20 parasitized cells [12-14].

21
22 Electrochemical measurements rely on the use of at least 2 electrodes. Currently, combination with
23 microfabrication-based technologies allows fabrication of micron-sized electrodes. Microelectrodes
24 have many advantages over conventional electrodes among which economy due to batch fabrication
25 [15], large current densities (low currents) due to enhanced mass transport [16], very short time
26 constants, low ohmic drop and possibility of integration and the development of portable systems
27 [17]. Microelectrodes, due to smaller currents, have higher impedances [18] and allow the study of
28 high resistivity samples [19]. Furthermore, the spatial resolution of microelectrodes offers the ability
29 to explore several cells [20] or even a single cell [21]. The measured impedance response is
30 consequently influenced by the geometry of the electrodes and optimization of electrode geometry
31 is a key factor in cell analysis as demonstrated by the number of paper dealing with this subject
32 [18,22,23]. Furthermore the sensing performance can be significantly improved by using
33 microfluidics to provide effective liquid manipulation and greater flexibility.

34 In this paper, we report the study of impedimetric microfluidic devices with improved sensitivity
35 targeting the immuno-detection of cells. The sensitivity of the system was evaluated as the capacity
36 of the electrodes to trap monocytes by immune-reaction with CD14 antibody immobilized on the
37 electrode surface [13] and to produce a significant impedance change. Several designs including
38 simple or interdigitated electrodes were tested and also compared to microfluidic measurements.

39

40 2. MATERIALS AND METHODS

41 2.1. Materials

42 2.1.1. Products

1 6-mercapto-1-hexanol (MH), 11-mercaptopundecanoic acid (MUA), N-ethyl-N-(dimethylaminopropyl)-
2 carbodiimide (EDC), N-hydroxysuccinimide (NHS), phosphate buffered saline (PBS) solution,
3 recombinant protein G (PG), bovine serum albumin (BSA), lipopolysaccharide (LPS), hydrogen
4 peroxide and sulfuric acid were purchased from Sigma-Aldrich (Saint-Quentin Fallavier, France). The
5 CD 14 and CD 16 antibodies were purchased from Miltenyi Biotec (Paris, France). Absolute ethanol
6 was purchased from Fisher Scientific (Illkirch, France) and deionized water was obtained using the
7 Milli-Q water system Millipore (Molsheim, France). DF-1050 films (Engineered Materials Systems,
8 Inc.), SU8 3050 resin (Microchem), 4'' glass substrates (Schott AF32), Polydimethylsiloxane (PDMS)
9 (Dow corning), hexamethyldisiloxane (HMDS) (Sigma Aldrich), and AZ Nlof 2035 (AZ Electronic
10 Materials) were used for the microfluidic device.

11 2.1.2. *Monocyte cell culture*

12 Monocytes (THP-1) were cultivated in Roswell Park Memorial Institute 1640 medium (RPMI 1640;
13 Sigma-Aldrich) supplemented with sodium bicarbonate (1.5 g/L; Lonza (Amboise, France)), d-(+)-
14 glucose (4.5 g/L; Sigma–Aldrich), L-glutamine (2 mM; Lonza), sodium pyruvate (1mM; Sigma-Aldrich),
15 4-(2-Hydroxyethyl)-1-piperazineethanesulfonic acid (10 mM; Sigma-Aldrich), 2-mercaptoethanol
16 (0.05 mM; Sigma-Aldrich) and 10% foetal bovine serum (Lonza). The cells were maintained at 37 °C in
17 a 5% CO₂ atmosphere.

18 The cell suspensions were prepared par dilution successives et comptage sur??

19 2.2. Methods

20 2.2.1. *Devices manufacturing process*

21 Devices were manufactured on glass substrates combining standard microfabrication processes
22 (electrodes) and thick photoresists technologies (microfluidics).

