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MICROMECHANICAL ANALYSIS OF THE SURFACE EROSION OF A COHESIVE SOIL BY MEANS OF A COUPLED LBM-DEM MODEL

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Abstract. The elementary mechanisms driving the ubiquitous surface erosion of cohesive geomaterials can be analysed from a micromechanical perspective combining well-known numerical techniques. Here, a coupled model combining the Discrete Element and Lattice Boltzmann methods (DEM-LBM) provides an insight into the solid-fluid interaction during the transient erosion caused by a vertical fluid jet impinging on the surface of a granular assembly. The brittle cementation providing cohesion between the solid grains is described here by means of a simple bond model with a single-parameter yield surface. The initial topology of the surface erosion tends to mimic the profile of fluid velocity directly above the soil surface. We find that both the rate of erosion and the magnitude of eroded mass depend directly on the micromechanical strength of the single solid bonds.

1 INTRODUCTION

The geomechanical assessment of the surface erodibility of soils is usually performed empirically, often by means of standard experimental tests such as the Jet Erosion Test (JET, see e.g. [1]) and the Hole Erosion Test (HET, see e.g. [2] and [3]). The soils analysed by

means of these tests are generally cohesive geomaterials, while the water flowing on their surface behaves as eroding agent.

The erodibility is commonly quantified in terms of the average hydrodynamic shear stress at the soil surface with respect to a threshold, the critical shear stress, for the initiation of erosion. However, in practice the eroding process is much more complex and involves local transient flows such as turbulent jets with intermittent spikes of local hydrodynamic stress. On the other hand, the derivation of a reliable empirical expression for the critical stress has been hindered by the large variety of sediment properties that are relevant for the inter-particle forces of cohesive soils and their complex relationships [4]. All this has led to a general lack of consensus over the robustness of the different testing procedures as well as on the analysis methods, in particular on the assumptions for the assessment of the critical shear stress [5].

From the theoretical side, the starting point of most numerical approaches employed so far to study the erosion of geomaterials is merely macromechanical with both water and soil described as continuous media. Different techniques have therefore been proposed in order to track the transient evolution of their interface, where mass exchange between phases (i.e. the actual erosion) takes place [6]. On the one hand, the purely Eulerian approaches permit the use of a fixed mesh but they do not allow for a precise definition of hydro-mechanical variables at the interface. In a similar vein, hybrid Eulerian-Lagrangian methods may show a good precision at the interface but they often lead to severe and time-consuming remeshing issues [6].

The aim of the present work is to introduce an alternative approach based on discrete-element simulations of a cohesive granular bed impacted by a fluid jet modelled by the Lattice Boltzmann method. This is a micro-mechanical approach, which allows for the investigation of different factors driving the elementary mechanisms of erosion, such as the detachment of particle aggregates at the soil surface (surface erosion) or the dislodgement of lumps of material below the free surface (mass erosion) [7].

We introduce below our numerical approach and its application to a JET test on a granular bed with increasing cohesion between grains. A simple model of inter-particle cohesion will be considered, and its consequences for the bed's erodibility will be discussed.

2 NUMERICAL METHOD

There are various coupled methods developed so far for the numerical simulation of fluid-solid interactions at the particle-scale. The approach adopted here combines the computational efficiency of the Lattice Boltzmann Method (LBM) for the simulation of fluids with the relative simplicity of the Discrete Element Method (DEM) for the simulation of solid particles. This approach has already been applied to several geomechanical problems (see e.g. [8-10]).

2.1 Solid phase. A DEM approach

The granular soil is described here by means of a smooth discrete element approach based on the Molecular Dynamics method [11]. We use a two-dimensional assembly of circular particles whose trajectories are computed by simple integration of Newton's equations of motion. The smooth inter-particle contact and friction laws are supplemented by cohesive interactions (see e.g. [12-14]). Here, we consider a simple cohesive law depicted in Figure 1

for contact interactions [12].

