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# **High resolution three dimensional structural microscopy by single angle Bragg ptychography**

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## **Abstract**

Coherent x-ray microscopy by phase retrieval of Bragg diffraction intensities enables lattice distortions within a crystal to be imaged at nanometer-scale spatial resolutions in three dimensions (3D). While this capability can be used to resolve structure-property relationships at the nanoscale under working conditions, strict data measurement requirements can limit the application of current approaches. Here, we introduce an efficient method of imaging 3D nanoscale lattice behavior and strain fields in crystalline materials with a new methodology: 3D Bragg projection ptychography (3DBPP). This method enables 3D image reconstruction of a crystal volume from a series of two dimensional x-ray Bragg coherent intensity diffraction patterns measured at a single incident beam angle. Structural information about the sample is encoded along two reciprocal space directions normal to the Bragg diffracted exit beam, and along the third dimension in real space by the scanning beam. We present our approach with an analytical derivation, a numerical demonstration, and an experimental reconstruction of lattice distortions in a component of a nanoelectronic prototype device.

## INTRODUCTION

Hard x-ray coherent diffraction microscopy methods based on inversion of Bragg diffraction intensities enable the sensitivity of x-rays to crystalline distortions in materials to be leveraged in order to reveal the interplay between structure and properties without disturbing environmental boundary conditions [1–5]. Such inversion-based approaches require that coherent diffraction patterns be numerically inverted into real space by determining the phase of the diffracted field, which is not measured experimentally. As was noted by Sayre [6] and experimentally demonstrated by Miao et al. [7], the phase and amplitude of x-ray scattering can be determined from redundant information contained in an oversampled diffraction intensity pattern. The resulting images contain quantitative information that encodes local physical parameters such as density and atomic displacement at sub-beam-size spatial resolutions. This principle has inspired the development of phase-retrieval-based coherent x-ray diffraction imaging approaches in recent decades that rely on iterative numerical methods to determine the sample structure [8].

The development of ptychography [9, 10] as a technique to determine the phase of scattering from an extended object has greatly expanded the range of samples that can be studied using coherent x-ray diffraction imaging. In ptychography, the structural information about the sample is encoded by measuring a series of diffraction patterns at a set of overlapping beam positions [11, 12]. The information obtained from the hundreds of overlapping diffraction patterns measured in a typical ptychography experiment greatly overdetermines the structure of the sample and leads to very robust reconstructions used to image a wide variety of samples [13, 14]. Moreover, the information redundancy is so large that additional parameters can simultaneously be retrieved, *e.g.*, the initial probe and positions [15], mode structure [16], multiple sample planes [17]. Thus, identifying new ways of leveraging the overdetermined nature of a ptychographic measurement can enable additional, unexpected components of a scattering system to be determined.

In this article, we exploit the information content of a set of 2D coherent diffraction patterns measured at a crystalline Bragg peak in order to reconstruct a 3D strain-sensitive image of an extended sample using a new technique, 3D Bragg Projection Ptychography (3DBPP). 3DBPP is a hybrid real / reciprocal space technique that uses the raster motion of a focused x-ray beam in combination with 2D Bragg diffraction intensity patterns measured at each position, eliminating the need to change the sample angle. The central concept underpinning our approach is shown in Figure 1. The projected structural profile within a column defined by the shape of the incident

x-ray beam can be determined from a Bragg diffraction intensity pattern, presuming the phases are known, via a Fourier transformation. At a given Bragg angle, translating the beam in two dimensions (into/out of the page and towards/away from the detector) results in diffraction patterns that yield structure profiles within different columns of the 3D crystal. With a set of structural profiles from overlapping beam positions, the known translational relationship of those profiles can be used to reconstruct the 3D morphology and strain of the crystal. In other words, each 2D diffraction pattern contains information regarding a projection of the 3D sample structure illuminated by the beam. When two or more projections are considered from beam positions that overlap, the 3D sample structure that is simultaneously consistent with the observed diffraction is constrained. To first order, as the beam size decreases and (to a certain extent) overlap increases, the reconstructed 3D structure is increasingly constrained and necessarily approaches the true structure. This 3D reconstruction concept is unique in that two dimensions of the problem are encoded in reciprocal space by the diffraction in the detector, and the third dimension is encoded in real space by the displacement of the beam towards the detector. In this way, our approach exploits the high angle of separation between the incident and diffracted wave vectors, as has been demonstrated in other work for 3D imaging from a single view [18, 19].

In 3DBPP, the localized columnar illumination of the beam intersecting the sample at a given position in the Bragg geometry connects the real and reciprocal space information. In practice, the phases of each diffraction pattern must also be determined. In this work, we show that this is possible, by exploiting the large information redundancy contained in a Bragg ptychography data set. As such, 3DBPP introduces a new avenue by which to unlock the information contained in a set of far-field coherent x-ray diffraction patterns that will enable materials phenomena to be visualized in 3D in working environments with simplified experimental requirements.

## **BACKGROUND**

3DBPP features concepts utilized in other reconstruction-based microscopy methods, specifically, from Bragg coherent diffraction imaging, ptychography, and tomography. Bragg coherent diffraction imaging is based on the measurement of the far-field intensity distribution in the vicinity of a Bragg peak via the Bragg *rocking curve* (changing the sample angle relative to the incoming beam and combining successive 2D slices into a 3D Bragg intensity pattern) [20]. A 3D image of a diffracting crystal can then be numerically retrieved from the measured intensity distribution using

