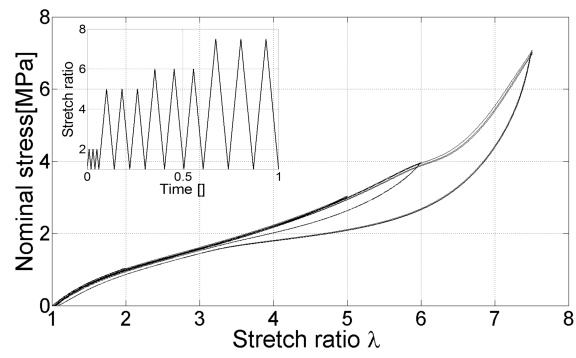
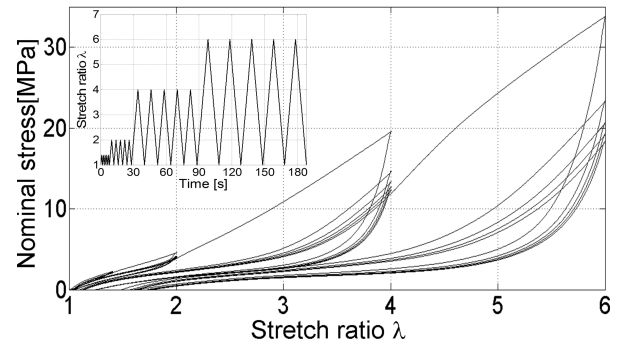


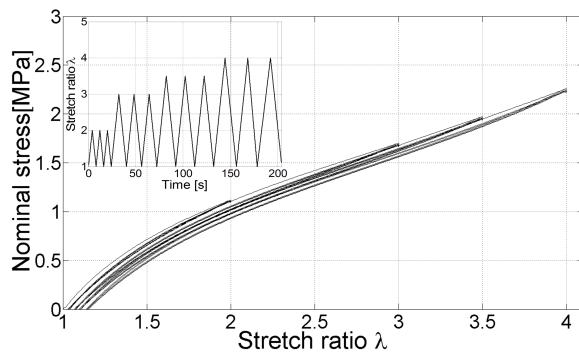
Figure 1: Specimen geometry: (a) front view; (b) side view