23 ***Microelectrodes fabrication (Figure 1a)***

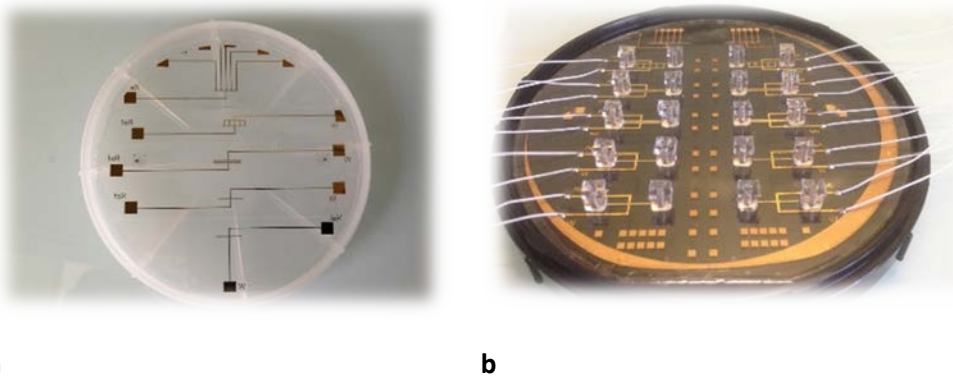
24 The glass substrates were first cleaned with a piranha solution to remove any organic residues. After
25 rinsing with deionized water, drying under a nitrogen flow, and exposure to an O₂ plasma (Tepla
26 600), the substrate was treated with hexamethyldisiloxane (HMDS) to improve adhesion of
27 photolithographic resists. The structuration of gold electrodes was processed following a classical
28 "lift off" technique. An AZ Nlof 2035 resist was spin-coated at "vitesse" and exposed to UV (635nm)
29 during "durée" with a "masqueur utilise". Than a titanium-gold layer respectively 50nm and 200 nm
30 thick was obtained by evaporation in a "marque machine" reactor.i. After the photoresist revelation
31 in acetone, the patterned gold layer was then covered with a 5 μm thick SU-8 photoresist
32 (Microchem) . SU-8 was spin coated at "vitesse" during "durée" and prebaked (PEB) at
33 "temperature" during "durée". The SU-8 was patterned using standard photolithography in order to
34 cover electric tracks and to protect electrodes periphery. This step allows to control precisely the
35 electrodes geometry and dimensions and to avoid unexpected electrochemical effects at the Ti/Au
36 interface. The last residues of unexposed resins were removed by O₂ plasma.

37 ***Microfluidic integration (Figure 1b)***

38 Microfluidic channels were patterned by standard lithography of a 100 μm thick SU8 layer deposited
39 on top of the electrodes wafer. As described extensively in Abgrall et al (ref) open channels were

1 then covered by lamination of a 25 μm thick “home-made” dry film of SU-8 and a final
2 photolithographic step allowed the realization of microfluidic inlets and outlets. To reduce
3 phenomenon of cracks and delamination of the layer originating from residual stress in the SU-8
4 photoresist, a 120°C hard bake was then applied to the system.

5 Fluidic connections were obtained either with the help of PDMS pads glued at each inlet/outlet of
6 the channels or with a mechanical support especially designed to handle the fluid and power supplies
7 of each chip. PDMS pads were obtained with Polydimethylsiloxane (PDMS) mixed with curing agent
8 at proportion of 10/1, degassed with nitrogen for 1 h, then coated on a clean silicon master, and
9 finally, annealed at 90 °C in an oven during 1 h. After 15 min exposure to an O₂ plasma, the pads
10 were stuck onto the wafer using a UV-sensitive glue.



11 **Figure 1: pictures of the devices built for the study** a) without and b) with microfluidic channels and
12 PDMS pads allowing circulation of fluids.

13 To reduce fabrication time and cost the SU-8 resist was also replaced by a novel epoxy dry film DF-
14 1050 (EMS) following the process described by Courson *et al.* [24]. Note that in this latter case the
15 mechanical support was used exclusively.

16 Finally, the wafer was diced using a diamond pen to individualize each microelectrode system.

17 2.2.2. Electrode modification

18 The cleaned electrodes were modified as described by Montrose *et al.* [13]. In absence of channels
19 the surfaces were modified through successive deposition of drops of the modifying agents for
20 various incubation times: a mixture of 11-mercaptoundecanoic acid (MUA) 1 mM and 6-
21 mercaptohexanol (MH) 10 mM for 18h/ a mixture of aqueous solutions of N-hydroxysuccinimide
22 (NHS) 15 mM and 1-Ethyl-3-(3-dimethylaminopropyl)-carbodiimide (EDC) 75 mM for 30 min / protein
23 G 100 g.mL⁻¹ in PBS 10 mM for 18h / BSA 143 g/L for 30 min and CD14 antibody X mM for 18h. In the
24 case of microfluidic devices the modification of electrodes were carried out under a flow of the
25 modifying agents using a Fluigent® MFCS-8C with an inlet pressure of 10 mbar and no outlet pressure
26 for different times : SAMs: 3 hours / NHS EDC: 30 min / PG: 3h / BSA: 30 min / Ab: 2h. This procedure
27 considerably reduced the time of the surface bio-functionalization to about 10 hours.