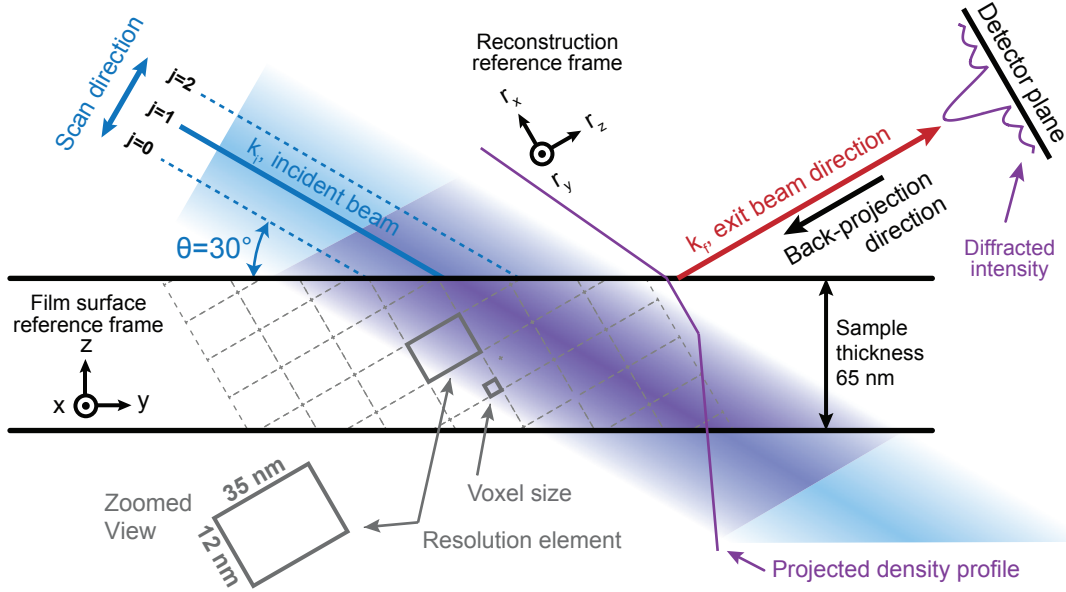


FIG. 1. **Encoding 3D structure at a single Bragg angle.** The sample shown here is a film with a thickness of 65 nm, corresponding to the thickness of the SiGe film measured in the experimental demonstration (Figures 3-5). For simplicity, the geometry shown depicts the 2D scattering plane and is used as the basis of the analytical derivation. Here, the area detector contains the  $r_x, r_y$  direction vectors, and measures reciprocal space coherent diffraction intensity patterns  $I_j(q_x, q_y)$  at each beam position ( $j = 0, 1, 2, \dots$ ). The  $r_z$  direction corresponds to the exit beam direction of the Bragg condition. The focused x-ray beam scan consists of displacing the beam normal to its propagation direction. The essence of 3DBPP is that structural information about the sample along  $r_x, r_y$  is encoded in the coherent diffraction patterns measured with the area detector ( $I_j(q_x, q_y)$ ), and the structure along  $r_z$  is probed directly by the scanning the beam with component of displacement along that direction. The  $r$  reference frame sets the orientation of the voxels of the 3D reconstruction and of the resolution element. As shown, the edges of the voxels and the resolution elements do not line up with surface of the film. Thus, for convenience, we introduce a second reference frame ( $x, y, z$ ) that is used in our discussion of the structural features of the thin film. In the experimental demonstration, this reference frame corresponds to low-index crystallographic directions in the SiGe crystal:  $x \parallel [110]$ ,  $y \parallel [-110]$ , and  $z \parallel [001]$ .

iterative algorithms with a constraint based on the rough dimensions of the sample [21]. Similar imaging capabilities can be realized for extended crystals (*e.g.* thin films) via ptychography applied to Bragg coherent diffraction patterns [14, 22–27]. However, for 3D Bragg ptychography, the requirement of full rocking curve measurements at each overlapping beam position results in long measurement times and uncertainties with regard to registration. 3DBPP avoids measuring the full angular rocking curve of the Bragg peak by exploiting the fact that a 2D far-field Bragg diffraction pattern is related to the Fourier transform of a 2D projection of the illuminated sample volume [28]. This relationship enables 3D imaging from 2D diffraction patterns by incorporating projection and back-projection operations utilized in computed tomography [29, Sec. 6.3.3] [30,

Sec. 6.2] into an iterative x-ray phase retrieval strategy. Thus, we relate a set of 2D high-angle Bragg coherent diffraction patterns measured at a fixed angle to a 3D real-space sample structure.

## PRINCIPLES OF 3D BRAGG PROJECTION PTYCHOGRAPHY

Due to the geometry of a crystalline Bragg condition, the angular diversity central to other 3D imaging modalities can be replaced by translational diversity of a localized beam. At a Bragg condition, the incident and scattered wavevectors are not collinear but, in the hard x-ray regime, are typically separated by tens of degrees. As a result, the spatial information that is collapsed along the exit beam direction in any individual 2D projection can be encoded in the data set by translating a localized x-ray beam in overlapping steps in the plane normal to  $\mathbf{k}_i$ , the propagation direction of the incident beam (Figure 2(a, b)).

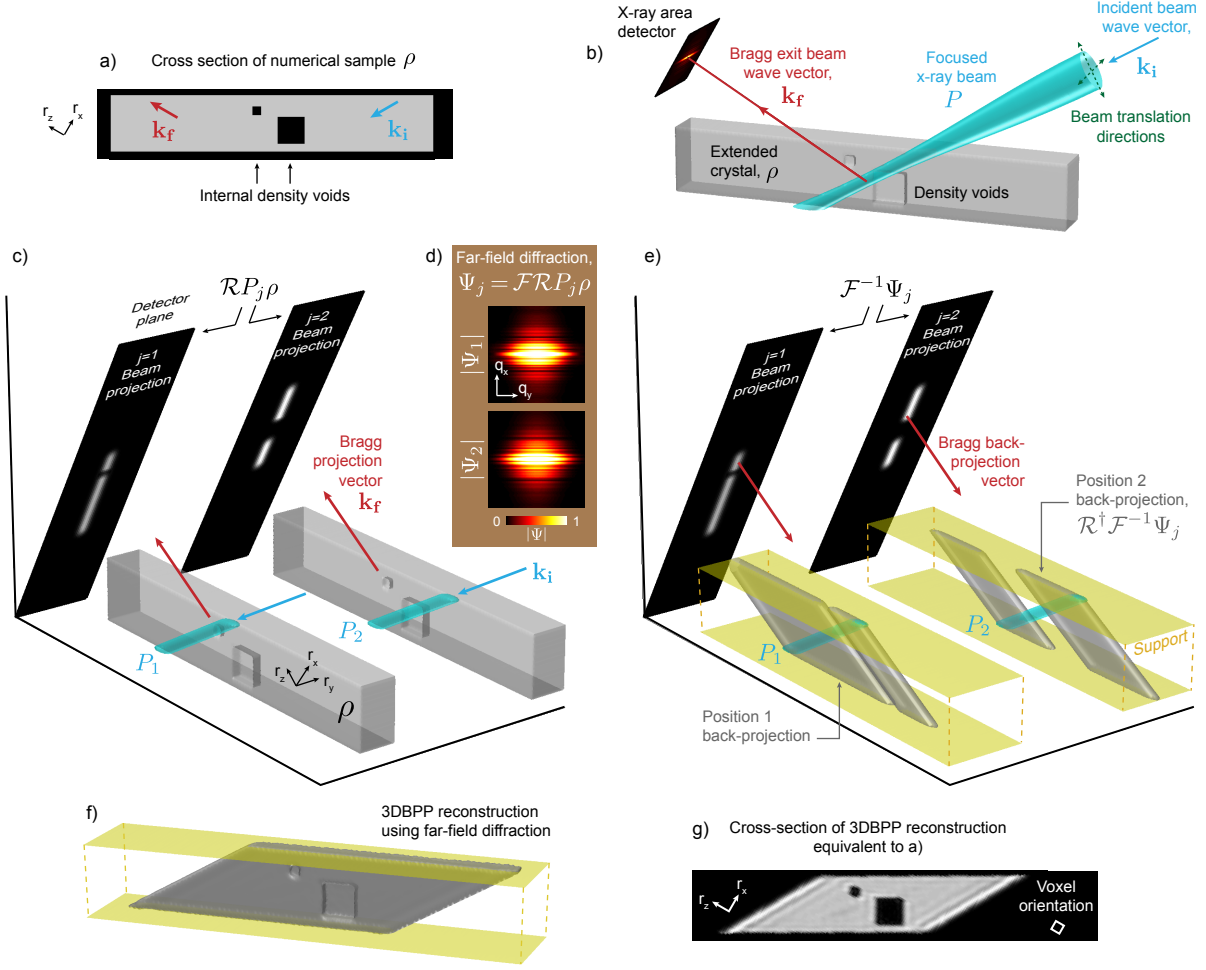
In 3DBPP, the inversion procedure is based on the description of the beam/crystal interaction in the Bragg geometry. At a given beam position, the intensity pattern recorded by the x-ray camera in the far field is the squared amplitude of the diffracted wave field  $\Psi_j$ :

