

# A review on dark fermentative biohydrogen production from organic biomass: Process parameters and use of by-products

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# ▶ To cite this version:

Anish Ghimire, Luigi Frunzo, Francesco Pirozzi, Eric Trably, Renaud Escudié, et al.. A review on dark fermentative biohydrogen production from organic biomass: Process parameters and use of by-products. Applied Energy, 2015, 144, pp.73-95. 10.1016/j.apenergy.2015.01.045 . hal-01164829

# HAL Id: hal-01164829 https://hal.science/hal-01164829

Submitted on 7 Aug 2023  $\,$ 

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1	A review of dark fermentative biohydrogen production from organic biomass: process
2	parameters and use of by-products
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#### 15 Abstract

16 Dark fermentation of organic biomass, i.e. agricultural residues, agro-industrial wastes and 17 organic municipal waste is a promising technology for producing renewable biohydrogen. In spite of its future potential, this technology needs further research and development to improve 18 19 the biohydrogen yield by optimizing substrate utilization, microbial community enrichment and 20 bioreactor operational parameters such as pH, temperature and H<sub>2</sub> partial pressure. On the other 21 hand, the technical and economic viability of the processes need to be enhanced by the use of 22 valuable by-products from dark fermentation, which mostly includes volatile fatty acids. This 23 paper reviews a range of different organic biomasses and their biohydrogen potential from 24 laboratory to pilot-scale systems. A review of the advances in H<sub>2</sub> yield and production rates 25 through different seed inocula enrichment methods, bioreactor design modifications and 26 operational conditions optimization inside the dark fermentation bioreactor is presented. The 27 prospects of valorizing the co-produced volatile fatty acids in photofermentation and bioelectrochemical systems for further H<sub>2</sub> production, methane generation and other useful 28 29 applications have been highlighted. A brief review on the simulation and modeling of the dark 30 fermentation processes and their energy balance has been provided. Future prospects of solid 31 state dark fermentation are discussed.

32

33 Keywords: Biofuels, biohydrogen, dark fermentation, H<sub>2</sub> yield, biomass valorization,

34 fermentation metabolites

#### 35 **1. Introduction**

Environmental friendly energy carriers and sources are the most highlighted topic in the energy and environmental sector. The current global energy demand is mostly dependent on reserves of fossil fuels, which are depleting, and the world is facing severe pollution problems from the byproducts of fossil fuels uses [1]. The scientific community has widely accepted the fact that the increasing  $CO_2$  level due to the use of fossil resources is impacting the greenhouse gas effect and global warming. Therefore, different ways to harness the energy from clean renewable sources are being developed but the search for reliable energy sources is still on.

43 In the past years, the research and development interests have been directed towards renewable 44 energy technologies like the anaerobic digestion (AD) of organic biomass and waste. For 45 alternative energy carrier, hydrogen could be a fuel of the future because of its high energy 46 content, environmental friendliness of production, and also because it can give substantial social, 47 economic and environmental credentials [2]. Hydrogen is a carbon-free clean fuel, as the final 48 by-product of its combustion is only water [2]. Hydrogen can also be helpful in addressing global 49 warming and increasing pollution problems. Furthermore, it is preferred over methane owing to 50 its wider industrial applications, i.e. H<sub>2</sub> is used in the synthesis of ammonia and hydrogenation of 51 edible oil, petroleum, coal and shale oil [3]. Hydrogen can be directly used either in combustion 52 engines because of its highest energy per unit weight, i.e. 143 GJ per ton [2] among known 53 gaseous biofuels or to produce electricity via fuel cell technologies [4]. Thus, the creation of a 54 hydrogen economy which incorporates the production and use of hydrogen as an energy carrier 55 could in the future lead to sustainable energy systems [1,5].

The major challenge in the use of this promising energy carrier lies in its sustainable production and storage. In commercial applications, hydrogen has been produced from natural gas (48%) and oil (30%) by steam reforming processes, and also by other industrial methods such as coal gasification (18%) and water electrolysis (4%) [6]. However, these processes are highly energy intensive and use non-renewable sources of energy which makes them less attractive from an environmental point of view. In order to produce a cleaner and more sustainable fuel, the hydrogen should come from processes that could avoid or minimize  $CO_2$  emissions.

Hydrogen can be produced from biological processes which are less energy intensive and more
environmental friendly in terms of global reduction of CO<sub>2</sub>. These renewable biohydrogen

65 producing technologies have potential to become cost competitive as they can use low value

- 66 waste biomass as feedstock [2], e.g. municipal, agricultural and industrial organic and
- 67 wastewater. Biohydrogen can be produced by both autotrophic and heterotrophic
- 68 microorganisms (Fig. 1) [7]. In autotrophic conversions (also known as direct or indirect
- 69 biophotolysis), solar energy is directly converted to hydrogen via photosynthetic reactions
- 70 mediated by photosynthetic microorganisms, i.e. microalgae, protists and photosynthetic
- 71 bacteria. Under heterotrophic conditions, the organic substrates are transformed into simpler
- 72 organic compounds with simultaneous production of molecular hydrogen [7,8]. There are two
- 73 types of heterotrophic conversions, photo-fermentation carried out by photosynthetic bacteria
- 74 and dark fermentation (DF) carried out by anaerobic bacteria that convert carbohydrates into
- 75 biohydrogen.



76 77

Fig. 1. Biological pathways to produce hydrogen

79 DF is the most studied and promising technology for biohydrogen production owing to its higher

- 80 production rates and treatment capacity for organic waste. Several substrates rich in
- 81 carbohydrates are also usable, such as first generation fuel crops (e.g. sugar cane, wheat, corn,

82 and sugar beets) as well as second generation biomass like agricultural residues and industrial

83 waste and wastewater [7]. In recent years, there are still increasing research activities in this

- 84 domain, as shown by the increasing number of peer-reviewed articles with "dark fermentation"
- 85 in the title (Fig. 2).





Fig. 2. Number of peer reviewed publications on DF published in the last decade [9,10]

88

89 At present, DF process development at industrial scale is limited by its lower hydrogen yield 90 compared to its theoretical maximum yield of 4 moles of  $H_2$  per moles of hexose, as well as the 91 estimated costs associated with the  $H_2$  production. There are areas for improvement to achieve higher H<sub>2</sub> vields and production rates by optimizing the design and operation of DF bioreactors 92 93 [11]. The  $H_2$  production cost in scaled-up systems can be minimized by using low cost renewable 94 materials such as waste biomass as feedstock [12,13]. Inoculum enrichment methods [8,14–17] 95 can improve the  $H_2$  yield, and pre-treatment of substrates can also enhance the biohydrogen 96 production by improving the biodegradability of substrates [18–20]. Recently, there has been 97 growing interest on coupled processes to obtain a higher H<sub>2</sub> yield by integrating DF with

98 processes like photofermentation (PF) [21,22] or bioelectrochemical systems [23–25]. Because 99 of the profitable production of biomethane, a coupled DF-methanogenic stage has also been a 100 popular choice which increases the sustainability of the coupled-process by improving the energy 101 recovery from DF residues [26–28].

102 The aim of this paper is to provide an updated overview of advancements in biohydrogen 103 production via DF of organic biomass. Regardless of the increasing number of research articles 104 and reviews published, there is a need to provide an extended overview of dark fermentative 105 biohydrogen production with the utilization of by-products and the future challenges and 106 prospects for its up-scaled development. This review provides an insight on the factors that 107 influence the biochemical pathways in dark fermentative biohydrogen production to increase the 108 H<sub>2</sub> yield and post-utilization of DF residues to realize its future sustainability. To summarize, this 109 review provides an extended insight on a) possible feedstock or substrate sources and their 110 biohydrogen potential (BHP), b) factors that influence the fermentative  $H_2$  yield: (i) inoculum 111 sources and enrichment methods, (ii) pre-treatment of substrates and (iii) bioreactor operation 112 and design (culture pH, temperature and OLR, HRT,  $H_2$  partial pressure, nutrients and elements 113 addition), c) utilization of DF residues, d) pilot scale systems and e) challenges and future 114 prospects: (i) modeling and simulation of DF process, (ii) energy balance and conversion of 115 organic carbon, (iii) natural pH control and (iv) future prospects of solid state dark fermentation.

#### 116 2. Microbiology and biochemical pathways of DF

In DF processes, carbohydrate-rich substrates are broken down anaerobically by hydrogenproducing microorganisms, such as facultative anaerobes and obligate anaerobes. Molecular hydrogen (H<sub>2</sub>) is produced in the process of disposing the excess electrons through the activity of the hydrogenase enzyme [8,29]. Under anaerobic environments, protons (H<sup>+</sup>) can act as electron acceptors to neutralize the electrons generated by oxidation of organic substrates, consequently producing H<sub>2</sub>. In contrast with aerobic respiration, where oxygen is reduced and water is the final product [7,30].

- 124 In the DF of glucose as the model substrate, H<sub>2</sub> -producing bacteria initially convert glucose to
- 125 pyruvate through glycolytic pathways producing adenosine triphosphate (ATP) from adenosine
- 126 diphosphate (ADP) and the reduced form of nicotinamide adenine dinucleotide (NADH) [8].

- 127 Pyruvate is further oxidized to acetyl coenzyme A (acetyl-CoA), carbon dioxide (CO<sub>2</sub>) and H<sub>2</sub> by
- 128 pyruvate ferredoxin oxidoreductase and hydrogenase. Depending on the type of microorganism
- 129 and environmental conditions, pyruvate may also be converted to acetyl-CoA and formate which
- 130 may be further converted into H<sub>2</sub> and CO<sub>2</sub>. Also, acetyl-CoA might be converted to acetate,
- butyrate, and ethanol [8]. DF of complex carbohydrates by mixed anaerobic microbiota can
- result in a wide range of intermediates and by-products depending on the operational parameters,
- 133 such as substrate type, substrate loading rate, pH, temperature and other operating and
- 134 environmental conditions, as they also influence the microbial community structure in
- 135 bioreactors. A representative biochemical pathway for DF of complex organic biomass is
- 136 presented in Fig. 3.



Fig. 3. Microbiological pathway of fermentative waste biomass degradation (Adapted and
 modified from [31])

140

- 141 These biochemical pathways (Fig. 3) can be mediated by strict anaerobes (*Clostridia*,
- 142 methylotrophs, rumen bacteria, methanogenic bacteria, archea, etc.), facultative anaerobes
- 143 (Escherichia coli, Enterobacter, Citrobacter), and even aerobes (Alcaligenes, Bacillus) [8].

Acetate and butyrate are the most common products of DF [32]. Common biochemical reactionsduring DF undertaken by facultative anaerobes are the following:

146 
$$C_6H_{12}O_6 + 2H_2O \rightarrow 2CH_3COOH + 2CO_2 + 4H_2$$
 (1)

(Acetic Acid)

148  $C_6H_{12}O_6 \rightarrow CH_3CH_2CH_2COOH + 2CO_2 + 2H_2$  (2)

149

150

147

(Butyric Acid)

151 stoichiometric yield of  $H_2$  is 4 moles for each mole of glucose (i.e. 544 mL  $H_2$ /g hexose at 25 °C)

152 as seen in equation 1, whereas the yield of  $H_2$  is 2 moles for a mole of glucose (i.e. 272 mL  $H_2/g$ 

153 hexose at 25 °C) when the final product is butyric acid (equation 2). However, the actual

154 hydrogen yield is lower than the theoretical yield as part of the substrate is utilized for biomass

production and the degradation of the substrates might follow other biochemical pathways

without hydrogen production [33,34]. Under some conditions, the metabolic pathways lead to
ethanol and acetate production, lowering the stoichiometric hydrogen yield to 2 moles of H<sub>2</sub> for a

mole of glucose (i.e. 272 mL  $H_2/g$  hexose at 25 °C) as represented in equation 3 [8]:

159 
$$C_6H_{12}O_6 + 2H_2O \rightarrow CH_3CH_2OH + CH_3COOH + 2CO_2 + 2H_2$$
(3)

A widely studied clostridia species, *Clostridium butyricum*, is responsible for the production of butyric acid as a major product of fermentation together with acetate and hydrogen [32]. Another fermentation pathway is the production of propionate by *Clostridium articum* which is a hydrogen consuming pathway (equation 4). Similarly, metabolic pathways leading to only ethanol and lactic acid production by *Clostridium barkeri* yield no hydrogen (equations 5 and 6) [35]:

166	$C_6H_{12}O_6 + 2H_2 \rightarrow 2CH_3CH_2COOH + 2H_2O$	(4)
167	$C_6H_{12}O_6 \rightarrow 2CH_3CH_2OH + 2CO_2$	(5)
168	$C_6H_{12}O_6 \rightarrow CH_3CHOHCOOH + 2CO_2$	(6)

Hawkes [32] and Kim [36] proposed the molar ratio of butyric to acetic acid (B/A ratio) as a
quantitative indicator to biohydrogen yield associated with microbial metabolic pathways. Kim
et al. [36] found that B/A ratios were directly proportional to H<sub>2</sub> yields (mol H<sub>2</sub>/mol hexose
consumed) during DF of sucrose in CSTR reactors operated at an organic loading rate (OLR) of