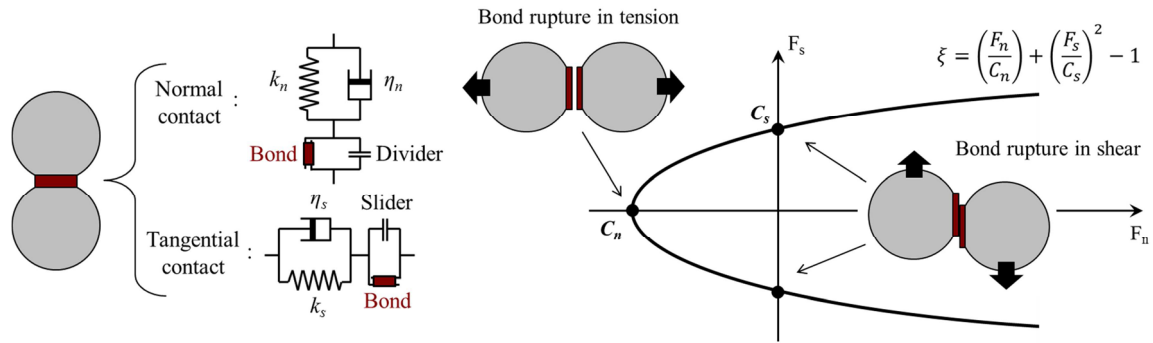


Figure 1: Left: Rheological model of solid contacts, after [14]; Right: Yield surface of cohesive bonds in the space of interaction forces

The interaction between two particles is thus formulated in terms of an interaction force F and an interaction moment M applied at the contact point. The interaction force is decomposed into its normal and shear components, F_n and F_s respectively, corresponding to the normal and tangential directions at the contact. The normal force F_n is described in terms of the local interpenetration δ_n by means of a classical Kelvin-Voigt viscoelastic relationship defined by the normal stiffness and damping coefficients, k_n and η_n . On the other hand, the shear force arising at a frictional (non-cohesive) contact is defined here by a viscous-regularized Coulomb law [15, 16] characterized by a static friction coefficient μ and a viscous coefficient of shear regularization k_s . In this way, the shear force is computed as a function of the sliding velocity δ_s , which in practice never really vanishes. Due to the small time steps considered here (in the order of 10^{-6} s), the quasi-static equilibrium of particles under the action of static friction forces is reached through residual micro-slips. The force moment acting on each particle's centre is defined from the shear force with the particle's radius as lever arm, and a rolling friction component that governs the rolling motion of the particles (relative rotation without sliding). The latter is analogous to the sliding friction in which the relative velocity of rotation replaces the sliding velocity, and the rolling friction coefficient μ_ω and the coefficient of regularization k_ω replace the sliding friction coefficient and its regularization factor [13, 15].

The ingredients presented so far describe the purely frictional contacts. In order to introduce cohesion allowing for tensile normal forces between the solid particles, a simple elastoplastic model with parabolic yield surface in the space of contact forces has been employed (Figure 1). In this way, a solid bond is defined for all particles initially at contact, featuring a linear elastic rheology characterized by the normal and shear bond stiffnesses $k_{n,b}$ and $k_{s,b}$. When a contact force reaches the yield surface, the bond is broken and the contact becomes purely frictional. For convenience, the normal and shear yield thresholds C_n and C_s are assumed to depend only on a single parameter $C = C_n = 2 \cdot C_s$, which represents the strength or degree of cementation of the solid bond. The relative strength of the bonds in the polydisperse assembly can be characterized by a dimensionless number defined as the ratio of bond cohesion to the particle's own buoyant weight. This cohesive Bond number would then be expressed as:

$$B = \frac{C}{\Delta\rho g V} \quad (1)$$

where $\Delta\rho$ is the submerged apparent density of the solid grains, g is the gravitational acceleration and V is the volume of the particle. In general it can be noted that $B \geq 0$ and that solid bonds with $B < 1$ are unstable and short-lived since any slight rearrangement of the assembly under its own weight has the potential to cause bond rupture. Our numerical tests show that the granular bed remains completely bonded under gravity for $B \geq 3$ for all particles in the sample.

2.2 Fluid phase. The LBM method

The transient flow of the fluid phase is described here by means of a classical D2Q9 scheme of the lattice Boltzmann method, which is an explicit finite difference scheme of the continuous Boltzmann equation [18, 19]. The LBM is based on a Cartesian lattice grid in the space and a discrete set of probability density functions and velocities of fluid particles at each grid point. The fluid dynamics are then computed in just two basic steps for the collision and advection of the fluid particles following a set of rules that ensure the conservation of mass, momentum and energy (i.e. the incompressible Navier-Stokes behaviour). However this only holds for low Mach numbers, i.e. when fluid velocity is much lower than the lattice speed. We used the generalized formulation of d’Humières with a multiple relaxation time (MRT) in order to overcome the well-known shortcomings of the classical Bhatnagar-Gross-Krook scheme (single relaxation time) [20, 21]. Hence, the fluid phase is fully defined by specifying the lattice grid size Δx and lattice speed c_s , the components s_α of the diagonal relaxation matrix \mathcal{S} (inverse of the different relaxation times) and the fluid material parameters of density ρ_f and kinematic viscosity ν [10].

