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Effects of radiation in turbulent channel flow: Analysis of coupled direct numerical simulations

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The role of radiative energy transfer on turbulent boundary layers is carefully analyzed, focusing on the effect on temperature fluctuations and turbulent heat flux. The study is based on direct numerical simulations of channel flows with hot and cold walls coupled to a Monte-Carlo method to compute the field of radiative power. In the studied conditions, the structure of the boundary layers is strongly modified by radiation. Temperature fluctuations and turbulent heat flux are reduced, and new radiative terms appear in their respective balance equations. It is shown that they counteract turbulence production terms. These effects are analyzed under different conditions of Reynolds number and wall temperature. It is shown that collapsing of wall-scaled profiles is not efficient when radiation is considered. This drawback is corrected by the introduction of a radiation-based scaling. Finally, the significant impact of radiation on turbulent heat transfer is studied in terms of turbulent Prandtl number. A model for this quantity, based on the new proposed scaling, is developed and validated.

Key words: Direct Numerical Simulation; Turbulence; Radiative transfer; Monte-Carlo simulation; Channel flow; Turbulent heat transfer

1. Introduction

Radiation plays an important role in many industrial applications, particularly in combustion systems such as boilers, gas turbines, rocket engines and furnaces. For instance, in gas turbines, a crucial part of the heat transferred from hot gas to the combustor solid walls comes from radiative energy transfer (Lefebvre & Ballal 2010). The importance of radiation is even higher in modern gas turbines as the pressure ratio increases, which makes the cooling of combustor walls more difficult. Moreover, radiation can influence the temperature distribution and hence the emission of pollutants in combustion systems. Therefore, an accurate prediction of radiation effects is important for the design of combustors.

Among the studies of radiation effects in turbulent flows, much attention has been given to the interaction between turbulence and radiation (TRI). Two aspects of TRI can be identified: the effects of radiation on the temperature and species concentrations

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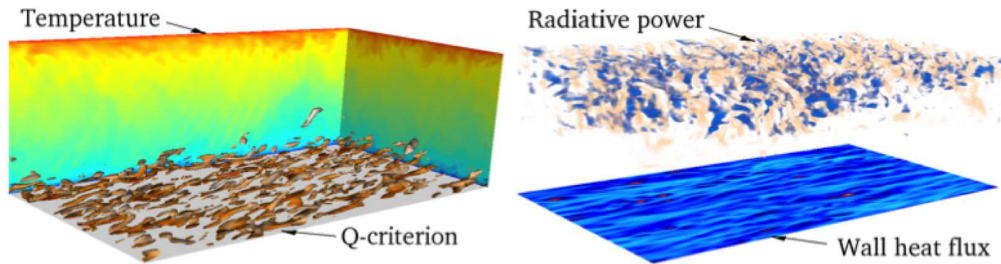


FIGURE 1. Snapshot of temperature (left, slices), turbulent eddies identified by the Q-criterion (left, near bottom wall only), wall heat flux (right, bottom wall only) and radiative power (right, volume rendering near the upper wall only).

turbulent fields and vice-versa. A comprehensive review about TRI can be found in Coelho (2007, 2012).

Regarding the effects of turbulence on radiation, it is observed that turbulence leads to an increase in medium transmissivity (Jeng & Faeth 1984; Gore *et al.* 1987), radiative power (Coelho 2004; Tessé *et al.* 2004) and heat losses (Li & Modest 2003; Tessé *et al.* 2004). Coelho *et al.* (2003) reported that, in a non-luminous turbulent jet diffusion flame, TRI enhanced the heat losses by a factor of 30% while a similar change in a luminous turbulent flame was also revealed by Tessé *et al.* (2004). Moreover, individual contributions to emission and absorption TRI have been isolated and quantified in a 1D premixed combustion system (Wu *et al.* 2005), a homogeneous isotropic non-premixed combustion system (Deshmukh *et al.* 2007) and a 1D turbulent non-premixed flame (Deshmukh *et al.* 2008). In the latter two studies involving coupled direct numerical simulations, the consistency of the radiative transfer solver with the order of spatial discretization error in the DNS solver has been improved by considering a high-order Monte-Carlo method from Wu *et al.* (2007). Gupta *et al.* (2009) have shown that the effects of temperature fluctuations on the mean radiative power in a non-reactive channel flow is negligible, while the presence of a turbulent flame that enhances temperature fluctuations makes TRI important. The prediction of such effects in Reynolds-averaged numerical simulations requires a specific modeling of the mean radiative power (Tessé *et al.* 2004; Haworth 2010). In large-eddy simulations, subgrid turbulence-radiation interactions are often neglected. A couple of studies (Gupta *et al.* 2013; Soucasse *et al.* 2014) have recently studied subfilter modeling of the radiative power.

By contrast to the former, only a few studies have been devoted to the effect of radiation on turbulence. Among them, Soufiani (1991) carried out a theoretical analysis of the influence of radiation on thermal turbulence spectra and it was concluded that radiation acted as a dissipation term and it could smooth the intensity of temperature fluctuations and modify the structure of the temperature variance spectrum. Damien *et al.* (2012) also reported that radiation modifies the level of temperature fluctuations and homogenizes the spectral distribution of energy. Moreover, it was reported that the Reynolds stress and turbulence structure in supersonic shear layers were modified by radiation (Ghosh *et al.* 2011).

The objective of this paper is to investigate the effects of radiation on the boundary layer structure of turbulent channel flows. It has already been reported by Zhang *et al.* (2013a) that radiation can significantly modify the mean temperature profile and consequently, the temperature wall law and the wall conductive heat flux. The different observed effects on the mean temperature profile have been explained by the antagonist behaviors of gas-wall and gas-gas radiative contributions. In the present study, Direct

Numerical Simulations (DNS) from Zhang *et al.* (2013a) of channel flows coupled with a reciprocal Monte Carlo method to deal with radiation are analyzed. The Monte-Carlo method solves the exact radiative transfer equation and accurate spectral radiative properties have been considered to account for strong spectral correlation effects in gases. Thus, regarding the description of the radiative energy transfer, the level of physical fidelity is in line with DNS. An instantaneous snapshot of the solution fields is shown in figure 1. The study focuses here on radiation effects on higher-order statistical moments such as turbulent transport heat flux and enthalpy root-mean-square (RMS). The modification of their respective budget equations is also investigated.

After a detailed description of the studied problem in section 2, effects of radiation are analyzed in a first channel flow configuration in section 3.1. Then, changes of radiation effects with wall temperature difference and bulk Reynolds number are reported in section 3.2 where a new turbulent scaling is proposed. Finally, the results related to the turbulent Prandtl number are given in section 3.3 and a model based on the proposed scaling is derived.

2. Problem description

In order to study accurately the effects of radiation on the structure of turbulent boundary layers, direct numerical simulations of a planar channel flow coupled with a reciprocal Monte-Carlo method for radiation calculations have been considered. The set of governing equations in the fluid is given by

$$\frac{\partial \rho}{\partial t} + \frac{\partial(\rho u_i)}{\partial x_i} = 0, \quad (2.1)$$

$$\frac{\partial(\rho u_i)}{\partial t} + \frac{\partial(\rho u_i u_j)}{\partial x_j} = -\frac{\partial p}{\partial x_i} + \frac{\partial \tau_{ij}}{\partial x_j} + S_i, \quad (2.2)$$

$$\frac{\partial(\rho h)}{\partial t} + \frac{\partial(\rho u_j h)}{\partial x_j} = \frac{\partial p}{\partial t} - \frac{\partial q_j^{cd}}{\partial x_j} + P^R \quad (2.3)$$

$$p = \rho r T, \quad (2.4)$$

where ρ , u_i , h , p and T are the fluid mass density, velocity components, enthalpy per mass units, pressure and temperature, respectively. h is expressed from the mixture thermal capacity at constant pressure c_p : $h = \Delta h_0 + \int_{T_0}^T c_p(T') dT'$, where T_0 is a reference temperature and Δh_0 the corresponding standard formation enthalpy. The viscous shear stress tensor τ_{ij} and the conductive flux vector q_i^{cd} are

$$\tau_{ij} = \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) - \frac{2}{3} \mu \left(\frac{\partial u_k}{\partial x_k} \right) \delta_{ij}, \quad (2.5)$$

$$q_i^{cd} = -\lambda \frac{\partial T}{\partial x_i}, \quad (2.6)$$

where μ is the dynamic viscosity, function of temperature computed like the mixture thermal capacity c_p by the CHEMKIN package (Kee *et al.* 1986, 1989). The thermal conductivity λ is computed from the Prandtl number $Pr=0.71$. P^R is the radiative power per unit volume. S_i is a uniform forcing source term which acts as a pressure gradient term and drives the channel flow to obtain the desired bulk Reynolds number Re_b .

The set of governing equations is solved with the finite-volume solver YALES2 (Moureau *et al.* 2011a,b) under a low Mach-number approximation. As detailed in Zhang *et al.*

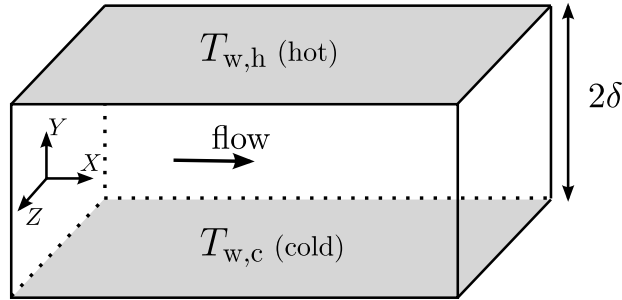


FIGURE 2. Computational domain of channel flow of half-width $\delta = 0.1$ m. The lower wall (resp. upper wall) is at temperature $T_{w,c}$ (resp. $T_{w,h}$; $T_{w,h} \geq T_{w,c}$).

| Case | Re_b | $T_{w,c}$ [K] | $T_{w,h}$ [K] | p [atm] |
|------|--------|---------------|---------------|-----------|
| A | 5 850 | 950 | 1 150 | 40.0 |
| B | 5 850 | 950 | 2 050 | 40.0 |
| C | 11 750 | 950 | 1 150 | 40.0 |

TABLE 1. Channel flow parameters: Bulk Reynolds number Re_b , wall temperatures and pressure.

(2013a), the numerical setup is composed of a centered fourth-order spatial discretization and a fourth-order time integration. The exact radiative transfer equation is solved with a Monte-Carlo method. The computation of the radiative power is here handled by an Optimized Emission-based Reciprocity Monte-carlo method (OERM) (Zhang *et al.* 2013a) where the statistical error on the radiative power is set to remain below 3% of the radiative power maximum value. In the radiative transfer solver, each grid cell is assumed isothermal. Spectral correlation effects in gases are very strong and it is outlined that the gray gas assumption is a myth, see Edwards (1976). In principle, the most accurate approach is a line-by-line model associated with a high-resolution and accurate spectroscopy database. Even with a Monte-Carlo method, such an approach cannot be carried out for unsteady coupled 3D simulations. To our knowledge, the today most accurate practical approach is the CK method based on accurate parameters directly issued from a high-resolution database (Taine & Soufiani 1999). In our case, the high resolution computations account for special effects of pressure on the spectral line wings that are not anymore lorentzian, and of line couplings (Perrin & Hartmann 1989). At high pressure, the weak absorption limit of the CK approach is accurate and also account for the aforementioned effect. This latter spectral description of gases properties has been retained here.

The studied configuration, a fully developed turbulent channel flow with two isothermal walls, is shown in figure 2. The computational domain is $2\pi\delta \times 2\delta \times \pi\delta$ where $\delta = 0.1$ m. Periodic boundary conditions are applied along X and Z directions. For radiation simulations, if a shot exits the domain, for instance, at the point (L_X, Y, Z) , it will then enter at the point $(0, Y, Z)$ with the same propagation direction. The medium is a non-reacting $\text{CO}_2\text{-H}_2\text{O-N}_2$ gas mixture characterized by the respective molar fractions 0.116-0.155-0.729.

Three computational cases from Zhang *et al.* (2013a) (cases C1, C3 and C4), called here A, B and C, are defined in table 1 by a set of bulk Reynolds number, pressure and wall temperatures ($T_{w,c}$ and $T_{w,h}$). Only high pressure cases are considered to enhance

radiative energy transfer. The three investigated cases A, B and C are characterized by a global medium Hotell's transmissivity at 1000 K of 0.271, which indicates a large optical thickness of the medium. In optically thinner cases such as atmospheric conditions, the radiative effects on the mean temperature profile has been observed to be similar to the ones at high pressure but smaller in magnitude (Zhang *et al.* 2013a). In case C, a wall temperature over 2000 K does not correspond to any practical combustion systems but the purpose is to have high temperature burnt gases away from the cold wall as found in combustors with large heat loads. The bulk Reynolds number Re_b is defined by

$$Re_b = \frac{\rho_b u_b \delta}{\mu_b} \quad \text{with} \quad \rho_b = \frac{\int_{-\delta}^{\delta} \bar{\rho} dY}{2\delta}, \quad u_b = \frac{\int_{-\delta}^{\delta} \bar{\rho} u dY}{\int_{-\delta}^{\delta} \bar{\rho} dY}, \quad \mu_b = \mu(T_b), \quad (2.7)$$

where T_b is the bulk temperature defined from the bulk enthalpy:

$$h(T_b) = \frac{\int_{-\delta}^{\delta} \bar{\rho} u h dY}{\int_{-\delta}^{\delta} \bar{\rho} u dY}. \quad (2.8)$$

Discretization details for each case are given in table 2. Cell sizes ΔX and ΔZ in the streamwise and spanwise directions are uniform, while the cell length ΔY is refined close to the walls. Non-dimensional cell sizes in table 2 are expressed in wall units from the wall mean density, viscosity and the friction velocity similarly to equation (3.2). When radiation is considered, these cases are referred as A_R, B_R and C_R, respectively and the emissivity ε of the opaque walls is set to 0.8. Cases with radiation A_R, B_R and C_R correspond to cases C1R1, C3R1 and C4R1 from Zhang *et al.* (2013a), respectively. These coupled direct numerical simulations with radiative energy transfer are five to ten times more expensive computationally than DNS without radiation. Because of the large computational cost of the radiation solver, the grid used for the radiation model is three times coarser in X direction and twice in Y and Z directions than the corresponding grid of the flow field. For the same reason, the radiative source term in the energy equation is updated every three time steps of the fluid solver. Such considerations can have an impact on the accuracy of the simulated turbulence-radiation interaction. Since the numerically well-resolved larger turbulent scales are mainly involved in this interaction, the impact of the present grid coarsening and update frequency of the radiative power is expected to be small. Besides, the variations of radiative power are located in the vicinity of the walls where the grid (the coarse one included) is refined. In order to carefully assess this effect, the radiative power was computed for a couple of instantaneous solutions on the fine grid with a stricter threshold on the statistical error to provide reference solutions. On instantaneous fields, small differences in the radiative power with the coarse grid results and default threshold are noticeable. However, as proper comparisons of turbulent fields requires statistical averages, the solutions have been averaged in homogeneous directions X and Z. It was finally verified that the single-point statistical first and second-order moments that involve the radiative power and that are here presented are not sensitive to the grid coarsening.

Without additional care, the Reynolds numbers differ between simulations with or without radiation. The source term in the momentum equation is adapted in order to keep the same bulk Reynolds number in both configurations. The friction Reynolds number based on the friction velocity in the channel boundary layers is nonetheless slightly different with or without radiation. Values have been reported in Zhang *et al.* (2013a). However, at least one characteristic of the flow, here chosen as the bulk Reynolds number, is consistent across simulations.

| Case | $n_X \times n_Y \times n_Z$ | ΔX^+ | ΔY^+ | ΔZ^+ |
|------|-----------------------------|--------------|--------------|--------------|
| | | hot/cold | | hot/cold |
| A | $110 \times 135 \times 110$ | 16.9/21.3 | [0.8—8.0] | 8.4/10.6 |
| B | $160 \times 163 \times 160$ | 8.9/22.4 | [0.8—8.0] | 4.4/11.2 |
| C | $200 \times 230 \times 200$ | 17.3/21.8 | [0.8—8.0] | 8.6/10.8 |

TABLE 2. Discretization of the simulated cases: n_X , respectively n_Y and n_Z , is the number of points in the X direction, respectively Y and Z direction. ΔX^+ and ΔZ^+ are given at the cold and hot sides for cases A, B and C without radiation.

3. Results

3.1. Results for reference cases A and A_R

Results are first presented for cases A and A_R. The effects of radiation on the boundary layer structure are analyzed in terms of the effects on the mean temperature field, on the enthalpy fluctuations and on the turbulent transport heat flux. Then, influence of temperature fluctuations on the radiative power is studied. In the following, $\bar{\phi}$ and $\tilde{\phi}$ denote Reynolds and Favre averages for any variable ϕ , respectively, while ϕ' and ϕ'' denote their respective fluctuating parts.

3.1.1. Mean temperature field

Owing to the small variation of mass density in the present conditions, mean velocity profiles (not presented here) are not affected by radiation when comparing cases A and A_R that are both characterized by a small wall temperature difference. However, the mean temperature profile, shown in figure 3 (a), is significantly modified by radiation over the whole domain. The mean temperature in wall units \bar{T}^+ is defined as,

$$\bar{T}^+ = \frac{|\bar{T} - T_w|}{T_\tau} \quad \text{with} \quad T_\tau = \frac{|\overline{q_w^{cd}}|}{\overline{\rho_w} \overline{c_{p_w}} u_\tau}, \quad u_\tau = \left(\frac{\overline{\tau_w}}{\overline{\rho_w}} \right)^{1/2}, \quad (3.1)$$

where $\overline{q_w^{cd}}$, $\overline{\rho_w}$, $\overline{c_{p_w}}$ and $\overline{\tau_w}$ are the mean conductive heat flux, mass density, thermal capacity and shear stress at the wall, respectively. The \bar{T}^+ profiles of cases A and A_R are plotted in figure 3 (b) as functions of the normalized wall distance y^+ that is given by,

$$y^+ = \frac{\overline{\rho_w} y u_\tau}{\overline{\mu_w}}, \quad (3.2)$$

where $\overline{\mu_w}$ is the mean dynamic viscosity at the wall. The obtained temperature wall law for case A_R strongly deviates from that of case A, showing a significant effect of radiation on the thermal boundary layer structure in the considered conditions. A detailed analysis of such radiation effects on the mean temperature field in different channel flow conditions has been realized (Zhang *et al.* 2013a). Opposite effects of radiation on the wall conductive heat flux and on the temperature wall law have been observed and they have been explained by the antagonist behaviors of gas-gas and gas-wall radiative contributions.