- 173 10.60 g Chemical Oxygen Demand (COD)/L, pH 5.5 and 12 h hydraulic retention time (HRT).
- 174 They also reported that a B/A ratio higher than 2.6 indicated an efficient H<sub>2</sub> production by
- anaerobic microbiota. In DF with mixed cultures, a B/A ratio of 3:2 is generally observed,
- 176 resulting in a H<sub>2</sub> yield of 2.5 moles H<sub>2</sub> per mole of hexose fermented as given in equation 7 [32]:

177  $4C_6H_{12}O_6 + 2H_2O \rightarrow 3CH_3CH_2CH_2COOH + 2CH_3COOH + 8CO_2 + 10H_2$  (7)

178 In contrast, Guo et al. [37] showed in their study performed with lignocellulosic substrates that

- this ratio might not give a good indication, particularly in batch tests where homoacetogenic
- 180 activity prevails. Therefore, higher acetate concentrations cannot always give an indication of a
- 181 higher H<sub>2</sub> yield. Some homoacetogens belonging to the genus *Clostridium* (e.g. *C. aceticum*) can
- 182 lower the H<sub>2</sub> yield by converting H<sub>2</sub> and CO<sub>2</sub> to acetate or can convert hexose directly to acetate
- 183 [32,36]. However, analysis of soluble metabolites can give an indication of the fermentation
- 184 pathways and thus the H<sub>2</sub> production performance.
- 185 Clostridia have been identified as the dominant hydrogen producing microorganisms in DF
  186 operated with mesophilic mixed cultures at a pH of 5.5 [38]. Fang and Zhang [38] identified that
  187 64.6% of all the microorganisms were affiliated with three *Clostridium* species (*Clostridiaceae*),
- 188 18.8% with Enterobacteriaceae, and 3.1% with Streptococcus bovis (Streptococcaceae) based
- 189 on the phylogenetic analysis of the rDNA sequences. Interestingly, Rafrafi et al. [39] reported
- 190 recently that sub-dominant species, in spite of their low abundance, can also have substantial
- 191 impact on the hydrogen production performance. The presence of some species like *E. coli* can
- aid in increasing the H<sub>2</sub> yield by diverting the metabolic pathways to acetate and butyrate
- 193 hydrogen producing pathways (equation 7), while some communities such as *Bacillus spp.* and
- 194 *Lactobacillus spp.* can lower the H<sub>2</sub> yield by diverting the pathway to lactate accumulation
- 195 (equation 6).
- 196 Other results of the identification of the microbial diversity by community fingerprinting
- 197 techniques in the thermophilic DF of rice straw showed that hydrolytic and fermentative bacteria
- 198 such as *Clostridium pasteurianum*, *Clostridium stercorarium and Thermoanaerobacterium*
- 199 *saccharolyticum* dominated in the sludge of a repeated fed-batch reactor [40]. Shin et al. [41]
- 200 detected the hydrogen producing microorganisms *Thermoanaerobacterium*
- 201 thermosaccharolytium and Desulfotomaculum geothermicum in a thermophilic acidogenic
- 202 culture, while *Thermotogales* strains and *Bacillus* species were detected in a mesophilic

- 203 acidogenic culture by Polymerase Chain Reaction (PCR)-Denaturing Gradient Gel
- 204 Electrophoresis (DDGE) analysis during DF of food waste. In another study, Quemeneur et al.
- 205 [42] investigated the potential of a molecular capillary electrophoresis-single strand
- 206 conformation polymorphism (CE-SSCP) fingerprinting method based on the *hydA* functional
- 207 genes to better describe the bacterial community dynamics in a mixed dark fermentative culture

at different pH conditions.

209 Some undesirable microorganisms which lower the total  $H_2$  yield might be present in mixed 210 cultures of fermentative microorganisms, either by consuming the H<sub>2</sub> produced or by altering the 211 biochemical pathways of the  $H_2$  synthesis [8]. The main  $H_2$  consumers include methanogens, 212 homoacetogenic bacteria and sulfate reducing bacteria (SRB). The activity of these hydrogen 213 consumers can be controlled by inoculum pre-treatment methods and bioreactor operating 214 conditions [30,43]. The activity of methanogens and SRB can be significantly inhibited by 215 operating at a pH below 6 along with the control of the HRT and OLR. Therefore, hydrogen 216 production via a mixed dark fermentative culture is a complex system, influenced by a number of 217 parameters such as substrate types, substrate pretreatment, inoculum type, inoculum enrichment 218 method, bioreactor design and operation.

#### 219 **3.** Potential sources of organic biomass for fermentative biohydrogen production

220 The substrate plays an important role in the H<sub>2</sub> yield, H<sub>2</sub> production rate and the overall economy 221 of the process. These are mainly dependent on the substrate's carbohydrate content, 222 biodegradation rate and bioavailability [12,13,16,43,44]. Carbohydrate rich substrates have been 223 extensively used in DF studies, in particular pure glucose, sucrose and starch mixtures [30]. But 224 renewable biohydrogen production requires the substrate or feedstock to come from renewable 225 resources [12,32]. Second generation biomass sources, such as waste biomass, are abundant and 226 thus can fulfill the promise for the supply of renewable substrates [13,14,43]. Besides 227 biohydrogen and volatile fatty acids as valuable by-products, DF also offers biological treatment 228 of the organic waste.

- 229 In more recent dark fermentative studies, complex substrates have been considered, such as the
- 230 organic fraction of municipal solid waste (OFMSW) [40,45–48], agricultural residues like
- 231 lignocellulosic biomasses (e.g. rice straw, wheat straw and corn stalks), agro-industrial wastes

- like those from food processing industries (e.g. olive mill wastewater and cheese whey),
- effluents from livestock farms and aquatic plants [13,14]. With the integration of DF within a
- biorefinery concept, the waste generated from biofuel production such as crude glycerol [25,49],
- 235 de-oiled algal cake [50], cotton seed cake [51] can be utilized as a substrate, while dark
- fermentative metabolites can be utilized in the production of micro-algal biomass [52–54] and
- biodiesel [55], which in turn can be serve as feedstock for DF processes.
- 238 Based on their availability, novel low-cost substrate sources need to be explored and assessed for 239 their biohydrogen potential (BHP). Table 2 presents the biohydrogen production potential of 240 different organic biomasses by dark fermentative process. The fermentation pathways depend on 241 substrates and on microbial metabolism [8]. It has been well established that the type of substrate 242 influences biohydrogen yields [37,56]. Monlau [57] and Guo [37] in their studies reported that 243 the soluble and readily accessible sugars represent the main fraction of biomass that can be 244 converted into hydrogen. However, the biohydrogen production also depends on a number of 245 parameters such as inoculum type and enrichment methods, bioreactor design and operation 246 conditions. The latter are covered in the next sections.

#### 247 **3.1 Agricultural residues**

248 Agricultural residues, which mainly include lignocellulosic wastes, are an economically viable 249 and renewable source of second generation carbon neutral biofuels [58]. These include plant 250 biomass waste, which generally contains cellulose, hemicellulose and lignin formed as products 251 of photosynthesis. Agricultural residues are produced when economically valuable products of 252 the crops are harvested and the residues such as straw, stover, peelings, cobs stalks, bagasse and 253 others are left over [58]. The 2010 global annual production of agricultural residues was around 254 5.1 billion dry tonnes [59]. The waste generated by the agricultural, forestry and aquaculture 255 sectors is increasing with the increasing population and thus the waste from this sector will be 256 increasing further in future. Guo et al. [43] have reported the potentials and challenges of 257 agricultural wastes as substrates for biohydrogen production. Examples of agricultural residues 258 as a potential feedstock sources for DF processes and recent advancements in their application 259 are discussed below.

#### 260 **3.1.1 Lignocellulosic waste**

261 Rice straw is an example of a typical agricultural residue. It is the world's third largest

agricultural residue, after maize and wheat, with a reported global yearly production of

approximately 916 million tons in 2009 [60]. Thus, the use of this abundant biomass as a

264 feedstock in dark fermentative hydrogen production might hold future potential for feedstock

supply. Similarly, wheat straw, barley straw, corn stalk, corn cobs and others could be potential

266 DF feedstock. The cellulose and hemicellulose part of these wastes can be hydrolyzed into

267 carbohydrates which are further biologically converted to organic acids and biohydrogen in DF

268 processes (Table 1). The composition of typical crop residues in terms of cellulose,

269 hemicellulose and lignin content is presented in Table 1.

### 270 **Table 1**

### 271 Composition of typical agricultural waste (% of dry matter)

Component	Rice straw <sup>a</sup> (%)	Wheat straw <sup>b</sup> (%)	Barley straw <sup>b</sup> (%)	Corn stalk <sup>b</sup> (%)	Corn cob <sup>b</sup> (%)
Cellulose	38.6	35.4	37.2	36.7	35.3
Hemicellulose	19.7	24.6	24.4	26.2	37.1
Lignin	13.6	17.7 <sup>c</sup>	16.1 <sup>c</sup>	16.9 <sup>c</sup>	16.4 <sup>c</sup>
Ash	-	6.9	6.4	4.1	1.5

<sup>a</sup> Data obtained from [61]; <sup>b</sup> Data obtained from [62]; <sup>c</sup> Acid insoluble lignin

273 The main limitation in the utilization of these valuable resources lies in the complex structure of

274 lignocellulosic materials: a cross-linking between polysaccharides (cellulose and hemicellulose)

and lignin via ester and ether linkages, which decreases their biodegradability [58,63–65].

Therefore, prior to DF, these biomasses are often subjected to physical, chemical and biological

pre-treatment to increase their digestibility [58,63–69].

### 278 **3.1.2 Livestock waste (manure)**

279 Livestock wastes include solid animal manure waste, fodder waste (which generally contains a

280 lignocellulosic fraction) and wastewater which includes urine and feces. A large quantity of

281 livestock manure comes from cattle feedlots, poultry and swine buildings, identified as pollution

282 sources, which pose threats to the atmospheric and water environment [70]. The current practices 283 of management of livestock waste include its application in agricultural fields as well as 284 biological stabilization or treatment such as composting and AD. The first management practice 285 contributes in uncontrolled greenhouse gas emissions (mainly CH<sub>4</sub>) from land applications. 286 Manure management practices can reduce direct and indirect greenhouse gas emissions by 287 generating energy in the form of biogas from the manure prior to its land application [70-72]. 288 However, manure substrates need physical and chemical treatment to inhibit the methanogenic 289 activity that consumes  $H_2$  [71,73]. Another, problem that might occur during the use of this 290 feedstock type is the inhibition of the biohydrogen production by ammonia as their high nitrogen 291 content might cause failure of the bioreactor: swine, poultry and dairy manure have a low C/N 292 ratio (C/N ratio of swine manure: 12.8) [74] and higher levels of ammoniacal nitrogen (cattle 293 slurry: 1040 -1925 mg/l and chicken manure 7000 - 12,800 mg/L) [75]. Salerno et al. [76] 294 reported that hydrogen production is possible at high concentrations up to 7.8 g N/L in 295 continuous flow systems if the microbial culture initially acclimated to a lower ammonia 296 concentration of 0.8 g N/L. total ammonia) However, the biohydrogen production decreases 297 when the total ammonia concentration would be increased to above 2 g N/L, which was in 298 agreement with the studies of Cavinato et al. [77]. Also, high sulfate concentrations in swine 299 manure can inhibit biohydrogen production due to the presence of hydrogen consuming sulfate 300 reducers [43].

Because of the high nitrogen content of animal manure, it can be used as a co-digestion substrate
for nitrogen supplementation of other agricultural residues to maintain a suitable carbon to
nitrogen ratio. Wu et al. [71] reported a H<sub>2</sub> yield of 1.18 and 1.63 mol H<sub>2</sub>/mol glucose in a
fermentation of swine manure supplemented with glucose. Xing et al. [72] achieved an enhanced
H<sub>2</sub> yield of 31.5 ml/g Volatile Solids (VS) with acidification pretreated dairy manures while
treating 70 g/L of substrate at operating pH 5.0.

#### 307 **3.2 Industrial waste**

308 Agro-industries waste such as palm oil mill wastewater [78–81] and olive mill wastewater

- 309 (OMWW) [82,83], tapioca industries and food industries such as brewery and dairy industries
- 310 [84–87] produce large quantities of carbohydrate rich non-toxic waste in the form of solid waste

311 and wastewater. It can be potential substrates for dark fermentative biohydrogen production. Ren

- et al. [88] demonstrated that waste molasses are an excellent substrate in a pilot scale system
- 313 operated under mesophilic conditions (35  $^{\circ}$ C) where very good results were obtained in terms of
- H<sub>2</sub> production rate (232 mL  $H_2/L/h$ ) and yield (5.016 mol  $H_2/mol$  glucose equivalent). The
- 315 production of large quantities of this type of waste biomass supports its utilization in up-scaled
- 316 DF systems for continuous biohydrogen production. Similarly, cheese whey, a waste by-product
- 317 generated from cheese manufacturing industries and characterized by high organic loads,
- 318 comprising mainly carbohydrates (lactose), protein and lipids, is a very good potential substrate
- 319 for biohydrogen production [24,89,90].