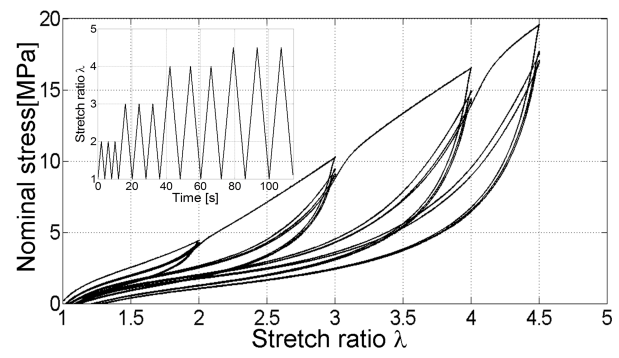
(a) NR0



(b) NR50

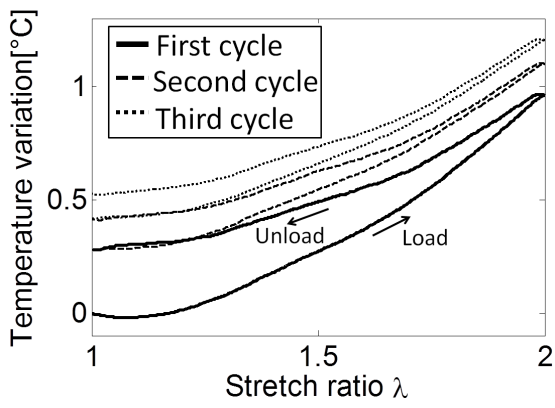


(c) SBR5

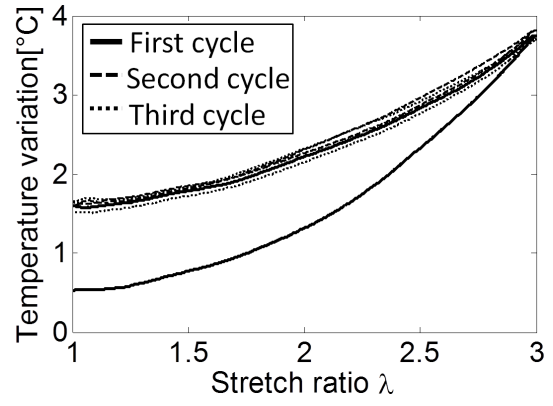


(d) SBR50

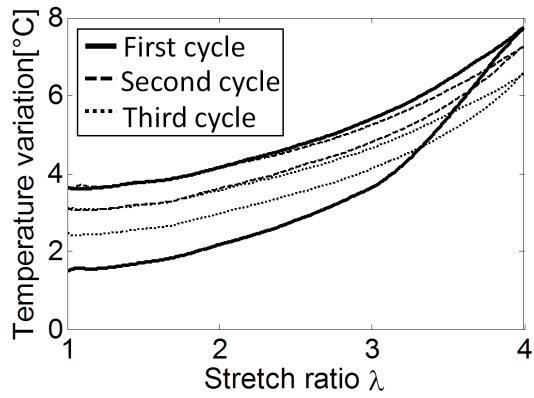
Figure 2: Loading conditions and mechanical responses obtained for the four compounds during cyclic uniaxial tensile tests



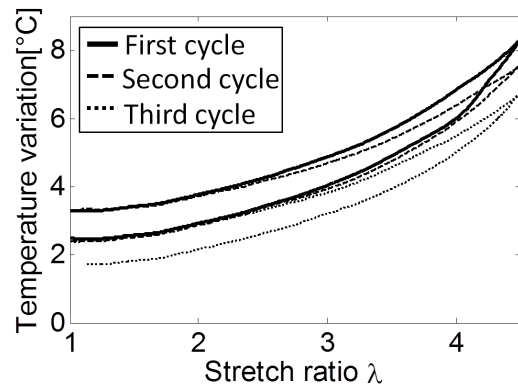
(a) $\lambda=2$



(b) $\lambda=3$

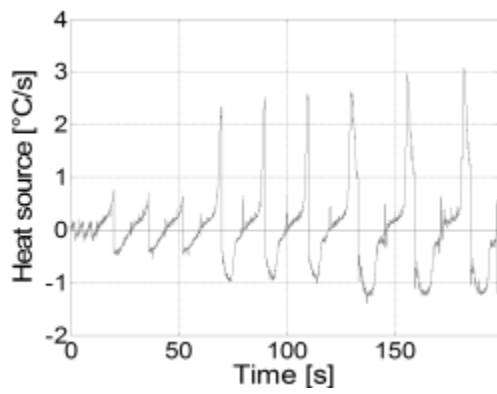


(c) $\lambda=4$

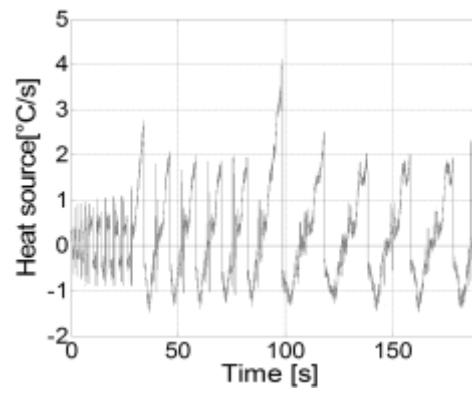


(d) $\lambda=4.5$

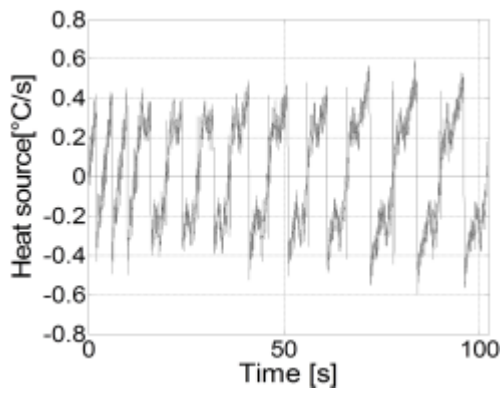
Figure 3: Temperature variation versus stretch ratio in SBR50



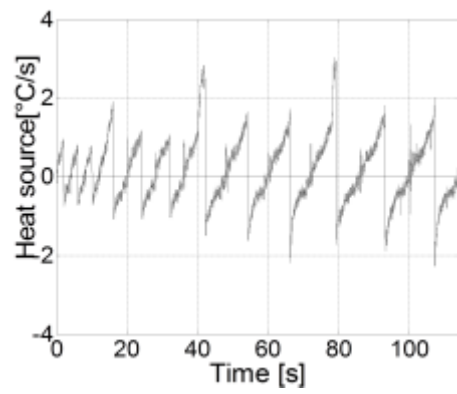
(a) NR0



(b) NR50



(c) SBR5



(d) SBR50

Figure 4: Heat source evolution obtained for the four compounds during cyclic uniaxial tensile tests