2.3 Solid-fluid coupling

The coupling between the fluid and solid phases and the computation of hydrodynamic forces on the particles are performed by means of the simple method for momentum exchange proposed by Bouzidi et al [22], which relies on a generalized bounce-back and linear interpolation strategy for arbitrary geometries in the LBM. The sub-cycling time integration technique proposed by Feng et al [23] was used to exploit the fact that the time step required for the fluid computation is generally much larger than that for particle dynamics. The number of DEM subcycles for each LBM step was nevertheless restricted to 2 in order to preserve the accuracy of the computed hydrodynamic forces on the solid particles. In order to account for fluid flow across a densely packed assembly of particles in two dimensions, a “hydraulic” radius slightly smaller than the particle radius was used [24, 25].

3 ANALYSIS OF JET EROSION

Figure 2 illustrates the general configuration of a jet erosion test and its relevant dimensions. The dimensions of the system were chosen to mimic our on-going physical tests [26] for a later comparison. We have an initial jet-bed distance $H = 70$ mm, a nozzle diameter of $d_0 = 5$ mm and average grain size $D_{mean} = 3$ mm. A size polydispersity ($D_{max}/D_{min} = 1.5$) was introduced in order to avoid crystalline configurations of the two-dimensional granular

sample.

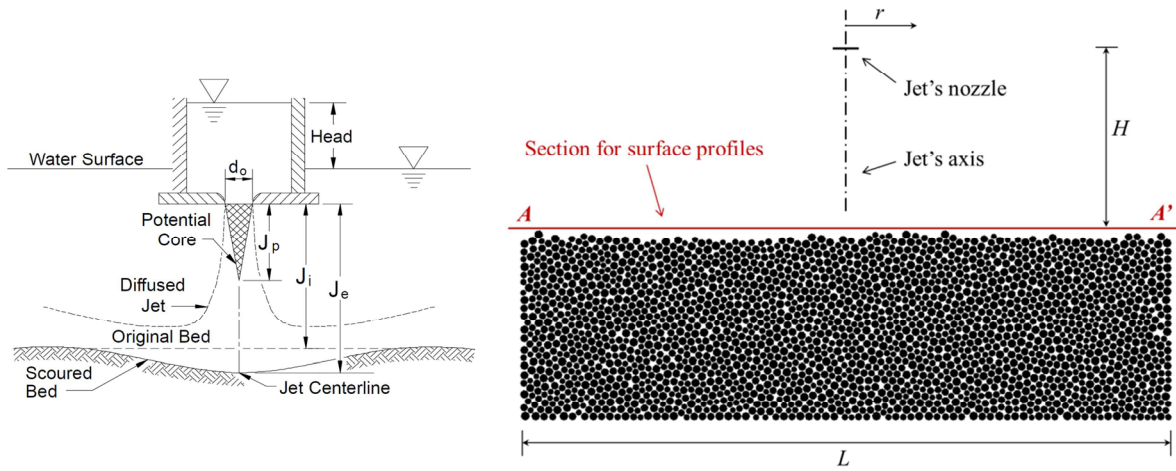


Figure 2: Left: Conceptual sketch of jet erosion test (source: [1]); Right: Spatial disposition of granular assembly, jet's nozzle and control section for fluid variables

The geometrical, material and rheological parameters of the system employed for these simulations are summarized in Table 1.

Table 1: Geometrical, material and model parameters adopted for the simulations

Solid phase		Fluid phase	
Particle mean size, D_{mean}	3×10^{-3} m	Jet's distance to surface, H	7×10^{-2} m
Polydispersity, D_{max} / D_{min}	1.5	Jet's nozzle size, d_0	5×10^{-3} m
Length of granular sample, L	2.63×10^{-1} m	Kinematic fluid viscosity, ν	5×10^{-5} m ² /s
Height of granular sample, H_s	8×10^{-2} m	Fluid density, ρ_f	847 kg/m ³
Particle density, ρ_s	2230 kg/m ³	Lattice grid size, Δx	2.3×10^{-4} m
Normal contact stiffness, k_n	1.1×10^5 N/m	Lattice speed, c_s	10 m/s
Shear contact stiffness, k_s	1.1×10^5 N/m	Hydraulic radius factor, R_h	0.8
Rolling stiffness, k_ω	$0.1 k_n$	Inlet fluid velocity, u_j	[0.8-1.5] m/s
Friction coefficients, $\mu = 3 \cdot \mu_\omega$	0.3		
Normal bond stiffness, $k_{n,b}$	$0.5 k_n$		
Shear bond stiffness, $k_{s,b}$	$0.2 k_n$		
Bond strength, $C = C_n = 2C_s$	[0-2.5] N		

The fluid flow may be described as an inertial laminar flow ($Re_{JET} \sim 80$ to 160), i.e. a flow in the transition from a laminar to a turbulent regime.

