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# Radiative transport and optical tomography with large data sets

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# Abstract

We consider the inverse problem of optical tomography in the radiative transport regime. We report numerical tests of a direct reconstruction method that is suitable for use with large data sets. Reconstructions of experimental data obtained from a noncontact optical tomography system are also reported.

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#### I. INTRODUCTION

The development of tools to probe the structure of highly-scattering media such as clouds, colloids and biological tissue is of fundamental interest and considerable applied importance. One such method, known as optical tomography (OT), is a biomedical imaging modality with unique capabilities to assess physiological function, such as blood volume and tissue oxygenation [1]. In a typical OT experiment, a material medium is illuminated by a narrow collimated beam and the light that propagates through the medium is collected by an array of detectors. In many instruments, the sources and detectors are coupled to the medium by means of optical fibers and the number of measurements which can be obtained varies from  $10^2-10^5$  source-detector pairs. More recently, noncontact imaging systems have been introduced, wherein a scanned beam and a lens-coupled CCD camera is employed to replace the aforementioned illumination and detection fiber-optics [2–4]. Using such a noncontact method, extremely large data sets of order  $10^7-10^9$  measurements can readily be acquired. The availability of such data sets has been shown to vastly improve the quality of images in OT [4–6].

The inverse problem of OT is to reconstruct the optical properties of a highly-scattering medium from boundary measurements. The standard computational approach to this problem is to minimize a penalized least-squares functional [1, 7–15]. Although such optimization methods are extremely flexible, they have very high computational cost and are not well suited to the large data sets of noncontact optical tomography. Direct reconstruction methods offer an alternative approach to optimization-based algorithms [16–23]. By direct reconstruction, we mean the use of inversion formulas and associated fast algorithms. Such formulas have been derived for particular experimental geometries, including those with planar boundaries. To date, these methods have been developed within the framework of the diffusion approximation (DA) to the radiative transport equation (RTE). We note that the DA is accurate when the energy density of the optical field varies slowly on the scale of the transport mean free path. The DA breaks down in optically thin layers, near boundaries and in strongly absorbing media, conditions that are frequently encountered in biomedical applications.

In this paper, we develop a fast image reconstruction algorithm for the inverse problem in the transport regime. The primary tools that we exploit are an integral equation formulation of the forward problem [30] and the recently derived plane-wave decomposition for the Green's function of the RTE [27–29]. Using this approach, we show that the *linearized* inverse problem can be formulated in terms of the inversion of a suitably defined Fourier-Laplace transform. We illustrate this result with numerical simulations and reconstructions of experimental data obtained from a noncontact OT system.

The remainder of this paper is organized as follows. In section II we introduce the linearized forward problem within the accuracy of the Rytov approximation. This is followed in section III by the derivation of the Fourier-Laplace inversion formula for the slab geometry. Numerically simulated reconstructions are presented in section IV. Reconstructions from experimental data are shown in section V. Our conclusions are presented in section VI. The derivation of the Green's function for the RTE with reflecting boundary conditions is given in the Appendix.

#### II. FORWARD PROBLEM

#### A. Radiative transport

The propagation of multiply-scattered light in a volume  $\Omega$  is taken to be governed by the RTE

$$\hat{\mathbf{s}} \cdot \nabla I + (\mu_a(\mathbf{r}) + \mu_s(\mathbf{r})) I = \mu_s(\mathbf{r}) \int A(\hat{\mathbf{s}}, \hat{\mathbf{s}}') I(\mathbf{r}, \hat{\mathbf{s}}') d^2 s' + S(\mathbf{r}, \hat{\mathbf{s}}) . \tag{1}$$

Here  $I(\mathbf{r}, \hat{\mathbf{s}})$  denotes the specific intensity at the point  $\mathbf{r}$  in the direction  $\hat{\mathbf{s}}$ , S is the source, and  $\mu_a$  and  $\mu_s$  are the absorption and scattering coefficients of the medium. The phase function A is normalized so that  $\int A(\hat{\mathbf{s}}, \hat{\mathbf{s}}') d^2 s' = 1$  for all  $\hat{\mathbf{s}}$ . The specific intensity is also assumed to obey the half-range boundary condition

$$I(\mathbf{r}, \hat{\mathbf{s}}') = R(|\hat{\mathbf{s}} \cdot \hat{\mathbf{s}}'|)I(\mathbf{r}, \hat{\mathbf{s}}) , \quad \hat{\mathbf{n}} \cdot \hat{\mathbf{s}}' < 0 \quad \text{on} \quad \partial\Omega .$$
 (2)

Here R is the reflection coefficient,  $\hat{\mathbf{n}}$  is the outward unit normal to  $\partial\Omega$ , and  $\hat{\mathbf{s}}$  are the incident and reflected directions at the boundary, respectively. See the Appendix for further details.