$$\langle I_j \rangle = |\Psi_j|^2, \quad (1)$$

where  $I_j$  is the intensity pattern corresponding to the  $j$ -th beam position. The intensity pattern recorded in the detector is subject to counting statistics, and so Equation 1 defines an expectation value  $\langle I_j \rangle$ . We adopt the convention [31] that in a coherent Bragg diffraction imaging experiment, the origin of reciprocal space ( $q_x = 0, q_y = 0, q_z = 0$ ) corresponds to a Bragg condition denoted by the reciprocal space vector  $\mathbf{G}_{\text{HKL}}$  for a given HKL-index Bragg reflection. At a Bragg condition, the diffracted wave  $\Psi_j$  is related to the 3D diffracting crystal  $\rho$  and the beam  $P_j$  (also referred to as the probe) according to [28, 32]:

$$\Psi_j = \mathcal{F}\mathcal{R}P_j\rho, \quad (2)$$

where  $\mathcal{F}$  is the (bidimensional) Fourier transform,  $\mathcal{R}$  is the (3D) *x-ray projection operator* along the exit beam direction [30, Sec. II.2]. In this Equation,  $P_j$  and  $\rho$  are complex-valued three dimensional quantities. The phase and amplitude of  $\rho$  are related to the Bragg structure factor [27], which is sensitive to atomic-scale structure in the material. Reconstructing  $\rho$  thereby enables local distortions of the crystal lattice to be imaged and quantified.



**FIG. 2. The principles of 3DBPP:** a) A 3D strain free crystal was generated ( $\rho$ ) containing two internal voids, and a 3DBPP experimental geometry was simulated (b) using a focussed gaussian beam profile at a high angle Bragg condition defined by the  $\mathbf{k}_i$  and  $\mathbf{k}_f$  incident and exit beam vectors. We define real space axes  $(r_x, r_y, r_z)$  such that  $\mathbf{k}_f \parallel r_z$  and  $(r_x, r_y)$  lie in the detector plane, conjugate to  $(q_x, q_y)$  in the far field. In order to calculate diffraction patterns, projections along  $\mathbf{k}_f$  of the illuminated crystal ( $\mathcal{R}P_j\rho$ ) in the  $(r_x, r_y)$  plane are determined (c) at beam positions that intersect the two voids in  $\rho$ . The far-field diffraction amplitudes  $|\Psi_j|$  determined by Fourier transforming the projections are shown in d). The inverse process is shown in e) where, starting from the far-field diffraction  $\Psi_j$ , the inverse Fourier transform again yields the 2D projections of the illuminated crystal. The operator critical to 3DBPP is the backprojection ( $\mathcal{R}^\dagger$ ) of the quantity  $\mathcal{F}^{-1}\Psi_j$  along the  $\mathbf{k}_f$  direction. The backprojection “stretches” the 2D projections along  $\mathbf{k}_f$  within a 3D support. In this case, the support is made of a pair of planes that limit the extent of the reconstruction in the  $z$  direction. Here, the backprojection intersects the probe at an oblique angle, effectively localizing the scattering volume. With 3DBPP,  $\rho$  was reconstructed (f,g) using these operators from a set of 2D coherent Bragg diffraction intensity patterns (See Methods for details).

For 3DBPP phase retrieval, a ptychographic inversion algorithm is used to reconstruct  $\rho$  from a set of  $J$  intensity patterns  $\{I_j\}_{j=0}^{J-1}$ . The numerical approaches that have successfully been used in transmission geometry ptychography experiments (i.e., difference MAP [12, 33], ordered-subset (OS) / Ptychographic Iterative Engine algorithm (PIE) [11, 34, 35] or gradient-type iterations [35–37]) can be adapted to accommodate 3DBPP by incorporating a new gradient based on the cost function  $\mathcal{Q}(\rho)$ :

$$\mathcal{Q}(\rho) = \sum_{j=0}^{J-1} \mathcal{Q}_j(\rho) \quad \text{with} \quad \mathcal{Q}_j(\rho) := \|\ |\Psi_j(\rho)| - \sqrt{I_j} \|^2. \quad (3)$$

In 3DBPP, this cost function yields the following gradient  $\partial_j$  for each probe position:

$$\partial_j = P_j^* \mathcal{R}^\dagger \mathcal{F}^{-1} \left( \Psi_j - \sqrt{I_j} \frac{\Psi_j}{|\Psi_j|} \right), \quad j = 0 \cdots J - 1, \quad (4)$$

where '\*' is the conjugate operator and  $\mathcal{R}^\dagger$  is the adjoint (i.e. *backprojection*) operator [30, Eq. 2.31] associated with the forward-projection operator  $\mathcal{R}$ . In this work, we incorporated the gradient (Equation 4) into an iterative OS/PIE algorithm [38] that progressively lowered the cost function  $\mathcal{Q}$  and reconstructed an image of the diffracting crystal  $\rho$  (see Methods).

Thus, a successful 3DBPP reconstruction must retrieve the three-dimensional spatial components encoded in a measured set of Bragg diffraction patterns. Conceptually, the 3D reconstruction is enabled by two factors. First, each individual intensity pattern, when phased, gives access to the projected scattering volume for each beam position (the quantity  $\mathcal{F}^{-1}\Psi_j$  in Figure 2). Second, the backprojection of this quantity is localized to a specific volume of the crystal because the relative probe positions are known and the angle between the incident and exit angle of the Bragg condition is non-zero. 3DBPP extracts this 3D information by utilizing overlapping probe positions in order to recover the relative phases of the diffraction patterns and a 3D reconstruction of  $\rho$ . The thin film reconstructions featured in this work were further constrained with a support that confined the extent of the object along the surface-normal direction (as shown in Figure 2). For other samples, different position-referencing constraints may be implemented that serve the same function. We also note that probe reconstruction has not been implemented in this study due to the fact that as stated in Refs [23, 25], retrieving both a 3D probe and 3D crystal in a Bragg ptychography experiment has been seen to adversely affect the reconstruction quality due to the lack of constraints along the propagation direction. In this work, the wavefunction of the probe at



the sample is known or determined *a-priori* and is not further refined during image reconstruction.

A numerical demonstration of 3DBPP is featured in Figure 2. We define a 3D thin-film object of uniform density, and introduce two cubic voids in the center of the film. A numerical set of 2D coherent diffraction patterns was generated using Equation 2 by scanning a purely real gaussian beam through the central region of the film in overlapping steps (probe profile shown in Sup. Figure S5). Using 3DBPP implemented with an OS/PIE inversion algorithm, the 3D internal structure of the film in the scanned field of view was successfully reconstructed from this set of 2D patterns (Figure 2(f, g)). (See Methods for more details on this numerical test, and Sup. Figure S12 for additional images of the reconstruction.)

We also emphasize that, as opposed to previous 3D Bragg ptychography approaches [23–25], this 3DBPP method is not one of pure Fourier synthesis in which the properties of the 3D reconstruction depend strictly on the measurement and sampling of a 3D volume of reciprocal space. 3DBPP is also distinct from multi-slice reconstruction methods [17], as it does not rely on higher order interactions between the beam and the sample. The following derivation highlights the means in which 3D spatial information is encoded in a scanning probe Bragg ptychography measurement at a single sample angle.