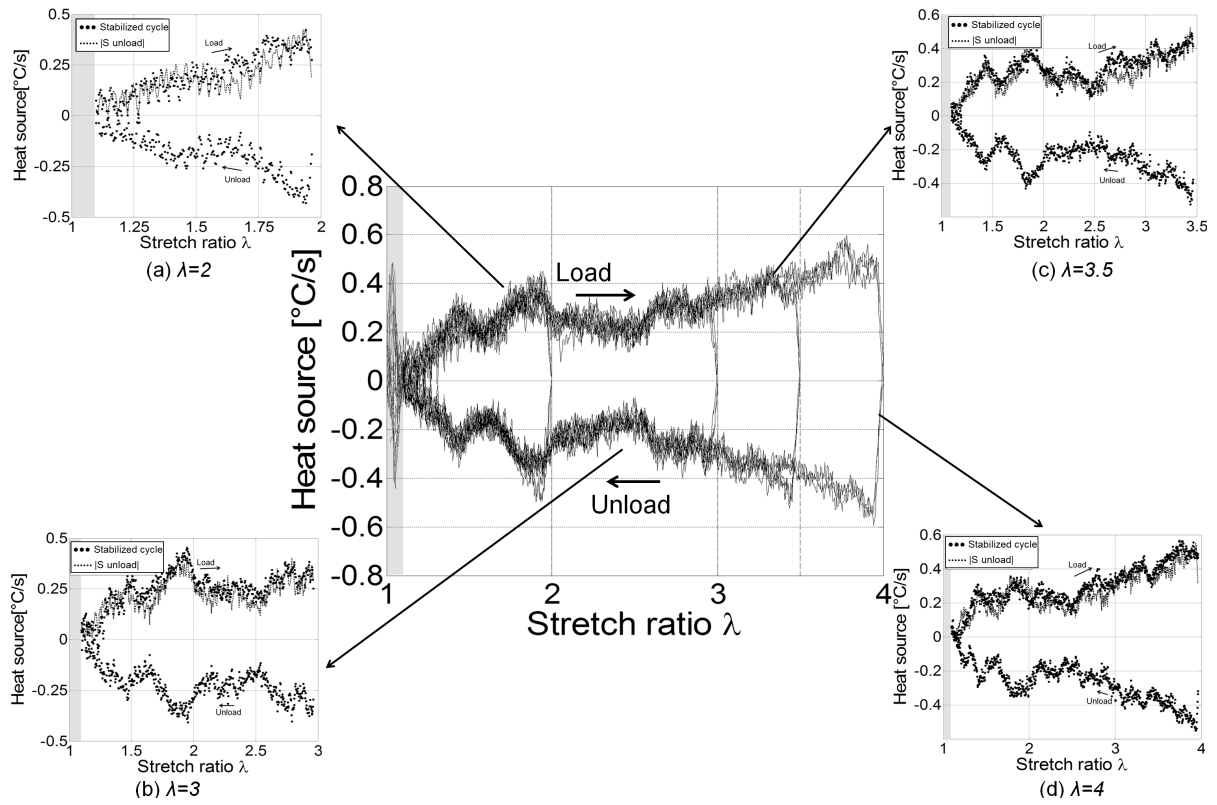


Figure 5: Heat source versus stretch ratio obtained for SBR5. The light continuous lines correspond to the absolute value of the heat source during unloading.

