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Research Article

Spectral Correlation of Multicarrier Modulated Signals and Its Application for Signal Detection

Haijian Zhang, Didier Le Ruyet (EURASIP Member), and Michel Terré

Electronics and Communications Laboratory, CNAM, 75141 Paris, France

Correspondence should be addressed to Haijian Zhang, haijian.zhang@cnam.fr

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Spectral correlation theory for cyclostationary time-series signals has been studied for decades. Explicit formulas of spectral correlation function for various types of analog-modulated and digital-modulated signals are already derived. In this paper, we investigate and exploit the cyclostationarity characteristics for two kinds of multicarrier modulated (MCM) signals: conventional OFDM and filter bank based multicarrier (FBMC) signals. The spectral correlation characterization of MCM signal can be described by a special linear periodic time-variant (LPTV) system. Using this LPTV description, we have derived the explicit theoretical formulas of nonconjugate and conjugate cyclic autocorrelation function (CAF) and spectral correlation function (SCF) for OFDM and FBMC signals. According to theoretical spectral analysis, Cyclostationary Signatures (CS) are artificially embedded into MCM signal and a low-complexity signature detector is, therefore, presented for detecting MCM signal. Theoretical analysis and simulation results demonstrate the efficiency and robustness of this CS detector compared to traditional energy detector.

1. Introduction

A cyclostationary process is an appropriate probabilistic model for the signals that undergo periodic transformation, such as sampling, modulating, multiplexing, and coding operations, provided that the signal is appropriately modeled as a stationary process before undergoing the periodic transformation [1]. Increasing demands on communication system performance indicate the importance of recognizing the cyclostationary character of communicated signals. The growing role of the cyclostationarity is illustrated by abundant works in the detection area and other signal processing areas. Spectral correlation is an important characteristic property of wide sense cyclostationarity, and a spectral correlation function is a generalization of the power spectral density (PSD) function. Recently, the spectral correlation function has been largely exploited for signal detection, estimation, extraction and classification mainly because different types of modulated signals have highly distinct spectral correlation functions and the fact stationary noise and interference exhibit no spectral correlation property. Furthermore, the spectral correlation function contains

phase and frequency information related to timing parameters in modulated signals.

In [1, 2], explicit formulas of the CAF and SCF for various types of single carrier modulated signals are derived. The cyclostationary properties of OFDM have been analyzed in [3, 4], and the formulas of CAF and SCF of OFDM signal are derived by a mathematic deduce process in [3], whereas the authors in [4] provide a straightforward derivation of CAF and SCF for OFDM signal by a matrix-based stochastic method without involving complicated theory. For FBMC signals, the second-order cyclostationarity properties of FBMC signal are exploited in [5, 6] for blind joint carrier-frequency offset (CFO) and symbol timing estimation.

The main objective of this article is to obtain the general formulas for calculating the CAF and SCF of MCM signals using a common derivation model. A particularly convenient method for calculating the CAF and SCF for many types of modulated signals is to model the signal as a purely stationary waveform transformed by a Linear Periodically Time-Variant (LPTV) transformation [7, 8]. Multicarrier modulated signal can be regarded as a special model with the multi-input transformed by LPTV transformation and one

scalar output. By modeling MCM signal into a LPTV system it is convenient to analyze MCM signal using the known LPTV theory. With the help of the mature LPTV theory, herein we derive the explicit formulas for nonconjugate and conjugate cyclic autocorrelation function and spectral correlation function of OFDM and FBMC signals, which are very useful for blind MCM signals detection and classification.

Cognitive Radio (CR) has recently been proposed as a possible solution to improve spectrum utilization via dynamic spectrum access, and spectrum sensing has also been identified as a key enabling functionality to ensure that cognitive radios would not interference with primary users. We are interested in various efficient (low Signal-to-Noise Ratio, (SNR), detection requirement of licensed signal) and low-complex methods for the detection of free bands at the worst situation that we know only few information about the received signal. Cyclostationary based detector is efficient and more robust than energy detector [9], which is highly susceptible to noise uncertainty. In most of practical situations, it is not very likely that the cognitive radio has access to the nature of licensed signal, hence rendering noise estimation impossible. The worse thing is that energy detector cannot differentiate between modulated signals, noise and interference. Feature detector such as cyclostationarity is, therefore, proposed for signal detection in CR context. An inherent cyclostationary detection method, by detecting the presence of nonconjugate cyclostationarity in some non-zero cyclic frequency, is proposed in [3]. Although this detector exhibits good detection performance, it cannot achieve the low SNR requirement of CR system specified by FCC. In addition, the computation of the proposed cyclostationarity detection algorithm is complex.

Therefore, in order to alleviate the computation complexity and achieve better detection performance for low SNR level, we apply a conjugate cyclostationarity detector by inserting Cyclostationary Signature [10] (CS), which is realized by redundantly transmitting message symbols at some predetermined cyclic frequency based on the theoretical spectral analysis and the fact that most of the MCM signals and noise do not exhibit conjugate cyclostationarity. Previous works introducing artificially cyclostationarity for OFDM signal at the transmitter can be found in [10–12]. In this paper, the signal detection between FBMC signal and noise is investigated. We implement the spectral detection of FBMC signal embedded by CS using a low-complexity conjugate cyclostationarity detector considering both AWGN and Rayleigh fading environments in the CR domain. Experimental results are provided to show the efficiency and the robustness compared to the traditional energy detector.