We assume that the scattering coefficient  $\mu_s$  is constant everywhere in the medium but the absorption coefficient  $\mu_a$  varies with position. We thus decompose  $\mu_a$  into a constant part  $\bar{\mu}_a$  and a spatially varying part  $\delta \mu_a$ :

$$\mu_a(\mathbf{r}) = \bar{\mu}_a + \delta \mu_a(\mathbf{r}) \ . \tag{3}$$

The RTE (1) thus becomes

$$\hat{\mathbf{s}} \cdot \nabla I + \mu_t I + \delta \mu_a(\mathbf{r}) I = \mu_s \int A(\hat{\mathbf{s}}, \hat{\mathbf{s}}') I(\mathbf{r}, \hat{\mathbf{s}}') d^2 s' + S , \qquad (4)$$

where  $\mu_t = \bar{\mu}_a + \mu_s$ . The solution to (4) is given by

$$I(\mathbf{r}, \hat{\mathbf{s}}) = I_0(\mathbf{r}, \hat{\mathbf{s}}) - \int d^3r' d^2s' G(\mathbf{r}, \hat{\mathbf{s}}; \mathbf{r}', \hat{\mathbf{s}}') \delta\mu_a(\mathbf{r}') I(\mathbf{r}', \hat{\mathbf{s}}') .$$
 (5)

Here  $I_0$  is the incident specific intensity, defined as the solution to (1) with  $\mu_a = \bar{\mu}_a$  obeying the boundary condition (2). The Green's function G satisfies the equation

$$\hat{\mathbf{s}} \cdot \nabla_{\mathbf{r}} G(\mathbf{r}, \hat{\mathbf{s}}; \mathbf{r}', \hat{\mathbf{s}}') + \mu_t G(\mathbf{r}, \hat{\mathbf{s}}; \mathbf{r}', \hat{\mathbf{s}}') = \mu_s \int A(\hat{\mathbf{s}}, \hat{\mathbf{s}}'') G(\mathbf{r}, \hat{\mathbf{s}}''; \mathbf{r}', \hat{\mathbf{s}}') d^2 s'' + \delta(\mathbf{r} - \mathbf{r}') \delta(\hat{\mathbf{s}} - \hat{\mathbf{s}}')$$
(6)

and obeys the boundary condition (2). Eq. (5) is the analog of the Lippmann-Schwinger equation for the RTE. It can be linearized by the Rytov approximation [1]:

$$-\ln\left(\frac{I(\mathbf{r},\hat{\mathbf{s}})}{I_0(\mathbf{r},\hat{\mathbf{s}})}\right) = \frac{1}{I_0(\mathbf{r},\hat{\mathbf{s}})} \int d^3r' d^2s' G(\mathbf{r},\hat{\mathbf{s}};\mathbf{r}',\hat{\mathbf{s}}') \delta\mu_a(\mathbf{r}') I_0(\mathbf{r}',\hat{\mathbf{s}}') . \tag{7}$$

It will prove convenient to introduce the data function  $\phi$ , which is defined by

$$\phi = -I_0 \ln(I/I_0) . \tag{8}$$

It follows from (7) that  $\phi$  obeys the integral equation

$$\phi(\mathbf{r}) = \int d^3r' d^2s' G(\mathbf{r}, \hat{\mathbf{s}}; \mathbf{r}', \hat{\mathbf{s}}') \delta\mu_a(\mathbf{r}') I_0(\mathbf{r}', \hat{\mathbf{s}}') . \tag{9}$$

## B. Slab geometry

For the remainder of this paper we consider a three dimensional slab-shaped medium, as shown in Figure 1. The incident field is taken to be generated by a point-source oriented in the inward normal direction located on the z=0 plane. Thus  $I_0 = G(\mathbf{r}, \hat{\mathbf{s}}; \boldsymbol{\rho}_s, 0, \hat{\mathbf{z}})$ , where  $\boldsymbol{\rho}_s$  is the transverse coordinate of the source. Light exiting the slab in the outward normal direction is collected by a point-detector that is located on the plane z=L. The integral equation (9) thus becomes

$$\phi(\boldsymbol{\rho}_s, \boldsymbol{\rho}_d) = \int d^3r d^2s \, G(\boldsymbol{\rho}_d, L, \hat{\mathbf{z}}; \mathbf{r}, \hat{\mathbf{s}}) G(\mathbf{r}, \hat{\mathbf{s}}; \boldsymbol{\rho}_s, 0, -\hat{\mathbf{z}}) \delta \mu_a(\mathbf{r}) , \qquad (10)$$

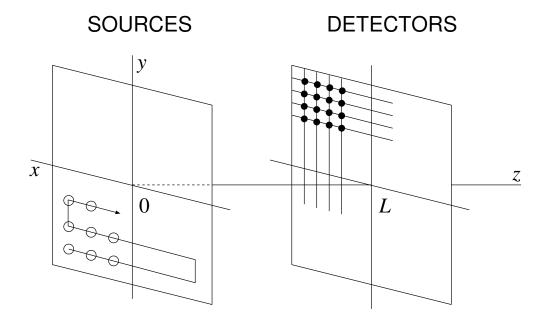


FIG. 1. Illustrating the slab geometry.

where  $\rho_d$  is the transverse coordinate of the detector.

To make further progress, we make use of the method of rotated reference frames to express the Green's function as an expansion in two-dimensional plane waves and spherical harmonics [27–29]. The details are presented in the Appendix, where it is shown that

$$G(\mathbf{r}, \hat{\mathbf{s}}; \mathbf{r}', \hat{\mathbf{s}}') = \int \frac{d^2q}{(2\pi)^2} e^{-i\mathbf{q}\cdot(\boldsymbol{\rho}-\boldsymbol{\rho}')} \sum_{l=0}^{\infty} \sum_{m=-l}^{l} k_{lm}(\mathbf{q}, z) Y_{lm}(\hat{\mathbf{s}}) Y_{lm}^*(\hat{\mathbf{s}}') , \qquad (11)$$

where  $\mathbf{r} = (\boldsymbol{\rho}, z)$  and  $k_{lm}$  is defined in (49). Using this result, we find that (10) becomes