3.1 Jet analysis

The transversal profile of fluid velocity right above the soil surface shows a typical shape

with a stagnation point under the jet's axis and the two local maxima at some distance from it ($r/H \sim 0.25$). These features are nevertheless strongly conditioned by the actual shape and roughness of the bed surface.

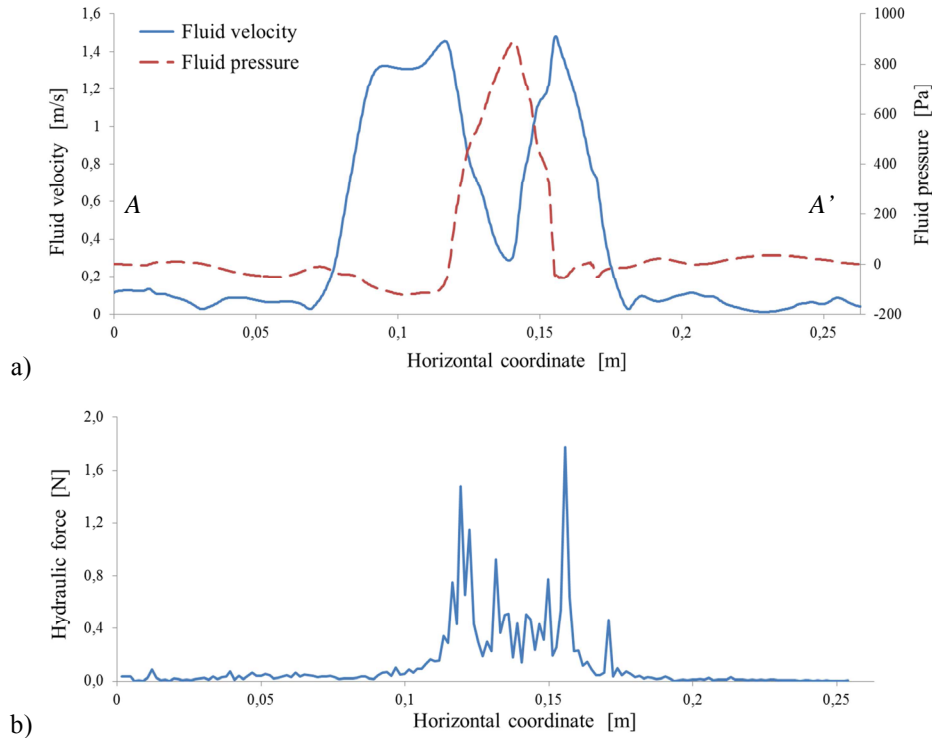


Figure 3: a) Transversal profiles of fluid velocity and pressure at control section A-A'; b) Integrated resultant of hydraulic forces acting on the solid particles at the soil's surface

The viscous drag forces acting on the soil surface are proportional to the fluid velocity and thus show a similar pattern of stagnation under the jet's axis and local maxima at $r/H \sim 0.25$ (Figure 3b).

3.2 Erosion process

The erosion process begins when the hydraulic shear stress at the soil surface exceeds a critical shear stress. For our configuration, this limit was reached for jet velocities equal to or greater than 0.6 m/s, in good agreement with our on-going experimental results [26]. As expected, the mobilization of solid particles then follows a pattern that is similar to the profiles of fluid velocity and hydraulic drag forces. Figure 4a shows the eroded profile of a cohesionless sample for a jet velocity of 0.8 m/s after 1.6 seconds of jet flow. At higher jet velocities and in the absence of cohesion, the picture becomes less clear due to the increased scouring depth, the ejection of solid particles and frequent avalanches of the scour pit walls.

In the presence of cohesive forces between particles, the erosion kinetics becomes slower but the initial topology of erosion does not change. Figure 4b shows the state of the granular sample for a cohesive strength of $C = 2.0$ N and a jet velocity of 1.5 m/s after roughly 0.5 seconds of jet flow. We observe a characteristic stagnation zone at the jet's axis and the

contiguous local maxima of scour depth. It is also observed that the grains are now detached either as single particles or in multi-grain clusters preserving a number of internal bonds.