For the sake of simplicity, we assume that the scanning probe moves in the direction of the exit beam ( $\mathbf{k}_f$ ), with a regular step-size  $\Delta$  (Figure 1 and Supplemental Figure S1). In this case, the complex-valued diffracted field  $\Psi_j(q_x, q_y)$  at the  $j$ -th probe position illuminating a 3D sample can be expressed as:

$$\Psi_j(q_x, q_y) = \iint_{r_x, r_y} g(r_x, r_y, r_z = j\Delta) e^{-i(r_x q_x + r_y q_y)} \mathbf{d}r_x \mathbf{d}r_y \times \frac{1}{(2\pi)^2} \quad (5)$$

where

$$g(r_x, r_y, r_z) := (\rho \otimes_{r_z} P^l)(r_x, r_y, r_z).$$

In this expression,  $\otimes_{r_z}$  is a 1D convolution operator that acts solely along the backprojection direction  $r_z$ , and the probe is written as  $P^l(r_x, r_y, r_z) := P(r_x, r_y, -r_z)$ . This expression (5) shows that, as expected for an area detector measurement,  $\Psi_j$  depends on two orthogonal reciprocal space directions  $q_x$  and  $q_y$  that encode structure along  $r_x$  and  $r_y$ . However, Equation (5) also clearly demonstrates that a *series* of Bragg diffraction patterns measured with a scanning beam also encodes sample structure along  $r_z$  — the direction to which any single diffraction pattern is insensitive. The unique capability of 3DBPP stems from its ability to exploit the dependence of

$\Psi_j$  on the sample structure along  $r_z$  without requiring angular diversity.

Under appropriate conditions, our OS/PIE 3DBPP approach can in principle reach sub-beam-size resolution along  $r_x, r_y, r_z$  because the 3DBPP inversion algorithm inherently deconvolves the object from the probe along the direction of backprojection. This deconvolution comes about because diffracted intensities ( $|\Psi_j|^2$ ) are measured, and a non-linear iterative phase retrieval algorithm must be invoked that relates  $|\Psi_j|^2$  directly to the sample estimate  $\rho$  (as opposed to  $g$ ). This approach provides a momentum-transfer-limited resolution limit in  $r_x, r_y$  (as is typical in 2D ptychography), and it “builds-in” a degree of probe deconvolution along the backprojection direction  $r_z$ . While sub-beam resolution is in principle obtainable, the extent to which the deconvolution in  $r_z$  is realized depends on spatial sampling and the signal to noise ratio of the data.

In the absence of noise, three conditions must be satisfied in order to enable a reconstruction with sub-beam-size resolution in three dimensions: 1) the sampling in the area detector is at least twice the Nyquist rate (as in typical coherent diffraction methods), 2) the spatial sampling rate  $\Delta$  (the probe scan step size) along  $r_z$  fulfills twice the Shannon-Nyquist condition with respect to the spectral bandwidth of the probe in that direction, and 3) the probe spectrum is non-zero over a wide range of spatial frequencies (*e.g.*, spectral tails that damp but do not extinguish high frequency terms). When *noisy* intensity patterns are considered, the maximum extent in  $q$ -space to which photons are detected from the central Bragg peak position limits the resolution along the  $r_x$  and  $r_y$  directions. The resolution along the third direction,  $r_z$ , depends on the ability to observe differences between intensity patterns from two overlapping probe positions displaced by a small  $\Delta$ . Typically, these differences manifest themselves in the weakly scattering high- $q$  regions of the diffraction patterns. Thus, the resolution along  $r_z$  also depends on the SNR of the measurement. With simulated data, we demonstrated sub-beam-size resolution along  $r_z$  with noise-free and noisy data (Figure 2, Sup Figure S2). However, under actual experimental conditions, we expect modest gains in  $r_z$  resolution beyond the probe size, as shown in our results in the next section. In addition, we expect the uniqueness of the 3DBPP reconstruction to be similar to other CDI experiments that are appropriately oversampled [39]. We also note that the nature of 3DBPP is such that there are no fundamental restrictions on the morphology or shape of the sample so long as the kinematic scattering approximation holds.

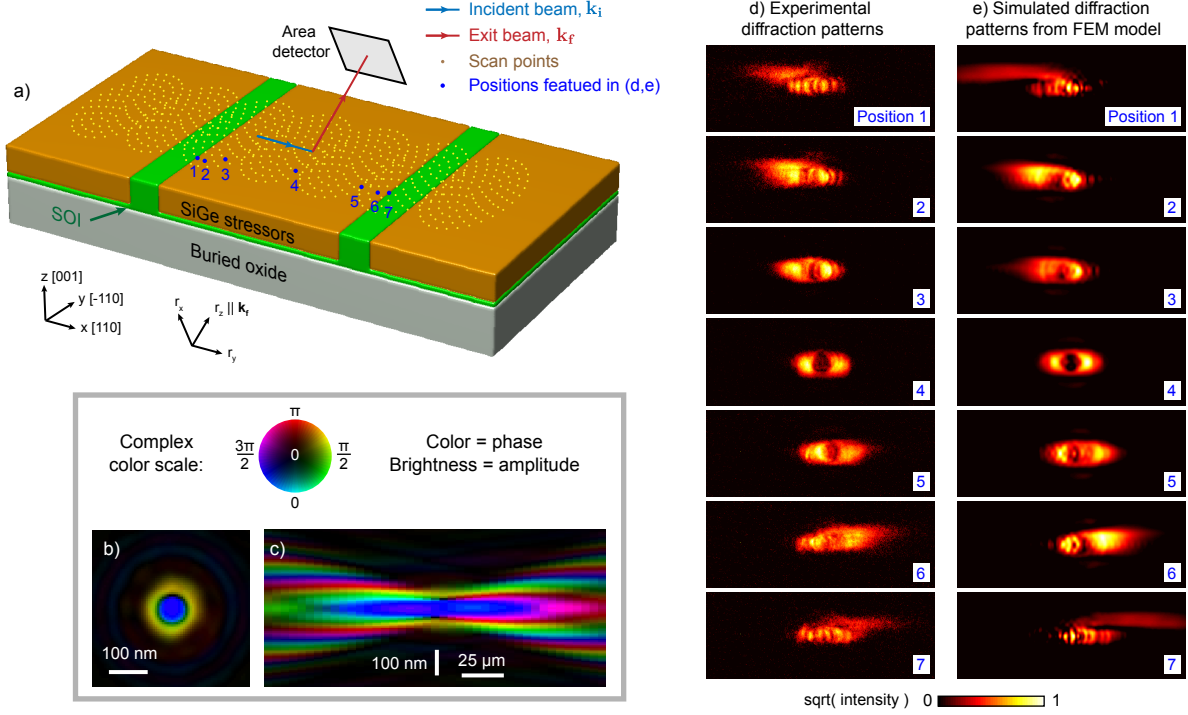


FIG. 3. **Experimental geometry.** (a) A schematic of the device architecture is shown featuring the embedded SiGe stressor geometry. For 3DBPP, coherent diffraction patterns were measured at the specular 004 SiGe Bragg peak at a set of beam positions that effectively overlapped in a series of spiral patterns. The diffraction patterns from all 707 positions were phased simultaneously with 3DBPP. (b,c) Prior to diffracting from the eSiGe, the beam wavefront was reconstructed using Fresnel ptychography of a test pattern in the transmission geometry. (d-e) Examples of 004 coherent Bragg intensity patterns used for 3DBPP imaging are shown from different regions of the stressor indicated in (a). Patterns (d-e) correspond to the positions indicated with blue dots in (a) from left to right. See Methods and Ref [40] for more details.