3.1.2. Fluctuations of enthalpy

Profiles of the enthalpy root-mean-square, $h_{\text{rms}} = \left(\widetilde{h'' h''} \right)^{1/2}$, in cases A and A_R are shown in figure 4 (a), where h_{rms} is scaled by the arithmetic mean of the wall temperatures

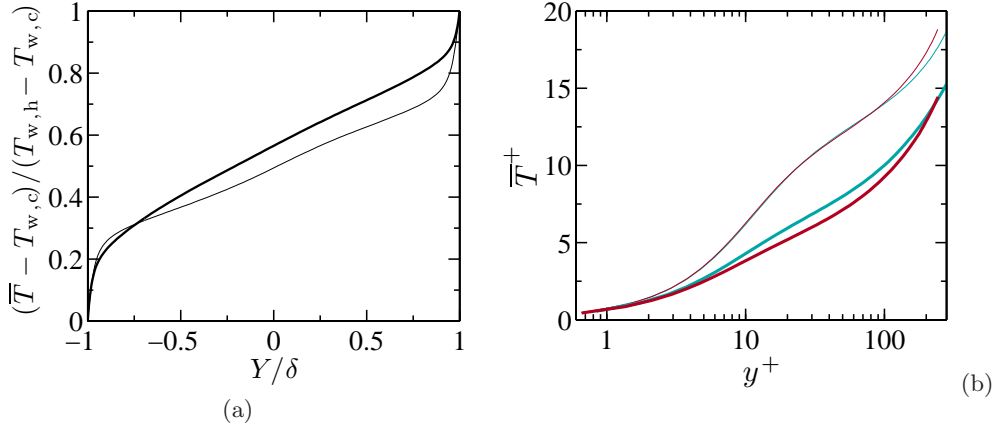


FIGURE 3. Profiles of mean temperature scaled by wall temperatures (a) and in wall units (b) on the cold side (blue color) and hot side (red color) in cases A (thin line) and A_R (thick line).

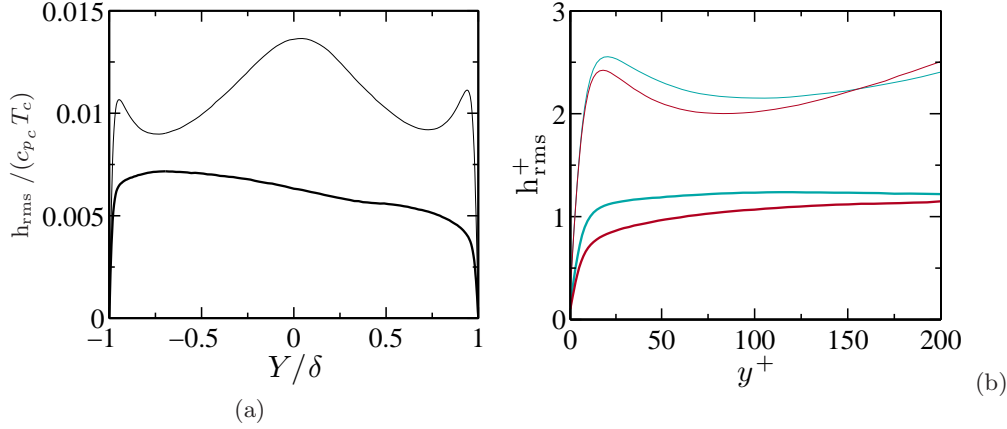


FIGURE 4. Profiles of enthalpy root-mean-square scaled by center temperature T_c and thermal capacity $c_{p,c}$ (a) and in wall units (b) on the cold side (blue color) and hot side (red color) in cases A (thin line) and A_R (thick line).

$T_c = (T_{w,c} + T_{w,h})/2$ and the arithmetic mean thermal capacity $c_{p,c}$, defined as the mean between the thermal capacities at the walls. In case A, without radiation, peaks of variance are located in the near wall regions as expected from standard boundary layer theory where production of turbulent fluctuations is maximal within the buffer layer. Because of the specific configuration where wall temperatures are different, a larger peak in h_{rms} appears in the core of the channel where, as explained by Debusschere & Rutland (2004), fluid pockets of high and low temperature converge from the hot and cold walls, respectively. In case A_R where radiation is accounted for, a significant reduction in enthalpy fluctuations is observed in the near wall region, especially on the hot side, and the central peak vanishes.

One effect of radiation on the absolute value of h_{rms} is the change in the mean wall conductive heat flux due to the modified mean temperature profile. Most of this effect can be filtered out by rescaling profiles with the friction temperature. The obtained wall-scaled profiles of enthalpy rms against y^+ are presented in figure 4 (b), where the

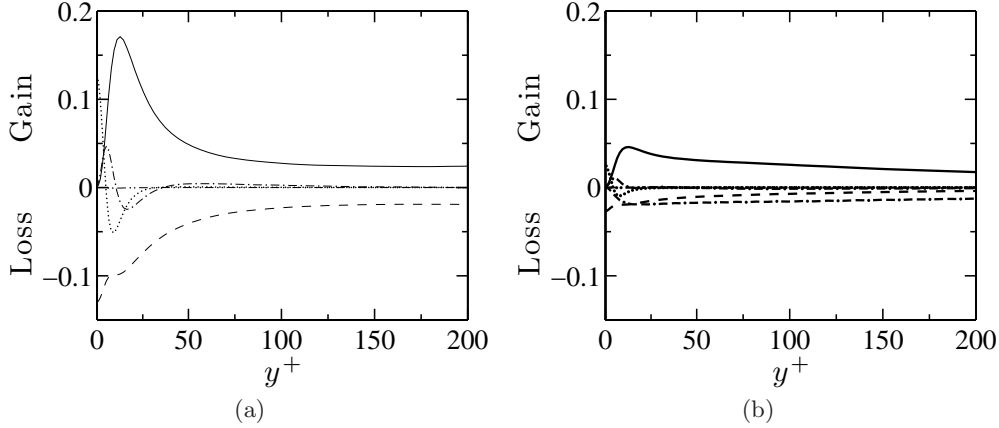


FIGURE 5. Budget of enthalpy variance (cold side only) in cases A (a) and A_R (b): Production (plain line); Molecular dissipation (dashed line); Radiative dissipation (dashed-dashed-dotted line); Turbulent diffusion (dashed-dotted line); Molecular diffusion (dotted line); Density-enthalpy correlation term (dashed-dotted-dotted line).

non-dimensional enthalpy rms h_{rms}^+ is defined as

$$h_{\text{rms}}^+ = \frac{h_{\text{rms}}}{c_{p_w} T_\tau}. \quad (3.3)$$

In spite of the wall scaling formulation, a large difference between results of cases A and A_R remains, indicating that the strong effect of radiation on fluctuations of enthalpy and temperature is a real modification of the boundary layer structure.

This point is further investigated by analyzing the balance of the enthalpy variance transport equation (see Appendix A) which, in the studied configuration, is

$$\underbrace{-\frac{\partial}{\partial y}(\overline{q_y^{cd} h'})}_{\text{I}} - \underbrace{\frac{1}{2} \frac{\partial}{\partial y}(\overline{\rho v'' h'' h''})}_{\text{II}} - \underbrace{\overline{\rho v'' h''} \frac{\partial \tilde{h}}{\partial y}}_{\text{III}} + \underbrace{q_i^{cd'} \frac{\partial h'}{\partial x_i}}_{\text{IV}} + \underbrace{h'' \overline{P R'}}_{\text{V}} + \underbrace{h'' \frac{\partial}{\partial y}(\overline{\rho v'' h''})}_{\text{VI}} = 0 \quad (3.4)$$

where the terms on the left hand side are molecular diffusion (I), turbulent diffusion (II), production (III), molecular dissipation (IV), correlation between enthalpy and radiative power fluctuations (V) and a term (VI) proportional to $\overline{h''} = -\frac{\rho' h'}{\rho}$ related to enthalpy-density correlation. For any quantities ψ and ϕ , cross-correlations between Favre and Reynolds fluctuations have the following properties: $\overline{\phi' \psi''} = \overline{\phi' \psi'}$ and $\overline{\phi'' \psi''} = \overline{\phi'' \psi''}$. Therefore, the correlation term between enthalpy and radiative power fluctuations can also be written as $\overline{h' P R'}$.

The different terms in equation (3.4) are scaled in wall units by $q_w^{cd^2} / \mu_w$ and compared in figure 5 (a) and (b) for cases A and A_R (only the results on the cold side are shown since they are similar on the hot side). On the one hand, in case A, production and molecular dissipation terms are dominant and decrease away from the wall as expected in such standard conditions. On the other hand, in case A_R, a third dominant term appears in the balance of enthalpy variance in addition to the latter two, that is the enthalpy-radiative-power correlation. Since this term appears as a negative contribution to the budget, it will be referred as radiative dissipation in the following. Hence, equilibrium between production and molecular dissipation away from the buffer layer for $y^+ > 30$ is replaced by a balance of production with molecular and radiative dissipations in the case with radiation. In the studied case, this equilibrium takes place sooner for $y^+ >$

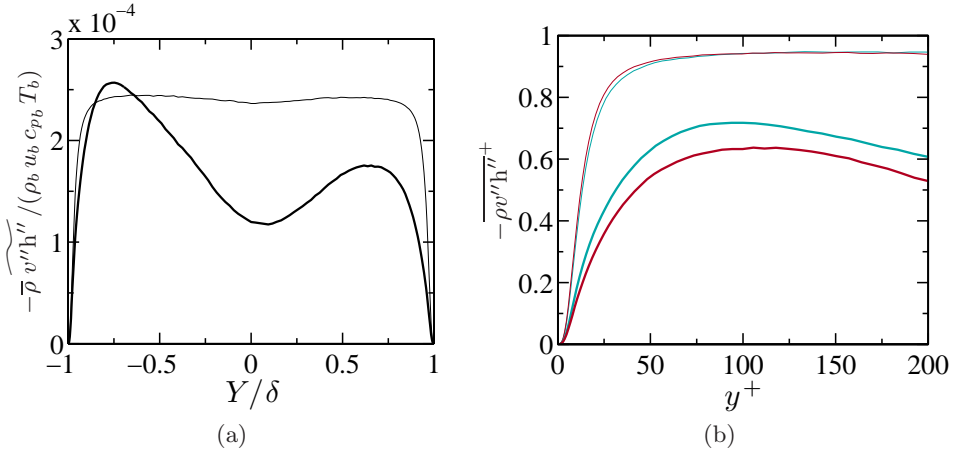


FIGURE 6. Profiles of wall-normal turbulent heat flux scaled by bulk variables (a) and in wall-units (b) on the cold side (blue color) and hot side (red color) in cases A (thin line) and A_R (thick line).

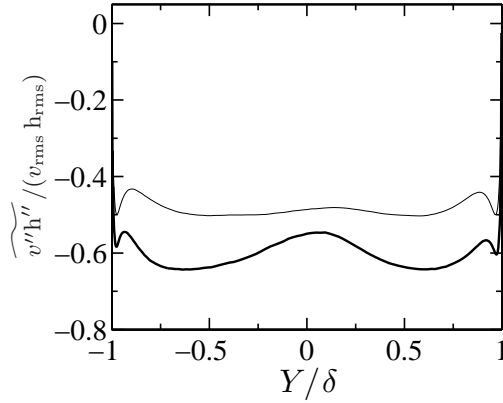


FIGURE 7. Profiles of correlation between enthalpy and wall-normal velocity fluctuations in cases A (thin line) and A_R (thick line).

20 and molecular dissipation remains weaker than radiative dissipation for $y^+ > 50$ approximatively.

For both cases A and A_R, the term related to $\overline{h''}$, mean of mass-weighted fluctuating enthalpy, is negligible because of the small density variations. Regarding the scaled production, it is reduced in case A_R because of the modification by radiation of the mean temperature field and of the turbulent heat flux (shown later). This decrease in production and the presence of an additional radiation-related dissipative term in the budget of enthalpy variance explain the smaller level of enthalpy fluctuations shown in figure 4 for the case with radiation.

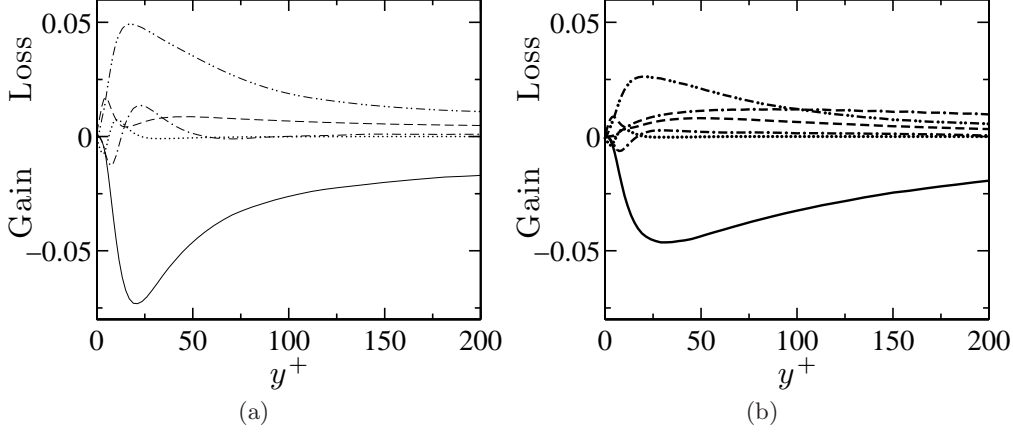


FIGURE 8. Budget of wall-normal turbulent heat flux (cold side only) in cases A (a) and A_R (b): Production (plain line); Molecular diffusion (dotted line); Turbulent diffusion (dashed-dotted line); Enthalpy-pressure-gradient correlation (dashed-dotted-dotted line); Molecular dissipation (dashed line); Velocity-Radiative power correlation term (dashed-dashed-dotted line).

3.1.3. Wall-normal turbulent heat flux

Profiles of wall-normal turbulent heat flux $\overline{\rho v'' h''}$ in cases A and A_R are presented in figure 6, where the wall-scaled turbulent heat flux is defined as

$$\overline{\rho v'' h''}^+ = \frac{\overline{\rho v'' h''}}{\overline{\rho_w} u_\tau c_{p_w} T_\tau} = \frac{\overline{\rho v'' h''}}{|q_w^{cd}|}. \quad (3.5)$$

The scaled wall-normal turbulent heat flux decreases when radiation is accounted for. The aforementioned reduction in enthalpy fluctuations due to radiation is a first explanation why the turbulent transfer is less efficient. This effect can be filtered out by looking at the correlation coefficient between enthalpy and wall-normal velocity fluctuations shown in figure 7. The resulting profile for case A_R is symmetrical, which shows that the asymmetry observed in figure 6 (a) for the case with radiation comes from the asymmetry of h_{rms} between the hot and cold walls (figure 4). The correlation between enthalpy and wall-normal velocity fluctuations is nonetheless stronger when radiation is accounted for. Other sources of disagreement between the two cases A and A_R than just the change in enthalpy rms are therefore at work.

One of these sources is the requirement for the turbulent heat flux to fulfill the mean balance equation of energy that is given by,

$$-\frac{\partial}{\partial y} \left(\overline{q_y^{cd}} + \overline{\rho v'' h''} \right) + \overline{PR} = 0. \quad (3.6)$$

Introducing the radiative flux vector q_i^R , the mean energy balance equation becomes a constant sum of energy fluxes,

$$\overline{q_y^{cd}} + \overline{\rho v'' h''} + \overline{q_y^R} = \overline{q_w^{cd}} + \overline{q_w^R}, \quad (3.7)$$

where $\overline{q_w^{cd}}$ and $\overline{q_w^R}$ are the wall conductive heat flux and wall radiative flux, respectively. Hence, the turbulent heat flux is constrained by conductive and radiative fluxes, establishing a strong two-way coupling of the radiative power field with the mean and the fluctuations of the temperature field.

The balance equation of the turbulent heat flux $\overline{\rho v'' h''}$ (see Appendix A) is

$$\begin{aligned} \underbrace{\frac{\partial}{\partial y} \left(\overline{\tau'_{22} h'} - \overline{q_y^{cd'} v'} \right)}_{\text{I}} & - \underbrace{\frac{\partial}{\partial y} \left(\overline{\rho v'' v'' h''} \right)}_{\text{II}} & - \underbrace{\overline{\rho v'' v''} \frac{\partial \overline{h}}{\partial y}}_{\text{III}} & - \underbrace{\left(\overline{\tau'_{2i} \frac{\partial h'}{\partial x_i}} - \overline{q_i^{cd'} \frac{\partial v'}{\partial x_i}} \right)}_{\text{IV}} \\ & + \underbrace{\overline{v'' P R'}}_{\text{V}} & - \underbrace{\overline{h' \frac{\partial p'}{\partial y}}}_{\text{VI}} & + \underbrace{\left(\overline{h'' \frac{\partial}{\partial y} \left(\overline{\rho v'' v''} \right)} + \overline{v'' \frac{\partial}{\partial y} \left(\overline{\rho v'' h''} \right)} \right)}_{\text{VII}} = 0. \end{aligned} \quad (3.8)$$

The seven terms on the left hand side are molecular diffusion (I), turbulent diffusion (II), production (III), molecular dissipation (IV), correlation between wall-normal velocity and radiative power fluctuations (V), enthalpy-pressure-gradient correlation (VI: EPG) and a term (VII) related to the average of Favre fluctuations of enthalpy and velocity. These terms, except for the last one which is again negligible, are shown for cases A and A_R in figure 8 where they are scaled by $|\overline{q_w^{cd'}}| \overline{\tau_w} / \overline{\mu_w}$. In case A, the predominant terms are the production and the EPG terms. Away from the wall, molecular dissipation accounts for the remaining balance. The enthalpy-pressure-gradient correlation can be split into two terms, a pressure-enthalpy-gradient correlation and a pressure-diffusion term:

$$-\overline{h' \frac{\partial p'}{\partial y}} = \overline{p' \frac{\partial h'}{\partial y}} - \overline{\frac{\partial p' h'}{\partial y}} \quad (3.9)$$

As shown by Kasagi *et al.* (1992), these two terms are of the same order of magnitude with opposite signs (not presented here). When radiation is taken into account, most of the terms are reduced in magnitude and broader. For $y^+ > 25$, the balance is split into production, the EPG term, the wall-normal velocity-radiative power correlation term and molecular dissipation which has the smallest contribution among these four terms. The EPG term is the largest loss term for $y^+ < 100$ until the velocity-radiative power correlation term takes over.