28

29 2.2.3. Impedimetric measurements

30 The cell trapping were carried out, either by placing a drop of cells suspension during 2 hours on
31 functionalized electrodes in the case of non-microfluidic devices or by applying a continuous flow of

1 cells suspensions for 30 min in channels (pressure drop of 10 mbar) before rinsing and impedance
2 measurements.

3 EIS measurements were performed using an Autolab PGSTAT 128n (Metrohm) and the NOVA
4 software. Experiments were performed in PBS 10 mM (pH = 7.4) containing 5 mM Fe^{III}/Fe^{II}
5 (Fe(CN)₆^{3-/4-} (1:1)). The impedance spectra were recorded from 100 mHz to 50 kHz at the free
6 potential with an alternating voltage of 10 mV. All experiments were performed at room
7 temperature in a Faraday cage.

8 In the case of open chips, the electrochemical measurements were performed in a drop of
9 electrolyte containing the redox probe using a SCE as reference immersed in the drop (scheme 1b).
10 In the case of microfluidic chips, the measurements were performed under a flow of electrolyte,
11 using a two electrode set-up, the reference and counter electrode being short-cut.

12 **3. RESULTS AND DISCUSSION**

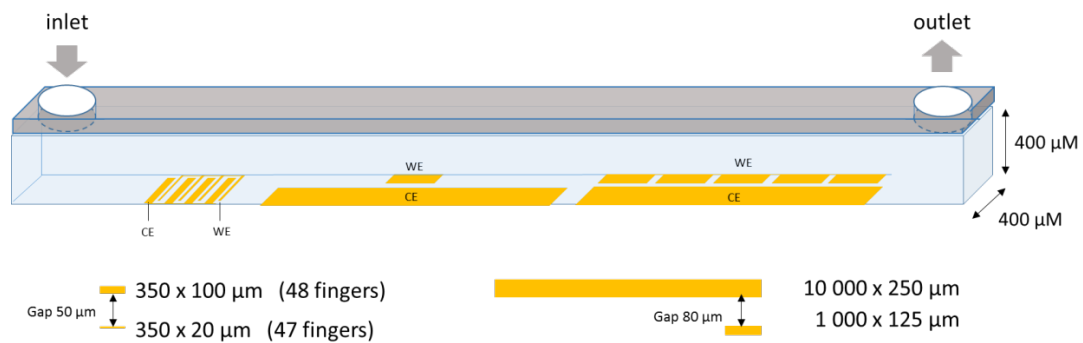
13 Previous experiments performed on macro-electrodes with different areas (1, 0.5, 0.04 cm²) have
14 demonstrated a strong increase in sensitivity when decreasing electrodes areas (90% of
15 improvement in ΔZ for 0.04 cm² area compare to 1 cm²) without any increase in the noise [13]. This
16 is in agreement with inverse proportionality between charge transfer resistance and the electrode
17 area. For this reason we decided to miniaturize working and counter electrodes using classical
18 technologies of microfabrication such as photolithography associated with lift off. Three geometries of
19 micro-electrode arrays were tested: simple, multiple and interdigitated electrodes as presented in
20 scheme 1a.