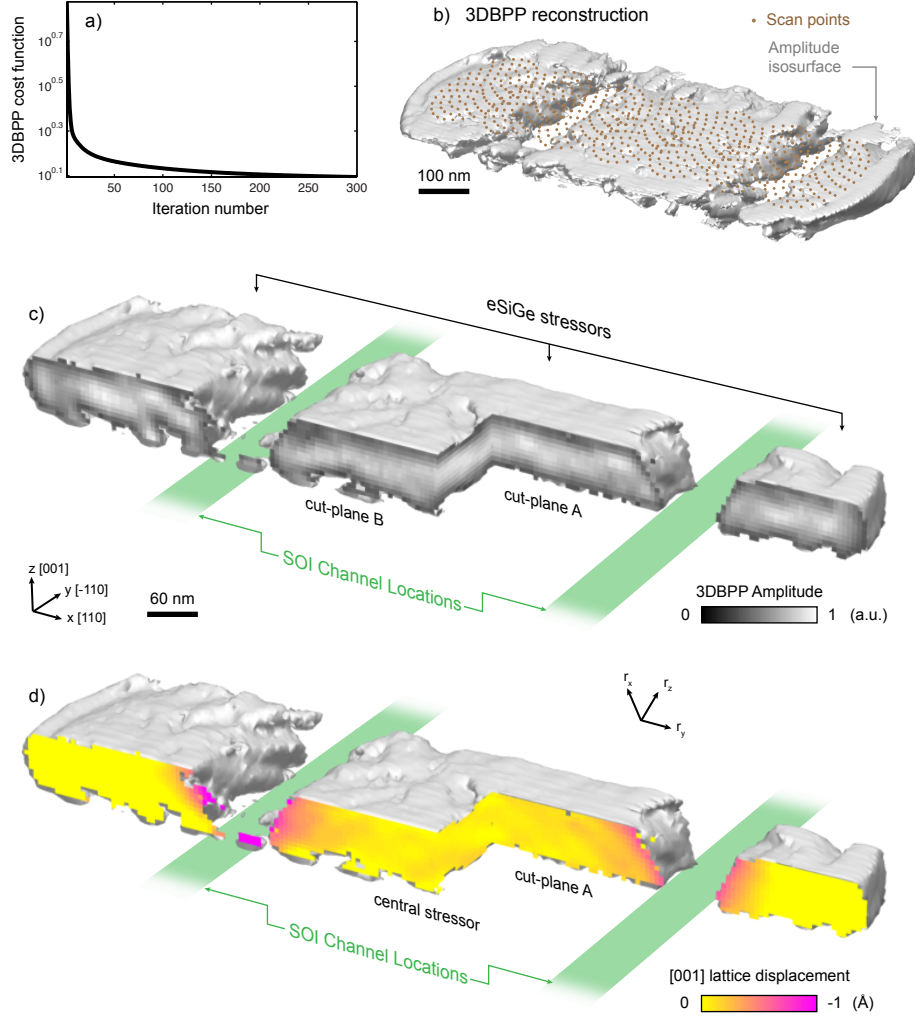
## EXPERIMENTAL DEMONSTRATION

To demonstrate 3DBPP, we imaged the internal lattice displacement field within a sub-micron-scale crystalline component of a semiconductor prototype device (Figure 3). The device structure consisted of periodic embedded SiGe (eSiGe) crystals 460 nm in width that were epitaxially grown to a thickness of 65 nm interstitially between 60-nm-wide linear silicon-on-insulator (SOI) channels (shown in Figure 3(a)). This sample design and processing (see Methods) resulted in a complex internal stress state and an accompanying strain field that evolves within the eSiGe stressors in the  $x$  (in-plane) and  $z$  (out-of-plane) directions, and is self-similar along the other in-plane direction,  $y$  [40]. In particular, the variation of the eSiGe strain field as a function of depth – variations to which 2D BPP is insensitive [40] – has a direct impact on the electron mobility within the SOI channels in this system and is a critical parameter for nanoscale device engineering.

Coherent nanodiffraction patterns were measured from several adjacent eSiGe stressor crystals with a zone-plate-focused hard x-ray beam at a symmetric 004 Bragg condition in which the angle between  $\mathbf{k}_i$  and  $\mathbf{k}_f$  was about  $60^\circ$  (see Methods and Figure 3). We note here that the experimental data collection methodology of 3DBPP is exactly the same as that of previously reported 2D BPP experiments [14, 26, 27, 40]. However, using our new imaging concept, 3D images can now be reconstructed from data that previously yielded 2D projection images [41]. Using these Bragg diffraction patterns, a 3DBPP reconstruction was generated using an iterative algorithm that incorporated the gradient in Equation 4 into an ordered subset / PIE framework [34, 35]. Because the coherent diffraction observed in the vicinity of the eSiGe 004 Bragg condition (denoted by the reciprocal space vector  $\mathbf{G}_{004}$ ) was well separated from scattering from the other components of the device (i.e. SOI and substrate), the reconstruction represents only the stressor structures. To aid in the determination of the relative phase relationship of the intensity patterns, a 90-nm-thick support that confined the extent of the reconstruction along  $z$  was incorporated into the reconstruction. This support constrained the intersection of each backprojection and respective probe function to within a physically realistic pair of parallel planes surrounding the 65-nm-thick film (see Methods). To describe the reconstruction, we adopted a coordinate system  $(x, y, z)$  such that the top surface of the stressor lies in the  $x, y$  plane, and  $z$  is the out-of-plane direction. This convention is distinct from the coordinate system of the reconstruction voxels  $(r_x, r_y, r_z)$  that are defined by the orientation of the area detector, as noted in the previous sections.

As expected for strained crystals, the resulting reconstructed 3D sample  $\rho$  is a complex-valued function,  $\rho = |\rho| \exp i\phi$ . The amplitude  $|\rho|$  is directly related to the electron density of the crystal and the phase  $\phi$  is sensitive to a component of the displacement field in the crystal given by  $\phi = \mathbf{G}_{004} \cdot \mathbf{u}$ , where  $\mathbf{u}$  is the crystalline displacement field relative to an arbitrary crystalline reference [20].