At large Reynolds number, the molecular dissipation in the balance equation of the turbulent heat flux becomes negligible away from the wall (Pope 2000). Extrapolating the present results to flows with a larger Reynolds number, two different types of behaviors can be expected away from the wall: i) When radiation is negligible or moderate, production of turbulent heat flux is equilibrated with the EPG contribution only; ii) When radiation is intense, a second region appears further away from the wall where production is equilibrated with the wall-normal velocity-radiative power correlation term only. For stronger and stronger radiative effects, the area where the radiative term becomes dominant gets closer and closer to the wall.

3.1.4. Radiative power field

The mean profile of the radiative power is shown in figure 9 (a). It is positive (resp. negative) in the very near wall region on the cold side (resp. hot side). Further away from the wall, the radiative power changes sign twice around $y^+ = 20$ and 100 on both sides. This shape of the mean radiative power has been explained by the different behaviors of gas-gas and gas-wall contributions to radiation (Zhang *et al.* 2013a).

One of the most studied aspects of turbulence-radiation interaction is the effect of turbulent fluctuations on the mean radiative power (Coelho 2012). Indeed, the mean

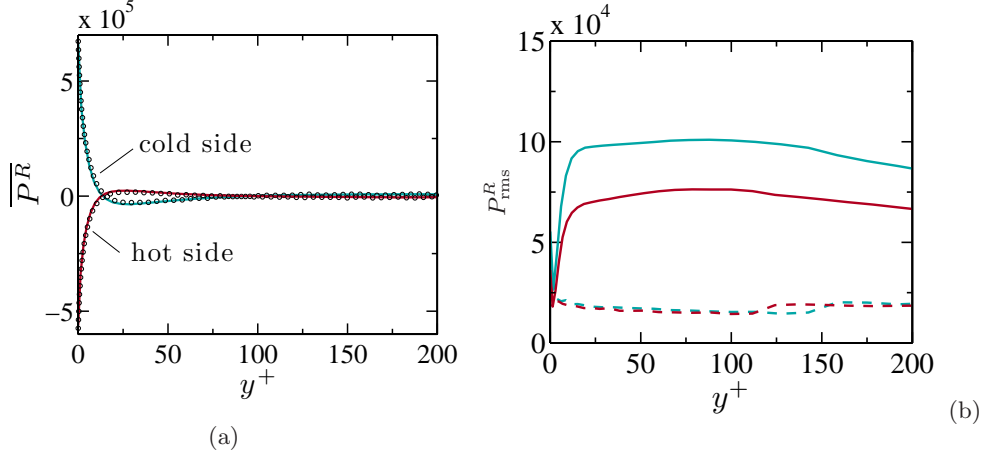


FIGURE 9. Profiles of mean radiative power $\overline{P^R}$ (a) and root-mean-square P_{rms}^R (b) in $\text{J}\cdot\text{m}^{-3}$ in case A_R on the cold side (blue color) and hot side (red color). (a) Circles : radiative power computed from the mean temperature field. (b) Plain lines: physical rms; Dashed lines: stochastic error.

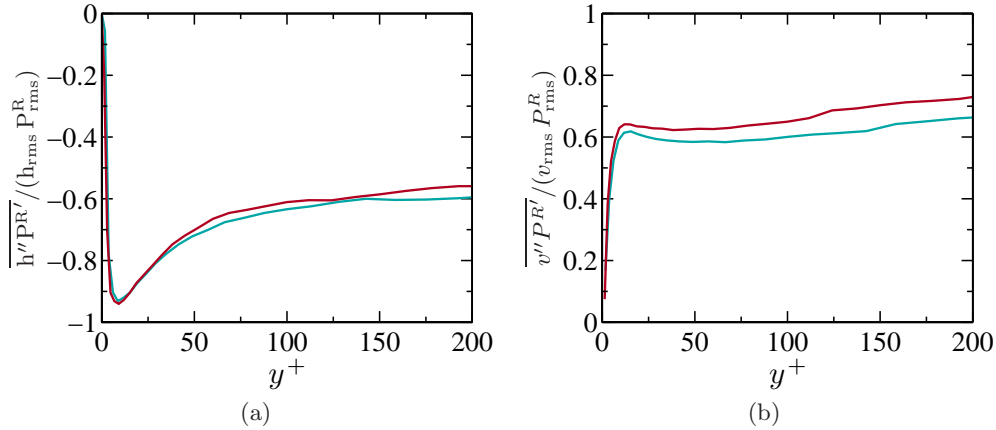


FIGURE 10. Correlation coefficients between radiative power and enthalpy (a) and between radiative power and wall-normal velocity (b) in case A_R on the cold side (blue color) and hot side (red color).

radiative power is given by

$$\overline{P^R} = \overline{P_a^R} - \overline{P_e^R} = \int_0^{+\infty} \left(\underbrace{\int_{4\pi} \overline{\kappa_\nu I_\nu} d\Omega}_{\text{Absorption}} - \underbrace{4\pi \overline{\kappa_\nu I_\nu^\circ(T)}}_{\text{Emission}} \right) d\nu, \quad (3.10)$$

where the spectral intensity I_ν , the equilibrium spectral intensity I_ν° and the spectral absorption coefficient κ_ν are integrated over frequency ν and solid angle Ω ranges. While I_ν° depends on the local temperature and κ_ν on the local state (composition, pressure and temperature), the spectral intensity I_ν at a given point is determined by the whole three-dimensional and instantaneous fields of temperature, pressure and composition. This latter property of the spectral intensity has led to numerous studies on the effects of turbulent fluctuations on the mean radiative power (Coelho 2007, 2012) since the mean radiative power cannot be computed from the mean fields of temperature, pressure

and composition as they do not correspond to any instantaneous realization of the flow. In the present study, channel flows with homogenous composition and thermodynamic pressure are considered. Therefore, only the temperature field determines the radiative fields and $\overline{P^R}$ cannot be computed in the general case from the three-dimensional field of mean temperature $\{\overline{T}\}$, *i.e.*

$$\overline{P^R(\{T\})} \neq P^R(\{\overline{T}\}). \quad (3.11)$$

To investigate this effect in the present case, the radiative power computed from the mean temperature field is also shown in figure 9 (a). No difference appears with the exact profile on both sides, where emission is dominant in the near-wall region of the hot wall, while absorption is dominant close to the cold wall. Consequently, turbulent fluctuations of temperature are not intense enough in the present boundary layer case to perturb the mean emitted and absorbed radiative power. This was also reported by Gupta *et al.* (2009) for non-reactive large-eddy simulation of channel flow. Due to the complexity of the absorption contribution, most studies in Turbulence-Radiation Interaction (TRI) focus on the effect of turbulent fluctuations on the emitted radiative power. Introducing the Planck mean absorption coefficient κ_P and neglecting high order correlation, the mean emitted radiative power is (Coelho 2007):

$$\overline{P_e^R} = 4\pi \int_0^{+\infty} \kappa_\nu I_\nu^0(T) d\nu = \overline{4\sigma\kappa_P T^4} = \underbrace{4\sigma\overline{T^4}}_{=P_e^R(\overline{T})} \left(1 + 6\frac{\overline{T'^2}}{\overline{T}^2} + 4\frac{\overline{\kappa_P' T'}}{\overline{\kappa_P T}} + \dots \right), \quad (3.12)$$

where σ is the Stefan-Boltzmann constant. In the present study with homogenous composition and pressure, the Planck mean absorption coefficient only depends on temperature. As fluctuations of temperature in turbulent boundary layers remain moderate (see Appendix B), $\kappa_P(T) \approx \kappa_P(\overline{T}) + \alpha T'$ can be linearized around the mean temperature \overline{T} , and the relative variation in the Planck mean absorption coefficient is given by

$$\frac{\kappa_P(T) - \kappa_P(\overline{T})}{\kappa_P(\overline{T})} = \beta \frac{T'}{\overline{T}}, \quad (3.13)$$

with $\beta = \alpha\overline{T}/\kappa_P(\overline{T})$. Finally, the effect of temperature fluctuations on the mean emitted power, quantified as the relative difference between $\overline{P_e^R}$ and $P_e^R(\overline{T})$, is

$$\frac{\overline{P_e^R} - P_e^R(\overline{T})}{P_e^R(\overline{T})} = \underbrace{(6 + 4\beta)}_\gamma \frac{\overline{T'^2}}{\overline{T}^2}. \quad (3.14)$$

For fluctuating level of temperature $T^{\text{rms}}/\overline{T}$ larger than $1/\gamma$, X% of temperature fluctuations results in TRI effects on the mean emitted radiative power larger than X%, and reciprocally. Dependency of the Planck mean absorption coefficient with temperature for H₂O and CO₂ are given by Rivière & Soufiani (2012), which shows that the introduced proportionality coefficient β varies between -1 (resp. 0.5) at 500 K and -2.3 (resp. -2.5) at 2500 K for H₂O (resp. CO₂). Hence, for various composition of exhaust gases, β ranges between -2.5 and 0.5 , yielding $|\gamma|$ within the range $4 - 8$. Consequently, the threshold between amplification and diminution of TRI effects on $\overline{P_e^R}$ corresponds to approximately $12 - 25\%$ of fluctuations in temperature. In the present case, maximum temperature fluctuations reach roughly 1% in cases A and C, and 5% in case B. When radiation is considered, these fluctuations are even lower as explained previously. With such levels of turbulent fluctuations in equation (3.14), the emitted radiative power is not affected and can be computed from the average field of temperature.

Understanding and quantifying when turbulent fluctuations affect the mean absorbed radiative power is a much more complex task and is out of the scope of the present study. Nonetheless, for all cases studied here (A_R, B_R and C_R), no effects of temperature fluctuations in the mean radiative power have been observed, including on the cold side where radiative absorption phenomena are dominant in the boundary buffer layer (see figure 9 (a)).

It is demonstrated in Appendix B that, in gaseous flows, the level of temperature fluctuations in turbulent boundary layers can be larger than the one observed in the studied cases for strongly heating or cooling systems but it does not exceed 30% and it decreases with Reynolds number. Moreover, coupling with radiation makes these temperature fluctuations smaller. Therefore, the absence of effects of temperature fluctuations on the mean radiative power is not necessarily limited to the present conditions and concerns a wide range of turbulent boundary layer conditions. In fact, much stronger interactions between turbulence and radiation are observed in combustion applications (Coelho 2012) where the heat release stemming from chemical reactions greatly enhances temperature fluctuations.

Although the mean radiative power is not influenced by temperature fluctuations in the present case, fluctuations of the radiative power field modify the balance in transport equations of enthalpy variance and turbulent heat flux, equations (3.4) and (3.8), and hence interact with the mean temperature field indirectly. In order to compute the relevant radiative power root-mean-square P_{rms}^R , it is necessary to subtract the standard error of the Monte-Carlo method from the total rms data. This specific treatment is only required for P_{rms}^R . Indeed, since the Monte-Carlo method is a stochastic approach, the computed time-averaged variance of radiative power is

$$\overline{P^{R^2}} = \overline{P_{\text{phys}}^{R^2}} + \overline{P_{\text{err}}^{R^2}} + 2\overline{P_{\text{phys}}^R P_{\text{err}}^R}, \quad (3.15)$$

where the instantaneous radiative power $P^R = P_{\text{phys}}^R + P_{\text{err}}^R$ is composed of the real physical value of radiative power, P_{phys}^R , that is estimated by the Monte-Carlo method with a controlled error, and of a stochastic error P_{err}^R . Assuming independency, between physical and stochastic fluctuations, the root-mean-square of radiative power is computed as

$$(P_{\text{rms}}^R)^2 = \overline{P_{\text{phys}}^{R^2}} = \overline{P^{R^2}} - \overline{P_{\text{err}}^{R^2}}, \quad (3.16)$$

using the statistical estimation of $\overline{P_{\text{err}}^{R^2}}$ provided by the Monte-Carlo approach. The profiles of radiative power root-mean-square P_{rms}^R and of the stochastic error $(\overline{P_{\text{err}}^{R^2}})^{1/2}$ are plotted in figure 9 (b). It has been verified by performing Monte-Carlo simulation on one snapshot with a higher accuracy and by averaging in homogeneous directions that profiles of averaged physical quantities are not modified. The chosen accuracy for coupled simulations is therefore good enough and a specific treatment is only necessary to extract the physical rms of radiative power. Contrary to the mean radiative power that abruptly vanishes away from the walls, fluctuations of radiative power do not disappear and their magnitude presents only slight variations for $y^+ > 20$.

As shown previously, the fluctuating radiative power introduces a new *radiative dissipation* term in equation (3.4) that is written as $\overline{h'' P^R}$. Since radiative power is the difference between absorbed and emitted powers, $P^R = P_a^R - P_e^R$, the radiative dissipation term is also composed of two terms:

$$\overline{h'' P^R} = \overline{h'' P_a^R} - \overline{h'' P_e^R}. \quad (3.17)$$

As explained by Ammouri *et al.* (1994), positive (resp. negative) fluctuations of enthalpy

yields a larger (resp. smaller) emitted radiative power. Therefore, radiative emission always leads to a negative contribution to the total radiative dissipation term. On the other hand, the absorbed part is mainly positive. The radiative dissipation could then be positive in some conditions. However, the corresponding correlation coefficient between enthalpy and radiative power shown in figure 10 (a) is negative and indicates that fluctuations of radiative power are fairly anti-correlated with local fluctuations of enthalpy or temperature, especially close to the wall. The radiative dissipation is then here dominated by its emission part.

In the balance equation (3.8) of the turbulent heat flux, the term $\overline{v''P^{R'}}$ related to the correlation coefficient shown in figure 10 (b) appears when radiation is taken into account. In the present case, this term is positive in the whole computational domain although there is no reason to generalize this result. It is worth noticing, by introducing the radiative energy flux, that this term can be split into two terms as done for the conductive heat flux in equation (3.8):

$$\overline{v''P^{R'}} = \overline{v'' \frac{\partial q^{R'}}{\partial x_i}} = - \frac{\partial}{\partial x_i} (\overline{q_i^{R'} v'}) + q_i^{R'} \frac{\partial v'}{\partial x_i} \quad (3.18)$$

It seems interesting to understand the sign of the term $\overline{v''P^{R'}}$ in view of the fair correlation between enthalpy and radiative power fluctuations. Indeed, one could argue that the fluctuation of wall-normal velocity leads to a fluctuation of enthalpy due to convection which finally generates a variation in the radiative power. In order to verify this effect, a first attempt could consist in passing over the convected enthalpy fluctuations and directly approximate the variation of radiative power as a result from convection and the shape of the mean profile $\overline{P^R}$. Turbulent diffusion of the mean radiative power with a gradient assumption would then lead to

$$\overline{v''P^{R'}} \propto - \frac{\partial \overline{P^R}}{\partial x_i} \quad (3.19)$$

Although this approximation gives the right sign for the term $\overline{v''P^{R'}}$ in the very near wall region on both sides, it becomes erroneous for $y^+ > 25$ where the gradient of the mean radiative power profile changes sign. Skipping the enthalpy fluctuations to understand the correlation between wall-normal velocity and the radiative power is therefore not appropriate.

Another approach is proposed by momentarily considering the fourth-order cross-moment $\overline{v''h''h''P^{R'}}$ which introduces enthalpy fluctuations as the vehicle that could explain the correlation mechanism between velocity and radiative power variations. Two high-order correlation coefficients C_1 and C_2 are then defined as

$$\overline{v''h''h''P^{R'}} = C_1 \widetilde{v''h''h''P^{R'}} \quad (3.20)$$

$$\overline{v''h''h''P^{R'}} = C_2 \widetilde{h''h''v''P^{R'}} \quad (3.21)$$

Finally, the term $\overline{v''P^{R'}}$ can be indirectly related to the high-order statistical moment by writing

$$\overline{v''P^{R'}} = C \frac{\widetilde{v''h''h''P^{R'}}}{\widetilde{h''h''}}, \quad (3.22)$$

where $C = C_1/C_2$ is computed from equation (3.22) and plotted in figure 11. The profile of the coefficient C is regular, positive and varies from approximately unity close to the walls to 2.7 in the core of the channel. Neglecting differences between Favre and Reynolds

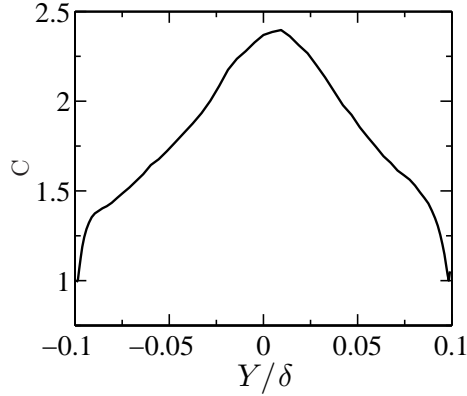


FIGURE 11. Correlation coefficient defined in equation (3.22) in case A_R.

fluctuations and inserting truncated Taylor series of $v' = ay^2$, $h' = by$ and $P^{R'} = c$ in the definition of C gives

$$C = \frac{\overline{b^2 ac}}{ab \overline{bc}} \quad (3.23)$$

The fact that $C = 1$ at walls indicates that c is proportional to b : Fluctuations of radiative power very close to the wall are mainly determined by local fluctuations of temperature.

Since the radiative dissipation term $h'' P^{R'}$ is negative, it can then be postulated from equation (3.22) that the term $\overline{v'' P^{R'}}$ appearing in equation (3.8) always has the opposite sign of the turbulent flux $\overline{\rho v'' h''}$. In the present configuration, this explains the positive sign of the correlation between wall-normal velocity and radiative power. As the term $\overline{v'' P^{R'}}$ presents a sign opposite to the one of the turbulent heat flux, it therefore appears as a loss term in equation (3.8). This loss mechanism described by equation (3.22) can be summarized as follows: A positive or negative variation of wall-normal velocity generates a fluctuation of enthalpy whose sign is determined by the direction of the turbulent heat flux; And this enthalpy fluctuation then induces a variation of opposite sign in radiative power.