$$\phi(\boldsymbol{\rho}_s, \boldsymbol{\rho}_d) = \int d^3r \int \frac{d^2q_1}{(2\pi)^2} \int \frac{d^2q_2}{(2\pi)^2} e^{i(\mathbf{q}_1 - \mathbf{q}_2) \cdot \boldsymbol{\rho}} e^{-i(\mathbf{q}_1 \cdot \boldsymbol{\rho}_s - \mathbf{q}_2 \cdot \boldsymbol{\rho}_d)} \kappa(\mathbf{q}_1, \mathbf{q}_2, z) \delta\mu_a(\mathbf{r}) , \qquad (12)$$

where

$$\kappa(\mathbf{q}_1, \mathbf{q}_2, z) = \sum_{l=0}^{\infty} \sum_{m=-l}^{l} (-1)^m k_{lm}(\mathbf{q}_1, z) k_{lm}^*(\mathbf{q}_2, L - z) .$$
 (13)

## III. INVERSE PROBLEM

The inverse problem consists of recovering the absorption  $\delta \mu_a$  from measurements of the data function  $\phi$ . To proceed, we assume that the sources and detectors are placed on square lattices with lattice spacings  $h_s$  and  $h_d$ , respectively. The positions of the sources

and detectors are given by

$$\boldsymbol{\rho}_s = h_s(n_{sx}\hat{\mathbf{x}} + n_{sy}\hat{\mathbf{y}}) , \quad \boldsymbol{\rho}_d = h_d(n_{dx}\hat{\mathbf{x}} + n_{dy}\hat{\mathbf{y}}) , \qquad (14)$$

where  $n_{sx}$ ,  $n_{sy}$ ,  $n_{dx}$ , and  $n_{dy}$  are integers. We introduce the Fourier transform of the data function:

$$\tilde{\phi}(\mathbf{q}_s, \mathbf{q}_d) = \sum_{\boldsymbol{\rho}_s, \boldsymbol{\rho}_d} e^{i(\mathbf{q}_s \cdot \boldsymbol{\rho}_s + \mathbf{q}_d \cdot \boldsymbol{\rho}_d)} \phi(\boldsymbol{\rho}_s, \boldsymbol{\rho}_d) . \tag{15}$$

Here the vectors  $\mathbf{q}_s$  and  $\mathbf{q}_d$  lie in the first Brillouin zone (FBZ) of the source and detector lattices:

$$-\frac{\pi}{h_s} \le q_s^{(x)}, \ q_s^{(y)} \le \frac{\pi}{h_s} \ , \qquad -\frac{\pi}{h_d} \le q_d^{(x)}, \ q_d^{(y)} \le \frac{\pi}{h_d} \ . \tag{16}$$

To compute the Fourier transform, we make use of (12) and the identity

$$\sum_{\rho} e^{i\mathbf{q}\cdot\boldsymbol{\rho}} = \left(\frac{2\pi}{h}\right)^2 \sum_{\nu} \delta(\mathbf{q} + \boldsymbol{\nu}) , \qquad (17)$$

where  $\nu$  denotes a reciprocal lattice vector and  $\mathbf{q} \in [-\frac{\pi}{h}, \frac{\pi}{h}] \times [-\frac{\pi}{h}, \frac{\pi}{h}]$ . We thus obtain

$$\widetilde{\phi}(\mathbf{q}_s, \mathbf{q}_d) = \frac{1}{h_s^2 h_d^2} \sum_{\boldsymbol{\nu}_s, \boldsymbol{\nu}_d} \int dz \, \kappa(\mathbf{q}_s + \boldsymbol{\nu}_s, -\mathbf{q}_d + \boldsymbol{\nu}_d, z) \widetilde{\delta \mu_a}(\mathbf{q}_s + \mathbf{q}_d + \boldsymbol{\nu}_s - \boldsymbol{\nu}_d, z) , \qquad (18)$$

where

$$\widetilde{\delta\mu_a}(\mathbf{q}, z) = \int d^2\rho \, e^{i\mathbf{q}\cdot\boldsymbol{\rho}} \delta\mu_a(\boldsymbol{\rho}, z) \ . \tag{19}$$

Next, we perform the change of variables

$$\mathbf{q}_s = \frac{\mathbf{q}}{2} + \mathbf{p} \;, \quad \mathbf{q}_d = \frac{\mathbf{q}}{2} - \mathbf{p} \;, \tag{20}$$

where  $\mathbf{q}_s$  and  $\mathbf{q}_d$  are two-dimensional vectors. We also assume that  $\delta \mu_a$  is transversely band-limited to the FBZs of the source-detector lattices (corresponding to the band limit  $\min\{2\pi/h_s, 2\pi/h_d\}$ ) and therefore put  $\boldsymbol{\nu}_s = 0$  and  $\boldsymbol{\nu}_d = 0$  in (18), which thus becomes

$$\Phi(\mathbf{q}, \mathbf{p}) = \int_0^L K(\mathbf{q}, \mathbf{p}, z) \widetilde{\delta \mu_a}(\mathbf{q}, z) dz , \qquad (21)$$

where

$$\Phi(\mathbf{q}, \mathbf{p}) = h_s^2 h_d^2 \tilde{\phi} \left( \frac{\mathbf{q}}{2} + \mathbf{p}, \frac{\mathbf{q}}{2} - \mathbf{p} \right) , \qquad (22)$$

$$K(\mathbf{q}, \mathbf{p}, z) = \kappa \left( \mathbf{p} + \frac{\mathbf{q}}{2}, \mathbf{p} - \frac{\mathbf{q}}{2}, z \right) .$$
 (23)

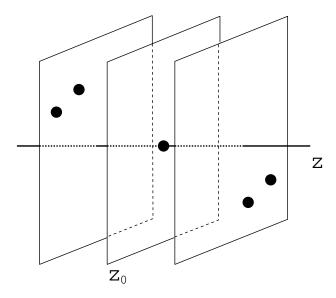


FIG. 2. Illustrating the set of five point absorbers.