The external shape of the reconstructed amplitude is shown in Figure 4b as an iso-surface corresponding to 27% of the maximum amplitude value. The reconstructed shape shows the eSiGe features expected of this prototype device, including the two missing strips in amplitude corresponding to the positions of SOI channels. The internal structure of the reconstructed stressors is shown in Figure 4(c,d). The vertical cuts through the reconstruction show that the amplitude is mostly homogeneous with well defined in-plane edges where the eSiGe meets the SOI. For this stressor, the displacement of the crystal lattice along the [001] direction,  $\mathbf{u}_{001}$ , was derived from the phase of the 3DBPP reconstruction and is shown in Figure 4(d). As expected for this device



**FIG. 4. 3D Bragg projection ptychography experimental results** Coherent diffraction patterns measured at the 004 SiGe Bragg peak were phased using 300 iterations of the OS/PIE algorithm adapted for 3DBPP. (a) The cost function,  $\mathcal{Q}(\rho)$ , is shown as a function of iteration number. (b) The isosurface of the amplitude of the resulting reconstruction, showing gaps at the positions of the SOI channels. The internal structure of the SiGe material in the field of view is revealed by way of cuts through the isosurface depicting the amplitude of the reconstruction, which is closely related to the material density (c), as well as the crystal lattice displacement along the [001] direction (d) which is derived from the phase of the reconstruction.

architecture,  $\mathbf{u}_{001}$  varies in the  $(x, z)$  plane. The key capability of 3DBPP is demonstrated by the fact that out-of-plane lattice distortions in this cross-section that require a 3D reconstruction were resolved with a fixed-angle scanning probe diffraction measurement.

A crucial issue in this study is the quantification of the resolution obtained in the reconstruction, as this will dictate the utility of 3DBPP in the measurement of lattice distortions in different nanoscale crystalline systems. We used the Fourier shell correlation (FSC) method as detailed in Refs [42, 43]. FSC is based on a spectral comparison of two independent reconstructions of  $\rho$

generated, in this case, by splitting the 3DBPP data into half-data sets that were phased separately (see Methods). Because FSC uses two half-data sets, the resolution estimates tend to be conservative. Using FSC, the spatial resolution along  $r_x, r_y, r_z$  were estimated to be 12, 29, and 35 nm respectively. In this experimental reconstruction, we achieved modest gains in spatial resolution beyond the probe size in the  $r_z$  direction ( $\text{FWHM}_{probe} = 46$  nm). With a higher signal-to-noise ratio and better knowledge of probe positions, we expect further gains (see Supplemental).

The structural fidelity of the method was evaluated by comparing a cross-section of the reconstruction with a linear elastic boundary element method (BEM) model of the eSiGe stressor under the nominal mechanical boundary conditions of the device [44]. Figure 5 (a-c) shows the amplitude, phase, and displacement field maps from an  $(x, z)$  cross-section of the central reconstructed stressor (cut-plane A in Figure 4) alongside those of the corresponding BEM model. In Figure 5 (b,e), the phase of  $\rho$  is shown as a color map superimposed on the amplitude distributions shown in (a,d). The BEM model shows that the out-of-plane component of the displacement field  $\mathbf{u}_{001}$  evolves within the  $(x, z)$  plane, increasing at the top corners to a value of approximately  $-2.5$  Å relative to the center (Figure 5 (f)) and an out-of-plane strain value,  $\epsilon_{zz}$ , of  $-0.0015$  relative to the center. This variation in  $\mathbf{u}_{001}$  is the result of an elastic response of the SiGe lattice due to a change from a near-biaxially stressed state at the center of the stressor to a more uniaxially stressed state at the eSiGe / SOI interface. This BEM model was used to generate model diffraction patterns at a series of positions in the stressor corresponding to experimental observations (Figure 3(d,e)). This comparison is an alternative means by which to verify the sensitivity of Bragg coherent diffraction to both morphology and strain in a crystal. In addition, the uncertainty in the reconstructed displacement field under these experimental conditions can be estimated by considering the standard deviation of displacement within a  $115 \times 17 \times 24$  nm<sup>3</sup> volume consisting of 240 voxels in the center of the reconstruction where the displacement field varies slowly. In this region we find an uncertainty (one standard deviation) of  $\sigma_{\mathbf{u}_{001}} = 0.02$  Å, and an uncertainty in out-of-plane strain ( $\Delta d/d$ ) of  $\sigma_{\Delta d/d} = 0.0002$ .

To evaluate the impact of noise in our reconstruction, the model  $\mathbf{u}_{001}$  displacement was converted to a complex crystal density  $\rho_{BEM}$  calculated for the 004 Bragg diffraction condition, and a Fourier filter consistent with our experimental signal level was applied (see Methods) to determine phase and amplitude distributions ( $\rho_{BEM}^{filt}$ ). The calculated BEM cross-section ( $\rho_{BEM}$ ) is shown in the left half of Figure 5(d,e), and  $\rho_{BEM}^{filt}$  is shown in the right half. As seen in Figure 5(d), the Fourier filter modified the rectangular cross-section of the amplitude because high-spatial-

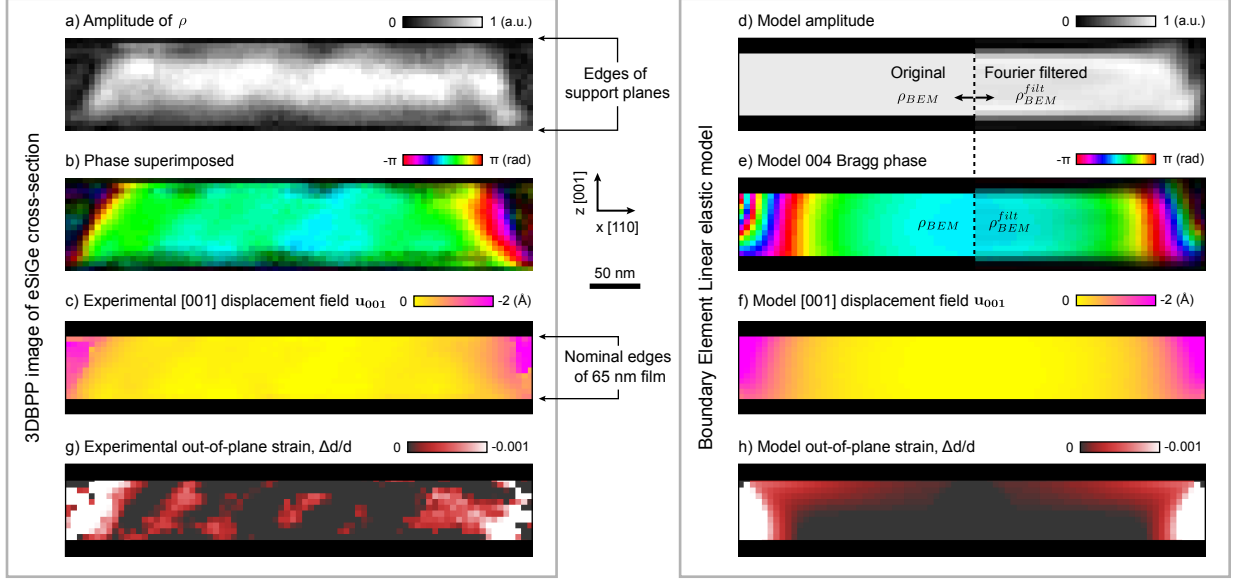


FIG. 5. **Comparison with linear elastic model:** A cut through the eSiGe stressor reconstruction is shown as both amplitude (a) and phase (b), with the edges of the 90-nm-thick support planes indicated. The cross section shown corresponds to cut-plane A in Figure 4(c). In (c), the phases in (b) were converted to units of lattice displacement along the [001] direction ( $u_{001}$ ) confined within an envelope representing the nominal edges of the 65-nm-thick film. For comparison, a boundary element method (BEM) linear elastic model of  $u_{001}$  in the stressor (f) was converted to the complex density expected for 004 Bragg diffraction,  $\rho_{BEM}$ . The amplitude and phase of  $\rho_{BEM}$  and  $\rho_{BEM}^{filt}$  are shown in (a,b) before and after application of a low-bandpass Fourier filter that replicates the experimental signal level.  $\rho_{BEM}$  and  $\rho_{BEM}^{filt}$  are shown on the left and right halves respectively of (d,e). Panels (g,h) show the experimental and model displacement fields converted to units of out-of-plane strain  $\epsilon_{zz}$  relative to center of the stressor.