3.1.5. Summary of radiation effects in turbulent channel flow

The coupling between the temperature and radiative fields has been carefully detailed through the analysis of DNS/Monte-Carlo results obtained in cases A and A_R. Figure 12 sums up the different interactions between Favre or Reynolds mean fields and fluctuating fields of velocity, temperature and radiation observed in the present channel flow simulations.

The feedback of mean temperature on velocity is done through the variation of temperature-dependent properties such as mean density and dynamic viscosity. In cases A and A_R characterized by a relative small difference of wall temperatures, this effect is negligible although it is effective in cases with larger temperature difference (Zhang *et al.* 2013a). On the other hand, impact of temperature fluctuations on the velocity field mainly through density variations is negligible in all investigated cases, making Reynolds and Favre averaging operations similar. In the specific configuration of a channel flow, convection by the mean velocity field does not influence the temperature field directly. It has obviously a major role in any general flow configuration. Besides, the fluctuations of velocity play a critical role in the obtained profiles of mean temperature and its root-mean-square through the turbulent heat flux and the production of enthalpy variance.

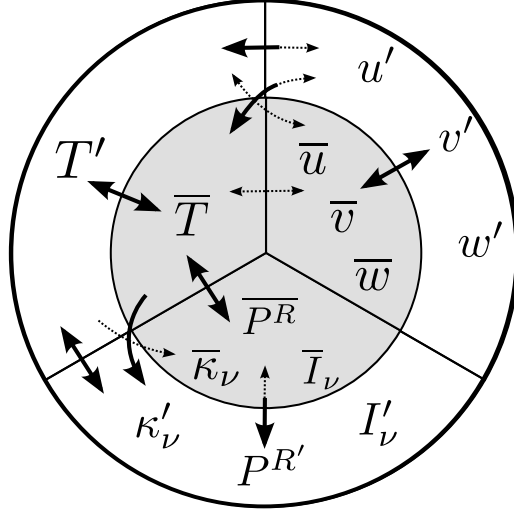


FIGURE 12. Scheme of coupling effects in turbulent channel flow with radiation. The fields of velocity (u, v, w), temperature (T) and radiative power (P^R) are split into mean and fluctuating components. Other quantities are considered for the radiation field: The spectral intensity (I_ν) and absorption coefficient (κ_ν). Main effects are represented by thick plain arrows while thin dotted arrows indicate negligible or null effects.

As outlined in Fig 12, the mean temperature and its fluctuations are tightly connected through the turbulent heat flux and the production term in the enthalpy variance balance equation. Similarly, the mean temperature field and the mean radiative power strongly depend on each other. The aforementioned modification of production in equation (3.4) is an indirect effect of radiation involving the two-way interaction between $\overline{P^R}$, \overline{T} and T' .

When radiation is accounted for, additional loss terms appear in the balance equations of enthalpy variance and turbulent heat flux, which make turbulent transport of the mean temperature field less efficient. The level of fluctuations of radiative fields is also determined from the magnitude of mean temperature and mean radiative fields.

Finally, it has been observed that the influence of fluctuating temperature and radiative fields is not noticeable on the mean radiative field. Such a property has been assumed in the development of a wall model for large-eddy simulations by Zhang *et al.* (2013b) to account for radiation effects within the inner structure of turbulent boundary layers.

3.2. Effects of wall temperature difference and Reynolds number

In this section, cases A, B and C are compared with and without accounting for radiation to enhance the effects of wall temperature difference and Reynolds number. Analysis of the results focuses on the turbulent heat flux, the enthalpy root-mean-square and the main contributing terms in their balance equations. Radiation effects prevent collapsing of scaled profiles when standard wall-scaling is used. A new scaling is proposed to improve collapsing of several profiles.

3.2.1. Effect of wall temperature difference

In comparison to the cases A and A_R, cases B and B_R are characterized by a large wall temperature difference (see table 1). Mean temperature profiles of these four cases are shown in figure 13. Small differences between cases A and B without radiation are due to noticeable effects of mean density variations. When accounting for radiation, the

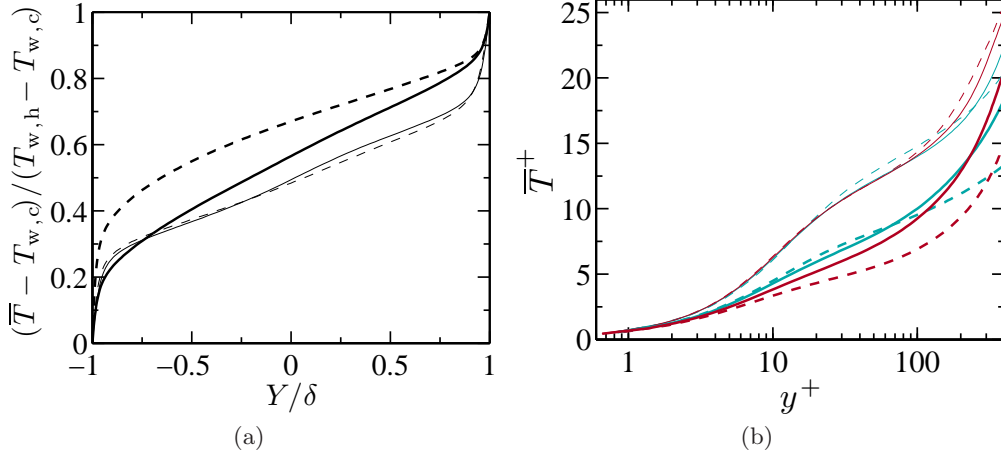


FIGURE 13. Profiles of mean temperature scaled by wall temperatures (a) and in wall units (b) on the cold side (blue color) and hot side (red color) in cases A (thin plain line), A_R (thick plain line), B (thin dashed line) and B_R (thick dashed line).

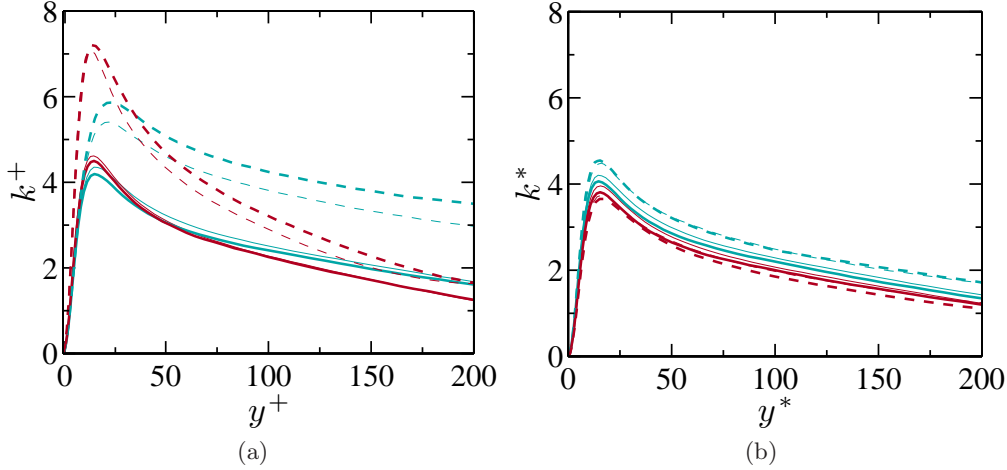


FIGURE 14. Profiles of turbulent kinetic energy on the cold side (blue color) and hot side (red color) in cases A (thin plain line), A_R (thick plain line), B (thin dashed line) and B_R (thick dashed line): (a) k^+ , scaled with standard wall-scaling. (b) k^* , scaled with semi-local scaling.

modification of the mean temperature in both \bar{T} and \bar{T}^+ profiles is stronger between case B and B_R because of the amplification of radiative effects at high temperature.

Profiles of mean velocity reported by Zhang *et al.* (2013a) exhibit a more significant impact of the mean density in cases B and B_R. The turbulent kinetic energy in wall units $k^+ = \overline{u_i'' u_i''} / (2u_\tau^2)$ is plotted in figure 14 (a). The variations of mean density prevent collapsing of the profiles, especially when comparing cases with small and large wall temperature difference. The effect of radiation on k^+ , associated with the changes in mean temperature profile and hence mean density, is small.

In order to improve the agreement between profiles corresponding to different cases, a semi-local scaling is applied: Non-uniformity of gas properties is considered by using local values of density, viscosity and thermal capacity (Huang *et al.* 1995; Coleman *et al.* 1995; Dailey *et al.* 2003). The corresponding friction velocity u_τ^* and friction temperature

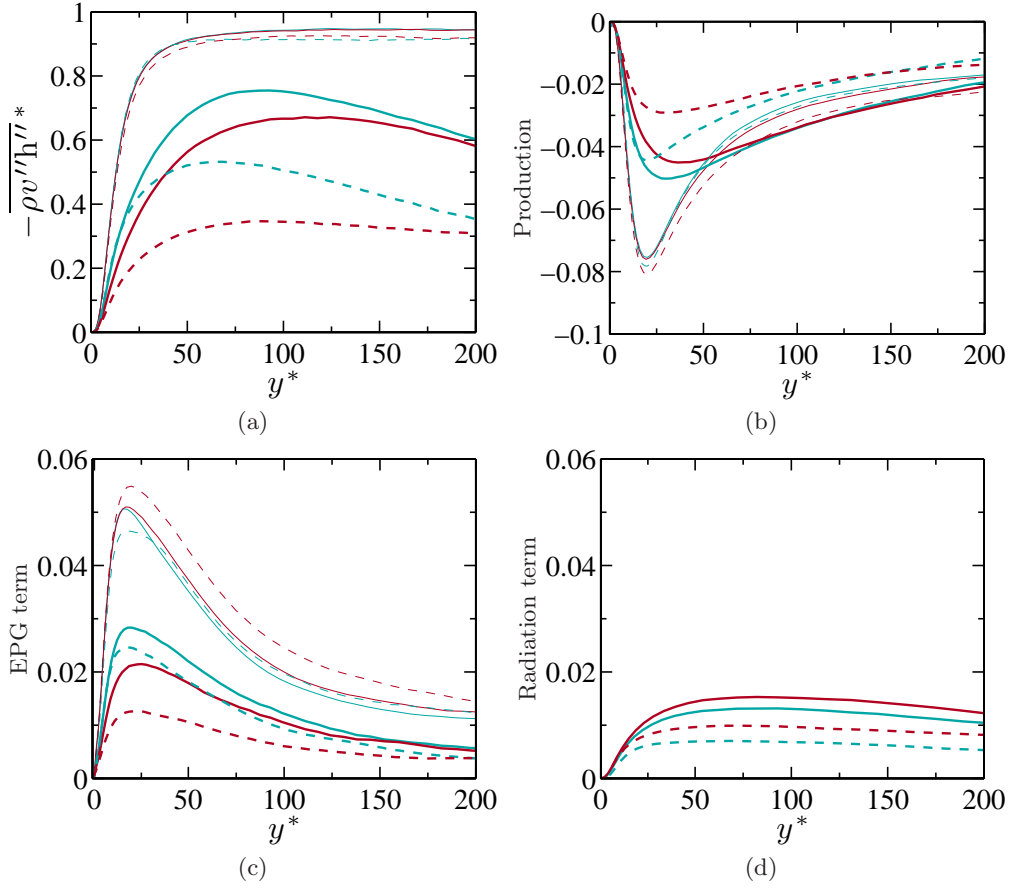


FIGURE 15. Profiles of turbulent heat flux (a) and its production term (b), EPG term (c) and correlation between velocity and radiative power (d) in semi-local scaled units on the cold side (blue color) and hot side (red color) in cases A (thin plain line), A_R (thick plain line), B (thin dashed line) and B_R (thick dashed line).

T_τ^* are then defined as:

$$u_\tau^* = \left(\frac{\overline{T_w}}{\overline{\rho}} \right)^{1/2}, \quad T_\tau^* = \frac{|\overline{q_w^{cd}}|}{\overline{\rho} c_p u_\tau^*}, \quad (3.24)$$

and the non-dimensional wall distance y^* is given by

$$y^* = \frac{\overline{\rho} y u_\tau^*}{\overline{\mu}}. \quad (3.25)$$

The turbulent kinetic energy in semi-local coordinates $k^* = k/u_\tau^{*2}$ is shown in figure 14 (b). Collapsing of k^* profiles is significantly improved, even for cases with radiation. Scaling of variables enables some cases variability to be filtered out, and the collapsing of their profiles outlines that the same underlying physical phenomenon is responsible for the shape of these profiles. Here, collapsing of k^* curves confirms that radiation affects turbulent kinetic energy indirectly through the change of temperature-dependent gas properties. Henceforward, semi-local scaling is used to normalize turbulent quantities.

The scaled turbulent heat flux, issued from the semi-local scaling,

$$\overline{\rho v'' h''}^* = \frac{\widetilde{\overline{\rho v'' h''}}}{\overline{\rho u_\tau^* c_p T_\tau^*}} = \frac{\widetilde{\overline{\rho v'' h''}}}{|\overline{q_w^{cd}}|} \quad (3.26)$$

does not differ from the one obtained with standard wall-scaling. Profiles of $\overline{\rho v'' h''}^*$ are compared in figure 15 (a). Good agreement between results of A and B is obtained. However, cases with radiation A_R and B_R are significantly different. Radiation effects are strongly dependent on temperature and non-linear, which explains why the deviation from cases without radiation is larger in case B_R because of higher temperatures.

The three dominant terms in the balance equation (3.8) of the turbulent heat flux, *i.e.* production, enthalpy-pressure-gradient correlation term (EPG) and radiation term, are also reported in figure 15. Following the semi-local scaling approach, these quantities are scaled by $|\overline{q_w^{cd}}| \overline{\tau_w} / \mu$. The collapsing of production and EPG term profiles corresponding to cases A and B is good except for the hot side in case B which presents a small difference that could not be corrected entirely by semi-local scaling.

In cases with radiation, the scaled production that is related to $-\widetilde{\overline{v'' v''}}^* \frac{d\overline{h^*}}{dy^*}$ is smaller in magnitude. Since, as shown for the turbulent kinetic energy k , the semi-local scaled root-mean-square of wall-normal velocity $\widetilde{\overline{v'' v''}}^*$ is barely affected by radiation through the mean density variation, the modification of the production magnitude is due to the change of scaled mean enthalpy gradient $\frac{d\overline{h^*}}{dy^*}$ that is tightly related to $\frac{d\overline{T^+}}{dy^+}$. Indeed, for y^+ between 10 and 30 where the production peaks, the variations between cases in the gradient of the scaled mean temperature (related to the slope of $\overline{T^+}(y^+)$ plotted in figure 13 (b)) agree with the differences observed for the peak value of the scaled production term. The differences of the wall-scaled enthalpy gradient are therefore responsible for the variations in the production term shown in figure 15 (b).

The enthalpy-pressure-gradient correlation term appearing in the transport equation of the turbulent heat flux is shown in figure 15 (c). It mostly compensates production for $y^* < 100$, and therefore the same variations between cases is retrieved. The last of the three dominant terms for cases with radiation in equation (3.8) is the scaled correlation between wall-normal velocity and radiative power $\overline{v'' P^{R'}}$. It is shown in figure 15 (d). The fact that $\overline{v'' P^{R'}}$ is larger in case A_R is not obvious as the magnitude of this radiative loss term is determined by multiple phenomena as described in section 3.1.4.

3.2.2. Radiation-based scaling

It has been shown that semi-local scaling works satisfactorily for cases without radiation by accounting for the effects of variable fluid properties. However, it cannot account for the specific role of radiation. Each case appears specific, although the same physical interpretation can explain the shapes and magnitudes of the observed profiles, as seen for the production term in equation (3.8). A new scaling is therefore derived to account for the variability of radiation effects.

As the mean energy balance equation without radiation is

$$\overline{q_y^{cd}}(Y) + \overline{\rho v'' h''}(Y) = \overline{q_w^{cd}}. \quad (3.27)$$

the turbulent heat flux is equal to the wall conductive flux $\overline{q_w^{cd}}$ outside of the viscous sublayer, where the conductive heat flux is negligible. The wall conductive flux $\overline{q_w^{cd}}$ is then the right quantity for scaling of the turbulent heat flux and to define the friction temperature. But, when radiation is taken into account, the mean energy balance equation

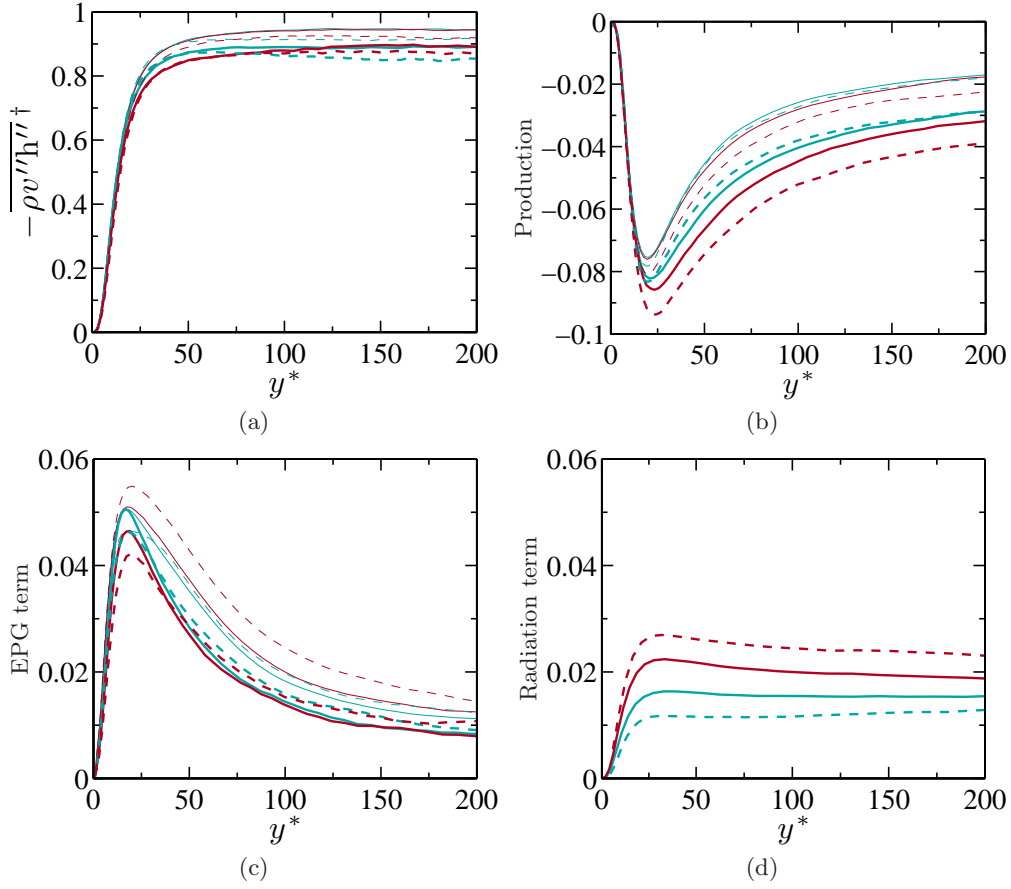


FIGURE 16. Profiles of turbulent heat flux (a) and its production term (b), EPG term (c) and correlation between velocity and radiative power (d) using radiation-based scaling on the cold side (blue color) and hot side (red color) in cases A (thin plain line), A_R (thick plain line), B (thin dashed line) and B_R (thick dashed line).