21 **3.1. Static measurements**

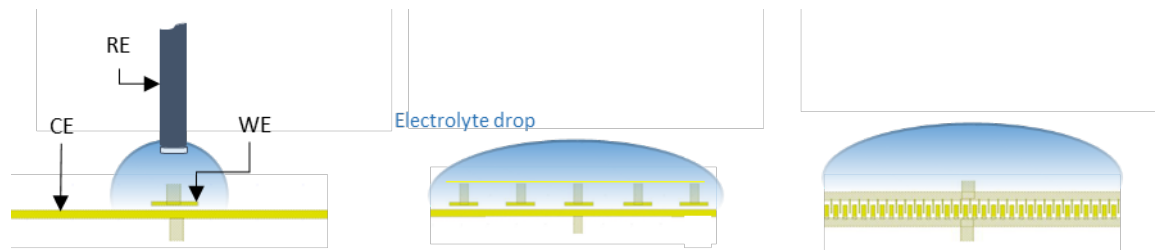
22 In order to qualify micro-electrodes behavior, static measurements were first performed. In this case,
23 both biofunctionalization of electrodes and impedimetric measurements were carried out using
24 drops as illustrated in Scheme 1b. The functionalization of electrodes with specific antibodies CD14
25 was carried out using self-assembled monolayers associated with protein G as previously described in
26 the literature [13]. Each modification step was characterized using electrochemical impedimetric
27 spectroscopy (data not shown). It was verified by applying the modification procedure to SU8 surface
28 that none of the reagents reacts with the resins surface. To study the sensitivity of the
29 immunosensor, monocyte concentrations ranging from 10³ to 10⁹ cells/mL were first deposited on
30 each microelectrode of various geometry previously functionalized with CD14 antibody. The
31 corresponding Nyquist diagrams are presented in Figure 2a-c. The semi-circle diameter increases
32 with the cell concentration due to the insulating character of cells which cover the electrodes and
33 block efficiently the electron transfer towards the redox probe. The maximum variations of
34 impedance were recorded at low frequency at 100 Hz (data not shown) demonstrating that the
35 diffusion of the redox probe was also modified by the presence of cells [25]. The variations of
36 impedance relative to the antibody layer ($\Delta Z_{/AB} = Z - Z_{AB}$) measured at 100 Hz, as a function of the
37 logarithm of cells concentrations are presented in Figure 2d. One can consider that the impedance
38 measured is the sum of the signal corresponding to the free and graft parts of the surface, which
39 means that the impedance is related to the surface coverage ratio. A free surface presents the lowest
40 impedance change $\Delta Z_{/AB}=0$ while a totally covered surface would present the highest one, $\Delta Z_{/AB}$ max.
41 The best sensitivity was recorded with simple electrodes in particular in the range of 10³ and 10⁵

1 cells/mL with a sensitivity $\Delta Z_{/AB} = 800 \Omega/\text{decade}$. The sensitivity was decreasing when the electrode
 2 surface increases to reach $\Delta Z_{/AB} = 200 \Omega/\text{decade}$ for multiple and interdigitated electrodes for the
 3 same range. The graph clearly demonstrates different profiles of sensitivity depending on the
 4 geometry; the impedance for electrodes having the smallest surface areas seems to saturate as when
 5 totally covered, whereas for electrodes with large areas, impedances increase exponentially with
 6 increasing concentrations of cells. The difference between simple and multiple electrodes can be
 7 easily explained by considering that the multiple electrodes corresponds to electrodes in parallel and
 8 in this case their impedance is given by : $1/Z = \Sigma (1/Z_i)$. The impedance of multiple electrodes would
 9 be equal to $Z_{\text{simple}}/5$. Furthermore one can note that impedances recorded with interdigitated
 10 electrodes were weaker than impedances recorded with other electrode types. This result could be
 11 explained by the hemi-spherical diffusion field at each interdigitated microelectrode overlapping
 12 with neighboring diffusion layers [26], and the concomitant redox cycling between electrode fingers
 13 enhancing the current and then decreasing the impedance.

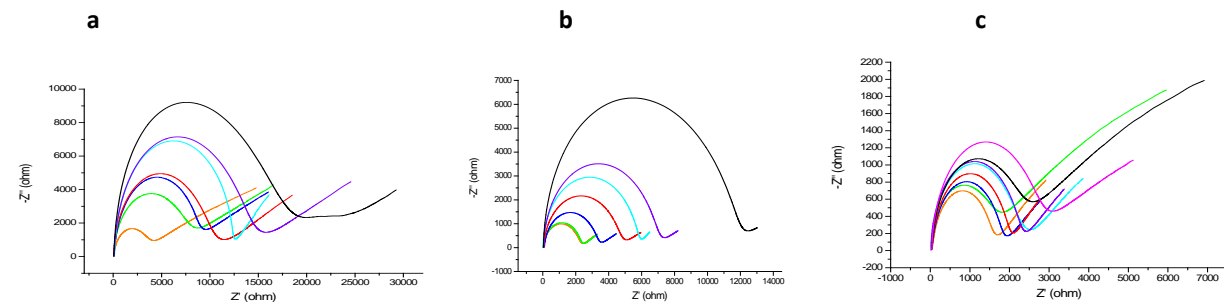
14 a)