#### 320 **3.3 Organic fraction of municipal waste (OFMSW)**

321 OFMSW generally constitutes food waste which contains a high biodegradable carbohydrates 322 fraction with 85-95% volatile solids and 75-85% moisture content making it a good substrate for 323 DF [43]. Food waste present in municipal waste is mainly responsible for methane emissions and 324 leachate production from landfills [91]. AD has been proposed as the most suitable treatment 325 option for OFMSW or food waste with energy recovery and other environmental credentials 326 [92]. Thus, food waste has been used extensively in DF experiments [41,77,93–95]. Gioannis et 327 al. [17] have reviewed the studies of DF processes utilizing OFMW or food waste for dark 328 fermentative biohydrogen production.

- 329 Large quantities of waste biosolids or sludge are generated from municipal wastewater treatment
- 330 plants which generally contain carbohydrates or polysaccharides and proteins [96]. Several
- 331 researchers have used the available carbohydrates present in these biosolids in fermentative
- hydrogen production [97,98]. However, the sludge needs pre-treatment, such as ultrasonication,
- acidification, sterilization, freezing-thawing or alkaline pre-treatment, to facilitate the
- fermentative process [96,98]. Besides, Kim et al. [97] demonstrated the usefulness of sewage
- sludge as co-substrate in the DF of food waste.

# **Table 2.**

227	$D_{1}C_{1}C_{1}C_{1}C_{1}C_{1}C_{1}C_{1}C$		. 1 .	1	•	1
<b>44</b> /	Ligrk termentative biobydrogen	notential of different	waste hiomass	under vorv	ing onergting	conditione
557			wasie biomass	unuer varv	me operanne	conditions
					0 0	

Substrate type	Microbial inoculum source	Reactor type	Temperature (°C)	рН	Maximum assessed H <sub>2</sub> yield (mL H <sub>2</sub> /g VS)	Maximum H <sub>2</sub> production rate	H <sub>2</sub> in biogas (%)	Reference
Food waste	Heat shock treated anaerobic sludge	Leaching Bed Reactor	37	-	310	91 L H <sub>2</sub> /L/h	10 - 55	[99]
Food waste	Thermophilic acidogenic culture	Batch	55	4.5	46.3	3 mL H <sub>2</sub> /g VS/h	23	[41]
Vegetable kitchen waste	Kitchen waste compost	Intermittent- CSTR	55	6.0	1.7 mmol H <sub>2/</sub> g COD	$1.0 L H_2 / L/d$	40	[100]
Food waste and sewage sludge	Anaerobic digester sludge	Batch	35	5.0-6.0	122.9 <sup>a</sup>	111:2 mL H <sub>2</sub> /g VSS/h	-	[97]
OFMSW	Anaerobic digestate	Semi- continuous CSTR	55	6.4	360	-	58	[45]
OFMSW	Non-anaerobic inocula (soil, pig excreta)	Packed bed reactor	38	5.6	99	-	47	[101]
Wheat straw	Cow dung compost	Batch	36	6.5	68.1	-	52	[102]
Rice straw	Wastewater treatment plant sludge	Batch CSTR	55	6.5 (initial)	24.8 mL/g TS	-	-	[40]

Corn stalk wastes with acidification pre-treatment	Enriched cow dung composts	Batch CSTR	55	5.5	149.69	7.6 mL H <sub>2</sub> /h	45–56	[46]
Rice slurry (5.5 g carbohydrate/L)	Anaerobic digester sludge	Batch	37	4.5 (initial)	346 <sup>b</sup>	2.1 L/g VS/d	45–56	[103]
Cheese whey	Adapted anaerobic sludge	Batch	55	-	111°	3.46 mL H <sub>2</sub> / L/h	-	[104]
Pig slurry	Mesophilic methanogenic sludge	CSTR	70	-	3.65	-	-	[105]
De-oiled algae cake	Anaerobic digester sludge	Batch	29 2	6 (initial)	66	0.08 ml/h	-	[50]

<sup>a</sup> mL H<sub>2</sub>/g carbohydrate COD, <sup>b</sup> mL H<sub>2</sub>/g carbohydrate, <sup>c</sup> mL H<sub>2</sub>/g total sugar, <sup>d</sup> mL H<sub>2</sub>/g algal biomass

### 339 4. Factors affecting DF pathways and H<sub>2</sub> yield

340 DF via mixed cultures is a complex system where environmental factors and bioreactor

341 operation conditions such as temperature, pH and H<sub>2</sub> partial pressure regulate metabolic

pathways of hydrogen producing microorganisms [8,30,43,106]. In addition, substrate types

343 and their pre-treatment methods, bioreactors configurations, inoculum sources and

- 344 enrichments also influence the biohydrogen production. Three categories of parameters that
- influence the DF pathways, and thus the yield of biohydrogen, can be distinguished (Fig. 4).
- 346 These parameters are reviewed below and compared in relation to H<sub>2</sub> yield and production
- 347 rate.



348

350

349

Fig. 4. Strategies to enhance the biohydrogen yield in DF of organic biomass

550

## 351 **4.1 Inoculum and enrichment methods**

352 The hydrogen producing seed inoculum or culture is very important for the startup of the

353 hydrogen production process. Several studies using pure cultures have been done using a

- 354 range of substrates (Table 3). Various species of *Clostridia* and *Enterobacter* are widely used
- in pure cultures (Table 3). Lee and Show [107] and Elsharnouby et al. [108] have reviewed
- the studies of DF performed with pure cultures. Table 3 presents some of the dark

357 fermentative biohydrogen studies done with pure cultures.

- 358
- 359

Culture	Substrate	Culture type	Temp. (°C)	рН	Optimum H <sub>2</sub> yield (mol H <sub>2</sub> /mol glucose eqv.) <sup>a</sup>	Reference
Enterobacter cloacae IIT-BT08	Glucose	Batch	36	6	2.2	[109]
Clostridium thermolacticum DSM 2910	Lactose	Continuous	58	7	1.5	[110]
Enterobacter cloacae DM 11	Malt, yeast extract & glucose	Continuous	37	6	3.9	[111]
<i>Caldicellulosiruptor</i> <i>saccharolyticus</i> DSM 8903	Hydrolyzed potato steam peels	Batch	70	6.9	3.4	[112]
Thermotoga neapolitana DSM 4349	Hydrolyzed potato steam peels	Batch	80	6.9	3.3	[112]
C. thermocellum DSM 1237and C. thermopalmarium DSM 5974	Cellulose	Batch	55	7	1.36	[113]
Clostridium thermocellum 7072	Corn stalk	Continuous (100 Liters)	55	7.2	0.45	[114]

361 Biohydrogen production studies using pure culture

<sup>a</sup> mol H<sub>2</sub>/mol glucose equivalent was calculated based on the information provided from

363 references at Standard Temperature and Pressure (STP) (0<sup>o</sup>C and Pressure 1 atm)

364

365 H<sub>2</sub> synthesizing bacteria exist commonly in environments such as soil, wastewater sludge and 366 compost. All these materials can thus be used as an inoculum for fermentative H<sub>2</sub> production [8]. Indeed, cow dung, anaerobic sludge, municipal solid waste, soil and compost are some of 367 the common sources of mixed cultures. A mixed culture of hydrogen producers is generally 368 369 preferred over a pure culture due to its practicability for environmental engineering 370 applications, economic benefits in operation (as it can economize asepsis costs), easiness in 371 control based on differential kinetics of microbial subgroups and broader feedstock choice [8,30,45]. However, enrichment of mixed cultures becomes necessary to enhance the 372 373 biohydrogen production on the one hand and inhibit hydrogen consumers such as

- 374 methanogens and homoacetogens on the other hand, as other trophic groups that readily
- 375 consume the produced hydrogen, such as *Clostridium* and *Enterobacter*, are often present in376 these mixed inocula [30].

Pre-treatment of the inoculum to obtain an enrichment of hydrogen producers often relies on
the spore forming characteristics of H<sub>2</sub> producers such as *Clostridium*, which is ubiquitous in
anaerobic sludge and sediments [8,84,115,116]. These organisms have a better chance to
survive the harsh conditions during the pre-treatment of the inoculum than the non-spore
forming bacteria such as methanogens and can germinate under favorable conditions [8,15].
Table 4 summarizes the common pre-treatment measures adopted for enrichment of hydrogen

383 producers.

384 Heat treatment of mixed cultures for the enrichment of H<sub>2</sub> producers is a simple, inexpensive

and effective method [8,30]. However, the effect of heat treatment might be different

depending on the inoculum source such as activated sludge or anaerobic sludge [30]. Some

387 studies [117,118] reported a lower hydrogen yield by a heat shock (HS) treated seed

inoculum than obtained by other pre-treatment methods. This could be due to the inhibition

389 of other non-spore forming hydrogen producing bacteria which might destabilize the main

390 hydrogen production pathways. Similarly, acid or base treatment is based on the notion that

the activity of methanogens drops sharply at a pH below 6.3 or above 7.8 [8], while the

activity of *Clostridia sp.* and other hydrogen producers is not affected by an acidic pH (less

393 than pH 6).

394 Other pre-treatment methods such as chemical pretreatment and aeration are directed towards 395 the selective inhibition of methanogens present in anaerobic sludge, which are very sensitive 396 to changes in environmental conditions. Besides being strict anaerobes, methanogens are 397 sensitive to many chemicals [8]. Thus, oxygen can inhibit their activity during aeration 398 [116,117]. Wang and Wan [116] aerated the inoculum sludge with air for 24 hours to inhibit 399 the activity of methanogens. Likewise, chemical inhibitors like sodium 2-bromoethasulfonic 400 acid (BESA), iodopropane, chloroform and acetylene are used to inhibit methanogens 401 [8,84,117–119]. Thus, selective inhibitors like chemical chloroform or BESA selectively 402 inhibit the activity of H<sub>2</sub> consumer methanogens. In methanogens, BESA functions by 403 inhibiting the activity of co-enzyme M reductase complex, which is a key co-enzyme of 404 methanogenesis [84,117].

405

408 Pre-treatment methods used to enriching hydrogen producing microorganisms in anaerobic409 sludge

Treatment	Description	Inoculum source	Reference
Heat	100 °C for 15 min	Anaerobic digested sludge	[116]
Heat	80°C, 90°C and 100°C for 15-30 min	Anaerobic sludge	[119]
Heat	Heating in boiling water bath for 10-30 min	Anaerobic granular sludge	[74, 75]
Heat	105 °C for 4 hour	Anaerobic granular sludge	[120]
Heat	Incubation at 90 °C for 1 hour	Anaerobic granular sludge	[121]
Heat	100–105 °C in oven for 2 hour	Cow dung compost	[122]
Acid	pH to 2 for 24 h and increasing pH to 5.5 by adding a 2 N NaOH solution	Anaerobic digested sludge	[123] [79]
Acid	pH 3 with 2 N HCl for 24 hours	Anaerobic digested sludge	[124]
Acid	pH to 3 with 1 N HCl for 30 min	Anaerobic digested sludge	[117]
Acid	pH 3 with 0.1 N HCl solution for 24 hours and adjusting back to pH 7	Anaerobic granular sludge	[125]
Base	pH of the sludge to 3 with 1 mol/L of NaOH for 24 hours	Anaerobic digested sludge	[116]
Base	pH 8, 9 and 10 with 1 mol/L of NaOH for 3 hours	Anaerobic sludge	[119]
Base	pH 12 with 1 M NaOH for 24 hours and adjusting back to pH 7 using 1 M HCl	Anaerobic digested sludge	[118]

Load shock	Sludge (50 ml) spiked with 40 g of	Anaerobic granular	[121]	
Load Shock	sucrose and acidification for 2 d	sludge		
	Sludge (50 ml) spiked with 500	Anonabia diaastad		
Load shock	mL of sucrose (50 g/L) and	Anaerobic digested	[118]	
	acidification for 2 d	sludge		
Chamical inhibition	10 mmol of BESA for 30 min and	Anaerobic digested	[60, 70]	
Chemical minorition	gravity separation for 2 h	sludge	[09, 70]	
Chamical inhibition	0.2  g/l DESA for $24  h$	Anaerobic granular	۲ <b>0</b> /۱	
	0.2 g/1 DESA 101 24 II	sludge	[04]	
Chamical inhibition	$0.10/(c_1/c_2)$ shlareforms for $24$ h	Anaerobic digested	[70]	
Chemical inhibition	0.1% (V/V) chloroform for 24 h	sludge	[/9]	
Aeration	Aerate with air for 24 hours	Anaerobic sludge	[116]	
Aeration	Flushing with air for 30 min	Anaerobic sludge	[117]	
Microwave irradiation	Microwave radiation for 1.5 min	Cow dung compost	[126]	