(3.7) becomes

$$\overline{q_y^{cd}}(Y) + \overline{\rho v'' h''}^\dagger(Y) = \overline{q_w^{cd}} - \Delta \overline{q^R}(Y) \equiv \overline{q^\dagger}(Y), \quad (3.28)$$

where $\Delta \overline{q^R}(Y)$ is the difference between the local radiative flux and the wall radiative flux,

$$\Delta \overline{q^R}(Y) = \overline{q^R}(Y) - \overline{q_w^R}. \quad (3.29)$$

The radiative fluxes $\overline{q^R}(Y)$ and $\overline{q_w^R}$ both contain the wall-wall radiative flux $\overline{q_{ww}^R}$ exchanged between the walls through the whole gaseous medium, that does not participate to the fluid energy balance and is zero if the walls are at the same temperature. This contribution is then suppressed in the definition of $\Delta \overline{q^R}(Y)$.

Similarly to the wall conductive flux $\overline{q_w^{cd}}$ in equation (3.27), $|\overline{q^\dagger}(Y)|$ is the right quantity for scaling of the turbulent heat flux for cases involving radiation. The sum of conductive and turbulent heat flux, equal to $\overline{q^\dagger}(Y)$, is a function of wall distance whose shape is determined by the intensity and nature of radiative energy transfer. For cases without radiation, $\overline{q^\dagger}(Y)$ turns back to the wall conductive flux.

The turbulent heat flux, normalized by $|\overline{q^\dagger}(Y)|$, $\overline{\rho v'' h''}^\dagger$ is plotted in figure 16 (a). In

comparison with figure 15 (a), the agreement between the different cases is significantly improved. Thanks to the radiation-based scaling, the scaled turbulent heat flux represents the relative strength of turbulent transport compared to conduction for all cases. For this reason, all profiles now present the same shape and reach a plateau. The remaining discrepancies concern the level of this plateau that is related to the remaining contribution of the conductive heat flux which, in the studied configurations with hot and cold walls, does not tend to zero in the core of the channel. The level of the plateau is then determined by the mean temperature gradient at the center of the channel and is different for each case. It is expected that, for symmetrical channel flows with the same wall temperatures or for external boundary layers, this effect is not present, making the proposed scaling even more efficient.

The three main terms in the balance equation of turbulent heat flux are also shown in figure 16, where the production, EPG contribution and radiative term are now scaled by $|\overline{q^\dagger}(Y)|\overline{\tau_w}/\mu$. The agreement between profiles is also much better when the radiation-based scaling is considered. In order to understand the effect of the scaling, the scaled production term is written as

$$\frac{-\overline{\rho v'' v''} \frac{d\tilde{h}}{dy}}{|\overline{q^\dagger}(Y)|\overline{\tau_w}/\mu} \approx -\overline{\rho v'' v''}^* \Pr \left(1 - \overline{\rho v'' h''^\dagger} \right), \quad (3.30)$$

where $\frac{d\tilde{h}}{dy} \approx \frac{\overline{c_p}}{\overline{c_p}} \frac{d\tilde{T}}{dy}$ is expressed from the mean energy balance equation. The improved agreement between scaled profiles of production is then issued from the obtained agreement between profiles of the turbulent heat flux. Discrepancies are nonetheless more noticeable in figure 16 (b) because the term $\left(1 - \overline{\rho v'' h''^\dagger} \right)$ outlines the aforementioned plateau mismatch. As the radiation-based scaling improves the collapsing of production profiles, its main counter-balancing terms, that are the contribution and radiation term, benefit from the same effect although the improved collapsing of profiles is not striking for the latter.

The enthalpy root-mean-square and the main terms in the enthalpy variance balance equation (3.4), production, molecular and radiative dissipations, are scaled using semi-local scaling and shown in figure 17. The transport equation terms are therefore scaled by $\overline{q_w^{cd^2}}/\overline{\mu}$. Once again, the good collapsing of profiles corresponding to cases without radiation demonstrate the efficiency of semi-local scaling to account for variable flow properties effects. Nonetheless, when radiation is taken into account, the rms of enthalpy, its production and molecular dissipation are totally different. As shown previously, then deviation from cases without radiation is stronger for higher temperatures.

The same results using radiation-based scaling are presented in figure 18. Defining a radiation-based friction temperature as

$$T_\tau^\dagger = \frac{|\overline{q^\dagger}(Y)|}{\overline{\rho} \overline{c_p} u_\tau}, \quad (3.31)$$

the normalized enthalpy h_{rms}^\dagger is scaled by $\overline{c_p} T_\tau^\dagger$ while the balance equation terms are scaled by the quantity $\overline{q^\dagger}(Y)^2/\overline{\mu}$. The radiation-based scaling allows similar shapes of h_{rms}^\dagger to be retrieved for all cases. Corresponding cases with and without radiation seem to collapse, although case B_R deviates from case A_R for $y^* > 75$. As the proposed radiation-based scaling accounts for variations of the turbulent heat flux profiles, the fact that the enthalpy rms does not directly depend on the turbulent heat flux can

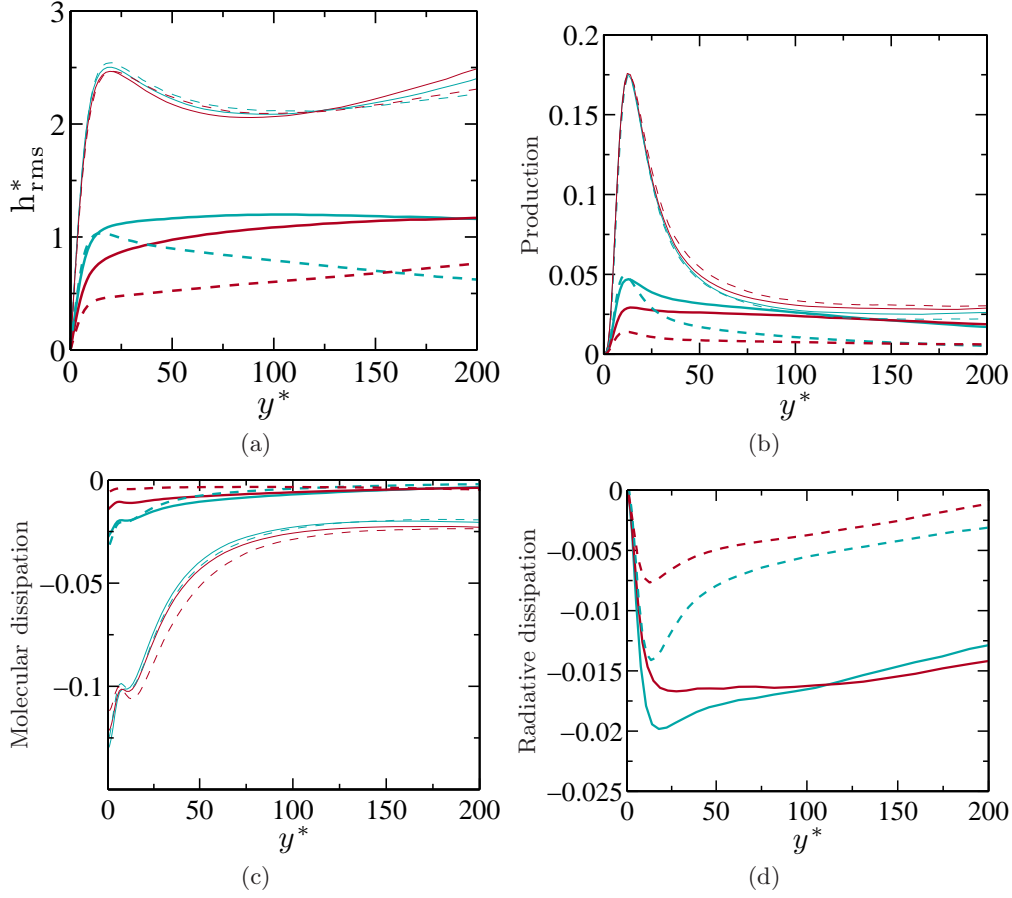


FIGURE 17. Profiles of enthalpy rms (a) and its production term (b), molecular dissipation (c) and radiative dissipation (d) using semi-local scaling on the cold side (blue color) and hot side (red color) in cases A (thin plain line), A_R (thick plain line), B (thin dashed line) and B_R (thick dashed line).

explain these discrepancies. On the other hand, the scaled production that is written as

$$\frac{-\overline{\rho v'' \widetilde{h''} \frac{d\widetilde{h}}{dy}}}{\overline{q^\dagger} (Y)^2 / \mu} \approx -\overline{\rho v'' h''}^\dagger \Pr \left(1 - \overline{\rho v'' h''}^\dagger \right), \quad (3.32)$$

simply depends on the turbulent heat flux and the obtained agreement between production profiles in figure 18 (b) is better. Production of enthalpy variance is mainly compensated by molecular and radiative dissipations which then individually show a fair agreement of their profiles using the new scaling. As radiation introduces an additional and significant loss term in the balance equation of enthalpy variance, the balance between production and molecular dissipation is strictly different between cases with and without radiation. That is why the agreement between profiles of molecular dissipation in figure 18 (c) is here correct only between cases with or without radiation, separately. However, switching progressively from a case without radiation to cases with more and more significant radiative effects, a continuous transition is expected. This trend is more visible in other studied cases and is detailed in the next section that deals with Reynolds number effects.

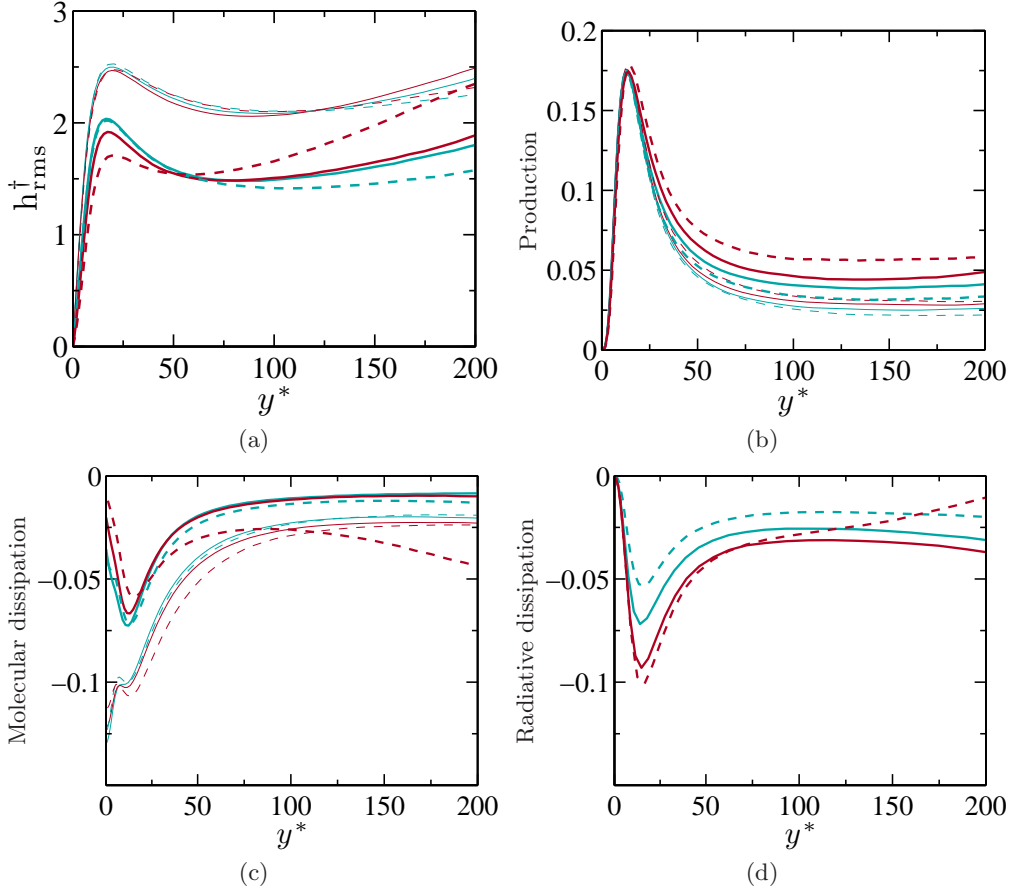


FIGURE 18. Profiles of enthalpy rms (a) and its production term (b), molecular dissipation (c) and radiative dissipation (d) using radiation-based scaling on the cold side (blue color) and hot side (red color) in cases A (thin plain line), A_R (thick plain line), B (thin dashed line) and B_R (thick dashed line).

Finally, it is worth noticing that the use of the radiation-based friction temperature T_τ^\dagger is not sufficient to improve the agreement between mean temperature profiles (see figure 19). Introducing the model of the turbulent diffusivity, the turbulent heat flux is related to the gradient of mean temperature. The mean energy balance equation in equation (3.28) also further constrain the relation between $\overline{\rho v'' h''}$ and the conductive flux, linked to the gradient of mean temperature. Therefore, the radiation-based friction temperature T_τ^\dagger can in fact properly scale the gradient of mean temperature for the different cases as it did for the turbulent heat flux. However, the radiation-based friction temperature T_τ^\dagger depends on the wall distance and this prevents it from appearing straightforwardly in the expression of the mean temperature after integration of the gradient $d\bar{T}/dy$.

3.2.3. Effect of Reynolds number

Figure 20 compares cases A and A_R to cases C and C_R, characterized by a larger Reynolds number, in terms of mean temperature profiles. On the one hand, radiation effects are reduced by the increased influence of turbulent transport, which makes the temperature profile in case C_R closer to those of cases without radiation. On the other

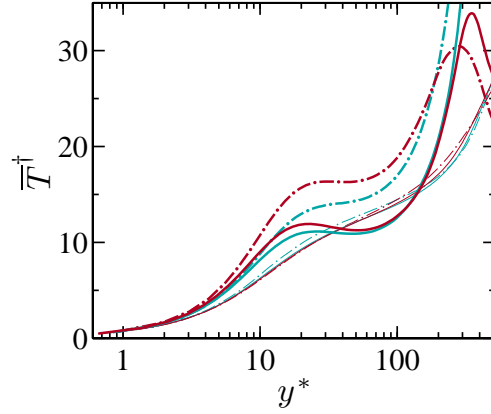


FIGURE 19. Profiles of mean temperature scaled by the radiation-based friction temperature T_r^\dagger on the cold side (blue color) and hot side (red color) in cases A (thin plain line), A_R (thick plain line), B (thin dashed line) and B_R (thick dashed line).

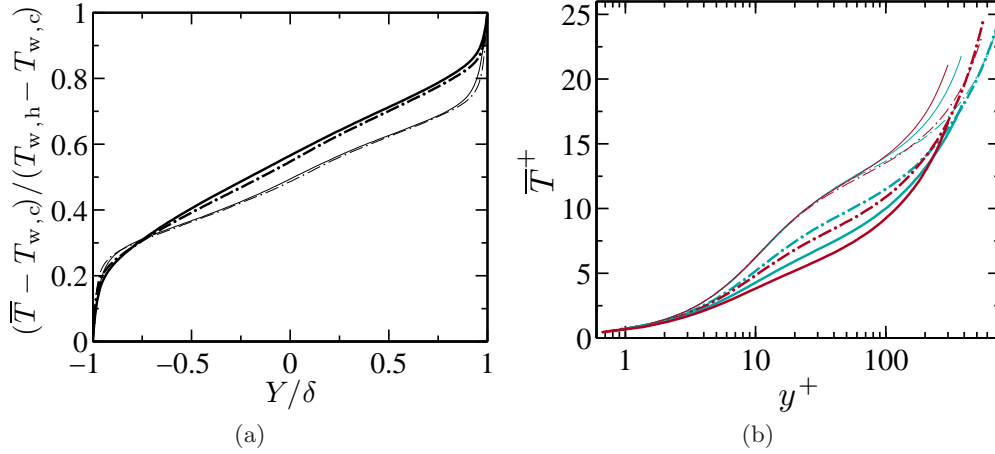


FIGURE 20. Profiles of mean temperature scaled by wall temperatures (a) and in wall units (b) on the cold side (blue color) and hot side (red color) in cases A (thin plain line), A_R (thick plain line), C (thin dashed-dotted line) and C_R (thick dashed-dotted line).

hand, a modification of the nature of radiative energy transfer has also been observed (Zhang *et al.* 2013a).

For cases A and C without radiation, a good agreement between profiles of mean turbulent heat flux is obtained by using semi-local scaling, as shown in figure 21. The same agreement is obtained for the main terms (production and EPG terms) in the balance equation of the turbulent heat flux. When radiation is accounted for in cases A_R and C_R, the profiles do not collapse on the ones of cases A and C. Nonetheless, results of case C_R sit between profiles of cases without radiation and the ones of case A_R, which is due to the weakened radiative effects at higher Reynolds number.

The same profiles are reported in figure 22 using the radiation-based scaling. As in section 3.2.2, agreement between profiles is significantly improved, except for the radiative term. It can be also noticed that results for case C_R remain between case A_R and case A/C.