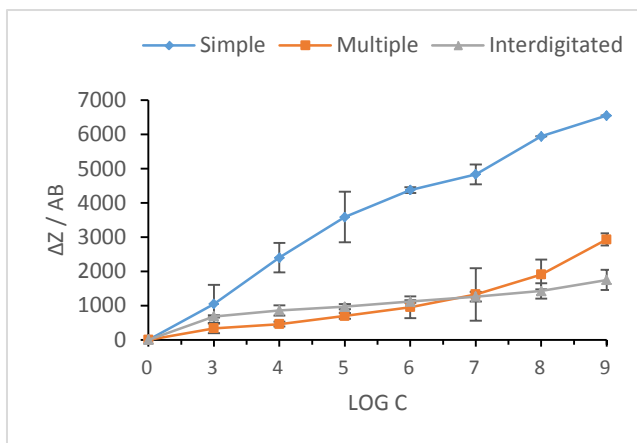
15
 16 b)



17 **Scheme 1:** a) three electrode geometries tested; b) impedimetric measurements were carried out
 18 through deposition of drops and immersion of the SCE reference electrode.
 19



20
 21 d)



2 **Figure 2- Influence of the electrode geometry in static mode.** Nyquist plot of CD 14 antibody
 3 modified electrodes, after incubation with monocytes suspensions (0 (–), 10^3 (–), 10^4 (–), 10^5 (–), 10^6
 4 (–), 10^7 (–), 10^8 (–), 10^9 (–) cells/mL) measured in 5 mM $K_3[Fe(CN)_6]/K_4[Fe(CN)_6]$ for (a) simple, (b)
 5 multiple, and (c) interdigitated microelectrode. Frequency range: 0.1 Hz to 50 kHz. d) Corresponding
 6 variation of impedance relative to the antibody layer measured at 100 Hz, as a function of the
 7 logarithm of cells concentrations.

8 We are aware that our static system consisting of a drop of cell suspension sitting on the
 9 microelectrodes is not ideal as the interaction of cells with a functionalized surface takes place
 10 mainly through sedimentation. Taking into account the radius of the sample drop (around 3 mm for
 11 200 μ L of electrolyte) and a sedimentation speed of cells of around 1×10^{-6} m/s, the fraction of cells
 12 reaching the modified surface within 2 hours is weak. For example for 10^6 cells/mL i.e. 200 000 cells
 13 in the drop, only 600 will be trapped on a single-electrode while the full coverage is reached for 1 000
 14 cells (cell radius estimated to 12 μ m). This low trapping ratio explained why the saturation appear for
 15 very high cell concentrations. Furthermore, trapping through sedimentation favors the non-specific
 16 grafting leading to not well organized layers and stacking.