413 Comparison of various inoculum pre-treatment methods for enriching hydrogen producing inocula

Inoculum source	Inoculum treatment methods	Substrate	Culture Temperature (°C)	Culture pH	Optimal pre- treatment method	Maximum H <sub>2</sub> Yield (mol H <sub>2</sub> /mol glucose eqv.) <sup>a</sup>	Maximum H <sub>2</sub> Production Rate (mL H <sub>2</sub> /L/h)	Reference
Anaerobic digested sludge	HS <sup>b</sup> , aeration, acid, base, BESA <sup>c</sup> and iodopropane	Sucrose	35	-	Base treatment	3.06	-	[117]
Anaerobic granular sludge	HS, acid and base	Glucose	35	-	Chloroform	1.55	-	[125]
Anaerobic sludge (UASB)	Acid, BESA, HS and their four combination	Dairy wastewate r	29	-	BESA	0.0317 <sup>d</sup>	-	[84]
Anaerobic digested sludge	Acid, base, HS, aeration and chloroform	Glucose	36	7	Heat shock treatment	1.9	120.4 mL H <sub>2</sub> /h	[116]
Anaerobic digested sludge	Acid, base, LS <sup>e</sup> , HS and BESA	Sucrose	60	5.5	Load shock treatment	1.96	11.2 mmol H <sub>2</sub> /L/h	[118]
Suspended & granular anaerobic sludge mixture	HS, chloroform and combination of both	Ground wheat solution	37	7	Repeated heat shock treatment	25.7 <sup>f</sup>	-	[127]
Enriched inoculum ( <i>Clostridium</i> pasteurianum)	Combination of acid with boiling and enzyme Viscozyme L <sup>g</sup>	Poplar leaves	35	7	2% Vicozyme L	44.92 mL H <sub>2</sub> /g- dry poplar leaves	-	[128]
Anaerobic sludge	HS, acid and base	Glucose	35	6.2	Heat treatment at 80°C for 30 min	3.84	-	[119]

- <sup>a</sup>Calculated based on the information provided from references at Standard Temperature (0<sup>o</sup>C and Pressure 1 atm), <sup>b</sup>HS = Heat shock, <sup>c</sup>BESA= 2-
- 415 bromoethanesulfonic acid,  $^{d}$ mmol H<sub>2</sub>/g COD,  $^{e}$ LS : Load shock,  $^{f}$ mL H<sub>2</sub>/g cells/h,  $^{g}$ Viscozyme L is a mixture of arabanase, cellulase, b-glucanase,
- 416 hemicellulose and xylanase

418 Evaluation of inoculum	pre-treatment methods to enha	ance the DF capacity	y of the inoculum
----------------------------	-------------------------------	----------------------	-------------------

419 sludge

Pretreatment Method	Energy Requirement	Chemical Requirement	Economic cost	Scale-up application
Heat shock treatment	+++	+	+ + +	++
Acid treatment	+	+ + +	+ +	+++
Chemical Treatment	+	+ + +	+ + +	++
Aeration	+++	+	+ +	+++
Load shock treatment	+ +	++	+	+++

420 + Less intensive; ++ Moderately intensive; +++ Very Intensive

421 The effect of inoculum enrichment methods on H<sub>2</sub> production is different based on the source of 422 inoculum (Table 5). However, in order to select an inoculum pre-treatment method for scaled-up 423 systems, several parameters needs to be considered, such as operational costs, feasibility or 424 complexity of the methods, time for the enrichment of the hydrogen producing seed, use of the 425 DF residues in the post treatment processes. Table 6 gives a simple assessment of the commonly 426 applied inoculum pre-treatment methods based on the authors' information from the literature. 427 The selection of chemical treatment methods such as using BESA inhibits the methanogens if 428 DF residues are to be used in AD. In addition, BESA is not environmental friendly and 429 expensive to use in large industrial scale [8]. Likewise, heat shock treatment requires large 430 energy inputs, which makes it less attractive for large scale applications. Acid and load shock 431 pre-treatment can be applied at large scale to select the hydrogen producing inocula without net 432 energy concerns.

In addition, there have been some dark fermentative studies done without the addition of seed
inoculum, utilizing the microorganisms present in the waste itself [129,130]. The fermentative
hydrogen production took longer than in the tests with inoculum supply. Nonetheless, inoculum
pre-treatment is important in the batch tests or process start-up, selection of hydrogen producing
microbial communities in the fermentative bioreactors are determined by the reactor operating
conditions or environmental conditions [87,131–133].

### 439 **4.2 Design and operation of bioreactors**

440 The process design for dark fermentation depends mostly on substrates which limits the

- 441 operational conditions of bioreactors such as culture temperature (mesophilic or thermophilic),
- 442 reactor configurations (reactor types, wet, semi-dry or dry conditions, etc.) and feeding modes

- 443 (mono substrate or co-substrates) [134]. Weiland [135] reported the several types of bioreactors
- 444 used for the conversion of agricultural biomass to energy through upscale AD systems.
- 445 Although these bioreactors are designed for biomethanation by AD, these can be used for
- biohydrogen production after modification of some operational parameters [43].
- 447

#### 448 **4.2.1 Bioreactor configuration**

449 Different DF bioreactor configurations have been used in laboratory studies for a wide range of 450 substrates (see Tables 2, 7 and 8). Most of the dark fermentative hydrogen production studies are carried out in a batch CSTR under wet conditions (<10 % total solids, TS). Besides CSTR, 451 452 many studies have been carried out in anaerobic fluidized bed reactor (AFBR), anaerobic 453 sequencing batch reactor (ASBR), fixed or packed bed reactors, UASB reactor, leaching bed 454 reactor, anaerobic baffled reactor, plug flow reactors, membrane bioreactor (MBR) and others 455 with an objective to enhance the biohydrogen yield and production rate. Recent research 456 [134,136–138] has been focusing on the future implications of high solids processes such as 457 semi-dry (10–20 % TS) and dry (>20 % TS) DF processes for biohydrogen production, as the 458 interests in the conversion of second generation lignocellulosic biomass (mostly agro-industrial

459 residues) is growing.

460 Studies have correlated the production of biohydrogen with microorganism density and different

461 cell retention strategies in bioreactors have been investigated [11,139,140]. The latter include

462 sludge granulation and biofilm systems to increase the microorganism content in the reactor.

463 The results of the studies showed that the volumetric hydrogen production rate of a bioreactor

464 depends on the ability to maintain a high microbial density. Gravala et al. [141] showed higher

465 hydrogen production rates in a UASB (which has a granular biomass retention) than a CSTR at

466 low retention times (19.05 and 8.42 mmol  $H_2/h/l$ , respectively at 2 h HRT), while the CSTR

467 reactor gave higher hydrogen yields at all HRTs tested.

468 Show et al. [142] compared the performance of a CSTR and an AFBR for biohydrogen

469 production using different biomass growth strategies with glucose as the substrate. The different

470 bioreactor configurations used in their research were: suspended sludge CSTR system, granular

- 471 sludge CSTR system, granular sludge AFBR system and biofilm AFBR system. The maximum
- 472 H<sub>2</sub> yield of their suspended sludge CSTR system, granule reactor and biofilm amounted to,
- 473 respectively, 1.92 mol  $H_2$ /mol glucose at a HRT of 6-12 hours, 1.83 $\pm$ 0.09 mol  $H_2$ /mol glucose at
- 474 a HRT of 0.5 hours and  $1.81 \pm 0.08$  mol H<sub>2</sub>/mol glucose at a HRT of 0.5 hours.

475 Besides the specific advantages of these different bioreactor systems, the major drawbacks are 476 the washout of hydrogen-producing bacteria at short HRT in CSTR systems, low conversion 477 rates in granular reactor systems and rapid biofilm development leading to fragmentation and 478 separation from supporting media in biofilm systems [140]. In another study by Zhang et al. 479 [139], the biofilm based and granule-based reactors were compared for their biohydrogen 480 production potential. The results of the study concluded that the granule-based system was 481 advantageous as it could give better results in terms of biomass retention without subjecting to 482 wash-out of the biomass support carriers.

The incompatibility of the use in high organic loading rates and rapid growth of microorganisms in biofilm systems makes them thus less attractive than granular systems. Show et al. [140] recommended the column-shaped granular reactor for fermentative biohydrogen production from wastewater though the system is not suitable for digestion of substrates with high solids content or for a longer retention time in which anaerobic granules may disaggregate. High rate bioreactors are necessary to convert complex organic biomass like OFMSW and agricultural waste.

490

#### 491 **4.2.2 Hydraulic retention time (HRT)**

492 The HRT can affect the hydrolysis of substrates and thus the production of intermediates and 493 products, thus affecting fermentative H<sub>2</sub> production. Besides, the hydrolysis HRT can also be 494 used as controlling parameter of the methanogenic activity. Some studies have demonstrated the effect of the HRT on the biohydrogen production in DF process [143–146]. The different 495 496 growth rates of hydrogen producers and consumers make it possible to use the HRT as a 497 controlling parameter to inhibit the activity of  $H_2$  consumers in the DF. It has been reported that 498 low HRTs favor hydrogen production as the methanogens are washed out, and hydrogen 499 production increases as the HRT decreases [143–145,147]. However, the optimum HRT for 500 biohydrogen production in DF depends on the type of substrates used as the hydrolysis rate 501 depends on the biodegradability of the substrates (Tables 2, 6 and 7).

502 However, the HRT alone is not sufficient to fully suppress the activity of methanogens [144].

503 Liu [144] investigated the effects of pH and HRT on hydrogen production using household solid

504 waste as a substrate in hyperthermophilic (70 °C) CSTR. The effect of the HRT (1, 2, 3, 4 and 6

- 505 days) at a constant pH of 7 and the effect of pH (5, 5.5, 6, 6.5 and 7) at constant HRT of 3 days
- 506 was investigated. The results of the experiments at different HRTs and constant pH 7 showed

- 507 unstable H<sub>2</sub> production with subsequent methanogenic activities at the end. However, a
- 508 combination of pH 5.5 and HRT of 3 days gave the optimum biohydrogen production condition.

### 509 **4.2.3 pH and temperature**

510 The operational pH and temperature are the most crucial parameters that determine the optimum

- 511 metabolic pathways of hydrogen synthesis as well as the inhibition of the hydrogen
- 512 consumption process which may occur simultaneously [35,148]. A acidic operational pH (below
- 513 6) mainly inhibits the methanogenic activity both under mesophilic and thermophilic conditions,
- 514 but the inhibition of hydrogen consuming homoacetogenic activity could only be achieved under
- 515 thermophilic conditions at the initial pH of 5.5 [124]. Thus, the control of the process pH and
- temperature plays an important role in achieving high biohydrogen conversion rates by
- 517 minimizing the activity of hydrogen consumers.

518 The pH is one of the key parameters that can influence the metabolic pathway as it may directly

519 affect the hydrogenase activity, an iron containing enzyme which plays a major role in DF

520 [149]. A acidic pH affects the activity of the hydrogenase enzyme while it is one of the

521 important parameters for the inhibition of methanogenic activities in a mixed culture system

522 [8,35].

523 The optimum pH range for biohydrogen production varies from pH 4.5 [35] to 9 [150] in DF of

524 sucrose. Table 8 provides optimum operating pH ranges in different studies. The possible

525 explanations for these disagreements of optimum pH in various researches can be explained by

526 the differences in inoculum sources, inoculum enrichment methods and substrates types and

527 OLR used in the different studies [30].

528 The culture pH influences the metabolic by-products and biohydrogen yields. In most of the

529 studies, acetate and butyrate are the major end products of favorable hydrogen synthesis

530 (equations 1, 2 and 7). From the Table 8, it can be seen that the neutral operational pH favors

531 acetate pathways while acidic pH favors the butyrate pathways. However, Khanal et al. [35]

532 concluded the independence of acetate and butyrate levels on different initial pH ranges studied

533 (4.5-7.5). Similarly, Luo et al. [151] reported butyrate as major acid in the DF of cassava stillage

- 534 in both BHP tests carried at the initial pH 5 and 7. Nevertheless, in another study by Luo et al.
- 535 [124], acetate was found as a major metabolic product when cultivation pH was 7 while butyrate
- 536 dominated at initial pH 5.5 in the BHP tests carried at mesophilic (37°C) conditions usingacid
- 537 pre-treated inoculum. Luo et al. [124] also reported the inhibition of homoacetogenesis can be
- achieved at pH 5.5 and thermophilic culture temperature. In a recent study of the DF of cheese

- 539 whey (from mozzarella production) at different pH ranges (5.5-7.7) and temperature 39 °C,
- 540 Gioannis [152] reported pH 6 as an optimal pH and acetate levels were higher in all the tests
- 541 except at pH 6.5 where butyrate and propionate levels were higher than acetate.
- 542 A lower pH ( $\leq$  4.5) favors the solvent production [153]. In DF of glucose by *Clostridium*
- 543 pasteurianum, a pH below 5 favors the production of butanol and acetone [149]. Selection of the
- 544 operational pH also depends on the substrate type and OLR which determines the concentration
- of VFA and thus the pH of the solution. The optimum temperature for DF processes varies with
- 546 the type of substrates and the operational pH (Table 8). The optimum pH for organic food waste
- 547 varies from 4.5 to 7, for lignocellulosic waste it varies from 6.5-7, whereas a neutral pH is
- optimal for animal manure [43]. However, Tang et al. [154] reported the optimum pH of 5.5 at
- $549 \quad 45 \text{ }^\circ\text{C}$  for the DF of cattle wastewater. Thus, it becomes important to determine the optimum pH
- 550 conditions for the selected substrate type, loading rate and operational temperature.
- 551 A range of operational temperatures, i.e. mesophilic (35°C), thermophilic (55°C) and extreme
- thermophilic (>65°C) has been studied to determine its effect on biohydrogen production
- 553 [41,45,155]. The studies have shown that the temperature can affect the metabolic pathway, thus
- shifting the composition of the by-products of DF (Table 8). Valdez-Vazquez et al. [45] reported
- 555 higher H<sub>2</sub> yields in thermophilic fermentation than in the mesophilic temperature range. Also
- acetic acid was a dominant by-product in thermophilic digestion, whereas butyrate was in
- 557 formed in a higher proportion in mesophilic digestion. Similarly, results of the extreme-
- thermophilic (70°C) DF of household organic waste done by Liu et al. [156] also showed acetic
- acid as the dominant by product in DF tests conducted at pH 7. In contrast, Shin et al. [41]
- showed acetate as major at mesophilic culture while butyrate levels and hydrogen production
- 561 was higher at thermophilic culture, obtained in DF of food waste carried at pH 5.5. In other
- study, Wang & Wan (2011) found the maximum substrate degradation efficiency, maximum H<sub>2</sub>
- 563 yield and production rate at 37.8 °C in DF of glucose. These studies suggest temperature
- influences biochemical pathways, although other factors such as culture pH, substrates types and
- 565 loading rates are equally important.
- 566 The H<sub>2</sub> yields depend on temperature as it affects the hydrolysis rate [41,45,143]. Biomass such
- 567 as agricultural residues require a high temperature to achieve a higher H<sub>2</sub> yield because a better
- 568 hydrolysis of lignocellulosic compounds is needed [43]. Kongjan & Angelidaki [155]
- 569 demonstrated biohydrogen production from extreme-thermophilic DF of wheat straw
- 570 hydrolysate. Similarly, thermophilic temperatures are favored in the DF of food waste [41]. In
- 571 contrast, easily biodegradable substrates prefer mesophilic temperatures for optimal H<sub>2</sub> yield.