For fixed  $\mathbf{q}$ , Eq. (21) defines a system of one-dimensional integral equations for the Fourier transform  $\widetilde{\delta\mu_a}$ . Following the general approach of [23], we construct the pseudoinverse solution of (21) and perform an inverse Fourier transform to obtain the inversion formula

$$\delta\mu_{a}(\boldsymbol{\rho}, z) = \int_{FBZ} \frac{d^{2}q}{(2\pi)^{2}} e^{-i\mathbf{q}\cdot\boldsymbol{\rho}} \sum_{\nu} \frac{R(\sigma_{\nu}(\mathbf{q}))}{\sigma_{\nu}^{2}(\mathbf{q})} \sum_{\mathbf{p}, \mathbf{p'}} \langle f_{\nu}(\mathbf{q}) | \mathbf{p} \rangle K^{*}(\mathbf{q}, \mathbf{p'}, z) \langle \mathbf{p'} | f_{\nu}(\mathbf{q}) \rangle \Phi(\mathbf{q}, \mathbf{p}) .$$
(24)

Here  $f_{\nu}$  and  $\sigma_{\nu}$  are the singular functions and singular values of the matrix M:

$$\sum_{\mathbf{p}'} \langle \mathbf{p} | M(\mathbf{q}) | \mathbf{p}' \rangle \langle \mathbf{p}' | f_{\nu}(\mathbf{q}) \rangle = \sigma_{\nu}^{2}(\mathbf{q}) \langle \mathbf{p} | f_{\nu}(\mathbf{q}) \rangle , \qquad (25)$$

where M is defined by

$$\langle \mathbf{p} | M(\mathbf{q}) | \mathbf{p}' \rangle = \int_0^L K(\mathbf{q}, \mathbf{p}, z) K^*(\mathbf{q}, \mathbf{p}', z) dz$$
 (26)

The regularizer R is introduced to limit the effect of small singular values. Common choices of R include the Tikhonov regularizer  $R(\sigma) = \sigma^2/(\sigma^2 + \epsilon)$  or the step function  $R(\sigma) = \theta(\sigma - \epsilon)$ , where  $\epsilon > 0$ . In our computations, both approaches give similar results.

#### IV. NUMERICAL SIMULATIONS

In this section we report the results of numerical reconstructions from simulated forward data. The medium to be reconstructed consists of a set of five point absorbers, as shown in

Figure 2. The absorbers are assumed to have the same scattering coefficients and phase functions as the medium in which they are embedded, but have different absorption coefficients. The absorption coefficient  $\delta \mu_a$  is given by

$$\delta\mu_a(\mathbf{r}) = \ell^{*2} \sum_{i=1}^5 \delta(\mathbf{r} - \mathbf{r}_i) , \qquad (27)$$

where the positions of the absorbers are  $(x_1, y_1, z_1) = (-4\ell^*, 2\ell^*, z_0 - \ell^*), (x_2, y_2, z_2) = (-2\ell^*, 4\ell^*, z_0 - \ell^*), (x_3, y_3, z_3) = (0, 0, z_0), (x_4, y_4, z_4) = (2\ell^*, -4\ell^*, z_0 + \ell^*), \text{ and } (x_5, y_5, z_5) = (4\ell^*, -2\ell^*, z_0 + \ell^*).$  The optical properties of the background medium are taken to be

$$\bar{\mu}_a = 0.05 \,\mathrm{cm}^{-1}, \quad \mu_s = 100 \,\mathrm{cm}^{-1}, \quad g = 0.9 \;.$$
 (28)

Note that  $\ell^* = 1.00 \,\mathrm{mm}$  in this case. The above values are typical for biological tissues in the near-IR spectral range. The data function  $\Phi$  is calculated according to Eq. (21) for a sample with prescribed  $\delta \mu_a$ . Gaussian noise with zero mean and a standard deviation of 1% of the average signal is added to the data function  $\Phi$  for each numerical experiment. Reconstructions of  $\delta \mu_a$  are calculated from (24) using the step function regularizer. The sum over l in the Green's function (11) is truncated at  $l = l_{max} = 9$ .

The source and detector positions are given by (14) with  $-N_s \leq n_{sx}, n_{sy} \leq N_s$  and  $-N_d \leq n_{dx}, n_{dy} \leq N_d$ . We also set  $N_d = 120$  and  $N_s = 120h_d/h_s$ . The wave vectors  $\mathbf{q}$  and  $\mathbf{p}$  are discretized as

$$\mathbf{q} = \frac{2\pi}{h_d(2N_{FBZ} + 1)} (j_x \hat{\mathbf{x}} + j_y \hat{\mathbf{y}}) , \quad -N_q \le j_x, j_y \le N_q ,$$

$$\mathbf{p} = \frac{2\pi}{h_d(2N_{FBZ} + 1)} (k_x \hat{\mathbf{x}} + k_y \hat{\mathbf{y}}) , \quad 0 \le k_x, k_y \le N_p - 1 ,$$
(29)

where  $N_{FBZ}$  is the number of points in the FBZ. We take  $N_q$  and  $N_p$  to be much smaller than  $N_{FBZ}$  to control numerical stability at high frequencies. We have found that  $N_{FBZ} = 120$ ,  $N_q = 28$ , and  $N_p = 7$  are suitable choices. Finally, we note that numerical integration over z in (26) is carried out using Simpson's rule, with discretionization  $z_j = j(L - 2\ell^*)/N_z + \ell^*$   $(j = 0, 1, ..., N_z)$ . For  $L = 10\ell^*$  and  $6\ell^*$  we take  $N_z$  to be 160 and 80, respectively.