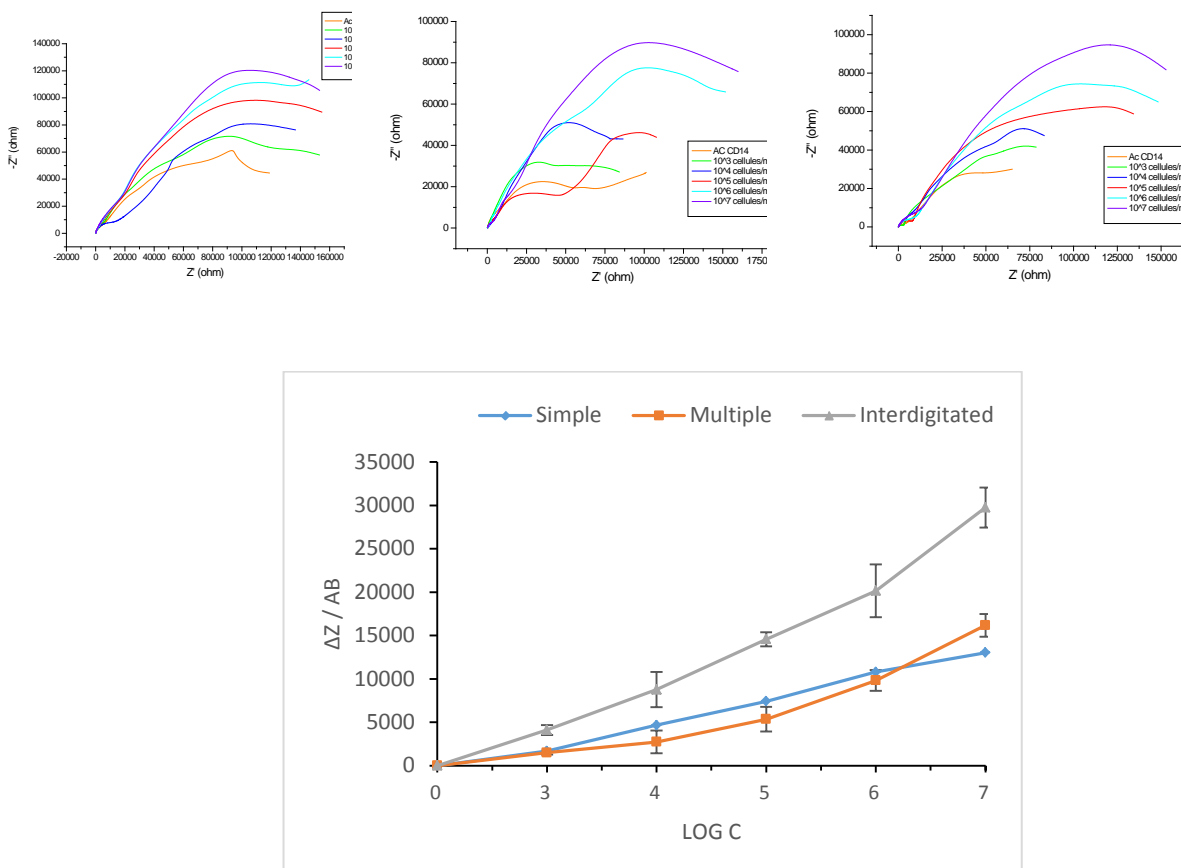
17 3.2. Microfluidic approach

18 Microfluidic integration offers numerous advantages compared to static approach. Beyond well-
 19 established potentialities of fluid handling, such as sample pretreatment, assays parallelization and
 20 others, in our case it also minimizes the sedimentation phenomenon and increases specific cell-
 21 electrodes interaction.

22 We manufactured microfluidic devices with channels (length: 14800 μ m, width: 500 μ m, height: 100
 23 μ m) and integrated electrodes of different designs. The surface of electrodes was functionalized
 24 inside assembled chips, which strongly shortened the functionalization time to only 10 hours and
 25 dramatically improved the homogeneity of the attached layers.

26 The impedimetric analyses were performed using a two electrodes set-up including a pseudo
 27 [counter + reference] electrode. The cell trapping was performed by applying a continuous flow of
 28 cells suspensions for 30 min on functionalized electrodes. After rinsing the electrodes, the impedance
 29 measurements were then performed under a flow of the PBS electrolyte containing the redox probe.
 30 The Nyquist diagrams and the corresponding variations of impedance recorded at 100 Hz for are
 31 presented for each geometry in Figure 3a and 3b respectively. The microfluidic mode induced a
 32 transition to a stationary mode (semi-infinite diffusion) characterized as demonstrated on diagrams
 33 by the apparition of dissymmetric loops of Leminscate type for all geometries (Figure 3a) instead of

