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Phase Relationship of Photodetected Signals of an Optical Feedback Interferometry Sensor

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Abstract

Optical Feedback Interferometry signals can be acquired by photodetection either from rear or front facet of the laser. We present a model that links both signals to the injection current. The comparison with experimental results validates the model.

I. INTRODUCTION

Optical feedback interferometry (OFI) is a well-known sensing technique where the back-scattered light from a distant target is re-injected into the laser cavity thus producing variation of the laser emitted power. OFI signals can be obtained by observation of the fluctuations in the output power either through the monitoring photodiode usually displayed in front of the laser rear facet (called rear PD signal) or through a photodiode that collects a part of the power emitted trough the front facet of the laser (called front PD signal) while using a beam splitter placed in the optical path between the front facet and the target as shown in Fig. 1.

The rear and front PD signals were first reported to be out-of-phase by Juskaitis *et al* [1], with clearer observations and better reasoning provided by Wang *et al* [2] and Randone *et al* [3]. In this paper, we present modeling results based on a previous work reporting the evolution of the PD signal with the injection current [4]. The developed model was validated experimentally over the entire injection current range.

II. THEORETICAL MODEL

Considering the schematic representation of OFI configuration shown in Fig. 2, interferometric signals can be observed in two different positions: using the electric field that propagates from the active cavity through the rear facet and is acquired by the rear photodiode, E_b , and the electric field that propagates through the front facet E_f . In the presence of a remote target, part of the back-reflected electric field is reflected from the laser front facet back towards the target (denoted as E_{ref}). E_f and E_{ref} are acquired by the front photodiode.

Solving Lang and Kobayashi equations [5] for both E_b and E_f , leads to the classical OFI equations

$$P_b = P_{b_0} [1 + m . \cos(\omega . \tau_{ext})]$$
(1)

$$P_f = P_{f_0} [1 + m . \cos(\omega . \tau_{ext})]$$
⁽²⁾

where P_b and P_f are the power under feedback at the back facet and the front facet respectively, P_{b0} and P_{f0} are the corresponding power of the solitary laser diode, *m* is the power modulation index, ω is the angular lasing frequency, and τ_{ext} is the round-trip time delay in the external cavity.

While on the rear PD, only E_b must be considered, on the front PD both E_b and E_{ref} are mixed leading to interferences so that the optical power photodetected P_{front} is

$$P_{front} = P_{f_0} [1 + (m - 2\sqrt{R_2 R_{ext}}) \cos(\omega \tau_{ext})]$$
(3)

where R_2 is the power reflectivity of the front facet and R_{ext} is the effective power reflectivity of the remote target.

The ratio of the modulation indices of the front and rear PD signals, M_R , can be expressed as

$$M_{R} = 1 - \frac{\tau_{I}}{\tau_{p}} \cdot \frac{R_{2}}{T_{2}} \cdot \frac{I - I_{th}}{I - I_{tr}}$$
(4)

where τ_l is the round-trip time delay within the active cavity, τ_p is the photon lifetime, T_2 is the front facet power transmission coefficient, *I* is the injection current, I_{th} and I_{tr} are the currents at threshold and transparency, respectively.

Expression (4) explicitly shows the evolution of the modulation indices ratio with injection current. Just above threshold, the ratio is positive, and then it gradually decreases with the increment of injection current until it becomes zero indicating no detection of the front signal. Further increment of the current leads to a negative ratio as the front PD signal changes sign. At high injection currents, the ratio becomes almost constant.





III. RESULTS AND DISCUSSION

In order to experimentally validate the developed analytical model, set of experiments were performed using the OFI sensor in the Doppler velocimeter configuration as shown in Fig. 1. The laser diode used was DFB laser (ML725B11F, $\lambda = 1310$ nm).

Fig. 3 shows both PD signals measured at different values of injection current. In Fig. 3(a), both signals are in-phase at 6 mA. Increasing the injection current to 9 mA, the front PD signal vanishes and is reduced to the noise level, as shown in Fig. 3(b). Further increment of injection current leads to the sign inversion of the front signal as shown in Fig. 3(c).

The model was simulated using the intrinsic laser parameters given in [6]. The theoretical curve in Fig. 4 that we obtain after minor fitting of the ratio of the reflectivity and transmission coefficients shows good agreement with the measurements.



Fig. 3. Normalized rear (upper blue trace) and front (lower green trace) PD signals at different bias currents: a) I = 6 mA, PD signals are in-phase, b) I = 9 mA, front PD signal vanishes, c) I=16 mA, signals are out-of-phase.



Fig. 4. Ratio of modulation indices as function of injection current: measured (green solid), and modeled (blue solid). The bias currents at which signals in Fig. 3 were measured are marked.

IV. CONCLUSIONS

An analytical model describing the phase and amplitude relationship of PD signals acquired through rear and front facet of the laser diode in while subject to optical feedback was presented and validated experimentally. The model explains well the observed phase inversion of the front PD signal as well as the inability to detect the signal at some point along the injection current range. This bias current can be either avoided when using an external photodetector in optical feedback interferometric application or considered when optical feedback is undesired.

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