## A. Results

Reconstructions of  $\delta\mu_a$  are shown in Figure 3. Results are shown for two different slab thicknesses  $L=6\ell^*, 10\ell^*$ . The source and detector lattice spacings are  $h_s=0.2\ell^*$  and

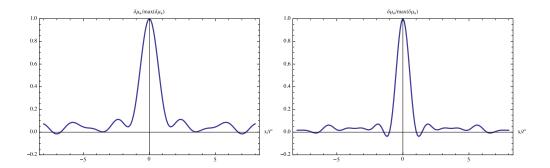


FIG. 3. The reconstructed  $\delta\mu_a(x,y=0,z=z_0)/\max[\delta\mu_a(x,0,z_0)]$  are shown as a function of  $x/\ell^*$ . The following cases are considered:  $L=10\ell^*$  and  $z_0=5\ell^*$  (left) and  $L=6\ell^*$  and  $z_0=3\ell^*$  (right).

 $h_d = 0.1\ell^*$ , respectively. In Figure 3 we take  $L = 10\ell^*$  and  $z_0 = 5\ell^*$  in panel (a) and  $L = 6\ell^*$  and  $z_0 = 3\ell^*$  in panel (b). The regularization parameter is set to be  $\epsilon/\sqrt{\ell^*} = 10^{-6}$  for (a) and  $\epsilon/\sqrt{\ell^*} = 10^{-5}$  for (b). We see that the absorber is clearly reconstructed in both panels. We will define the resolution as the full width at half maximum (FWHM) of the point spread function of the central absorber. Thus the resolution is approximately  $2.0\ell^*$  in (a) and  $1.5\ell^*$  in (b).

#### B. Computational Complexity

The reconstructed images are obtained in 90 sec using a four-cpu parallel machine of 1.3 GHz Itanium-2 processors. The most computationally expensive part of the reconstruction is the calculation of the kernel  $K(\mathbf{q}, \mathbf{p}, z)$ , which is obtained from  $k_{lm}$ . To compute  $k_{lm}$ , the Wigner function  $d_{mM}^l$  and  $f_{Mn}^{(\pm)}$  must be calculated. For each q (0 <  $q \le q_{max}$ ), the construction of  $d_{mM}^l$  requires  $O((l_{max}+1)(l_{max}+2)(l_{max}+3))$  floating point operations and the calculation of  $f_{Mn}^{(\pm)}$  requires  $O((l_{max}+1)^6)$  floating point operations. Therefore when q is approximated by  $n_q$  discrete points, the computation of  $k_{lm}$  requires  $O(N_z n_q l_{max}^8)$  floating point operations. Thus the computation of K requires  $O(N_q^2 N_p^2 N_z l_{max}^2)$  floating point operations.

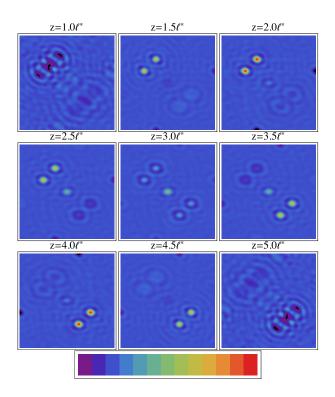


FIG. 4. (Color online) Tomographic reconstruction of  $\delta\mu_a$  for five point absorbers in a slab with  $L=6\ell^*$  and for  $z_0=L/2$ . The function shown by the color scale is  $\delta\mu_a(\mathbf{r})/\max_{\mathbf{r}}[\delta\mu_a(\mathbf{r})]$ . The field of view in each panel is  $16\ell^* \times 16\ell^*$ .

## V. EXPERIMENTAL RESULTS

#### A. Experimental Setup

We have tested the reconstruction algorithm with experimental data using a previously described noncontact OT system [4]. The source is a continuous-wave stabilized diode laser operating at a wavelength of 785 nm with an output power of 6 mW. The sample chamber is a rectangular box, constructed of clear acrylic, of depth 1 cm with square faces of area 15 cm × 15 cm. The chamber is filled with a scattering medium in which the objects to be imaged are placed. The medium consists of a 1% solution of Intralipid in water. The beam is scanned by a pair of mirrors on one face of the sample and the transmitted beam is imaged onto a CCD.

A tomographic data set is acquired by raster scanning the beam over a  $29 \times 29$  square lattice with a lattice spacing of 3.21 mm. This yields 841 source positions within a 9 cm

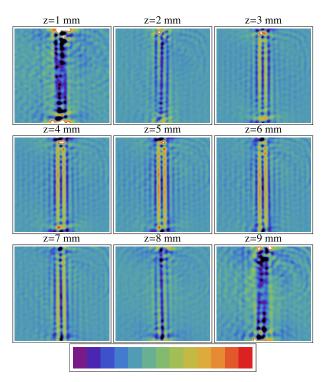


FIG. 5. (Color online) Reconstructions of two rods with 3 mm spacing. The field of view is  $6 \,\mathrm{cm} \times 6 \,\mathrm{cm}$ . The number above each panel shows the distance from the source plane.