frequency components not experimentally observed in our measurement were filtered out [35]. In the center of  $\rho_{BEM}^{filt}$ , the amplitude remains homogeneous, but the amplitude envelope falls off near the top corners where the internal displacement field of the crystal is expected to vary more rapidly. As a result of this displacement field, the phase evolves by  $\sim 2\pi$  in the top corners of the stressor before the amplitude envelope drops off. These features in  $\rho_{BEM}^{filt}$ , which come about from the predicted internal lattice behavior of the stressor as well as the limited dynamical range in the measured intensity, are all observed in the experimental 3DBPP reconstruction (Figure 5a,b).

## DISCUSSION & CONCLUSION

Our experimental results demonstrate that 3D images of strained crystals can be reconstructed without angular diversity at resolutions appropriate for nanoscale imaging. However, certain factors must be considered for a successful experiment. In particular, the effectiveness of localizing

sample structure along the beam propagation direction (via the  $P_j$  and  $\mathcal{R}^\dagger$  operators) is maximized when  $\mathbf{k}_f$  is perpendicular to  $\mathbf{k}_i$  (i.e.  $2\theta = 90^\circ$ ) and vanishes when  $\mathbf{k}_f$  is parallel to  $\mathbf{k}_i$  (i.e.  $2\theta = 0^\circ$  or  $180^\circ$ ). In addition, because the method involves successive backprojections, the reconstruction is susceptible to noise amplification that degrades the image at high iteration numbers in a manner analogous to computed tomography reconstructions with noisy data (see Supplemental).

Efficient three dimensional microscopy of strain fields in targeted regions of nanoscale crystals under balanced, undisturbed boundary conditions will enable powerful new studies of *in-situ* materials behavior. By utilizing an inversion strategy that efficiently uses Bragg diffracted photons from a simpler experiment, 3DBPP is a significant step in the development of 3D x-ray microscopy, especially in cases where sample rotation is prohibitive. As compared to Bragg ptychography with rocking curves, 3D images of crystals can be reconstructed using single-angle diffraction patterns measurements at a series of points. Furthermore, our approach simplifies the experimental requirements such that 3DBPP can be implemented on a wide range of coherent synchrotron x-ray beamlines, potentially using a variety of different focusing optics including pinholes and mirrors. In this capacity, the environmental compatibility and flexible field of view of 3DBPP is complementary to 3D atomic-resolution electron tomography of extremely small volumes of material [45]. More broadly, the integration of projection and backprojection operations into a phase retrieval algorithm can potentially be applied to address challenges in transmission geometry computed tomography, including the alignment of radial projections with incoherent computed tomography and potentially enabling global 3D inversion of tomographic far-field coherent diffraction patterns.

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## METHODS

**Numerical 3DBPP demonstration:** A numerical sample in the shape of a rectangular cuboid (Figure 1) was generated that was  $40 \times 30 \times 190$  pixels in dimension with two cubic voids in the sample with respective edge lengths of 7 and 17 pixels. The numerical object (denoted as  $\rho$ ) was purely real and had a uniform density outside of the voids. Figure 1(a) shows a cross-section through the middle of  $\rho$ , showing the two voids in density. The isosurfaces in Figure 1(b,c,f) all depict the density from one outside edge of the object to the central cross-sectional plane shown in (a). Though the entire numerical object is not depicted in the isosurfaces, this visualization helps emphasize and clarify the position and shape of the voids before and after 3DBPP reconstruction. The object is symmetric about the plane in (a).

The numerical probe used for this example was purely real with a gaussian amplitude profile with a full width at half max of 4 pixels. To simulate a high-angle Bragg condition similar to the eSiGe experiment, the incident angle of the probe and the angle of the exit beam ( $\mathbf{k}_i$  and  $\mathbf{k}_f$ ) were both set to  $30^\circ$  with respect to the top surface of the object. In order to generate a simulated data set, the position of the probe was scanned through the object in a  $5 \times 61$  point grid with a two pixel step size. At each point  $j$ , coherent Bragg intensity patterns were calculated according to  $\langle I_j \rangle = |\mathcal{FRP}_j \rho|^2$ . The resulting noise-free intensity patterns were phased using the OS/PIE 3DBPP algorithm described in the text to generate a reconstruction. The support used in the reconstruction (yellow surfaces in Figure 1) consisted of parallel planes separated by 40 pixels, matching the dimension of the original object in the  $z$  direction. This support acted only to constrain the top and bottom surfaces of the object, as in the experimental eSiGe reconstruction. The final reconstruction in Figure 1(g) was generated after 200 iterations of the 3DBPP algorithm. The resolution of this reconstruction along  $\mathbf{k}_f$  was found to be 2.6 pixels, demonstrating sub-beam-size resolution of 3DBPP along the projection direction (see Supplemental).

**Sample preparation:** The sample was a lithographically prepared prototype device [46], consisting of a series of 460-nm wide trenches etched into a silicon-on-insulator (SOI) wafer. The trenches were subsequently filled with epitaxial embedded  $\text{Si}_{0.8}\text{Ge}_{0.2}$  (eSiGe) stressors that were 65 nm thick, as confirmed by transmission electron microscopy. The geometry and mechanical boundary conditions of these epitaxial device components are such that strain gradients are expected to build up near the vertical interface between the eSiGe and SOI channel regions. The device SOI/eSiGe architecture shown in Figure 4(a) repeats for  $> 100$  periods in the  $x$  direction,

and is invariant and self-similar in the  $y$  direction for tens of microns.

**Data collection:** The coherent diffraction measurements were done at the Hard X-ray Nanoprobe beamline [47–49]. A Fresnel zone plate was used to focus 9 keV energy x-rays with wavelength  $\lambda = 0.137$  nm to a 46 nm diameter focal spot (FWHM intensity of the central focus peak). Prior to collecting nanodiffraction patterns from the eSiGe stressors, the complex wavefront of the beam was determined in the focal plane with transmission-geometry Fresnel ptychography using a test object [50], (Figure 3(b-c)). Using wavefront propagation, the wave field of the beam about the focus was calculated in order to determine the 3D probe function in the Bragg geometry. The depth of focus of this zone plate optic was  $\sim 30$   $\mu\text{m}$ , and the focal plane was determined experimentally within  $\pm 5$   $\mu\text{m}$ . Thus, during 3DBPP phase retrieval, we assume that the eSiGe crystal lies in the focus of the lens and that the uncertainty of the focal plane can be neglected due to the long depth of focus. Similarly, we assume that changing the position of the beam along the  $y$  direction by  $< 2$   $\mu\text{m}$  does not significantly modify the probe profile at the sample.