Similar observations are obtained for the enthalpy root-mean-square and for its pro-

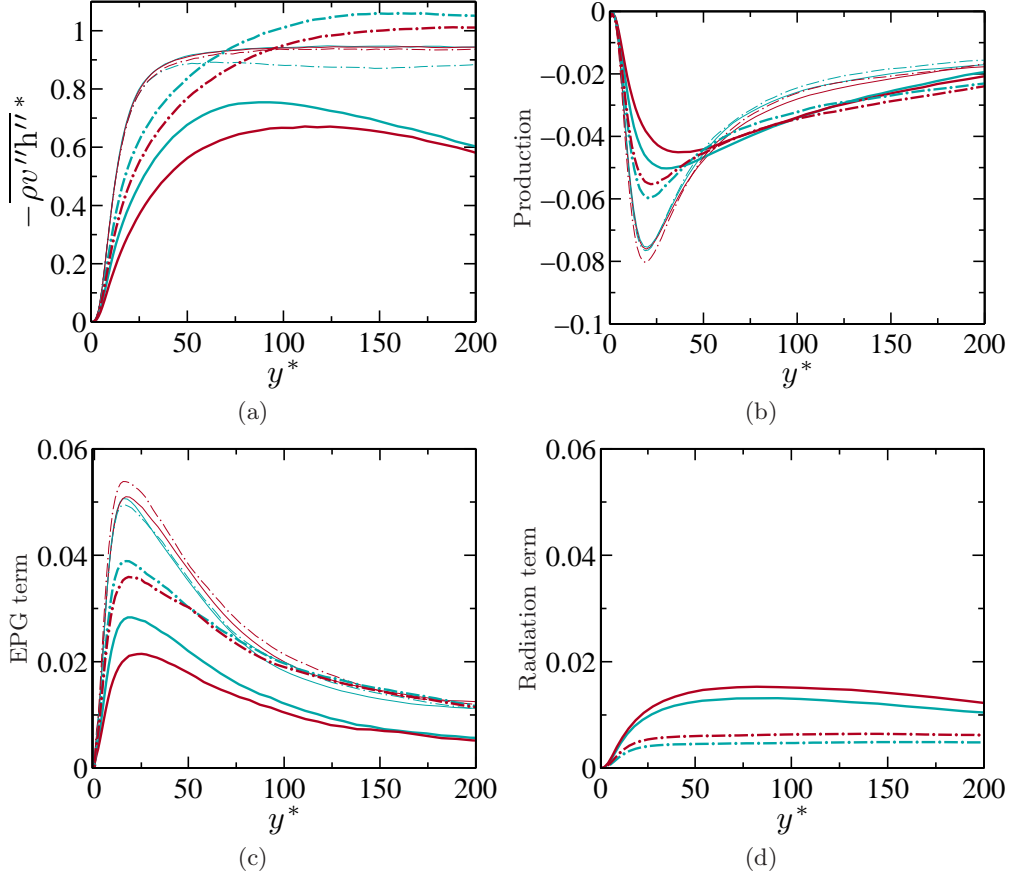


FIGURE 21. Profiles of turbulent heat flux (a) and its production term (b), EPG term (c) and correlation between velocity and radiative power (d) in semi-local scaled units on the cold side (blue color) and hot side (red color) in cases A (thin plain line), A_R (thick plain line), C (thin dashed-dotted line) and C_R (thick dashed-dotted line).

duction and dissipation terms shown in figure 23 and 24 using semi-local scaling and radiation-based scaling, respectively. Contrary to the comparison between cases A_R and B_R, it clearly appears in figure 24 (d) that the scaled molecular dissipation profiles exhibit a transition between cases without radiation and cases with stronger and stronger radiative energy transfer. Consequently, although profiles of production correctly collapse with the proposed radiation-based scaling, its necessary splitting into two dissipative terms prevents collapsing for molecular and radiative dissipation profiles separately. The balance between molecular and radiative dissipations is controlled by the importance of radiation so that a smooth transition between profiles of different cases can be expected when radiative energy transfer increases from being negligible to strongly dominant.

With the same arguments, the profiles of EPG and radiation terms in the balance equation of the turbulent heat flux cannot entirely collapse with the proposed radiation-based scaling. The balance between the two terms is determined by the weight of radiation effects.

For the sake of clarity and brevity, only high-pressure cases have been studied. In atmospheric conditions, similarly to the studied case C with a higher Reynolds number, the relative magnitude of radiative energy transfer compared to turbulent transport

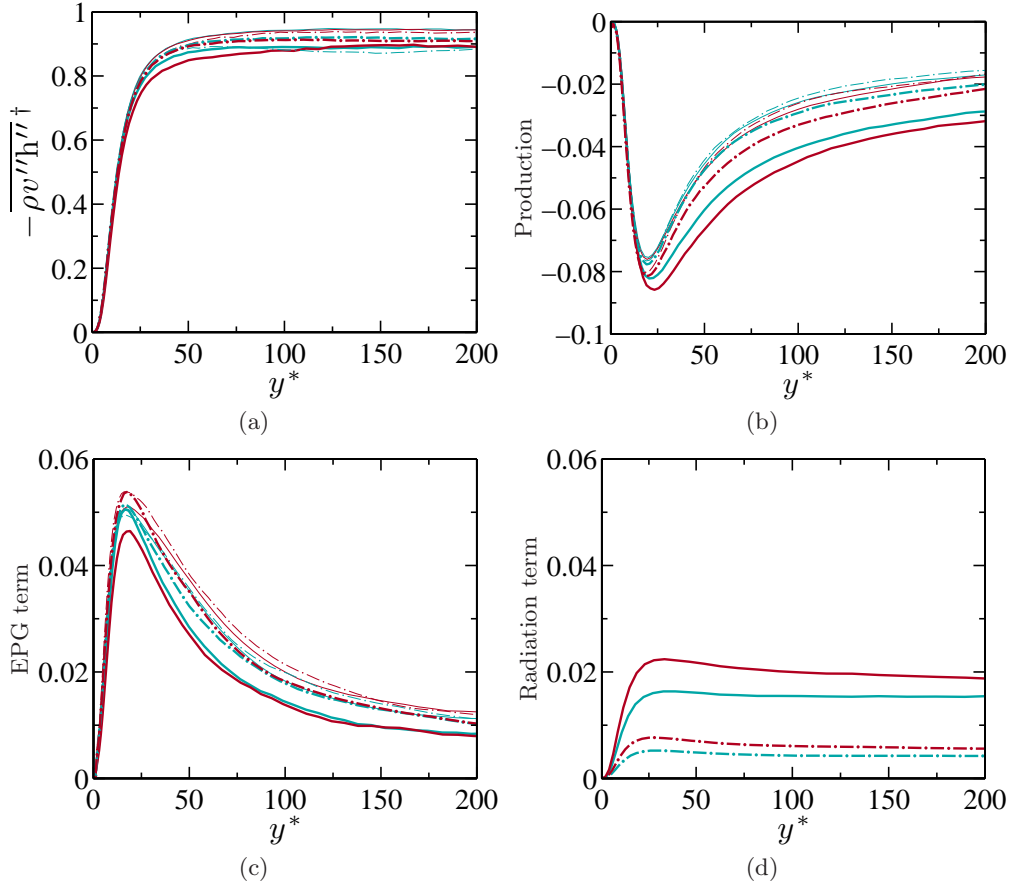


FIGURE 22. Profiles of turbulent heat flux (a) and its production term (b), EPG term (c) and correlation between velocity and radiative power (d) using radiation-based scaling on the cold side (blue color) and hot side (red color) in cases A (thin plain line), A_R (thick plain line), C (thin dashed-dotted line) and C_R (thick dashed-dotted line).

decreases. Compared to high pressure cases, profiles at atmospheric pressure are then closer to corresponding cases without radiation. The various effects of wall temperatures, wall emissivities, pressure and Reynolds number have been extensively studied on the mean temperature profile by Zhang *et al.* (2013a). As seen in the present study, no universal profile appears: Each case is different from the other. Additional effects that have not been investigated such as different reflection laws, possibly including spectral effects, would also yield to different profiles. Nonetheless, for all these cases that have not been studied here, the different additional terms due to radiation in the balance equations of enthalpy root-mean-square and turbulent heat flux remain and the associated physical interpretation derived here is expected to remain valid. This is especially true for the radiation-based scaling designed in equation (3.28) to properly scale the turbulent heat flux in any radiative conditions by accounting for the balance between the conductive heat flux and the turbulent heat flux only.

3.3. Effects on the turbulent Prandtl number

Previously shown results have outlined the effect of radiation on the turbulent heat flux. A simple model of turbulent heat transfer is based on the turbulent Prandtl number Pr_t

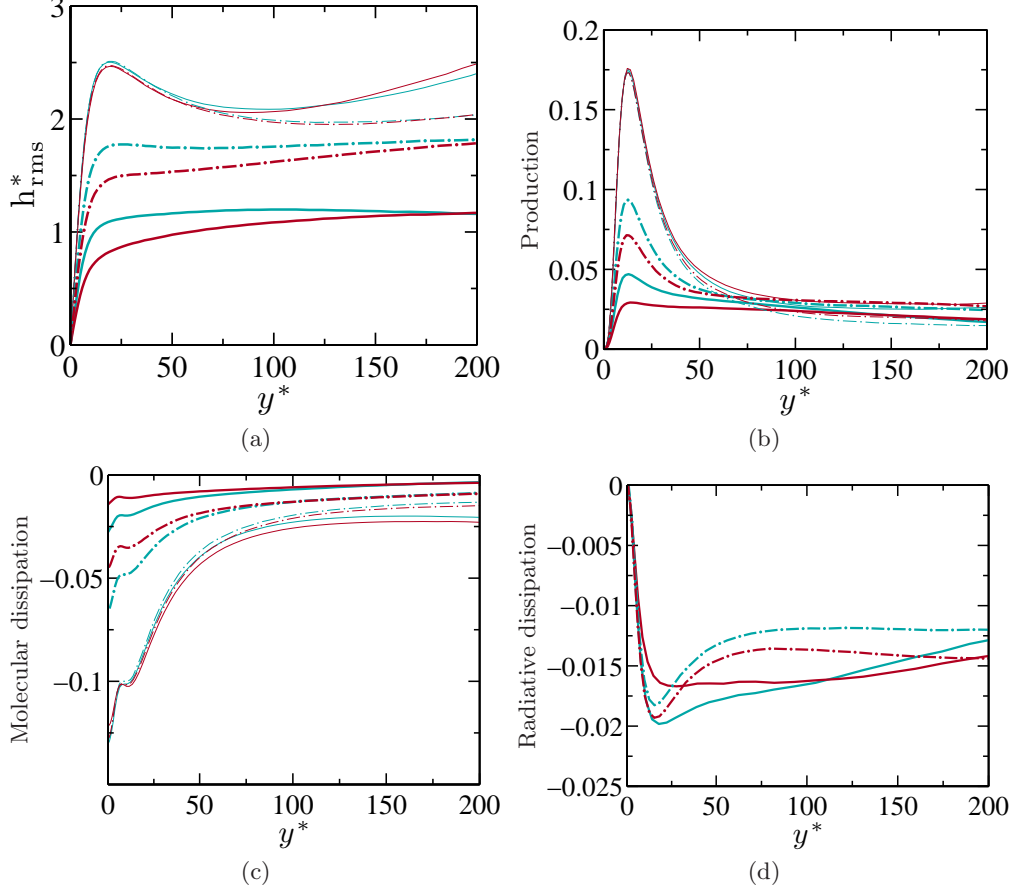


FIGURE 23. Profiles of enthalpy rms (a) and its production term (b), molecular dissipation (c) and radiative dissipation (d) using semi-local scaling on the cold side (blue color) and hot side (red color) in cases A (thin plain line), A_R (thick plain line), C (thin dashed-dotted line) and C_R (thick dashed-dotted line).

that is extensively used to relate the thermal eddy diffusivity a_t to the turbulent eddy viscosity ν_t . It is defined as

$$\text{Pr}_t = \frac{\nu_t}{a_t} = \frac{-\overline{\rho u'' v''}}{-\overline{\rho v'' h''} / \overline{c_p}} \frac{d\overline{T}/dY}{d\overline{u}/dY}. \quad (3.33)$$

This definition can alternatively be based on the gradient of Favre average of temperature and velocity. As mentioned earlier, the difference between Reynolds and Favre averaging approaches is small in the studied conditions. The turbulent Prandtl number concept can be erroneous for complex configurations. It is however valid for inhomogeneous turbulent flows in one directions such as turbulent boundary layers. Computational cost becoming tremendous for wall-resolved Large-Eddy Simulation (LES) as the Reynolds number increases (Piomelli 2008), wall models are necessary in order not to resolve the boundary inner layer. Thus, when considering heat transfer in wall-modeled LES (Benarafa *et al.* 2007; Larsson *et al.* 2011; Kawai & Larsson 2012; Zhang *et al.* 2013b), the turbulent Prandtl number model, which is here a valid approach, is a primordial component of

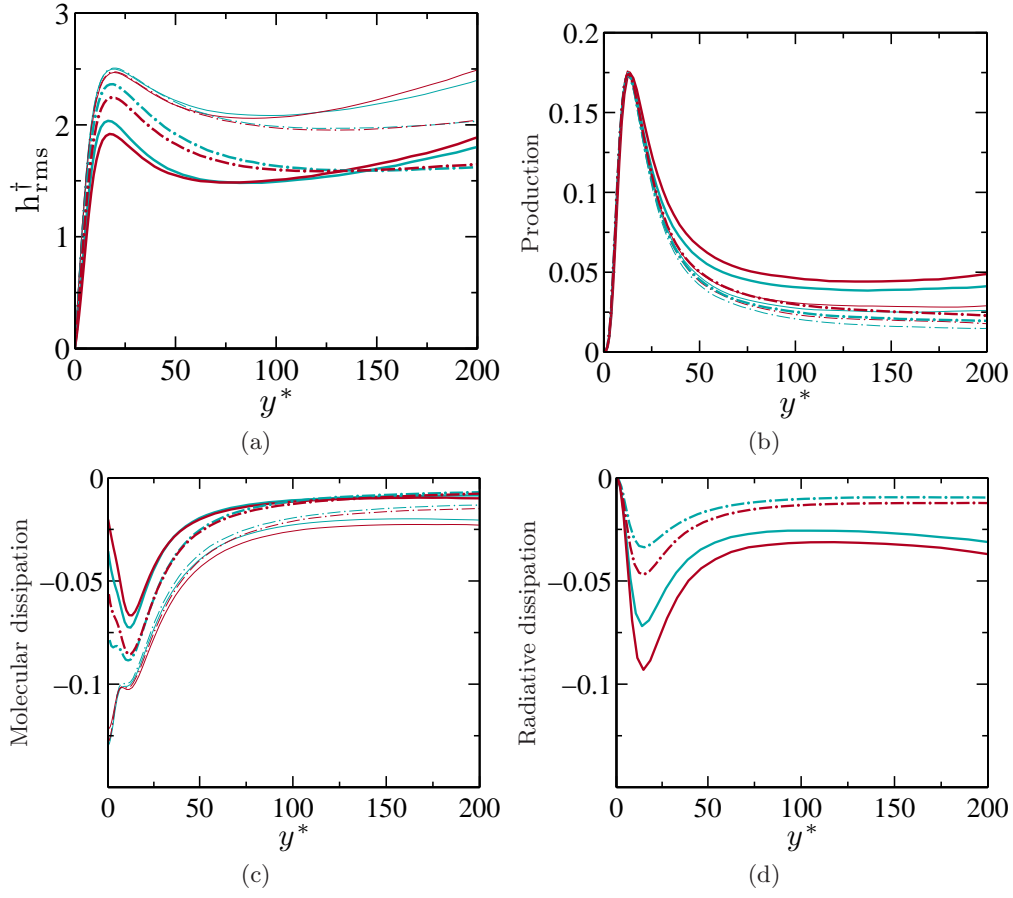


FIGURE 24. Profiles of enthalpy rms (a) and its production term (b), molecular dissipation (c) and radiative dissipation (d) using radiation-based scaling on the cold side (blue color) and hot side (red color) in cases A (thin plain line), A_R (thick plain line), C (thin dashed-dotted line) and C_R (thick dashed-dotted line).

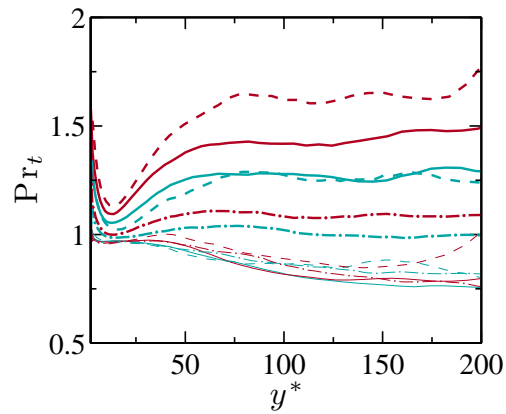


FIGURE 25. Profiles of the turbulent Prandtl number on the cold side (blue color) and hot side (red color) in cases A (thin plain line), A_R (thick plain line), B (thin dashed line), B_R (thick dashed line), C (thin dashed-dotted line) and C_R (thick dashed-dotted line).

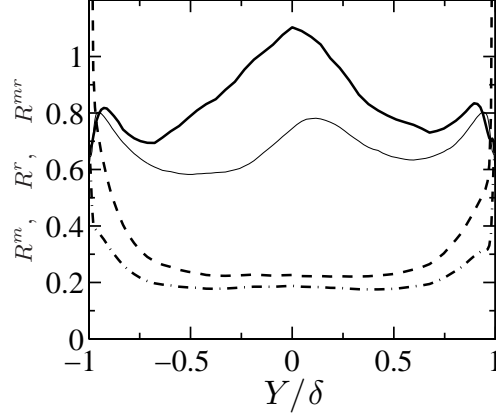


FIGURE 26. Profiles of time scale ratio R^m in cases A (thin plain line) and A_R. In case A_R, different definitions of the thermal time scale are based on: Molecular dissipation only (R^m : thick plain line); Radiative dissipation only (R^r : thick dashed line); Both dissipation terms (R^{mr} : thick dashed-dotted line).

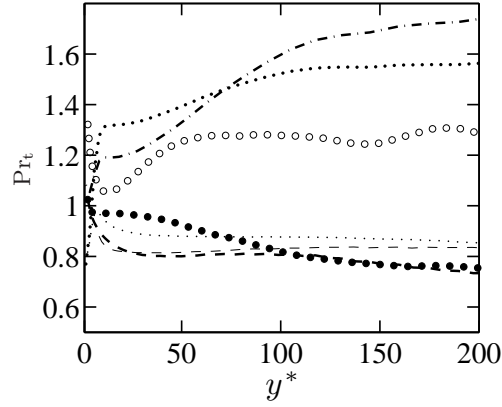


FIGURE 27. Comparison of predicted turbulent Prandtl number with DNS results in cases A and A_R (only the cold side is shown). Case A: DNS (filled circles); Model A^m (thin dotted line); Model B^m (thin dashed line). Case A_R: DNS (empty circles); Model B^m (thick dashed line); Model A^{mr} (thick dotted line); Model B^{mr} (thick dashed-dotted line).

the wall model. The DNS results are then here analyzed in terms of resulting turbulent Prandtl number in order to understand the impact on heat transfer wall modeling.