 $\times$  9 cm area centered on the optical axis. For each source, a 397  $\times$  397 pixel region of interest is read out from the CCD. This results in 157,609 detectors arranged in a square lattice with an effective lattice spacing equivalent to 0.36 mm. Thus a data set of  $1.3 \times 10^8$  source-detector pairs is acquired.

#### B. Two Rods

In this section, we show the reconstruction of a pair of black metal rods. The rods have a diameter of 3 mm and are suspended in the midplane of the sample chamber. The optical properties of the background medium are

$$\bar{\mu}_a = 0.02 \,\mathrm{cm}^{-1}, \quad \mu_s = 20 \,\mathrm{cm}^{-1}, \quad g = 0.65, \quad k = 0.02 h_d^{-1}, \quad \ell = 20 h_d ,$$
 (30)

where  $k = \sqrt{c\mu_a/D}$  and  $h_d = 0.36$  mm is the lattice spacing on the detector plane. These parameters yield a transport mean free path of  $\ell^* = 1.4$  mm.

Initially, we set the separation of the rods to be 3 mm and take  $l_{max} = 9$ . In Figure 5, tomographic images are displayed with a slice separation of 1 mm. It can be seen that in the central slice, which is equidistant from the source and the detector planes, that the rods are

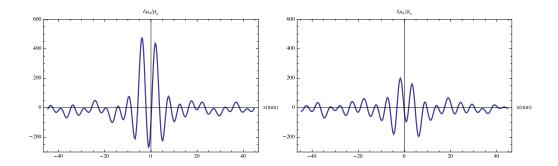


FIG. 6. Reconstructed  $\delta \mu_a/\bar{\mu}_a$  of the metal rods with (left) 3 mm spacing and (right) 2 mm spacing along the x-axis in the central plane at y=0 and z=5 mm.

well resolved. The shallower and deeper slices show that the rods remain well resolved but with a smaller diameter, as expected. Figure 6 shows a plot of the reconstruction along the line passing through the centers of both rods in the central slice. The distance between the peaks is 5.8mm, which slightly underestimates the center-to-center separation of the rods. The FWHM of the peaks is 2.3mm, which underestimates the diameter of the rods.

In a second experiment, we set the separation between the rods to be 2mm. In this case the reconstructed image is poorly resolved. The right panel in Figure 6 shows a two-dimensional plot in the central slice. It is important to note that the reconstructed contrast is not expected to be quantitative owing to the strong absorption in the interior of the metal rods. However, as previously noted, the shape of the rods is recovered well.

## C. Lemon and Lotus Root Slices

In a final set of experiments, a lemon or lotus root slice of thickness approximately 4 mm is placed in the center of the sample chamber. The background medium consists of 0.7% Intralipid plus 0.07% India ink, with optical properties

$$\bar{\mu}_a = 0.4 \,\mathrm{cm}^{-1}, \quad \mu_s = 20 \,\mathrm{cm}^{-1}, \quad g = 0.65, \quad k = 0.13 h_d^{-1}, \quad \ell = 20 h_d \ .$$
 (31)

Reconstructions of the lemon and lotus root are shown in Figures 7 and 8, respectively. A number of structural features of the lemon including the endocarp, mesocarp, central column and septa are readily visualized. Likewise, root tubes of varying diameter are observable.

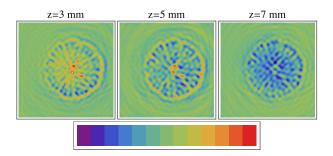


FIG. 7. (Color online) RTE reconstructions of a lemon slice. The field of view is  $9 \text{ cm} \times 9 \text{ cm}$ . The number above each panel shows the distance from the source plane.

# VI. DISCUSSION

In summary, we have investigated the inverse problem of optical tomography in the radiative transport regime. We have developed and tested a fast image reconstruction algorithm that is applicable to the large data sets of noncontact optical tomography. Our results are illustrated by numerical simulations and reconstructions from experimental data in model systems.

We conclude with several remarks. First, the spatial resolution of the reconstructed images in numerical simulations is clearly superior to that obtained in experiments. There are a number of contributing factors that explain this finding. These include the finite size of the source and detector grids, the presence of shot noise in the detected light and noise in the CCD array. We have also not accounted for systematic errors associated with non-idealities in the optical system, such as reflections from the lens surface. Finally, the reconstructions we have performed are carried out within a linearization of the RTE. It may be expected that a nonlinear reconstruction may overcome some of the above limitations, particularly with respect to quantitative recovery of the absorption. One possible approach to this problem is inversion of the Born series, which has been carried out for the case of the DA [20–22]. Inversion of the linearized forward problem is the first step in this procedure, which can be carried out by the method developed herein.

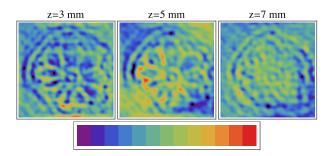


FIG. 8. RTE reconstructions of a lotus-root slice. The field of view is  $9 \,\mathrm{cm} \times 9 \,\mathrm{cm}$ . The number above each panel shows the distance from the source plane.

#### APPENDIX: GREEN'S FUNCTION FOR THE RTE

In this appendix, we outline the calculation of the Green's function for the RTE using the method of rotated reference frames (MRRF). The MRRF was described in [27–29]. Here we summarize the necessary results for the case of the slab geometry with reflecting boundaries. We note that the MRRF has also been extended to the case of reflecting boundaries in the half-space geometry [31].