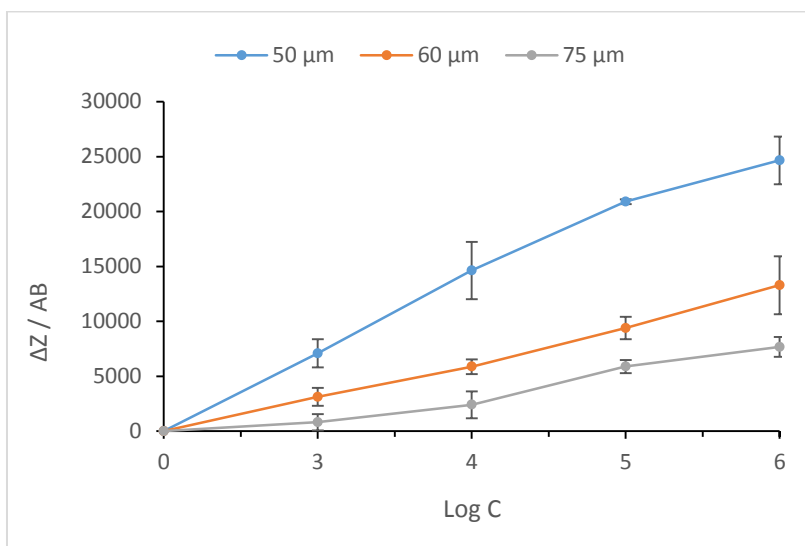
1 the classical Warburg line recorded in static mode. The values of the impedance changes $\Delta Z_{/AB}$
 2 recorded in this case are much greater than the ones recorded in the static mode. The variation of
 3 impedance ΔZ increases for 10^6 cells/mL by a factor 2, 12 and 18 for simple, multiple and
 4 interdigitated electrodes respectively. This increase could originate from different factors, including
 5 an increase in the probability of cell trapping and a better organization of cells on the electrode due
 6 to presence of a laminar flow, and the change of the measuring mode from three to two electrodes.
 7 For interdigitated electrodes the sensitivity increased from 200 to 4 000 Ω per $\log[\text{cells}]$, making this
 8 geometry the most sensitive in the microfluidic mode. This could originate from the fact that
 9 interdigitated electrode structures distribute the detection of localized changes to a larger sensing
 10 surface [27] (length 20 times larger than for simple electrodes). Furthermore, the trapping of cells on
 11 electrode edges modifies the inter-electrode space and consequently, the conductivity between
 12 electrodes has even stronger impact on the impedance when the distance between the electrodes is
 13 small. This can explain the great impedance changes recorded for interdigitated electrodes having a
 14 gap of 50 μm compared to the others with a gap of 180 μm . These results are in accordance with the
 15 works of Couniot and co-workers [28] which have demonstrated (using bacteria) a correlation
 16 between the interdigitated inter-electrode space and the detection sensitivity. The mean sensitivity
 17 is indeed larger for smaller electrode gaps but the electrical response is noisier. They established that
 18 the optimal electrode gap is approximately four times the bacteria diameter [28].



19 **Figure 3- Influence of the electrode geometry in microfluidic mode** ; Nyquist plot of CD 14 antibody
 20 modified electrodes, after incubation with monocytes suspensions (0 (–), 10^3 (–), 10^4 (–), 10^5 (–), 10^6
 21 (–), 10^7 (–), 10^8 (–), 10^9 (–) cells/mL) measured in 5 mM $\text{K}_3[\text{Fe}(\text{CN})_6]/\text{K}_4[\text{Fe}(\text{CN})_6]$ for (a) simple, (b)
 22 multiple, and (c) interdigitated microelectrode. Frequency range: 0.1 Hz to 50 kHz. Corresponding

1 variation of impedance relative to the antibody layer measured at 100 Hz, as a function of the
2 logarithm of cells concentrations for measurements carried out in a microfluidic mode with different
3 geometries.

4
5 Therefore, 3 different gap values were tested: 50, 60 and 75 μm . After functionalization of the
6 electrodes, a range of cell concentration of 10^3 to 10^6 cells/mL was applied on each interdigitated
7 design. The corresponding variations of the relative impedance module $\Delta Z_{/AB}$ as a function of the
8 logarithm of cell concentrations are presented in Figure 4. The results clearly demonstrate that the
9 sensitivity increases when the gap decreases. The sensitivity recorded on the range tested varies
10 from 1280 Ω /decade for the gap of 75 μm to 2200 Ω /decade for 60 μm and 4111 Ω /decade for the
11 gap of 50 μm . These results are in accordance with the factor 4 between the gap and the scale of the
12 target cell mentioned in literature [28], assuming that the diameter of monocytes used (THP1) varies
13 around 12-13 μm .