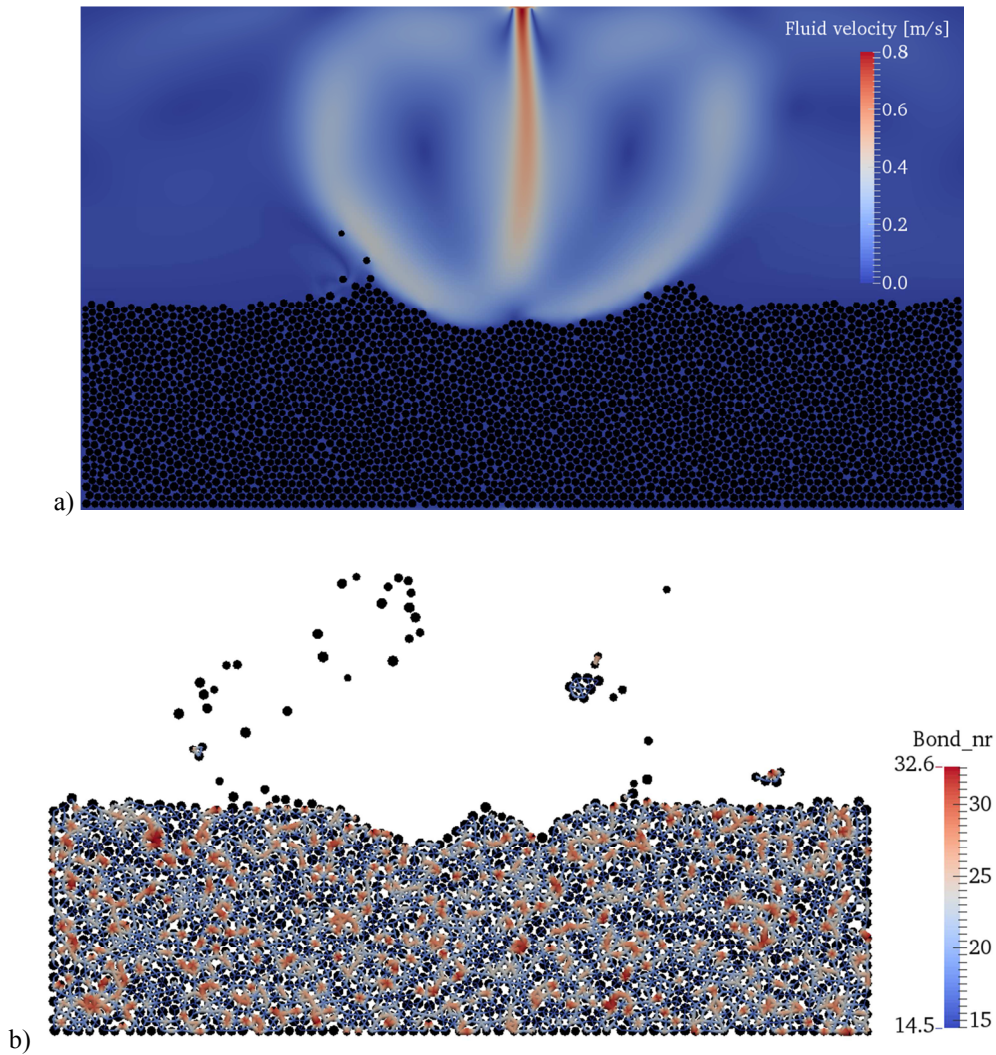


Figure 4: Initial topology of surface erosion; a) Cohesionless sample (bond strength $C = 0$ N), jet velocity $u_j = 0.8$ m/s; b) Cohesive sample ($C = 2$ N), jet velocity $u_j = 1.5$ m/s

In order to quantify and evaluate the erosion kinetics in a consistent manner for both the cohesive and cohesionless samples, it is necessary to specify an erosion criterion allowing us to distinguish between eroded and non-eroded particles. The cumulative particle displacement can be misleading for this purpose since it integrates the persistent residual micro-displacements of the particles, which can add up to significant magnitudes. Therefore it seems more appropriate to differentiate the particles as a function of an instantaneous quantity such as the kinetic energy:

$$K_i = \frac{1}{2}mv_i^2 + \frac{1}{2}I\omega_i^2 \quad (2)$$

where m , I , v_i and ω_i are the particle's mass, moment of inertia, translational velocity and angular velocity, respectively. In this way, if a particle attains at any moment a kinetic energy above a given threshold, it is classified as eroded. In this study, a threshold of 2×10^{-5} Joules allowed us to discriminate well the particles at the debonding front separating the cohesive assembly from the detached and re-settled particles (see Figure 5a), and thus was adopted as erosion criterion.