We begin by noting that the Green's function for the RTE in the slab geometry satisfies the equation

$$(\hat{\mathbf{s}} \cdot \nabla + \mu_t) G(\mathbf{r}, \hat{\mathbf{s}}; \boldsymbol{\rho}_0, 0, \hat{\mathbf{z}}) = \mu_s \int A(\hat{\mathbf{s}}, \hat{\mathbf{s}}') G(\mathbf{r}, \hat{\mathbf{s}}'; \boldsymbol{\rho}_0, 0, \hat{\mathbf{z}}) d^2 s' + \delta (\boldsymbol{\rho} - \boldsymbol{\rho}_0) \delta(z) \delta (\hat{\mathbf{s}} - \hat{\mathbf{z}}) ,$$
(32)

together with the boundary conditions

$$G(\mathbf{r}, \hat{\mathbf{s}}_r; \boldsymbol{\rho}_0, 0, \hat{\mathbf{z}}) = R(|\hat{\mathbf{s}}_i \cdot \hat{\mathbf{z}}|)G(\mathbf{r}, \hat{\mathbf{s}}_i; \boldsymbol{\rho}_0, 0, \hat{\mathbf{z}}) , \quad \hat{\mathbf{n}} \cdot \hat{\mathbf{s}} < 0 , \quad z = 0, L .$$
 (33)

The reflection coefficient R is given by [26, 32–36]

$$R(x) = \begin{cases} \frac{1}{2} \left[ \left( \frac{x - nx_0}{x + nx_0} \right)^2 + \left( \frac{x_0 - nx}{x_0 + nx} \right)^2 \right] & x \ge x_c ,\\ 1 & x < x_c , \end{cases}$$
(34)

where  $x_0 = \sqrt{1 - n^2(1 - x^2)}$ ,  $x_c = \sqrt{n^2 - 1}/n$  and n is the index of refraction in the slab walls. See Figure 9. We assume that the phase function A is given by

$$A(\hat{\mathbf{s}}, \hat{\mathbf{s}}') = \sum_{l=0}^{l_{max}} \sum_{m=-l}^{l} A_l Y_{lm}(\hat{\mathbf{s}}) Y_{lm}^*(\hat{\mathbf{s}}') , \qquad (35)$$

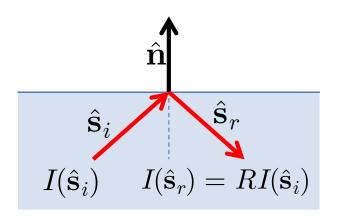


FIG. 9. Illustrating the reflecting boundary condition.

where  $A_0=1,\ A_1=g\in[0,1),\ {\rm and}\ A_l\in[0,1)\ (l=2,3,\dots).$  We adopt the Henyey-Greenstein model [25], and set

$$A_l = g^l , \quad l = 0, 1, 2, \dots$$
 (36)

In the MRRF [27–30], the specific intensity is given as a superposition of eigenmodes  $I_{\mu}^{(+)}$  and  $I_{\mu}^{(-)}$ , where

$$I_{\mu}^{(+)}(\mathbf{r},\hat{\mathbf{s}};\mathbf{q}) = e^{i\mathbf{q}\cdot\boldsymbol{\rho} - Q_{\mu}(q)z} \sum_{l=0}^{l_{max}} \sum_{m=-l}^{l} \frac{(-1)^{m}}{\sqrt{\sigma_{l}}} e^{-im\varphi_{\hat{\mathbf{q}}}} \langle l|\phi_{\mu}\rangle d_{mM}^{l}[i\tau(q\lambda_{\mu})]Y_{lm}(\hat{\mathbf{s}}) , \qquad (37)$$

$$I_{\mu}^{(-)}(\mathbf{r},\hat{\mathbf{s}};\mathbf{q}) = e^{i\mathbf{q}\cdot\boldsymbol{\rho} + Q_{\mu}(q)z} \sum_{l=0}^{l_{max}} \sum_{m=-l}^{l} \frac{(-1)^{l}}{\sqrt{\sigma_{l}}} e^{-im\varphi_{\hat{\mathbf{q}}}} \left\langle l|\phi_{\mu}\right\rangle d_{m,-M}^{l}[i\tau(q\lambda_{\mu})] Y_{lm}(\hat{\mathbf{s}}) , \qquad (38)$$

where

$$Q_{\mu}(q) = \sqrt{q^2 + 1/\lambda_{\mu}^2} \ . \tag{39}$$

Here  $\lambda_n(M)$  and  $|\phi_n(M)\rangle$  be eigenvalues and eigenvectors of matrix B(M) defined by

$$B(M)_{ll'} = \sqrt{\frac{l^2 - M^2}{(4l^2 - 1)\sigma_{l-1}\sigma_l}} \delta_{l',l-1} + \sqrt{\frac{(l+1)^2 - M^2}{[4(l+1)^2 - 1]\sigma_l\sigma_{l+1}}} \delta_{l',l+1} , \qquad (40)$$

where  $\sigma_l = \bar{\mu}_a + \mu_s(1 - g^l)$ ,  $l, l' = |M|, |M| + 1, \dots, l_{max}$ , and  $M = 0, \pm 1, \pm 2, \dots$  Note that we make use of a multi-index  $\mu = (M, n)$  which runs over the set  $\{(M, n) | \lambda_n(M) > 0\}$ . The  $d_{mM}^l$  are analytically continued Wigner's d-functions, which can be recursively computed [27]. The Green's function can be expressed as

$$G(\mathbf{r}, \hat{\mathbf{s}}; \, \boldsymbol{\rho}_0, 0, \hat{\mathbf{z}}) = \sum_{\mu} \int \frac{d^2q}{(2\pi)^2} e^{-i\mathbf{q}\cdot\boldsymbol{\rho}_0} \times \left[ f_{\mu}^{(+)}(q; n) I_{\mu}^{(+)}(\mathbf{r}, \hat{\mathbf{s}}; \mathbf{q}) + f_{\mu}^{(-)}(q; n) e^{-Q_{\mu}(q)L} I_{\mu}^{(-)}(\mathbf{r}, \hat{\mathbf{s}}; \mathbf{q}) \right] . \tag{41}$$