The profiles of Pr_t are presented in figure 25 for all studied cases. The profile of the turbulent Prandtl number in boundary layers has been widely studied (Kays 1994) and results for cases without radiation are consistent with channel flow simulations in the literature with air ($Pr = 0.71$) and fixed temperature at the wall (Kim & Moin 1987; Kong *et al.* 2000): The value is close to unity at the wall and decreases along the wall-normal distance, reaching an asymptotic value for high Reynolds number flows. Deviation of case B from cases A and C is attributed to mean density effects. Cases with radiation exhibit much stronger differences: The obtained profiles of turbulent Prandtl number are all above the standard ones without radiation. Profiles for cases A_R, B_R and C_R on the two sides of the channel are all different from each other but have the same pattern: Pr_t decreases from a value larger than unity at the wall until $y^* \approx 15$, then increases between $y^* = 15$ and 75 to reach a plateau beyond. The value $y^* = 75$ also corresponds to

the value where the radiation-based turbulent heat flux reaches a plateau (see figures 15 and 22). This result is due to the fact that Pr_t is related to $\overline{\rho v'' h''}^\dagger$:

$$\text{Pr}_t \propto \frac{\overline{dT/dY}}{\overline{-\rho v'' h''}} \approx \frac{1}{\lambda} \frac{\left(1 - \overline{\rho v'' h''}^\dagger\right)}{\overline{-\rho v'' h''}^\dagger} \quad (3.34)$$

Finally, the effects of Reynolds number and wall temperature difference are consistent with previous results: Case C_R is closer to results without radiation while the hot wall profile in case B_R presents the largest difference.

Since radiation can modify the profile of the turbulent Prandtl number significantly, a dedicated model for Pr_t in wall-modeled LES is necessary. Obviously, considering a constant turbulent Prandtl number or algebraic functions of Pr_t from Kays (1994) only valid for equilibrium turbulent boundary layers is not appropriate since these approaches are not accounting for radiation. Four-equations closure models developed for Reynolds Averaged Numerical Simulations (RANS) are then first investigated because these more comprehensive models can calculate variable turbulent Prandtl numbers. These models usually use the time scale ratio $R = \tau_t/\tau_u$, where the velocity turbulent time scale τ_u and thermal turbulent time scale τ_t are defined as

$$\tau_u = \frac{k}{\epsilon}, \quad \tau_t = \frac{\widetilde{h'' h''}}{2\epsilon_h}, \quad (3.35)$$

and ϵ and ϵ_h are dissipation terms of the turbulent kinetic energy k and enthalpy variance, respectively. When radiation is accounted for, there are two types of dissipation, i.e. molecular and radiative dissipations, denoted here as ϵ_h^m and ϵ_h^r respectively. Therefore, three thermal time scales can be defined:

$$\tau_t^m = \frac{\widetilde{h'' h''}}{2\epsilon_h^m}, \quad \tau_t^r = \frac{\widetilde{h'' h''}}{2\epsilon_h^r} \quad \text{and} \quad \tau_t^{mr} = \frac{\widetilde{h'' h''}}{2(\epsilon_h^m + \epsilon_h^r)} \quad (3.36)$$

The first one is only based on molecular dissipation, the second one only on radiative dissipation and the third one on the sum of these two previous effects. The different corresponding time scale ratios $R^m = \tau_t^m/\tau_u$, $R^r = \tau_t^r/\tau_u$ and $R^{mr} = \tau_t^{mr}/\tau_u$ are shown in figure 26 in case A and A_R. The common time scale ratio R^m based on thermal molecular dissipation is larger than the others in case A_R while the one based on radiative dissipation R^r is much smaller. Finally, the combination of the two dissipative terms in the definition of R^{mr} leads to the shortest thermal turbulent time scale. As radiation dissipation dominates, this latter definition is close to the one based on radiative dissipation only.

Different models for the thermal turbulent diffusivity a_t , which use the time scale ratio R as input and lead to different expressions of the turbulent Prandtl number, are now considered. These models are completed with four transport equations for k , ϵ , $\widetilde{h'' h''}$ and ϵ_h to compute the different turbulent time scales. Here, DNS data are used to assess their accuracy. The turbulent thermal diffusivity a_t is modeled as

$$a_t = C_\lambda k \tau_m f_\lambda, \quad (3.37)$$

where τ_m is a mixed time scale expressed from τ_u and R , $C_\lambda = 0.1$ a model constant usually set to retrieve the asymptotically constant turbulent Prandtl (≈ 0.85) in air at high Reynolds number and f_λ is a damping function accounting for low-Reynolds effects at the immediate vicinity of the wall. Two formulations for τ_m are considered. The first

one (referred as model A) used by Nagano & Kim (1988) and Soufiani *et al.* (1990) is written as

$$\tau_m = \tau_u (2R)^m \quad \text{with} \quad m = 0.5, \quad (3.38)$$

while the second formulation (referred as model B) from Abe *et al.* (1995) can be given by

$$\tau_m = \tau_u \frac{2R}{R + C_m} \quad \text{with} \quad C_m = 0.5. \quad (3.39)$$

For each of these models, the thermal turbulent time scale and the corresponding ratio R can be evaluated either only from the molecular dissipation (models A^m and B^m) or from the total dissipation term, sum of molecular and radiative dissipative terms (models A^{mr} and B^{mr}). The latter approach was already proposed by Ammouri *et al.* (1994). Models A^m, A^{mr}, B^m and B^{mr} are *a priori* tested using DNS profiles of time scale ratios R^m and R^{mr} to compute a_t . Damping functions f_λ for A^m and A^{mr} are taken from Soufiani *et al.* (1990), and for models B^m and B^{mr} from Abe *et al.* (1995). The predicted profiles of a_t are combined with the turbulent viscosity profiles extracted from DNS results to compute profiles of turbulent Prandtl number Pr_t that are presented in figure 27.

In case A, without radiation, predictions of models A^m and B^m are similar and tend to an asymptotic value of Pr_t . Agreement with the DNS data is correct although the turbulent Prandtl number obtained in DNS does not reach a plateau and keeps decreasing. This behavior can be attributed to low-Reynolds effects in the core of the channel but also to the specific configuration of different wall temperatures, which leads to an increase of enthalpy fluctuations, starting here at $y^+ \approx 100$, in the center of the channel (see figure 4).

With radiation, results of model B^m (and A^m, not presented here) show that, if only the molecular dissipation is accounted for, the turbulent Prandtl number is significantly underestimated and that a wrong trend is predicted. On the other hand, when both molecular and radiative dissipations are accounted for in the definition of the thermal time scale, the turbulent Prandtl number predicted by models A^{mr} and B^{mr} is correctly enhanced by radiation effects but the discrepancies with the DNS profile of case A_R remain important.

Using previous results with the radiation-based scaling, another model for Pr_t is proposed to account for radiation effects in turbulent boundary layers. In section 3.2, it has been demonstrated that the non-dimensional turbulent heat flux, when normalized with radiation-based scaling, agree well between different cases with and without radiation, *i.e.*,

$$\overline{\rho v'' h''}_R^\dagger \approx \overline{\rho v'' h''}_0^\dagger, \quad (3.40)$$

where subscript indices R and 0 correspond to quantities in cases with and without radiation, respectively. For cases with radiation, the thermal turbulent diffusivity can then be written

$$a_{t,R} = \frac{1}{\bar{\rho}_R \bar{c}_{p,R}} \frac{\overline{\rho v'' h''}_R}{d\bar{T}_R/d\bar{y}} \approx \frac{1}{\bar{\rho}_R \bar{c}_{p,R}} \frac{|\overline{q_R^\dagger(Y)}|}{d\bar{T}_R/d\bar{y}} \overline{\rho v'' h''}_0^\dagger \quad (3.41)$$

For cases without radiation, $\overline{\rho v'' h''}_0^\dagger$ is expressed as

$$\overline{\rho v'' h''}_0^\dagger = \frac{\overline{\rho v'' h''}_0}{|q_{w,0}^{cd}|} = \frac{a_{t,0}}{\bar{a}_0 + a_{t,0}} \frac{d\bar{T}_0/d\bar{y}}{|d\bar{T}_0/d\bar{y}|} = \frac{\nu_{t,0}}{\bar{a}_0 \text{Pr}_t^0 + \nu_{t,0}} \frac{d\bar{T}_0/d\bar{y}}{|d\bar{T}_0/d\bar{y}|}, \quad (3.42)$$

where a_0 is the thermal diffusivity. From equations (3.41) and (3.42), the turbulent

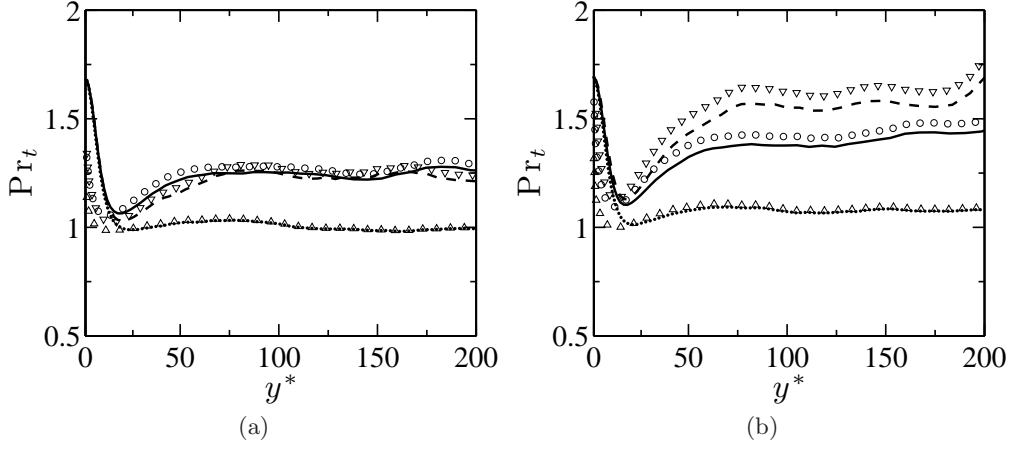


FIGURE 28. Profiles of modeled turbulent Prandtl number on the cold side (a) and hot side (b) compared to DNS results in cases A_R (DNS: Circles; Model: Plain line) , B_R (DNS: Down-pointing triangles; Model: Dashed line) and C_R (DNS: Up-pointing triangles; Model: Dotted line).

Prandtl number $\text{Pr}_{t,R}$ that accounts for radiation effects can be calculated as

$$\text{Pr}_{t,R} = \frac{\nu_{t,R}}{a_{t,R}} = \bar{\rho}_R \bar{c}_{pR} \frac{|\overline{dT}_R/d\bar{y}|}{|\overline{q}_R^\dagger(Y)|} \frac{\nu_{t,R} (\overline{a}_0 \text{Pr}_t^0 + \nu_{t,0})}{\nu_{t,0}}. \quad (3.43)$$

Neglecting radiation effects on the velocity field, $\nu_{t,0}$ can then be replaced with $\nu_{t,R}$. Assuming also that $a_R \approx a_0$ finally gives

$$\text{Pr}_{t,R} = \bar{\rho}_R \bar{c}_{pR} \frac{|\overline{dT}_R/d\bar{y}|}{|\overline{q}_R^\dagger(Y)|} (\overline{a}_R \text{Pr}_t^0 + \nu_{t,R}), \quad (3.44)$$

Effects of radiation are included through $\overline{q}_R^\dagger(Y)$ which is related to the radiative flux and through the change of the mean temperature profile in the term $|\overline{dT}_R/d\bar{y}|$. When no radiative energy transfer is considered, the right-hand-side of equation (3.44) simplifies to Pr_t^0 , profile of turbulent Prandtl number in cases without radiation. This last piece of the model can either be given by an algebraic formula or by a more complex model. Here, the formula proposed by Kays (1994) is considered:

$$\text{Pr}_t^0 = \frac{1}{0.5882 + 0.228(\nu_{t,R}/\overline{\nu}_R) - 0.0441(\nu_{t,R}/\overline{\nu}_R)^2 \left[1 - \exp\left(\frac{-5.165}{\nu_{t,R}/\overline{\nu}_R}\right) \right]}. \quad (3.45)$$

Equations (3.44) and (3.45) are the base of a turbulent Prandtl model accounting for radiation, to be applied in turbulent boundary layers: It can be used in RANS simulations but also in wall-model for large eddy simulations. Using DNS data to evaluate equations (3.44) and (3.45), results of the proposed model are compared with DNS results in figure 28 for all studied cases. The agreement of the model with DNS is impressive, showing the importance of the radiation-based scaling. The validity of the model is nonetheless limited to equilibrium boundary layers since it is the scope of the investigated cases and of equation (3.45).

4. Conclusion

Direct numerical simulations of turbulent channel flows of burnt gases composition under different conditions (Reynolds number, wall temperature difference) are analyzed with and without accounting for radiative energy transfer, computed with a Monte-Carlo method. In addition to the modification of the mean temperature profiles and associated wall laws, fluctuations of temperature and turbulent heat transfer are significantly reduced by radiation in the studied conditions for two main reasons. On the one hand, radiation indirectly influences production terms that appear in the balance equation of these quantities by changing gradients of the mean temperature field. On the other hand, the additional radiative power source term in the energy balance equation generates new terms in transport equations of enthalpy variance and turbulent heat flux. The two new terms, correlations between radiative power and enthalpy fluctuations and between radiative power and wall-normal velocity fluctuations, appear as loss terms in these equations. There is therefore a strong interaction between the fluctuations of radiative power and temperature. The latter then influences the mean temperature field through turbulent transport. However, the widely studied impact of turbulent fluctuations on the mean radiative power is negligible in the considered channel flows where no combustion takes place.

The different types of impact of radiation on the turbulent heat flux, the enthalpy variance and their transport equation terms are shown to be different in each case, for different wall temperature and different Reynolds numbers. The usual collapsing of wall-scaled variable profiles under these different conditions is then not retrieved when radiation is taken into account. This effect is corrected by introducing a radiation-based scaling in order to correctly quantify the balance between molecular diffusion and turbulent transport. Very good agreements between profiles of scaled turbulent heat flux and other related variables such as production terms are obtained for all studied cases. The balance between scaled molecular dissipation (or the enthalpy-pressure-gradient term) and the radiation loss term, that both compensate production outside of the boundary buffer layer, is determined by the magnitude of radiative energy transfer.

Finally, using radiation-based scaling, a model for the turbulent Prandtl number in boundary layers with radiation effects is proposed. *A priori* validation shows that profiles of turbulent Prandtl number that are significantly different from the cases without radiation are accurately predicted. This model can be used in RANS or wall-modeled LES when radiation is able to modify the boundary layer structure.

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Appendix A. Derivation of transport equations for enthalpy root-mean-square and turbulent heat flux

In a low Mach-number formulation, the pressure in the enthalpy equation (2.3) is the thermodynamic pressure which is constant in the studied cases. The enthalpy equation

can then be simplified to

$$\frac{\partial(\rho h)}{\partial t} + \frac{\partial(\rho u_j h)}{\partial x_j} = -\frac{\partial q_j^{cd}}{\partial x_j} + PR. \quad (\text{A } 1)$$

Averaging equation (A 1) makes the turbulent heat flux appear on the right-hand-side and gives

$$\frac{\partial}{\partial t} (\overline{\rho h}) + \frac{\partial}{\partial x_j} (\overline{\rho u_j h}) = -\frac{\partial \overline{q_j^{cd}}}{\partial x_j} + \overline{PR} - \frac{\partial}{\partial x_j} (\overline{\rho u_j'' h''}). \quad (\text{A } 2)$$

A transport equation for $\widetilde{h}^2/2$ is obtained by multiplying equation (A 2) by \widetilde{h} :

$$\frac{\partial}{\partial t} \left(\overline{\rho} \frac{\widetilde{h}^2}{2} \right) + \frac{\partial}{\partial x_j} \left(\overline{\rho} \widetilde{u}_j \frac{\widetilde{h}^2}{2} \right) = -\widetilde{h} \frac{\partial \overline{q_j^{cd}}}{\partial x_j} + \widetilde{h} \overline{PR} - \widetilde{h} \frac{\partial}{\partial x_j} (\overline{\rho u_j'' h''}). \quad (\text{A } 3)$$

Similarly, a transport equation for $\overline{h^2}/2$ is obtained by multiplying equation (A 1) by h and averaging, which gives

$$\frac{\partial}{\partial t} \left(\overline{\rho} \frac{\overline{h^2}}{2} \right) + \frac{\partial}{\partial x_j} \left(\overline{\rho} \overline{u}_j \frac{\overline{h^2}}{2} \right) = -\overline{h} \frac{\partial \overline{q_j^{cd}}}{\partial x_j} + \overline{h PR}. \quad (\text{A } 4)$$

The transport equation for the enthalpy rms $\widetilde{h}''^2/2 = \overline{h^2}/2 - \widetilde{h}^2/2$ is written by subtracting equation (A 3) from equation (A 4):

$$\frac{\partial}{\partial t} \left(\overline{\rho} \frac{\widetilde{h}''^2}{2} \right) + \frac{\partial}{\partial x_j} \left(\overline{\rho} \left(\overline{u}_j \frac{\overline{h^2}}{2} - \widetilde{u}_j \frac{\widetilde{h}^2}{2} \right) \right) = -\overline{h} \frac{\partial \overline{q_j^{cd}}}{\partial x_j} + \widetilde{h} \frac{\partial \overline{q_j^{cd}}}{\partial x_j} + \overline{h PR} - \widetilde{h} \overline{PR} + \widetilde{h} \frac{\partial}{\partial x_j} (\overline{\rho u_j'' h''}). \quad (\text{A } 5)$$

The second term on the left-hand-side can be written as

$$\overline{u}_j \frac{\overline{h^2}}{2} - \widetilde{u}_j \frac{\widetilde{h}^2}{2} = \frac{1}{2} \widetilde{u}_j \widetilde{h}''^2 + \widetilde{h} \widetilde{u}_j'' h'' + \frac{1}{2} \widetilde{u}_j'' h'' h''. \quad (\text{A } 6)$$