Figure 5b shows the time evolution of the relative eroded mass (i.e. the proportion of eroded particles compared to the total mass of the granular assembly) for different strengths of the cohesive bonds and a jet velocity of 1.5 m/s.

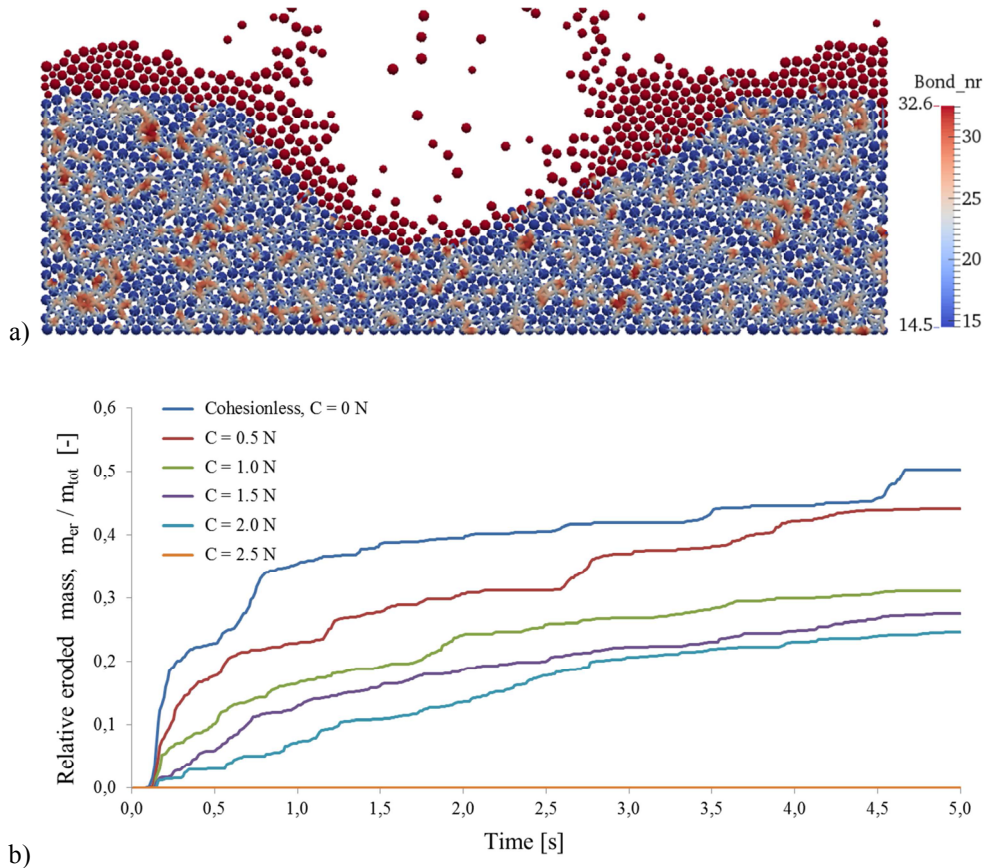


Figure 5: a) Eroded state of soil surface for $C = 2$ N after $t = 5$ s, with particle discrimination in terms of kinetic energy (red: eroded particles; blue: intact particles); b) Erosion kinetics in dependence of the bond strength

The purely frictional sample ($C = 0$ N) shows a sharp increase of eroded mass when the fluid jet reaches the soil surface and after 5 seconds half of the assembly has already been eroded. This proportion is significantly reduced by the introduction of cohesion, while the complete absence of erosion is achieved when the bond strength is $C = 2.5$ N. Therefore, the critical cementation degree for the beginning of erosion in the presented conditions should feature a micromechanical bond strength somewhere between 2 and 2.5 N.

4 CONCLUSIONS

We used a coupled DEM-LBM model to investigate the micromechanics of surface erosion of cohesive geomaterials under the action of a fluid jet flow. We showed that for a given jet flow, there is a critical value of inter-particle cohesion for which surface erosion occurs. We presently work on the influence of more complex cohesion laws and the relation between the micromechanical and macroscopic yield thresholds.

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