The coefficients  $f_{\mu}^{(+)}(q;n)$  and  $f_{\mu}^{(-)}(q;n)$  are determined by the boundary conditions and are solutions to the linear system

$$\begin{pmatrix} \mathcal{M}^{(++)}(q) & \mathcal{M}^{(+-)}(q) \\ \mathcal{M}^{(-+)}(q) & \mathcal{M}^{(--)}(q) \end{pmatrix} \begin{pmatrix} f^{(+)}(q;n) \\ f^{(-)}(q;n) \end{pmatrix} = \begin{pmatrix} v^{(+)} \\ v^{(-)} \end{pmatrix} , \tag{42}$$

where  $M \ge 0$ ,  $m \ge 0$ ,  $l = m + 1, m + 3, \dots$ ,

$$v_{lm}^{(+)} = \delta_{m0} \sum_{l'} \mathcal{B}_{ll'}^{0}(\infty) \sqrt{\frac{2l'+1}{4\pi}} , \qquad v_{lm}^{(-)} = 0 , \qquad (43)$$

and

$$\mathcal{M}_{lm,Mn}^{(++)} = \sum_{l'} c_{lm,Mn}^{l'} , \quad \mathcal{M}_{lm,Mn}^{(--)} = (-1)^{M+m} \mathcal{M}_{lm,Mn}^{(++)} , \qquad (44)$$

$$\mathcal{M}_{lm,Mn}^{(+-)} = (-1)^{M+m} \mathcal{M}_{lm,Mn}^{(-+)} , \quad \mathcal{M}_{lm,Mn}^{(-+)} = e^{-Q_{\mu}(q)L} \sum_{l'} (-1)^{l'} c_{lm,Mn}^{l'} , \qquad (45)$$

$$c_{lm,Mn}^{l'} = \left[ \mathcal{B}_{ll'}^{m}(\infty) - (-1)^{l'+m} \mathcal{B}_{ll'}^{m}(n) \right] \frac{1}{\sqrt{\sigma_{l'}}} \left\langle l' | \phi_{\mu} \right\rangle \\ \times \left\{ d_{mM}^{l'}[i\tau(q\lambda_{\mu})] + (1 - \delta_{M0})(-1)^{M} d_{m-M}^{l'}[i\tau(q\lambda_{\mu})] \right\} . \tag{46}$$

Here,  $\mathcal{B}_{ll'}^m(n)$  is given by

$$\mathcal{B}_{ll'}^{m}(n) = \frac{1}{2} \sqrt{\frac{(2l+1)(2l'+1)(l-m)!(l'-m)!}{(l+m)!(l'+m)!}} \int_{0}^{1} dx \, P_{l'}^{m}(x) P_{l'}^{m}(x) R_{n}(x) . \tag{47}$$

We note that  $\mathcal{B}_{ll'}^{-m}(n) = \mathcal{B}_{ll'}^{m}(n)$  and  $\mathcal{B}_{ll'}^{m}(\infty)$  is defined by  $\mathcal{B}_{ll'}^{m}(n)$  with  $R_n(x) \equiv 1$ . We also note that  $f_{-Mn}^{(\pm)}(q;n) = (-1)^M f_{Mn}^{(\pm)}(q;n)$ . Finally the Green's function in the slab geometry is obtained as [27]

$$G(\mathbf{r}, \hat{\mathbf{s}}; \boldsymbol{\rho}_0, 0, \hat{\mathbf{z}}) \simeq \int \frac{d^2q}{(2\pi)^2} e^{-i\mathbf{q}\cdot(\boldsymbol{\rho}-\boldsymbol{\rho}_0)} \sum_{l=0}^{l_{max}} \sum_{m=-l}^{l} Y_{lm}(\hat{\mathbf{s}}) i^m k_{lm}(\mathbf{q}, z) , \qquad (48)$$

where the functions  $k_{lm}(\mathbf{q},z)$  are given by

$$k_{lm}(\mathbf{q}, z) = (-i)^{m} e^{-im\varphi_{\mathbf{q}}} \sum_{M \ge 0, n} \frac{\langle l | \phi_{n}(M) \rangle}{\sqrt{\sigma_{l}}}$$

$$\times \left[ e^{-Q_{Mn}(q)z} f_{Mn}^{(+)}(q; n) + (-1)^{l+m+M} e^{-Q_{Mn}(q)(L-z)} f_{Mn}^{(-)}(q; n) \right]$$

$$\times \left[ d_{mM}^{l} [i\tau(q\lambda_{n}(M))] + (1 - \delta_{M0})(-1)^{M} d_{m,-M}^{l} [i\tau(q\lambda_{n}(M))] \right] ,$$
(49)

with  $\varphi_{\mathbf{q}}$  the angle of  $\mathbf{q}$ .

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