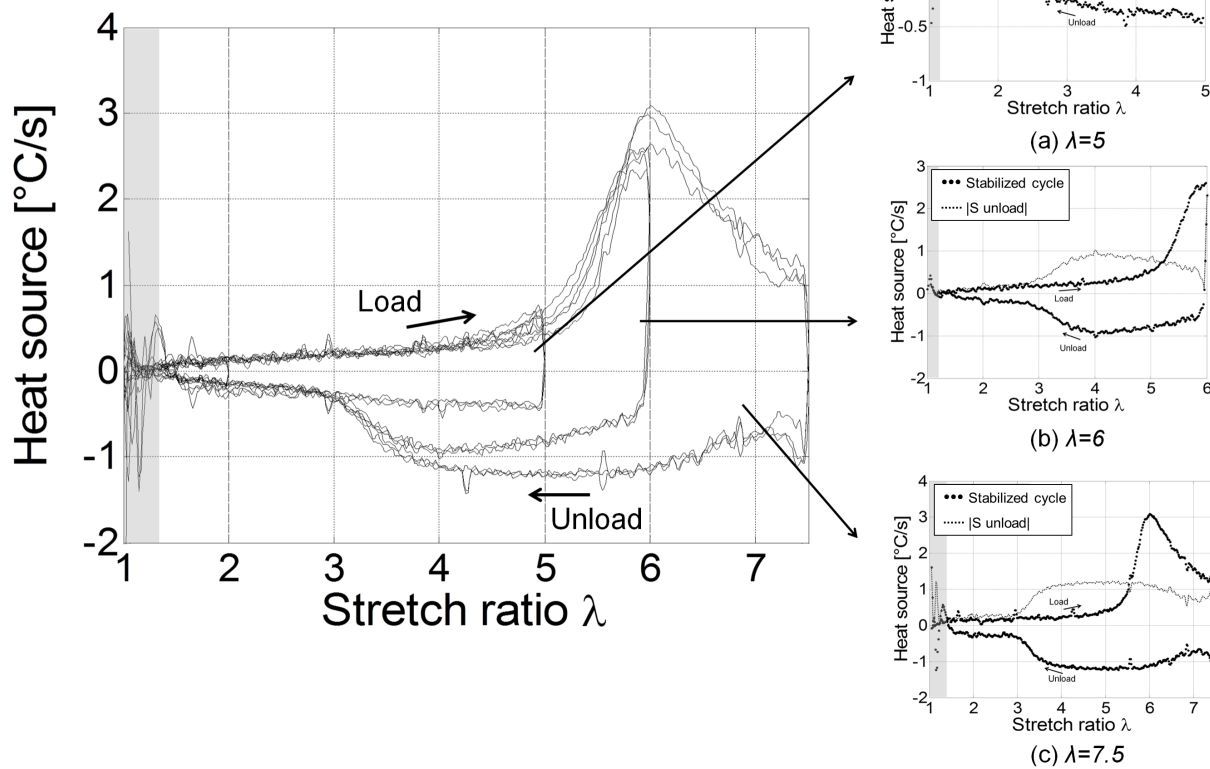


Figure 6: Heat source versus stretch ratio obtained for NR0. The light continuous lines correspond to the absolute value of the heat source during unloading.