- 572 The difference between the optimum operational temperatures is due to the difference in the
- 573 fraction of easily biodegradable compounds present in the feed substrate and the difference in
- 574 the inoculum used. Table 8 reports ranges of optimum temperatures which vary depending on
- 575 the type of substrate and inoculum used.
- 576 There are some techno-economic studies done, which compare the mesophilic and thermophilic
- 577 operation of DF processes. A thermophilic process seems to be more economical because of its
- 578 higher yield and lower requirement of feedstock in comparison to mesophilic DF processes
- 579 [158]. Foglia et al. [158] reported better economic performance for thermophilic DF in
- 580 comparison to mesophilic operation of the process converting sugars to produce hydrogen, CO<sub>2</sub>
- and organic acids followed by a photo-heterotrophic fermentation in two step process.
- 582

### 583 4.2.4 H<sub>2</sub> partial pressure

- 584 The partial pressure of hydrogen inside a biohydrogen reactor can influence the dark
- 585 fermentative biohydrogen production as a lower partial pressure in the head space of the reactors
- facilitates the mass transfer of hydrogen from the liquid to gas phase [111,159]. During the
- 587 fermentation process, the hydrogenase is involved in reversibly oxidizing and reducing
- 588 ferredoxin. If the hydrogen concentration in the liquid phase increases, the oxidation of
- 589 ferredoxin becomes less favorable and the reduction of ferredoxin takes place [44], thus
- 590 reducing the H<sub>2</sub> production..
- 591 Lee et al. [160] studied the effect of the reduced partial pressure on the hydrogen production in a
- 592 CSTR reactor. Reduction in the partial pressure during the DF could lead to improvement in H<sub>2</sub>
- 593 production. At a HRT of 6 h, they found an optimum hydrogen yield and hydrogen production
- $f_{2}$  efficiency of 4.50 mol H<sub>2</sub>/mol sucrose and 56.2% respectively. Similarly, the reduced pressure
- of 380 mmHg gave a higher yield than the partial pressure of 760 mm Hg in another study doneby Mandal et al. [111].
- 597 In the AD process, the H<sub>2</sub> and CO<sub>2</sub> partial pressure is reduced by methanogens by their
- 598 conversion into CH<sub>4</sub>. Jung et al. [161] reported strategies to remove dissolved H<sub>2</sub> from the
- 599 mixed liquor, including avoiding supersaturation by strong mixing, sparging with N<sub>2</sub> and CO<sub>2</sub>
- and application of a H<sub>2</sub>-permeable membrane to withdraw dissolved H<sub>2</sub> from the mixed liquor.
- 601 Similarly, the partial pressure of H<sub>2</sub> could be reduced directly by decreasing the operating
- 602 pressure in the reactor using a vacuum pump [160]. Mandal et al. [111] reduced the partial
- pressure of H<sub>2</sub> in a methanogenic reactor by adjusting the saline level of the gas collector using a

- 604 peristaltic pump. However, the use of vacuum pumps increases the cost of the process, while the
- sparging with  $N_2$  and  $CO_2$  might render the recovery of  $H_2$  difficult due to the dilution of the  $H_2$
- 606 stream. An effective way to reduce the H<sub>2</sub> partial pressure would be to continuously collect the
- 607 produced gas phase from the reactor.

# 610 Examples of innovative continuous DF bioreactors

Major substrate	Biomass retention system	Reactor type	Optimum HRT (hours)	Optimum Organic Loading Rate (OLR)	Optimum H <sub>2</sub> production index	Reference
Glucose	Granule	CSTR	0.5	10 g glucose/L	H <sub>2</sub> yield 1.81 mol H <sub>2</sub> /mol glucose	[162]
Cheese whey	Granule	UASB reactor	6	20 g COD/L/d	H <sub>2</sub> Production Rate 0.36-0.38 L H <sub>2</sub> /L/d	[163]
Food waste	Biofilm	Batch pilot scale up-flow rector (packed with coir pith)	0.50 m/day <sup>a</sup>	50 g COD/L	H <sub>2</sub> Production Rate 9.67 LH <sub>2</sub> /L/h	[164]
Food waste (pre-treated with alkali)	Suspended	ASBR (fill: 0.5 h; reaction: 8 h; settle: 3 h & discharge: 0.5 h)	36	30 g COD/L	H <sub>2</sub> yield0.69 mol H <sub>2</sub> /mol hexose <sub>added</sub>	[165]
Tequila vinasse	Suspended	ASBR (fill: 3 min; reaction: 5.33 h; settle: 30 min & discharge: 7 min) with 50% volumetric exchange rate	12	3 g COD/L	H <sub>2</sub> Production Rate 50.5 mL H <sub>2</sub> /L/h	[166]
Kitchen waste	Suspended	Inclined plug-flow reactor (inclined at 20°)	168 (7 days)	$6.5 \text{ kgVS/m}^3/\text{d}$	H <sub>2</sub> yield 72 mL H <sub>2</sub> /g VS	[167]
Municipal food waste & kitchen wastewater	Suspended	Anaerobic baffled reactor (ABR)	38.4 (1.6 days)	29 g COD <sub>total</sub> /L/d	H <sub>2</sub> Production Rate 6 L H <sub>2</sub> /d	[48]
Glucose	Suspended	Anaerobic membrane bioreactor (MBR)	12 (SRT <sup>a</sup> )	5.8 g glucose/L	H <sub>2</sub> Production Rate 640 mL H <sub>2</sub> /h	[168]

611 <sup>a</sup>Up-flow velocity, <sup>b</sup>SRT= Solid Retention Time

Substrate type	Microbial inoculum	Optimum pH	Optimum Temperature (°C)	Reactor type	HRT (days)	Maximum H <sub>2</sub> Yield (mL H <sub>2</sub> /g VS)	Major acid type produced	Reference
Food waste	Heat shock treated anaerobic sludge	6.3	35	Leaching Bed Reactor	25	310	Acetate	[99]
Cassava stillage	Heat treated UASB sludge	7	60	Batch CSTR	3.5	53.8	Butyrate	[151]
Cassava stillage	Heat treated UASB sludge	5	60	Batch CSTR	3.5	66.3	Butyrate	[151]
OFMSW	Untreated anaerobic digestate	5.5	37	Semi- continuous CSTR	21	165 <sup>a</sup>	Butyrate	[45]
OFMSW	Untreated anaerobic digestate	6.4	55	Semi- continuous CSTR	21	360 <sup>a</sup>	Acetate	[45]
Wheat Straw	Cow dung compost	7.0	36	Batch CSTR	6.25	68.1	Acetate and butyrate	[102]
Vegetable kitchen waste	Enriched from kitchen waste compost	7.0	55	Batch CSTR	7.0	0.57 <sup>b</sup>	Butyrate and lactate	[133]
Cattle wastewater	Mixed wastewater sludge, cow dung compost, chicken manure compost, river sludge	5.5	45	Batch CSTR	1.25	319 <sup>c</sup>	Butyrate	[154]
Rice straw	Heat treated wastewater sludge	6.5	55	Batch CSTR	6.5	24.8 <sup>d</sup>	Acetate, butyrate	[40]

613 Effects of operational temperature and pH on fermentative hydrogen production

 $614 \qquad ^{a} mL \; H_{2}/g \; VS_{removed}, \; ^{b} \; mmol \; H_{2}/g \; COD, \; ^{c} \; mL \; H_{2}/g \; COD_{consumed}, \; ^{d} \; mL/g \; TS$ 

#### 615 **4.3 Substrate pre-treatment for enhanced H<sub>2</sub> yield**

616 Fermentative biohydrogen production from lignocellulosic substrates is limited by biological 617 hydrolysis [19]. The complex organic substrates cited earlier, such as lignocellulosic biomasses, demand physical, chemical, biological or a combination of these pre-treatments to enhance the 618 619 degradation process, system performance and biogas production [60,64,65,69]. These pre-620 treatment methods reduce the crystallinity of the cellulose and increase the surface area of the 621 materials to improve the separation of the lignin and hemicellulose fractions [169]. There have 622 been some studies on the effect of the pre-treatment on fermentative biohydrogen production 623 [61,155,170,171]. These pre-treatment methods have in most cases a positive influence on the H<sub>2</sub> 624 yield, as the biohydrogen production depends on the soluble fraction of sugars or carbohydrates. 625 Physical pre-treatment methods which generally include mechanical comminution (chopping, 626 grinding, milling), irradiation with gamma-rays, electro-beam or microwaves, hydrothermal 627 treatment, high pressure steaming or pyrolysis are effective in breaking the crystallinity, 628 increasing the accessible surface area and decreasing the degree of polymerization [69]. 629 Chemical methods such as ozonolysis, acid or alkaline hydrolysis, solvent extraction, explosion 630 with steam ammonia fiber or  $CO_2$  are effective in increasing the surface area, delignification and 631 also decreasing the crystallinity and rendering the partial or complete hydrolysis of 632 hemicelluloses. These physical and chemical treatment methods can be promising for industrial 633 applications as they are rapid. However, these methods demand energy and chemical inputs. 634 Moreover, lignocellulosic substrates can also be biologically treated with fungi and 635 actinomycetes which provide delignification and partial hydrolysis of cellulose, while some 636 enzymes (hemicellulase and cellulase) can aid in the hydrolysis and degradation of the 637 lignocellulosic materials [60].

638 The physical pre-treatment, especially the reduction of substrate particle size, has an effect on the

biogas yield and process kinetics [172–174]. Chen et al. [40] investigated the effects of the rice

640 straw particle size and concentration on cumulative dark fermentative biohydrogen production.

They used a meshed rice straw concentration of 30 g TS/L with five particle sizes (<0.297,

642 0.297-0.58, 0.58-1.19, 1.19-10 and >10 mm) as the substrate at an initial cultivation pH 6.5 and

temperature of 55 °C. The results of the study showed that rice straw of a particle size <0.297

644 mm gave the highest cumulative  $H_2$  production (191 mL  $H_2/L$ ) with a  $H_2$  yield of 6.4 mL/g TS.

645 The substrate with a larger particle size had an extended lag phase and lower hydrogen 646 production. This can be explained by the fact that decreasing the particle size increases the 647 substrate availability for microbial hydrolysis and fermentation. Kongjan & Angelidaki [155] 648 pretreated wheat straw at 180 °C for 15 min to obtain a hydrolysate which mostly contained 649 hemicellulose leaving the cellulose and lignin in solid form. The hydrolysate was used as the 650 substrate for fermentative hydrogen production. Similarly, Zhang et al. [46] reported the use of 651 acid pretreated corn stalks for fermentative biohydrogen production. The biohydrogen yield from 652 acid pretreated corn stalks was higher than of that of untreated waste. However, mostly physical 653 pretreatment methods are applied in combination with chemical or biological pre-treatment 654 methods to obtain better and rapid hydrolysis of substrates (Table 9).

655 The effect of pre-treatment methods for different lignocellulosic substrates have a diverse effect 656 on the hydrolysis of soluble sugars and release of inhibitory products [175–178]. This needs to 657 be further investigated for the selection of suitable pre-treatment methods. These studies have 658 shown that the pre-treatment methods can enhance the system performance enhancing the biogas 659 production. However, the selection of a pre-treatment process should be based on effectiveness, 660 energy balance, economic feasibility and environmental sustainability [18]. In addition, some 661 studies have reported that during the pre-treatment of lignocellulosic biomass, various 662 undesirable compounds are released which exert inhibitory effects on microorganisms [63,175– 663 177]. The most commonly reported inhibiting substances which are released during the pre-664 treatment processes are furfural, hydroxyl-furfural and phenolic substances. Quéméneur et al. 665 [63] and Monlau et al. [179] investigated the inhibition and control of these inhibitors on 666 biohydrogen production. Thus, the selection of pre-treatment methods for lignocellulosic 667 substrates should also consider these aspects.