Inserting this expression in equation (A 5) gives

$$\begin{aligned} \frac{\partial}{\partial t} \left(\overline{\rho} \frac{\widetilde{h}''^2}{2} \right) + \frac{\partial}{\partial x_j} \left(\overline{\rho} \widetilde{u}_j \frac{\widetilde{h}''^2}{2} \right) &= \underbrace{-\overline{h} \frac{\partial \overline{q_j^{cd}}}{\partial x_j} + \widetilde{h} \frac{\partial \overline{q_j^{cd}}}{\partial x_j}}_{\text{I}} + \underbrace{\overline{h PR} - \widetilde{h} \overline{PR}}_{\text{II}} \\ &+ \underbrace{\widetilde{h} \frac{\partial}{\partial x_j} (\overline{\rho u_j'' h''}) - \frac{\partial}{\partial x_j} (\widetilde{h} \overline{\rho u_j'' h''})}_{\text{III}} \\ &- \frac{1}{2} \frac{\partial}{\partial x_j} (\overline{\rho u_j'' h'' h''}). \end{aligned} \quad (\text{A } 7)$$

With the following simplifications on terms I, II and III,

$$\begin{aligned} \text{I: } -\overline{h} \frac{\partial \overline{q_j^{cd}}}{\partial x_j} + \widetilde{h} \frac{\partial \overline{q_j^{cd}}}{\partial x_j} &= -(\overline{h} + h'') \frac{\partial \overline{q_j^{cd}}}{\partial x_j} + \widetilde{h} \frac{\partial \overline{q_j^{cd}}}{\partial x_j} \\ &= -\overline{h''} \frac{\partial \overline{q_j^{cd}}}{\partial x_j} = -\overline{h''} \frac{\partial \overline{q_j^{cd}}}{\partial x_j} - \overline{h''} \frac{\partial \overline{q_j^{cd'}}}{\partial x_j}, \end{aligned} \quad (\text{A } 8)$$

$$\text{II} : \quad \overline{\tilde{h} P^R} - \widetilde{\overline{h} P^R} = \overline{(\tilde{h} + h'') P^R} - \widetilde{\overline{h} P^R} = \overline{h'' P^R} = \overline{h'' P^R} + \overline{h'' P^{R'}}, \quad (\text{A } 9)$$

$$\text{III} : \quad \tilde{h} \frac{\partial}{\partial x_j} (\overline{\rho u_j'' h''}) - \frac{\partial}{\partial x_j} (\widetilde{\overline{\rho u_j'' h''}}) = -\overline{\rho u_j'' h''} \frac{\partial \tilde{h}}{\partial x_j}, \quad (\text{A } 10)$$

equation (A 7) becomes

$$\begin{aligned} \frac{\partial}{\partial t} \left(\overline{\frac{\tilde{h}''^2}{2}} \right) + \frac{\partial}{\partial x_j} \left(\overline{\rho \tilde{u}_j \frac{\tilde{h}''^2}{2}} \right) &= -\overline{h'' \frac{\partial q_j^{cd'}}{\partial x_j}} + \overline{h'' P^{R'}} - \overline{\rho u_j'' h''} \frac{\partial \tilde{h}}{\partial x_j} \\ &\quad - \frac{1}{2} \frac{\partial}{\partial x_j} \left(\overline{\rho u_j'' h'' h''} \right) + \overline{h''} \left(-\frac{\partial \overline{q_j^{cd}}}{\partial x_j} + \overline{P^R} \right). \end{aligned} \quad (\text{A } 11)$$

For any quantities ψ and ϕ , cross-correlations between Favre and Reynolds fluctuations have the following properties: $\overline{\phi' \psi''} = \overline{\phi' \psi'}$ and $\overline{\phi' \widetilde{\psi''}} = \overline{\phi'' \psi''}$. The first term on the right-hand-side is written as

$$-\overline{h'' \frac{\partial q_j^{cd'}}{\partial x_j}} = -\overline{h' \frac{\partial q_j^{cd'}}{\partial x_j}} = -\frac{\partial}{\partial x_j} (\overline{q_j^{cd'} h'}) + \overline{q_j^{cd'} \frac{\partial h'}{\partial x_j}} \quad (\text{A } 12)$$

Only assuming constant thermodynamic pressure, the general transport equation for the enthalpy rms is therefore given by

$$\begin{aligned} \frac{\partial}{\partial t} \left(\overline{\frac{\tilde{h}''^2}{2}} \right) + \frac{\partial}{\partial x_j} \left(\overline{\rho \tilde{u}_j \frac{\tilde{h}''^2}{2}} \right) &= -\frac{\partial}{\partial x_j} (\overline{q_j^{cd'} h'}) + \overline{q_j^{cd'} \frac{\partial h'}{\partial x_j}} + \overline{h'' P^{R'}} - \overline{\rho u_j'' h''} \frac{\partial \tilde{h}}{\partial x_j} \\ &\quad - \frac{1}{2} \frac{\partial}{\partial x_j} \left(\overline{\rho u_j'' h'' h''} \right) + \overline{h''} \left(-\frac{\partial \overline{q_j^{cd}}}{\partial x_j} + \overline{P^R} \right). \end{aligned} \quad (\text{A } 13)$$

In the investigated channel flow configuration, averaged quantities do not depend on the homogeneous directions X and Z and the left-hand-side is null. The transport equation therefore becomes

$$0 = -\frac{\partial}{\partial y} (\overline{q_y^{cd'} h'}) + \overline{q_y^{cd'} \frac{\partial h'}{\partial x_j}} + \overline{h'' P^{R'}} - \overline{\rho v'' h''} \frac{\partial \tilde{h}}{\partial y} - \frac{1}{2} \frac{\partial}{\partial y} \left(\overline{\rho v'' h'' h''} \right) + \overline{h''} \left(-\frac{\partial \overline{q_y^{cd}}}{\partial y} + \overline{P^R} \right). \quad (\text{A } 14)$$

In the channel flow configuration, equation (A 2) gives

$$-\frac{\partial \overline{q_y^{cd}}}{\partial y} + \overline{P^R} = \frac{\partial}{\partial y} (\overline{\rho v'' h''}).$$

Modifying accordingly the last term in equation (A 14) finally gives equation (3.4) given in section 3.1.2:

$$\boxed{-\frac{\partial}{\partial y} (\overline{q_y^{cd'} h'}) - \frac{1}{2} \frac{\partial}{\partial y} (\overline{\rho v'' h'' h''}) - \overline{\rho v'' h''} \frac{\partial \tilde{h}}{\partial y} + \overline{q_i^{cd'} \frac{\partial h'}{\partial x_i}} + \overline{h'' P^{R'}} + \overline{h''} \frac{\partial}{\partial y} (\overline{\rho v'' h''}) = 0}$$

The transport equation for the quantity $\widetilde{v'' h''}$ is obtained similarly by subtracting the one for \tilde{h} from the transport equation for $\tilde{v} h$. The transport equation of \tilde{v} is given by

$$\frac{\partial}{\partial t} (\overline{\rho \tilde{v}}) + \frac{\partial}{\partial x_j} (\overline{\rho \tilde{u}_j \tilde{v}}) = -\frac{\partial \overline{p}}{\partial y} + \frac{\partial \overline{\tau_{2j}}}{\partial x_j} - \frac{\partial}{\partial x_j} (\overline{\rho u_j'' v''}). \quad (\text{A } 15)$$

By multiplying equation (A 15) by \tilde{h} , equation (A 2) by \tilde{v} and summing them, a transport equation for $\tilde{v}\tilde{h}$ is obtained:

$$\frac{\partial}{\partial t} (\overline{\rho\tilde{v}\tilde{h}}) + \frac{\partial}{\partial x_j} (\overline{\rho\tilde{u}_j\tilde{v}\tilde{h}}) = -\tilde{h} \frac{\partial \overline{p}}{\partial y} + \tilde{h} \frac{\partial \overline{\tau_{2j}}}{\partial x_j} - \tilde{v} \frac{\partial \overline{q_j^{cd}}}{\partial x_j} + \tilde{v} \overline{PR} - \tilde{h} \frac{\partial}{\partial x_j} (\overline{\rho u_j'' v''}) - \tilde{v} \frac{\partial}{\partial x_j} (\overline{\rho u_j'' h''}). \quad (\text{A } 16)$$

Similarly, multiplying the instantaneous transport equation for v by h , multiplying the one for h by v and averaging the sum gives

$$\frac{\partial}{\partial t} (\overline{\rho v h}) + \frac{\partial}{\partial x_j} (\overline{\rho u_j v h}) = -\overline{h} \frac{\partial \overline{p}}{\partial y} + \overline{h} \frac{\partial \overline{\tau_{2j}}}{\partial x_j} - \overline{v} \frac{\partial \overline{q_j^{cd}}}{\partial x_j} + \overline{vPR}, \quad (\text{A } 17)$$

where

$$\overline{\rho v h} = \overline{\tilde{u}_j \tilde{v} h} + \overline{\tilde{h} u_j'' v''} + \overline{\tilde{v} u_j'' h} + \overline{u_j'' v'' h''}. \quad (\text{A } 18)$$

The transport equation for $\tilde{v}\tilde{h}$ can therefore be written as

$$\begin{aligned} \frac{\partial}{\partial t} (\overline{\rho\tilde{v}\tilde{h}}) + \frac{\partial}{\partial x_j} (\overline{\rho\tilde{u}_j\tilde{v}\tilde{h}}) &= -\overline{h} \frac{\partial \overline{p}}{\partial y} + \overline{h} \frac{\partial \overline{\tau_{2j}}}{\partial x_j} - \overline{v} \frac{\partial \overline{q_j^{cd}}}{\partial x_j} + \overline{vPR} \\ &- \frac{\partial}{\partial x_j} (\overline{\rho u_j'' v'' h''}) - \frac{\partial}{\partial x_j} (\overline{\rho u_j'' v'' h}) \frac{\partial}{\partial x_j} - (\overline{\rho u_j'' h'' \tilde{v}}). \end{aligned} \quad (\text{A } 19)$$

Subtracting equation (A 17) from equation (A 19) and carrying out simplifications similar to equations (A 8), (A 9) and (A 10) finally gives the following general transport equation for the turbulent heat flux:

$$\begin{aligned} \frac{\partial}{\partial t} (\overline{\rho v'' h''}) + \frac{\partial}{\partial x_j} (\overline{\rho u_j'' v'' h''}) &= -\overline{h'} \frac{\partial \overline{p'}}{\partial y} + \frac{\partial}{\partial x_j} (\overline{\tau'_{2j} h'}) - \overline{\tau'_{2j}} \frac{\partial \overline{h'}}{\partial x_j} \\ &- \frac{\partial}{\partial x_j} (\overline{q_j^{cd'} v'}) + \overline{q_j^{cd'}} \frac{\partial \overline{v'}}{\partial x_j} + \overline{v'' PR'} - \overline{\rho u_j'' v''} \frac{\partial \overline{h}}{\partial x_j} - \overline{\rho u_j'' h''} \frac{\partial \overline{v}}{\partial x_j} \\ &- \frac{\partial}{\partial x_j} (\overline{\rho u_j'' v'' h''}) + \overline{h''} \left(-\frac{\partial \overline{p}}{\partial y} + \frac{\partial \overline{\tau_{2j}}}{\partial x_j} \right) + \overline{v''} \left(\overline{PR} - \frac{\partial \overline{q_j^{cd}}}{\partial x_j} \right) \end{aligned} \quad (\text{A } 20)$$

In the channel flow configuration, the left-hand-side is null, averaged quantities only depend on the Y direction and $\tilde{v} = 0$. Consequently, equation (A 20) can be simplified to equation (3.8) used in section 3.1.3:

$$\boxed{\begin{aligned} \frac{\partial}{\partial y} (\overline{\tau'_{22} h'} - \overline{q_y^{cd'} v'}) - \frac{\partial}{\partial y} (\overline{\rho v'' v'' h''}) - \overline{\rho v'' v''} \frac{\partial \overline{h}}{\partial y} - \left(\overline{\tau'_{2i}} \frac{\partial \overline{h'}}{\partial x_i} - \overline{q_i^{cd'}} \frac{\partial \overline{v'}}{\partial x_i} \right) \\ + \overline{v'' PR'} - \overline{h'} \frac{\partial \overline{p'}}{\partial y} + \left(\overline{h''} \frac{\partial}{\partial y} (\overline{\rho v'' v''}) + \overline{v''} \frac{\partial}{\partial y} (\overline{\rho v'' h''}) \right) = 0. \end{aligned}} \quad (\text{A } 21)$$

Appendix B. Level of temperature fluctuations in thermal boundary layers

In a turbulent thermal boundary layer, the peak of root-mean-square temperature is located in the buffer layer. The peak value and position have been shown to depend on both Reynolds number and Prandtl number (Kim & Moin 1987; Kawamura *et al.* 1998,

1999; Abe *et al.* 2004). Hence, the maximum temperature rms is

$$T_{\text{rms}}^{\text{max}} = T_{\text{rms}}(y_{\text{BL}}^+(\text{Re}, \text{Pr})) = T_{\text{rms}}^{+, \text{max}}(\text{Re}, \text{Pr}) T_{\tau}, \quad (\text{B } 1)$$

where y_{BL}^+ is the position of the peak and $T_{\text{rms}}^{+, \text{max}}$ is the maximum temperature rms, both in wall units. In air with $\text{Pr} = 0.71$, optimum value of temperature rms in wall units and its position become Reynolds-independent at sufficiently high Reynolds number (Kasagi *et al.* 1992; Kawamura *et al.* 1998, 1999; Kong *et al.* 2000; Abe *et al.* 2004). For air, it is found that $y_{\text{BL}}^+ \approx 12$ and $T_{\text{rms}}^{+, \text{max}} \approx 2.5$.

Common approximations of the friction coefficient and Nusselt number in ducts are

$$c_f = \frac{\bar{\tau}_w}{\rho u_b^2} \approx \alpha \text{Re}^{-0.2}, \quad \text{Nu} = \frac{|\overline{q_w^{cd}}| D_h}{|T_w - T_b| \lambda} \approx \beta \text{Re}^{0.8} \text{Pr}^{0.5} \quad (\text{B } 2)$$

where u_b is the bulk velocity, T_b the bulk temperature, D_h the hydraulic diameter of the duct and $\text{Re} = \rho u_b D_h / \mu$. The constant coefficients are $\alpha = 0.023$ and $\beta = 0.022$ in air. The friction temperature is defined as $T_{\tau} = |\overline{q_w^{cd}}| / (\rho c_p u_{\tau})$ where

$$u_{\tau} = \left(\frac{\bar{\tau}_w}{\rho} \right)^{1/2} = u_b c_f^{1/2} \quad \text{and} \quad |\overline{q_w^{cd}}| = \frac{\text{Nu} |T_w - T_b| \lambda}{D_h}. \quad (\text{B } 3)$$

Introducing the friction coefficient and Nusselt number formulas in equation (B 2), the friction temperature is written as

$$T_{\tau} = \alpha^{-0.5} \beta \text{Re}^{-0.1} \text{Pr}^{-0.5} |T_w - T_b|. \quad (\text{B } 4)$$

As the friction velocity u_{τ} increases faster with the Reynolds number than the conductive heat flux, the friction temperature decreases with the Reynolds number and so is the maximum temperature rms. The relative variation of temperature is

$$\frac{T_{\text{rms}}^{\text{max}}}{\bar{T}(y_{\text{BL}}^+)} = \frac{T_{\text{rms}}^{+, \text{max}}(\text{Re}, \text{Pr})}{\text{sign}(T_b - T_w) \bar{T}^+(y_{\text{BL}}^+(\text{Re}, \text{Pr})) + \frac{T_w}{T_{\tau}}}. \quad (\text{B } 5)$$

Introducing equation (B 4), it is found that

$$\frac{T_{\text{rms}}^{\text{max}}}{\bar{T}(y_{\text{BL}}^+)} = \frac{T_{\text{rms}}^{+, \text{max}}(\text{Re}, \text{Pr})}{\text{sign}(T_b/T_w - 1) \bar{T}^+(y_{\text{BL}}^+(\text{Re}, \text{Pr})) + \alpha^{0.5} \beta^{-1} \text{Re}^{0.1} \text{Pr}^{0.5} |T_b/T_w - 1|^{-1}}. \quad (\text{B } 6)$$

Finally, in air, the following result is obtained for the relative variation of temperature:

$$\frac{T_{\text{rms}}^{\text{max}}}{\bar{T}(y_{\text{BL}}^+)} = \frac{2.5}{6.9 \text{sign}(T_b/T_w - 1) + 5.8 \text{Re}^{0.1} |T_b/T_w - 1|^{-1}}, \quad (\text{B } 7)$$

where $\bar{T}^+(y_{\text{BL}}^+ = 12) \approx 6.9$ is calculated from the formula proposed by Kader (1981). Equation (B 7) is plotted in figure 29 for several values of the ratio T_b/T_w which is less (resp. greater) than unity in heating (resp. cooling) systems. The level of temperature fluctuations decreases with the Reynolds number in all cases and is larger in strongly heating and cooling systems. Using equation (B 7), the estimated levels of fluctuations in cases without radiation A, B and C are 1.4%, 4.8% and 1.3% on the hot side, and 1.6%, 7.3% and 1.5% on the hot side, respectively. These numbers match fairly the results obtained in numerical simulations. Given the trends observed in figure 29, fluctuations of temperature can be expected to remain below 30% in most turbulent boundary layers in gaseous flows. Compressibility effects and viscous heating have here been neglected.

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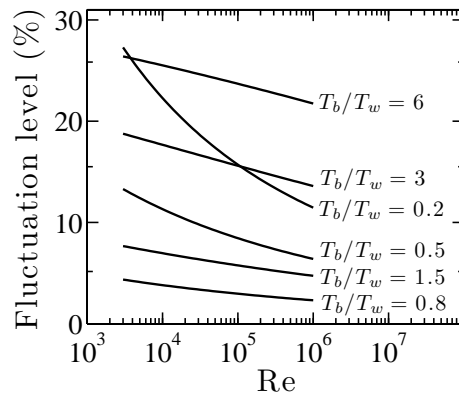


FIGURE 29. Relative variation of temperature $T_{\text{rms}}^{\text{max}}/T(y_{\text{BL}}^+)$ as a function of the Reynolds number for several values of T_b/T_w .

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