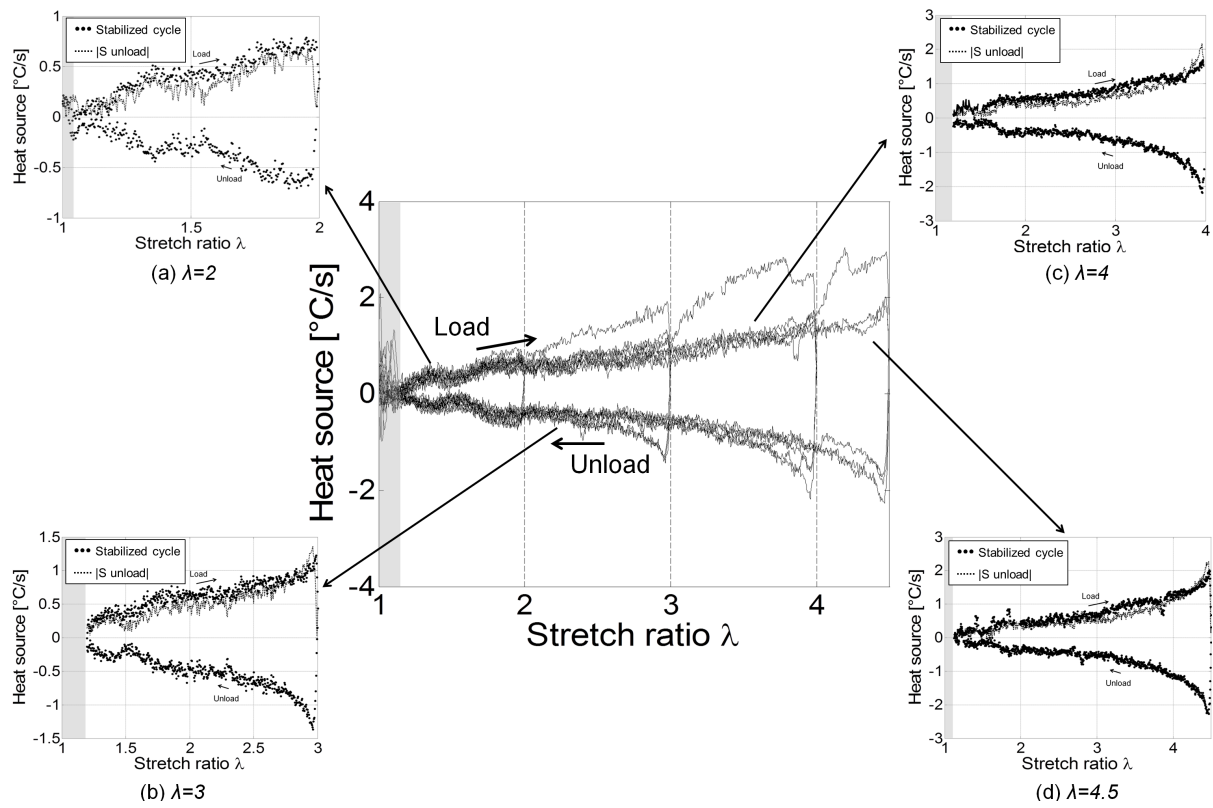


Figure 7: Heat source versus stretch ratio obtained for SBR50. The light continuous lines correspond to the absolute value of the heat source during unloading.

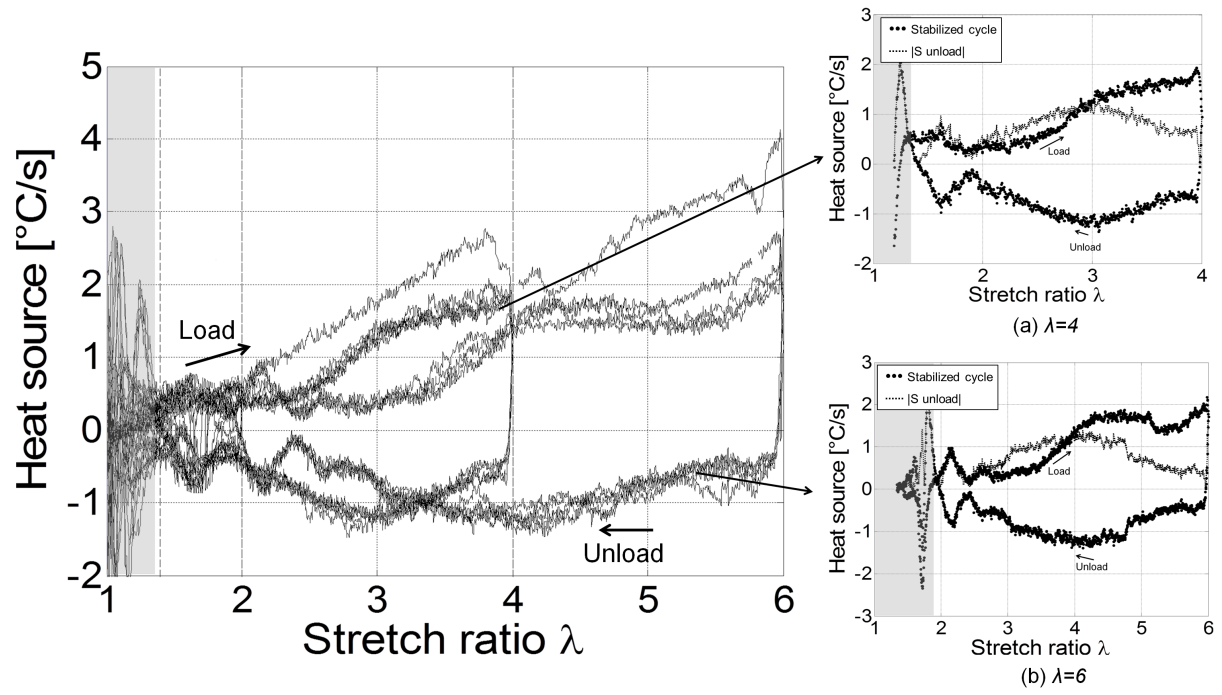
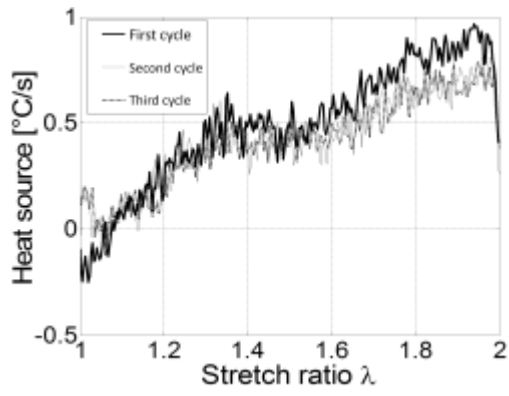
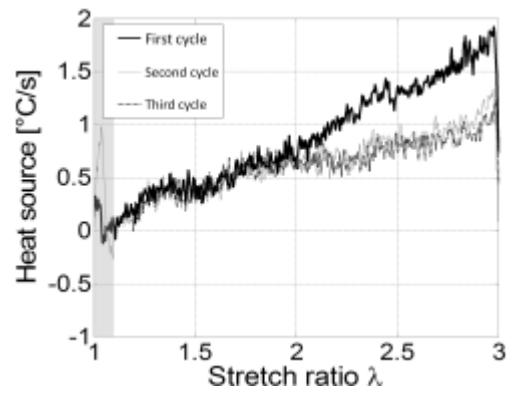