For 3DBPP imaging, coherent nanodiffraction patterns were measured with an area detector at the 004 eSiGe Bragg condition with 10 second exposures. In this symmetric diffraction geometry the incident and exit wave vectors,  $\mathbf{k}_i$  and  $\mathbf{k}_f$ , were separated by  $59.5^\circ$ . The beam was scanned normal to  $\mathbf{k}_i$  in a series of spiral-like patterns with an effective step size of  $\sim 13$  nm separating adjacent points, defining an effective field of view of  $\sim 900 \times 200$  nm on the surface of the device. In total, 707 coherent Bragg diffraction patterns were phased, covering a sample area shown in Figure 3(a). Examples of coherent Bragg diffraction patterns from this data set measured at different positions of a single stressor are shown in Figure 3(d-f). Further details can be found in Ref [40], especially with regard to our implementation of the spiral patterns employed in order to mitigate beam damage.

**Inversion procedure:** In this work, we adapted the OS/PIE (Ordered-Subset / Ptychographic Iterative Engine) algorithm that was originally described in Ref [11] and further investigated in Ref [35]. Our 3DBPP phase-retrieval iteration is a variation of this algorithm that can be implemented by modifying the relationship between the probe, the object, and the sample exit wavefield. Thus, equations 2 and 6 in Ref [11] change from:

$$\psi_j = P_j \rho, \quad \text{and,} \quad \hat{\psi}_j = \mathcal{F}^{-1} \left( \sqrt{I_j} \frac{\Psi_j}{|\Psi_j|} \right), \quad (6)$$

to, respectively:

$$\psi_j = \mathcal{R}P_j\rho, \quad \text{and,} \quad \hat{\psi}_j = \mathcal{R}^\dagger \mathcal{F}^{-1} \left( \sqrt{I_j} \frac{\Psi_j}{|\Psi_j|} \right). \quad (7)$$

(Note that variables in the above equations were slightly changed from those in Rodenburg and Faulkner such that they correspond to the nomenclature of the current manuscript.) As described in the manuscript,  $\mathcal{R}$  and  $\mathcal{R}^\dagger$  are projection and backprojection operators. These operators transform dimensions from 3D to 2D and vice-versa, and they allow a phase retrieval approach originally designed for 2D imaging (such as the PIE) to be adapted for 3D imaging. In addition, a (real-space) support constraint consisting of two parallel planes separated by 90 nm was applied to each new update of  $\rho$  such that amplitude outside the volume between the planes was set to zero. A pseudo-code of the OS/PIE 3DBPP phasing algorithm is given in the Supplemental. The reconstruction from experimental data was obtained with a total of 300 iterations performed by this OS/PIE 3DBPP phasing algorithm, the iteration being started with a 3D estimate  $\rho^{(0)}$  consisting of random real values. The beam wavefront reconstructed from test pattern data (Figure 3(b)) was used to generate a 3D incident focused-beam probe  $P$  that is invariant apart from spatial shifts ( $P_j(\mathbf{r}) = P(\mathbf{r} - \mathbf{r}_j)$  with  $\mathbf{r}_j$  the  $j$ -th probe position). We note also that this probe estimate  $P$  was not further refined during the OS/PIE 3DBPP phase retrieval. The constant step-size parameter  $\beta$  was set to 0.8 during all the OS/PIE iterations [34], but an additional multiplicative scalar factor of the form  $1/\max(|P|^2)$  was used to aid in the convergence of the inversion [35].

**Estimation of the spatial resolution.** In order to estimate the spatial resolution of our experimental 3DBPP reconstruction, we follow a Fourier shell correlation (FSC) approach similar to that outlined by van Heel and Schatz for cryo-TEM tomography [42] and that has recently been utilized for small-angle ptychography [43]. In this approach, the spectra of two independent images of the same object are compared. The correlation of the spectra from the two images as a function of spatial frequency provides a means of estimating image resolution. One variant of FSC used in cryo-TEM requires that the data set be “split” into independent data sets. Both half-data sets are independently reconstructed and compared. Here, we split our data set into even and odd-indexed spiral positions. As shown in Supplemental Figure S6, two half-data sets were created consisting of alternating beam position indices along the spirals.

In 3DBPP reconstructions, spatial resolution varies directionally. To accommodate this, we modify the FSC approach to be sensitive to azimuthal direction. This is done by performing FSC on spatial frequencies filtered by a cylindrical mask that passes through the origin in Fourier space.

Changing the orientation of the cylindrical mask enables the spatial resolution along different azimuthal directions to be estimated. (Details of this analysis are given in the Supplemental.)

The results of our direction-sensitive FSC analysis are shown in Sup. Figure S9, applying a 1/2-bit resolution criterion as in [42, 43]. The resolution was estimated along the  $(r_x, r_z)$ ,  $(r_y, r_z)$ , and  $(r_x, r_y)$  planes through the SiGe reconstruction. The spatial resolution of the reconstruction was found to depend on direction, and is highest along the surface normal of the film. From this analysis, we estimate that along the  $r_x, r_y, r_z$  directions, the spatial resolution is 12, 29, and 35 nm respectively.

**Fourier filtered BEM model:** At an exposure time of 10 seconds, the experimental Bragg coherent diffraction signal from the eSiGe stressors fell below the noise level of the detector at a signal level of  $\sim 0.25\%$  of the maximum observed intensity, below which diffracted signal was not detected. This effectively removed high-frequency components of the diffracted Bragg peak measurement at each position. Because of the finite measured signal, our experimental reconstruction can be thought of as a low-bandpass filtered version of the reconstruction that would have been obtained with noise-free high-dynamic-range data.

In order to compare the results of the linear elastic model with our experimental reconstruction, a comparable low-bandpass filter was utilized. The BEM model, when converted to  $\rho_{BEM}$  for the 004 Bragg condition (Figure 4(d,e)), contains high spatial frequency features (sharp edges, rapidly varying phase ramps) that would not all be detected at the signal level corresponding to our experiment. To represent  $\rho_{BEM}$  in a manner that was consistent with the finite experimental signal, frequency components of the Fourier transform of  $\rho_{BEM}$  that fell below 0.25% of the maximum intensity of the FT were zeroed. The inverse Fourier transform of this quantity yielded  $\rho_{BEM}^{filt}$ , which is an estimate of a 3DBPP reconstruction of the BEM model that is consistent with the signal-to-noise ratio of our experiment. In thresholding to zero at high spatial frequencies, Poisson noise effects were neglected. However, thresholding served as a first-order approximation of the low-bandpass filtering effect of low signal at high  $q$ .

**Data availability** The experimental data that supports the plots within this paper and other findings of this study are hosted at Argonne National Laboratory and can be accessed by contacting the corresponding author.

**Code availability** Matlab routines for implementing 3DBPP image reconstruction from an example numerical data set are available for download by visiting: <http://XXX>



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## **AUTHOR CONTRIBUTIONS**

The 3DBPP method was established by SH, MA and VC following the original idea of SH. Samples were prepared by CM and JH. Experimental measurements were performed by SH, MH, CM, and PF. All authors contributed to the writing of the manuscript.

## **ADDITIONAL INFORMATION**

The authors declare no competing financial interests.