668

Substrate	H <sub>2</sub> yield	Pretreatment	Reactor	Temperature	Reference	
	(mL H <sub>2</sub> /g VS)	methods	mode	( <sup>0</sup> C)		
Rice straw	24.8 <sup>a</sup>	Size reduction, <0.297mm	Bath	55	[40]	
Wheat stalks	17.6	Size reduction, 1 mm	Batch	35	[180]	
Wheat straw	212 <sup>b</sup>	Hydrothermal (180 <sup>0</sup> C for 15 min)	Continuous UASB reactor	70	[155]	
Corn Stover	2.84 <sup>c</sup>	Steam explosion, 190.220 °C for 3-5 min	Batch	35	[181]	
Corn Stover	3.0 <sup>c</sup>	Acidic steam explosion (1.2% H <sub>2</sub> SO), 180 and 200 °C for 1–3 min	Batch	35	[181]	
Beet-pulp	$\begin{array}{c} 66.7 \\ \pm 10.1^d \end{array}$	Alkaline at pH 12 using 2 M NaOH for 30 min. + Microwaves (170 <sup>o</sup> C for 30 min)	Batch	35±2	[182]	
Bagasse	300	100 <sup>o</sup> C for 2 h +4% NaOH (w/v) + cellulase (20 FPU/g)	Batch	55	[170]	
Grass	72.2 <sup>e</sup>	4% HCl (w/v), boiled 30 min.	Batch	35	[183]	
Grass	39.5 <sup>e</sup>	4% NaOH (w/v), boiled 30 min.	Batch	35	[183]	
Corn stalks	209.8	1.5% H <sub>2</sub> SO <sub>4</sub> , 121 $^{0}$ C for 60 min+ 9.4 IU/g of cellulase 52 $^{0}$ C at pH4.8 in 0.1 M sodium citrate buffer at 5% (w/v)	Batch	36±1	[184]	
Corncobs	107.9	100 °C, 30 min and 1% HCl (w/w))	Batch	36	[171]	

670 Examples of different pre-treatment methods applied to complex substrates used in DF

<sup>671</sup> <sup>a</sup>mL/g TS, <sup>b</sup>mL H<sub>2</sub>/g sugars, <sup>c</sup>mol H<sub>2</sub>/mol glucose, <sup>d</sup>mL H<sub>2</sub>/g COD, <sup>e</sup>mL H<sub>2</sub>/g dry grass
### 672 **4.3.1 Addition of nutrients and trace elements**

673 Microorganisms in fermentation processes require nutrients for bacterial activity and growth.

Thus, nutrients such as nitrogen, phosphate, metal ions and other micronutrients are needed in

675 fermentation processes for enzymatic activities and biomass growth, which affects the H<sub>2</sub>

676 production. Biomass rich in carbohydrates such wheat wastes and palm oil effluents may be

677 deficient in nutrients (such as nitrogen, phosphorous) or minerals (such as trace metals).

678 Therefore, nutrients or micro nutrients must be provided as supplement for optimum microbial

activities for biohydrogen conversion from carbohydrate rich substrates [185–188].

#### 680 Nitrogen and phosphorous

681 Nitrogen has great significance for hydrogen producers as it is an important component of

682 proteins, nucleic acids and enzymes. Similarly, besides being an important nutrient, phosphate

also serves in buffering the biochemical reactions [30]. In the thermophilic DF of palm oil mill

effluents (POME), O-Thong et al. [78,81] showed that supplementing iron (257 mg Fe<sup>2+</sup>/L),

adjusting the C/N ratio from 95 to 74 (using peptone as nitrogen source) and the C/P ratio from

686 650 to 559 (using Na<sub>2</sub>HPO<sub>4</sub>·2H<sub>2</sub>O) could enhance H<sub>2</sub> production. In these studies, the hydrogen

687 production rate increased by 60% [78] and COD removal improved from  $35.5\pm9.8$  to  $62.2\pm2.8\%$ 

688 [81] compared to raw POME without nutrient supplementation.

Likewise, Argun et al. [185] studied the effects of the C/N and C/P ratio on the hydrogen yield

and specific H<sub>2</sub> production rate in DF of wheat powder solution by supplementing nitrogen and

691 phosphorous. The results of the study showed the highest  $H_2$  yield of 281 NmL  $H_2/g$  starch were

692 obtained at a C/N ratio of 200 and C/P ratio of 1000. However, there are some disagreements in

the carbon to nitrogen and phosphorous ratios. Lin and Lay [188] achieved a 500% and 80%

694 increased hydrogen yield and hydrogen production rate at a C/N ratio of 47 compared with the

blank. Similarly, O-Thong et al. [78,81] attained an optimum hydrogen production and COD

removal at a C/N ratio of 74 and a C/P ratio of 559. Several studies have used integration of co-

697 substrates as a strategy to maintain the appropriate C/N ratio; examples includes use of swine

manure as a source of nitrogen in co-fermentation with vegetable waste [189] and use of cassava

699 starch in co-fermentation with microalgae *Chlorella pyrenoidosa* [190].

### 700 Metal ions and micronutrients

- 701 Higher concentrations of metal ions exert inhibitory effects on the hydrogen producers
- [8,191,192]. However, trace amounts of some metal ions enhance the reactor performance [193].
- 703 Karadag & Puhakka [193] found that iron and nickel improved the reactor performance and H<sub>2</sub>
- production was enhanced by 71%. O-Thong et al. [78] obtained the optimal hydrogen production
- when the substrate contained 257 mg Fe<sup>2+</sup>/L during the thermophilic DF of POME.

### 706 **4.3.2 Inhibition due to heavy metals**

- 707 Toxic heavy metals such as cadmium (Cd), chromium (Cr), zinc (Zn), copper (Cu), nickel (Ni),
- and lead (Pb) which may be present in industrial and municipal solid waste may lead to upset or
- 709 ultimately failure of anaerobic reactors [8]. Altaş et al. [194] studied the inhibitory effect of
- 710 heavy metals on methane-producing anaerobic granular sludge. The order of toxicity for the
- 711 individual heavy metals in decreasing order was: Zn (most toxic, 7.5 mg/L) >Cr (27 mg/L) >Ni
- 712  $(35 \text{ mg/L}) \approx \text{Cd}$  (least toxic, 36 mg/L).
- Lin and Shei [191] showed the relative toxicity of the heavy metals to fermentative hydrogen
- 714 production was in the order of Zn>Cu>Cr. The maximum concentration of these metals that
- reduced the hydrogen producing activity by 50% was 4.5 mg Zn/L, 6.5 mg Cu/L and 60 mg Cr/L
- [191]. However, Li and Fang [192] reported the relative toxicity to H<sub>2</sub> production in the
- following order: Cu (most toxic)>>Ni~ Zn > Cr > Cd > Pb (least toxic). The bioactivity of the
- sludge was reduced to 50% of the control at 30 mg Cu/L, 1600 mg Ni and Zn/L, 3000 mg Cr/L,
- 719 3500 mg Cd/L and >5000 mg Pb/L.

### 720 **5.** Use of by-products

The low process yield and the incomplete conversion of organic biomass are two major

- bottlenecks for commercial dark fermentative biohydrogen production [12,27]. As overviewed in
- 723 Section 4, dark fermentative biohydrogen can be enhanced by suitable substrate selection,
- inoculum enrichment strategies, and optimal operation of bioreactor or substrate pre-treatment.
- However, a single DF system cannot achieve beyond the highest yield of 4 moles H<sub>2</sub> per mole
- hexose, as DF has a maximum yield of 33% (on sugars) [27]. Besides, DF residues mainly
- contain volatile acids, major by-products of the DF process, which need to be utilized to achieve
- complete conversion of the organic biomass. The dual systems are integrated by the conversion
- of carbohydrates to organic acids in the first stage (DF) and the use of conversion by-products in

- 730 the second stage, either to  $H_2$  (photofermentation, bioelectrochemical cells) or CH<sub>4</sub> (AD). Also,
- 731 AD can be considered as the final stabilization stage to stabilize the residues of DF,
- 732 photofermentation and bioelectrochemical cells. Figure 5 shows an example of different
- 733 possibilities of integrating DF to other post treatment processes.



- 737
- 738 A number of studies have been carried out combining DF either with photofermentation [195–
- 739 202] or/and using bio-electrochemically assisted microbial reactor [142,203–206] for improving
- 740 the biohydrogen yield or with the AD process for improving the economic viability [89,106,207–
- 741 210]. Light dependent fermentative processes could be a good option for a second stage H<sub>2</sub>
- production, because of its higher substrate conversion efficiency, and being less energy intensive 742
- 743 and environmental friendly [211]. On the other hand, bio-electrochemically assisted microbial
- 744 fuel cells are also an option to treat the effluents from DF and increase the H<sub>2</sub> yield [212].
- 745 Likewise, the economic viability of the DF process could be enhanced by AD as a final

step.Some examples of integrated processes of DF combined with post treatments are presentedin Table 10.

# 748 **5.1 Photofermentation**

749 Under anaerobic conditions, purple non sulfur (PNS) photosynthetic bacteria carry out anaerobic 750 photosynthesis using light as energy source for synthesizing hydrogen [213,214]. The PNS 751 bacteria use the captured light energy to produce ATP and high energy electrons through reverse 752 electrons flow which reduces ferredoxin (Fig. 6). Then, the ATP and reduced ferredoxin drives 753 the proton reduction to hydrogen by nitrogenase [215]. The research attention in these organisms 754 is increasing because of their higher biohydrogen yield potential and better light utilization 755 proficiency as they are able to absorb and utilize both visible (400 - 700 nm) and near infrared 756 (700 – 900 nm) light. Moreover, they are able to use a wide variety of substrates [213].



757

Fig. 6. Schematic presentation of photofermentation (adapted and modified from [215])

The ability of PNS organisms to convert the organic acids to biohydrogen makes

- 760 photofermentation a good post treatment for biohydrogen production from DF effluents. An
- example of integrated dark and photofermentative conversion of acetic acid to biohydrogen is thefollowing:

763 **DF:** 
$$C_6H_{12}O_6 + 2H_2O \rightarrow 2CH_3COOH + 2CO_2 + 4H_2$$
 (8)

- 764 **Photofermentation:**  $CH_3COOH + 2H_2O$  Light energy  $4H_2 + 2CO_2$  (9)
- 765 Depending on the operating conditions of the bioreactors and other parameters described earlier
- (See section 4), DF might follow different pathways rather than only the acetic acid pathway,
- therefore, a theoretical biohydrogen potential of DF effluents containing acetate, propionate and
- butyrate can be written as follows [216,217]:
- 769 Lactate:  $C_3H_6O_3 + 3H_2O \rightarrow 6H_2 + 3CO_2$  (10)
- 770 Propionate:  $C_3H_6O_2 + 4H_2O \rightarrow 7H_2 + 3CO_2$  (11)
- 771 Butyrate:  $C_4H_8O_2 + 6H_2O \rightarrow 10H_2 + 4CO_2$  (12)
- 772 PNS species such as Rhodospirillum rubrum, Rhodopseudomonas palustris, Rhodobacter
- sphaeroides and Rhodobacter capsulatus, Rhodopseudomonas faecalis have been widely used in
- photofermentation studies for H<sub>2</sub> production [213,214], while some studies have been done with
- mixed cultures isolated from wastewater sludge [218–220] Yangling et al. [221] evaluated the
- 776 microbial community dynamics in a mixed photofermentative culture enriched from a digestate
- from AD of pig dung and found the prevalence of mostly *Rhodopseudomonas palustris*.
- 778 Redwood et al. [21] presented different integration strategies for combining two step dark and 779 photofermentation processes. Nath et al. [201] studied the combined dark and photo fermentation 780 for biohydrogen production using glucose as the substrate. DF was carried by *Enterobacter* 781 cloacae strain DM11, followed by photofermentation by *Rhodobacter sphaeroides* strain 782 O.U.001 using the spent medium from the DF which mainly contained acetic acid. The 783 combined hydrogen yield was higher than a single biohydrogen system, i.e. 1.86 mol H<sub>2</sub>/mol 784 glucose in DF and 1.5-1.72 mol H<sub>2</sub>/mol acetic acid in the photofermentation. Similarly, 785 combining the two fermentation processes, Chen et al. [211,222] and Tao et al. [222] attained a 786 total yield of 10.25 mol H<sub>2</sub>/mol sucrose and 6.63 mol H<sub>2</sub>/mol sucrose respectively. In a study by 787 Su et al. [195], a yield of 4.16 mol  $H_2$  mol/mol glucose was obtained from photo fermentation of 788 DF effluents using glucose as the substrate, which increased the total yield to 5.48 mol H<sub>2</sub>/mol 789 glucose.
- Other researchers have used effluents from DF of diverse substrate types in photofermentativebiohydrogen production. Argun et al. [202] use the DF effluent of ground wheat solution with

792 the  $H_2$  yield of 781 ml/g total VFA. In another studies by Su et al. [196,197], cassava starch and 793 water hyacinth were used as the substrates in DF and its effluent was utilized successfully for 794 photofermentative biohydrogen production. The studies reported the increase in total H<sub>2</sub> yield 795 from 240.4 mL H<sub>2</sub>/g starch to 402.3 mL H<sub>2</sub>/g starch [196] and 76.7 to 596.1 mL H<sub>2</sub>/VS [197] 796 using Rhodopseudomonas palustris. These studies have shown that combined dark and 797 photofermentation is a potential technology for biohydrogen production using diverse substrates. 798 Some drawbacks of photofermentative systems include the inherent high energy demand 799 associated with the nitrogenase enzyme, lower solar conversion efficiencies and economic issues 800 of anaerobic photobioreactors covering large areas [33]. However, these inefficiencies can be 801 overcome by developing an efficient photobioreactor [223,224]. Besides the presence of light 802 conditions, the culture medium of photofermentation should be under ammonia limitation and 803 the absence of oxygen, as both inhibit the nitrogenase activity [225–227]. Higher ammonia 804 concentrations (in excess of 2-5 mmol) can be detrimental to hydrogen production [225,228]. 805 Thus, the effective removal of ammonia from DF residues can be a bottleneck in coupling 806 photofermentation with DF processes. Therefore, the substrates with a high C/N ratio seem more 807 suitable for H<sub>2</sub> conversion in these systems. Nonetheless, several ammonia removal strategies 808 such as stripping, natural zeolites and selective membranes can be applied which could facilitate 809 the coupling of these two processes. [229,230].