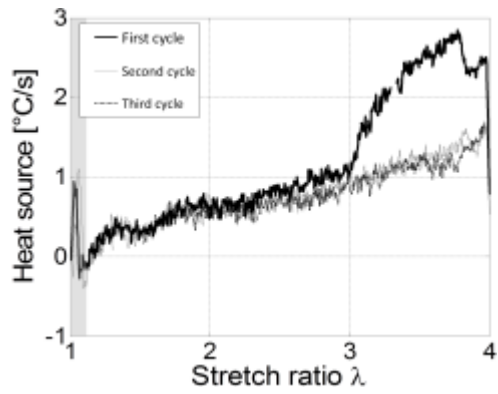
Figure 8: Heat source versus stretch ratio obtained for NR50. The light continuous lines correspond to the absolute value of the heat source during unloading.



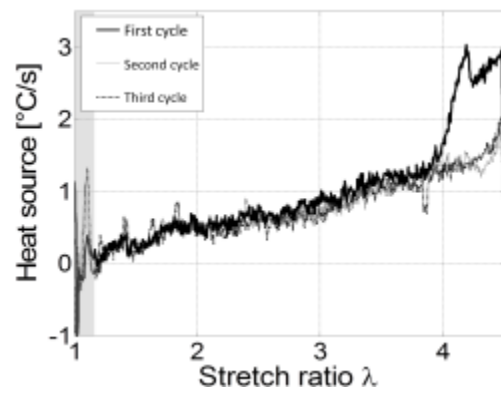
(a) $\lambda=2$



(b) $\lambda=3$

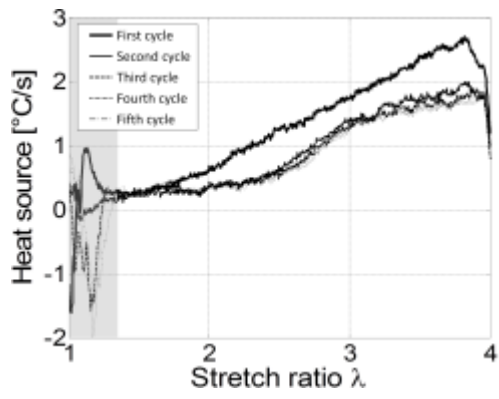


(c) $\lambda=4$

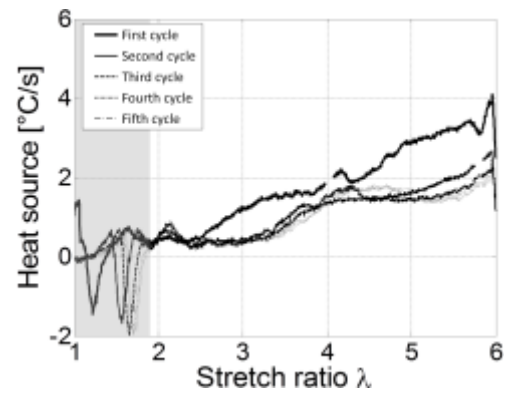


(d) $\lambda=4.5$

Figure 9: Heat source obtained during the loading phase for SBR50



(a) $\lambda=4$



(b) $\lambda=6$

Figure 10: Heat sources obtained during the loading phase for NR50