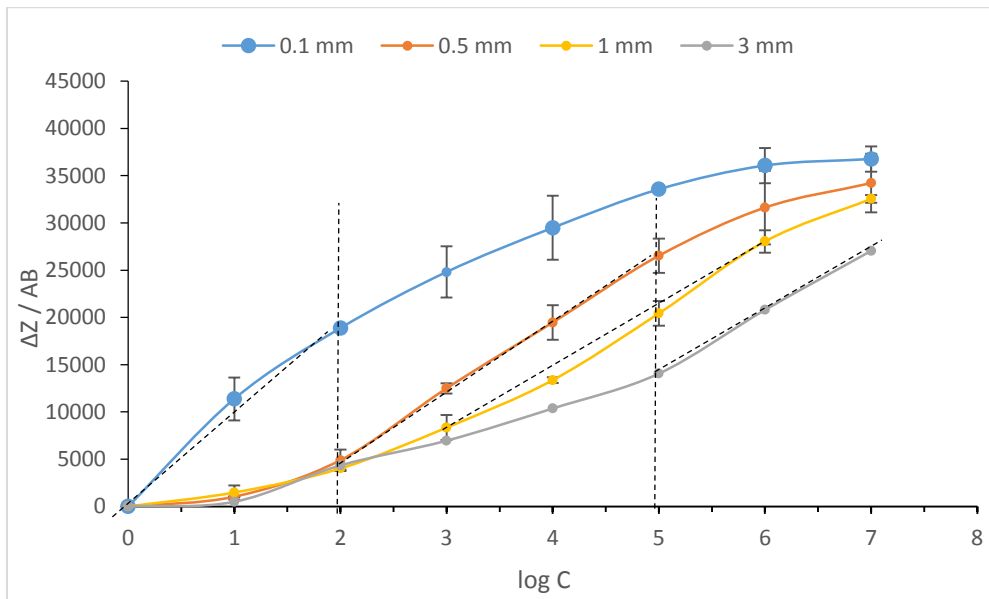


14

15 **Figure 4: Influence of the gap.** Variation of impedance relative to the antibody layer measured at 100
16 Hz, as a function of the logarithm of cells concentrations for measurements carried out in a
17 microfluidic mode with interdigitated electrodes for different values of gap: 50, 60 and 75 μm .

18 Another parameter has to be taken into account and it concerns the area of the electrode and more
19 specifically the length and number of strands. Four different lengths were tested: 0.1, 0.5, 1 and 3
20 mm which comprise respectively 1, 2, 4 and 14 fingers of same dimension (20 μm x 350 μm) with a
21 given gap equal to 50 μm . For this study, the fabrication process was slightly modified by replacing
22 SU8 resin by laminated DF films to reduce processing time. Furthermore, to overcome **micro-welds**
23 and PDMS bonding pads allowing microfluidic circulation of fluids, a new measurement system was
24 set up at LAAS. Both electrical and fluidic parts were managed by the mechanical support, in which
25 each chip was incorporated to be tested individually. The corresponding variations of the impedance
26 module are presented in Figure 5. According to the surface, it is clearly observed that for the 0.1 mm
27 a rapid saturation due to a total coverage appear while for the 3 mm (surface ratio 14), the $\Delta Z_{/AB}$
28 increases continuously with cell concentration due to a partial coverage. The two others systems
29 present intermediate behaviors: an increase of the signal tending to saturate. All interdigitated size
30 have comparable maximum sensitivities (> 6000 Ω /decades) but for specific cell concentration range.
31 The 0.1 mm electrode has a maximum sensitivity until 10^2 cells, and after that the sensitivity

1 decreases due to the surface saturation. Furthermore with this area the device allowed a detection
2 limit below 5 cells/mL (LOD = 3xSD/slope). For the 0.5 mm microelectrode, the sensitivity is
3 maximum in a cell concentration ranging from 10^2 to 10^5 cells/mL and 10^6 for 1 mm electrodes
4 before it starts to decrease. In the case of 3 mm electrode, the sensitivity increases from 10^5
5 cells/mL. These results demonstrate that there is a threshold beyond which a surface is exploitable
6 for a given slice of concentration. A too large area is not suitable to detect rare events. For early
7 diagnostic i.e. detection of low number of cells, the 0.1 mm microelectrode seems to be the most
8 suitable.



9

10 **Figure 5: Influence of the electrode length.** Variation of impedance relative to the antibody layer
11 measured at 100 Hz, as a function of the logarithm of cells concentrations for measurements carried
12 out in a microfluidic mode with interdigitated electrodes for different lengths: 0.1, 0.5, 1 and 3 mm
13 (surface ratio 1, 2, 4 and 14).

14

15 CONCLUSION

16 In this paper we demonstrate by employing monocytes, how the immunodetection of
17 subpopulations of cells is strongly enhanced by using interdigitated electrodes with small inter-
18 electrodes gap compared to electrodes with simple geometries. These performances are linked to
19 strong minimization of the redox cycling between electrode fingers upon cell trapping. Furthermore
20 we also demonstrate that the slice of cell concentration for which the sensitivity is the maximum is
21 proportional to the electrode size. Moreover, the interdigitated electrodes with smallest area that
22 were fabricated (0.1 mm length) allowed to detect cells in solutions with concentrations smaller than
23 5 cells/mL, opening thus new perspectives for the detection of rare events such as the tracking of
24 circulating stem cells, for example.

25

26 ACKNOWLEDGEMENTS

1 The authors would like to thank the Région Midi-Pyrénées and the University of Toulouse for
2 financial support.

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