In addition to biohydrogen production, accumulation of poly-hydroxybutyrate (PHB) could raise future interests, as it possess economic value as a biodegradable polymer [231]. Thus, energy recovery and economic sustainability of the commercial development of DF depends also on the development of the post-treatment processes like photofermentation.

### 814 **5.2 Microbial Electrolysis Cells**

815 Biohydrogen production from DF residues is also possible through an emerging technology

- 816 known as electrohydrogenesis or biocatalyzed electrolysis or microbial electrolysis
- 817 [24,25,27,29,203,232]. Electrochemically assisted Microbial Fuel Cells (MFCs) or Microbial
- 818 Electrolysis Cell (MECs) or Bioelectrochemical Systems (BES) use microorganisms to catalyze
- the biochemical reactions at the anode and/or cathode, producing protons and electrons from the
- 820 oxidation of organic matter [142,206,212]. MECs should not be confused with MFCs, the former

is an electrolysis reactor which produces hydrogen, while a MFC is a fuel cell that produces
electricity [212]. In MECs, hydrogen can be produced at the cathode by applying a small circuit
voltage, theoretically 0.14 V [212] (Fig. 7). Some exoelectrogenic microorganisms which are
capable of electron transfer to an electrode (anode) include genera *Geobacter, Shewanell* and *Pseudomonas sp.* [24,206,212], while the function and the community of microorganisms at the
cathode is not known [212]. The evolution of hydrogen in BESs can be represented in the
following reactions:

828	$C_6H_{12}O_6 + 2H_2O \rightarrow 2CH_3COOH + 2CO_2 + 4H_2$	(13)
829	Anode: $CH_3COOH + 2H_2O \rightarrow 2CO_2 + 8e^- + 8H^+$	(14)
830	Cathode: $8H^+ + 8e^- \rightarrow 4H_2$	(15)

831 A minimum theoretical voltage required to produce hydrogen at pH 7 is - 410 mV (Normal 832 Hydrogen Electrode). However, the anode potential produced by the oxidation of organic matter 833 is approximately 300 mV. Thus, hydrogen can theoretically be produced at the cathode by 834 applying a circuit voltage higher than 110 mV (i.e.  $V_{applied} = V_{anode} - V_{cathode} = 410-300 \text{ mV}$ ), 835 though it has been found that a minimum applied voltage of more than 250 mV is needed due to 836 ohmic resistance and electrode over potential [7,206]. This applied voltage required is 837 considerably lower than 1210 mV, a theoretical voltage needed for hydrogen production via 838 electrolysis of water at neutral pH conditions [206].



Fig. 7. Schematic diagram of two chambered MEC separated by a proton exchange membrane
and power supply (adapted and modified from [206])

Lalaurette et al. [233] tested a two stage process, combining DF using cellulose as a substrate

- and MEC systems for hydrogen production. This improved the total hydrogen yield to 9.95 mol
- 844 H<sub>2</sub>/mol glucose from the fermentative hydrogen yield of 1.64 mol H<sub>2</sub>/mol glucose using
- cellulose. Similarly, Liu et al. [203] used the volatile acids accumulated in fermentation of waste
- 846 activated sludge as a carbon source for biohydrogen production in a MEC with a H<sub>2</sub> yield and
- 847 production rate of 1.2 mL H<sub>2</sub>/mg COD and 120 mL H<sub>2</sub>/g VSS/d, respectively. The results from
- the analysis of the electrohydrogenesis end products showed that more than 90% of the acetate
- 849 and propionate were converted to hydrogen, but with lower conversion of n-butyrate and n-
- valerate (<20%). Likewise, Moreno et al. [24] obtained 94.2 L H<sub>2</sub>/kgVS from the two stage DF-
- 851 MEC systems using cheese whey wastewater.

852 The MECs are still under research and development. One of the challenges to MECs is to 853 suppress the methanogenic activity during the electrohydrogenesis with mixed cultures as it 854 negatively affects the H<sub>2</sub> production rate. Hu et al. [234] has proposed to inhibit the 855 methanogenic activity by exposing the cathodes to air. They studied a single chambered MEC to 856 investigate the hydrogen production using mixed and pure culture (Shewanella oneidensis MR-857 1). The major objective was to reduce the potential losses associated with the membrane and 858 increase the energy recovery of the process. Studies of the long term performance of MEC 859 systems are needed to further develop and achieve the technical and economic edge of this 860 technology.

### 861 **5.3 Anaerobic digestion**

862 Anaerobic Digestion (AD) is a proven biological waste treatment method for volume reduction, 863 waste stabilization and biogas recovery (CH<sub>4</sub>) from organic waste [92]. The AD process can be 864 combined with DF to achieve further conversion of end products of DF and the residues from 865 photofermentation and MECs systems (Fig. 5). Photofermentation requires a clear medium for 866 efficient light utilization. Thus, the residue from the filtration of DF effluents, microbial biomass 867 produced in photofermentation and the residues from MECs (if any) can be utilized in AD for the 868 final stabilization. The two stage processes combining biohydrogen production in the first stage 869 and AD in the second stage not only increase the sustainability of the process, but also guarantee 870 the complete treatment of the organic waste [27].





Fig. 8. Two-stage process for hydrogen and methane production

873

874 A number of studies have been done on dual systems [89,106,207–210,235]. DF followed by AD 875 (Fig. 8) has shown technical and economic feasibility of the integrated process up to pilot scale 876 [77,94]. Wang and Zhao [236] ran a successful pilot scale unit consisting of hydrolysis-877 acetogenesis for H<sub>2</sub> generation in a rotating drum of 200 liters, followed by a methanogenesis 878 stage in 800 liters reactor. Likewise, Cavinato et al. [207] established successful two stage 879 conversion of hydrogen and methane from organic waste. Similarly, Antonopoulou et al. [237] 880 investigated two stage hydrogen and methane production using sweet sorghum with a H<sub>2</sub> yield of 881 10.41 L H<sub>2</sub>/kg sweet sorghum and methane yield of 29 L CH<sub>4</sub>/kg sweet sorghum utilizing DF 882 residues as a sole substrate in AD, while Kvesitadze et al. [238] got the cumulative  $H_2$  yield of 883 104 L H<sub>2</sub>/g VS and methane yield of 520 L CH<sub>4</sub>/g VS using OFMSW. Similarly, Antonopoulou 884 et al. [237] showed the feasibility of two stage hydrogen-methane process using cheese whey. 885 Jung et al. [239] showed that two stage  $H_2$ -CH<sub>4</sub> conversion from molasses is economically 886 feasible. Ruggeri et al. [209] used energy balance as a tool to determine the sustainability of 887 integrated DF and AD, which showed the positive energy gain. Similarly, Schievano et al. [240] 888 reported 8%-43% increment of energy in two stage system in comparison to a single stage AD. 889 Thus, in light of recent popularity of two stage AD processes for treating high strength 890 wastewater or concentrated solids, the former stage can be modified to be used for hydrogen 891 production [43]. Also, the DF process can be seen as a pre-treatment stage if the organic waste of 892 interest is subjected to complete stabilization [236]. Thus, in order to improve the economic 893 competence of commercial DF, AD could provide an attractive solution [241].

### 894 **5.4 Other applications**

- 895 Besides conversion of volatile fatty acids and other reduced carbon sources to biomethane or
- biohydrogen in biological processes, VFAs can be used in various applications: biological
- nutrient removal from wastewater [242,243], sulfur and sulfate reduction [244,245], biopolymer
- 898 (such as polyhydroxybutyrate) production [83] and microbial lipids production [55,246]. Lim et
- al. [242] studied the use of volatile fatty acids produced from food waste as carbon sources in the
- 900 removal of nitrogen and phosphorous from municipal wastewater in a sequential batch reactor
- 901 (SBR) [242]. Similarly, Elefsiniotis et al. [243] studied the denitrification process, removal of
- 902 nitrate-nitrogen (20 to 200 mg/L) using VFA generated from the AD of starch rich industrial and
- 903 municipal wastewater as a carbon source in batch reactors.
- 904 Similarly, a "carboxylate platform" or third biorefinery platform has been introduced to generate
- a mixture of carboxylates as intermediate for the production of complex fuels utilizing waste
- 906 biomass [247]. Ntaikou et al. [83] investigated the combined production of biohydrogen and
- 907 biopolymers from the DF of olive mill wastewater and the use of DF effluents which mostly
- 908 contained VFAs in SBR using polyhydroxyalkanoates (PHAs) producing bacteria culture.
- Tuna et al. [248] uses the volatile fatty acids produced in DF processes for hydrogen production
- 910 by electrohydrolysis. Hydrogen was generated by applying a low voltage in the range of 1-3 V
- 911 DC current to DF effluents of wheat powder containing different VFAs concentrations. The
- 912 applied voltage of 2 V and 10.85 g/L of total VFA gave the highest energy efficiency of 56%.

# **Table 10**

First Stage: I	DF							Second Stage: Photo fe	ermenta	tion				
Substrate type	Microbial Inoculum	pН	T (°C)	HRT days	Max. H <sub>2</sub> Prod. Rate	Max. H <sub>2</sub> Yield	Dominant end products	Process & Microbial Inoculum	pН	T (°C)	HRT days	Max. Biogas Prod. Rate	Max. H <sub>2</sub> Yield	Reference
Sucrose	Clostridium pasteurianum	7	37	-	-	3.85 mol H <sub>2</sub> /mol sucrose	Butyrate and acetate	Rhodopseudomonas palustris WP3-5	7.1	32	96 hours	25.2 mL H <sub>2</sub> /L/h	4.03 mol H <sub>2</sub> /mol sucrose	[211]
Sucrose	Heat treated Cattle dung and sludge from biogas plant	6	38	Batch	360 mL H <sub>2</sub> /L/h	3.67 mol H <sub>2</sub> /mol sucrose	Butyrate and acetate	Rhodobacter sphaeroids SH2C	7	30	Batch	-	4.06 mol H <sub>2</sub> /mol sucrose	[222]
Acid hydrolyzed sugarcane bagasse	Enterobacter aerogenes MTCC 2822	6.8	38	Batch	1000 mL H <sub>2</sub> /L	-	Butyrate and acetate	Rhodopseudomonas BHU 01	6.8	34	Batch	755 ml/L	-	[22]
First Stage: I	DF							Second Stage: AD						
Substrate type	Microbial Inoculum	pН	T (°C)	SRT days	Max. H <sub>2</sub> Prod. Rate	Max. H <sub>2</sub> Yield	Dominant end products	Process & Microbial Inoculum	рН	T (°C)	SRT days	Max. CH <sub>4</sub> Prod. Rate	Max. CH4 Yield	Reference
OFMSW	Heat treated sludge from biogas plant	5.2	37	2	640 mL H <sub>2</sub> /d	43 mL H <sub>2</sub> /g VS added	Acetate and butyrate	Sludge from biogas plant	7.5	37	15	7475 mL CH4/g VS added	500 mL CH <sub>4</sub> /g VS added	[106]
Food waste	Indigenous microbial cultures from food waste	5.2– 5.8	40	6.66	-	65 mL H <sub>2</sub> /g VS	Acetate and butyrate	Anaerobic granular sludge from UASB	6.8	40	26.67	-	546 mL CH4/g VS	[236]

# 914 Examples of operational conditions and system performances of integrated DF systems

Micro algae (Chlorella vulgaris)	Clostridium thermocellum	-	55	Batch	-	53.4 mL H <sub>2</sub> /g VS	Acetate and butyrate	Anaerobic granular sludge from ASBR	-	55	batch	22.38 mL CH <sub>4</sub> /g VS·d	320.6 mlCH4/g VS	[249]
First Stage: DF								Second Stage: Bioelectrochemical systems						
Substrate type	Microbial Inoculum	pН	T (°C)	HRT days	Max. H <sub>2</sub> Prod. Rate	Max. H <sub>2</sub> Yield	Dominant end products	Process & Microbial Inoculum	рН	T (°C)	HRT days	Max. H <sub>2</sub> Prod. Rate	Max. H <sub>2</sub> Yield	Reference
Molasses	-	-	-	Batch	700 mL H <sub>2</sub> /L/d	0.27 mol H <sub>2</sub> /mol COD	Ethanol, acetic and butyric acid	Domestic wastewater	6.7- 7.0	25	Batch	1410 mL H <sub>2</sub> /L/d	-	[250]
Corn Stover	Clostridium thermocellum	6.8	50	Batch	0.25 L H <sub>2</sub> /L/h	1.67 mol H <sub>2</sub> /mol- glucose	Acetic acid and ethanol	Inoculum from microbial fuel cell Wastewater	7.3	-	Batch	1 L/L/d	750 mL/g COD	[233]
Corn stalk	Microwave irradiation pre- treated cow dung	7.0	36	Batch	$\frac{1.73}{H_2/m^3}\frac{m^3}{d}$	129.8 mL H <sub>2</sub> /g corn stalk	Acetate, butyrate, propionate, ethanol	Spent dark fermentation medium (Single chambered cell)	7.0	36	Batch	$\begin{array}{c} 3.43 \pm \! 0.12 \\ m^3 \ H_2 \! / m^3 \\ d \end{array}$	257.3 mL H <sub>2</sub> /g corn stalk	[232]

### 916 **6. Pilot scale applications**

917 Most DF studies have been carried out in laboratory scale batch, semi-semi-continuous or

- 918 continuous reactors. To the best of our knowledge, no studies have reported on the industrial
- 919 or full scale application of DF processes. Limited studies have been done on pilot-scale
- 920 applications of DF processes [77,88,94,167,251,252]. Ren et al. [88] studied a 1.48 m<sup>3</sup>
- 921 continuous flow anaerobic reactor for 200 days at an OLR of 3.11-85.57 kg COD/m<sup>3</sup>/d fed
- 922 with molasses. The maximum hydrogen yield was 26.13 mols H<sub>2</sub>/kgCOD removed in the
- 923 OLR range of  $35-55 \text{ kg COD/m}^3/d$  and a maximum production rate of  $5.57 \text{m}^3 \text{ H}_2/\text{m}^3$
- 924 reactor/d was reached. Jayalakshmi et al. [167] worked with a plug-flow inclined DF reactor
- 925 of volume 0.15  $m^3$  with kitchen waste as the substrate. The reactor gave a H<sub>2</sub> yield of 72 mL
- 926  $H_2/gVS$  added.
- 927 Another reported long term pilot-scale study was carried out at Fen Chia University
- 928 (Taiwan), comprising of two feedstock storage tanks (0.75m<sup>3</sup> each), a nutrient storage tank
- 929 (0.75m<sup>3</sup>), a mixing tank (0.6 m<sup>3</sup>), an agitated granular sludge bed fermenter (working volume
- 930 0.4 m<sup>3</sup>), a gas-liquid-solid separator (0.4 m<sup>3</sup>) and a control panel. A pilot-scale high-rate
- reactor was operated for a period of 67 days under mesophilic conditions (35 °C) at an OLR
- 932 of 40-240 kg COD/m<sup>3</sup>/d with sucrose as the substrate. An OLR of 240 kg COD/m<sup>3</sup>/d gave a
- hydrogen production rate of 15.59  $m^3/m^3/d$  and a hydrogen yield of 1.04 mol H<sub>2</sub>/mol sucrose.
- In another study, Cavinato et al. [77] carried out a two-stage pilot-scale thermophilic DF and
- AD of food waste for the production of, respectively, biohydrogen and methane with
- recirculation of AD effluents to DF to control the pH (5-6). The organic loading rate of 16.3
- $kgTVS/m^3d$  was maintained with a HRT of 3.3 days in the DF stage, yielding 66.7 L H<sub>2</sub>/kg
- 938 TVS.
- 939

# 940 **7. Challenges and future prospects**

### 941 **7.1 Modeling and simulation**

942 Several researches have been proposed to integrate DF processes with AD, photofermentation

- 943 or bioelectrochemical systems to utilize the VFAs produced to increase its viability.
- 944 Modeling of kinetic parameters and biohydrogen production becomes important for the
- design, analysis and operation of the fermentative processes. Also, the predictive capacity of
- 946 the model for end products helps to design the downstream processes. Several models have

- been proposed to describe the biohydrogen production, growth of hydrogen fermenters,
- 948 substrate consumption and intermediate biochemical processes [253–255]. With increasing
- 949 research on DF, the modeling of the biohydrogen production process could be of primary
- 950 interest to achieve a better understanding of the DF pathways and control of the process.
- Parameters such as substrate concentration, pH, temperature, and HRT affect the H<sub>2</sub> yield and
- 952 production rate and the nature of the end products (See section 4). Wang and Wan [254]
- reviewed existing mathematical models such as the Modified Gompertz model for product
- formation (H<sub>2</sub> production), the Logistic model for biomass growth [256], substrate utilization
- based on Monod Kinetics, the Arrhenius model for temperature effects, pH inhibition models
- based on the IWA Anaerobic Digestion Model no. 1 (ADM1) [257] and the Modified
- 957 Luedeking-Piret models for the formation of by-products [256].

958 There is, however, a need to upgrade the different kinetic models, including complex 959 biochemical processes, which involve the fermentative biohydrogen production such as hydrolysis, acidogenesis and H<sub>2</sub> production from complex substrates (Fig. 2). The IWA 960 961 ADM1 has been used extensively to model AD processes [173,174,257,258]. ADM1 is a 962 structured mathematical model based on the COD balance of composite substrates and 963 includes a number of biochemical processes involving disintegration of substrates such as 964 hydrolysis, acidogenesis, acetogenesis and methanogenesis, biomass growth and decay 965 processes and the physical interaction of the gas-liquid phases. Because of the similarity of 966 some initial biochemical and physical processes, a modified ADM1 has been proposed to 967 model dark fermentative biohydrogen production processes [31,253,255]. Nonetheless, a model that can simulate the process and predict the formation of all the major intermediates 968 969 and biohydrogen considering all influencing parameters is a present necessity.

# 970 **7.2 Energy balance and COD conversion**

- The net energy gain in DF processes is an important issue that has been addressed by few
- 972 researchers [209,259,260]. The energy balance is an important factor for the process
- 973 sustainability. Higher culture temperatures have been suggested in the literature
- 974 [40,41,45,133,261] for maximizing H<sub>2</sub> yield, without considering the net energy gain [259].
- 975 Some studies [209,259] suggested that DF processes have to be operated at ambient
- 976 temperature in order to obtain a positive net energy. After evaluation of literature data on DF
- 977 of different substrates, Perera et al. [259] reported the net energy gain in dark fermentative
- 978 processes is positive when the process temperature is below 25 °C. In another study by

- Ruggeri et al. [209], the optimum working temperature of 20 °C has been recommended
- 980 which offers 20% of the available energy. However, these studies have suggested to couple
- 981 DF processes with AD, microbial fuel cells, bioelectrochemical systems or photofermentation
- to obtain a more positive net energy balance from the recovery of energy from the DF end-
- 983 products and residues.

Perera et al. [259] reported that DF combined with BES or DF with AD can result in positive

- 985 energy yield. Similarly, Ruggeri et al. [209] found that the AD step after DF can deliver a
- positive net energy with 40-90% available energy. Su et al. [196] obtained a higher
- conversion efficiency of the heat value in DF from 13.3% to 46.0% when combined with
  photofermentation. This was due to an increase of the H<sub>2</sub> yield from 1.59 to 5.48 mol H<sub>2</sub>/mol
- 989 glucose.
- 990 Lower rates of COD reduction efficiencies could be a concern if the DF process aims to treat
- the waste biomass. The conversion of COD to hydrogen is low; theoretically 16 g of COD
- 992 reduction is achieved per mole of H<sub>2</sub> obtained. However, the COD is remained in the by-
- products as VFAs and alcohols. Mohammadi et al. [79] obtained 0.41 mmol H<sub>2</sub>/g COD from
- mesophilic DF of POME with a COD removal efficiency of 86%. In another study, O-Thong
- 995 et al. [78] obtained a COD removal efficiency of 55% with  $H_2$  yield of 0.142 LH<sub>2</sub>/L POME.
- Nonetheless, it has been suggested from the studies (presented in Table 10), that combining
- 997 DF processes with AD, BES or PF, will not only improve the energy recovery, but give
- higher COD reduction efficiencies and provide complete treatment of organic wastebiomasses.

### 1000 **7.3 pH control**

1001 Unlike AD processes where the production of acidity from VFAs generation is balanced by 1002 alkalinity of the systems, DF processes are unstable because of the continuous production of 1003 acidity (VFAs production). As discussed in earlier (See Section 4.2.3), a very low pH can 1004 inhibit the hydrogen production, while the acidic range (5-6) favors H<sub>2</sub> production depending 1005 on the type of substrate. The use of an excessive amount of buffers, acids or base to maintain 1006 the pH acidic can decrease the sustainability of the process and increase the salt concentration 1007 of the DF effluents.

- 1008 One of the sustainable solutions could be to explore substrates with a higher pH or alkalinity
- 1009 to equilibrate the system. Choi et al. [56] suggested the use of substrates with a high pH to
- 1010 replace the use of buffers. Life Cycle Analysis (LCA) of two-step thermophilic DF followed

1011 by photofermentation of potato peels, showed that most of the impact was generated by the 1012 use of phosphate buffer during the process [262]. To provide natural buffering, Cavinato et al. [261] recycled the reject water (effluent) from the AD step in the two-step DF and AD. 1013 1014 The AD reject water provided the alkalinity to maintain the pH in the DF step around 5.5, 1015 giving a H<sub>2</sub> yield of 51 L/kgVS of food waste fed with a H<sub>2</sub> content of 37% in the biogas. 1016 However, the major concern with the recirculation of the AD reject water is the activity of 1017 methanogens present in the reject water, which could affect the purity of the biohydrogen 1018 produced in the DF step. In addition, inhibition of H<sub>2</sub> production due to higher levels of 1019 ammonia present in the reject water could be another concern as reported in the study by 1020 Cavinato et al. [77]. Thus, long term studies to assess the effect of reject water recirculation 1021 from the AD step on the  $H_2$  content in biogas produced from DF could open further doors to 1022 ensure the sustainability of DF systems.

# 1023 **7.4 Solid State Dark Fermentation (SSDF)**

1024 Anaerobic reactors are generally categorized into wet (<10% TS), semi-dry (10–20% TS) and dry (>20% TS) processes [263]. However, some categorized wet digestion for low (<15% 1025 1026 TS) substrates and dry digestion of high solids (>15% TS) processes [134]. By increasing the TS content, dry fermentation processes can be operated at a high OLR with little water 1027 1028 addition, which offers advantages such as smaller reactor volume, easy handling of the digestate residues and technical simplicity [134,263]. This could be attractive for 1029 1030 commercialization of these processes. However, the drawbacks of SSDF are the low H<sub>2</sub> 1031 yields due to mass and energy transfer limitations, which affects the product formation [137]. 1032 Using agro-industrial wastes (70% sugarcane bagasse, 15% of pineapple peelings and 15% of waste activated sludge) under mesophilic conditions, Robledo-Narváez [137] found a 1033 1034 decrease in H<sub>2</sub> yield (3 mmol H<sub>2</sub>/g TS) at a TS content higher than 18 % TS in a tested TS 1035 content range from 15-35%. Similar results were obtained by Valdez-vazquez and Poggi-1036 Varaldo [138], where highest H<sub>2</sub> productivity and yield (463.7 NmL/kg.d and 54.8 N mL/g 1037 VS removed, respectively) was obtained at a TS of 20.9 % using organic solid waste (paper 1038 (40%) and food (60%) wastes) for the tested TS range from 20.9 – 35.1 % TS. Likewise, 1039 Motte et al. [136] also reported 19 % TS as the limit to achieve higher H<sub>2</sub> production performance during the DF of wheat straw, as metabolic pathways shifted towards lactic acid 1040 1041 formation at higher TS content. Further research is required on SSDF in order to elucidate the mechanisms involved during dark fermentation at high TS contents. This research couldprovide practical solutions for biohydrogen production from organic solid waste.

#### 1044 **8.** Conclusions

1045 DF technology has an excellent future potential for biohydrogen production as renewable 1046 biomass can be used as a feedstock and the integration with other systems could foster a 1047 higher H<sub>2</sub> yield and economic feasibility. The economic considerations and production at industrial scale recommend a continuous bioprocess. Thus, more research on continuous DF 1048 1049 processes needs to be carried out to demonstrate the long term operational feasibility of 1050 continuous process. Microbial community of hydrogen producers and innovative substrates 1051 needs to be explored. The use of spent dark fermentation residues in photofermentation and 1052 or electrochemical systems as a secondary step could pave the way towards sustainable 1053 biohydrogen production in up-scaled systems. Finally, anaerobic digestion is required to 1054 further stabilize the residues generated from the upstream processes. The future design and 1055 configuration of industrial scale dark fermentative processes is expected to be similar as of 1056 anaerobic digestion processes, with some modifications in process parameters [43]. The 1057 available two stage methane producing plants can be modified for dark fermentation [264], 1058 while solid state dark fermentation opens new opportunities for biohydrogen production from 1059 renewable biomass.

### 1060 Acknowledgements

The authors would like to acknowledge the Erasmus Mundus Joint Doctorate Programme
ETeCoS<sup>3</sup> (Environmental Technologies for Contaminated Solids, Soils and Sediments) under
the EU grant agreement FPA No 2010-0009. This research was further supported by the
project "Modular photo-biologic reactor for bio-hydrogen: application to dairy waste – REMIDA" from the Agriculture Department of the Campania Region in the context of the
Programme of Rural Development 2007-2013, Measure 124.

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