The remainder of this paper is organized as follows: Section 2 presents the basic definition of spectral correlation. The fundamental concepts of LPTV system are mentioned in Section 3. Through the aforementioned theoretical knowledge, Section 4 analyzes and derives the theoretical formulas of nonconjugate and conjugate cyclic autocorrelation and spectral correlation functions of OFDM and FBMC signals. In Section 5, corresponding spectral analysis for FBMC

signals with CS is investigated. A low-complexity CS detector is presented in Section 6. Simulation results are given in Section 7. Finally, conclusions are drawn in Section 8.

2. Definition of Cyclic Spectral Correlation

A complete understanding of the concept of spectral correlation is given in the tutorial paper [8]. This section is a very brief review of the fundamental definitions for spectral correlation.

The probabilistic nonconjugate autocorrelation of a stochastic process $x(t)$ is

$$R_x(t, \tau) = E \left[x \left(t + \frac{\tau}{2} \right) x^* \left(t - \frac{\tau}{2} \right) \right], \quad (1)$$

where the superscript asterisk denotes complex conjugation. $x(t)$ is defined to be second-order cyclostationary (in the wide sense) if $R_x(t, \tau)$ is the periodic function about t with period T_0 and can be represented as a Fourier series:

$$R_x(t, \tau) = \sum_{\alpha} R_x^{\alpha}(\tau) e^{j2\pi\alpha t}, \quad (2)$$

which is called *periodic autocorrelation function*, where the sum is taken over integer multiples of the fundamental frequency “ $1/T_0$ ”. The Fourier coefficients can be calculated as

$$R_x^{\alpha}(\tau) = \lim_{T \rightarrow \infty} \frac{1}{T} \int_{-T/2}^{T/2} R_x(t, \tau) e^{-j2\pi\alpha t} dt, \quad (3)$$

where $\alpha = \text{integer}/T_0$, and $R_x^{\alpha}(\tau)$ is called the *cyclic autocorrelation function*. The idealized *cyclic spectrum function* can be characterized as the Fourier transform

$$S_x^{\alpha}(f) = \int_{-\infty}^{\infty} R_x^{\alpha}(\tau) e^{-j2\pi f \tau} d\tau. \quad (4)$$

In the nonprobabilistic approach, for a time-series $x(t)$ that contains second-order periodicity, synchronized averaging applied to the lag product time-series “ $y(t) \triangleq x(t + \tau/2)x^*(t - \tau/2)$ ” yields

$$\begin{aligned} \hat{R}_x(t, \tau) &\triangleq \lim_{N \rightarrow \infty} \frac{1}{2N+1} \sum_{n=-N}^N x \left(t + nT_0 + \frac{\tau}{2} \right) \\ &\quad \cdot x^* \left(t + nT_0 - \frac{\tau}{2} \right), \end{aligned} \quad (5)$$

which is referred to as the *limit periodic autocorrelation function*. The nonprobabilistic counterpart of (3) is given by

$$\hat{R}_x^{\alpha}(\tau) \triangleq \lim_{T \rightarrow \infty} \frac{1}{T} \int_{-T/2}^{T/2} x \left(t + \frac{\tau}{2} \right) x^* \left(t - \frac{\tau}{2} \right) e^{-j2\pi\alpha t} dt, \quad (6)$$

which is recognized as the *limit cyclic autocorrelation function*. The *limit cyclic spectrum function* can be characterized as the Fourier transform like (4):

$$\hat{S}_x^{\alpha}(f) = \int_{-\infty}^{\infty} \hat{R}_x^{\alpha}(\tau) e^{-j2\pi f \tau} d\tau. \quad (7)$$

The limit cyclic spectrum function is also called *spectral correlation function*. Fourier transform relation in (7) is called the *cyclic Wiener relation*.

In summary, the limit cyclic autocorrelation can be interpreted as a Fourier coefficient in the Fourier series expansion of the limit periodic autocorrelation like (2). If $\hat{R}_x^\alpha(\tau) \equiv 0$ for all $\alpha \neq 0$ and $\hat{R}_x(\tau) \neq 0$, then $x(t)$ is *purely stationary*. If $\hat{R}_x^\alpha(\tau) \neq 0$ only for $\alpha = \text{integer}/T_0$ for some period T_0 , then $x(t)$ is *purely cyclostationary* with period T_0 . If $\hat{R}_x^\alpha(\tau) \neq 0$ for values of α that are not all integer multiples of some fundamental frequency $1/T_0$, then $x(t)$ is said to *exhibit cyclostationary* [1]. For modulated signals, the periods of cyclostationarity correspond to carrier frequencies, pulse rates, spreading code repetition rates, time-division multiplexing rates, and so on.

In paper [8], an useful modification of the CAF called *conjugate cyclic autocorrelation function* is given as

$$R_{x^*}^\alpha(\tau) = \lim_{T \rightarrow \infty} \frac{1}{T} \int_{-T/2}^{T/2} R_x^*(t, \tau) e^{-j2\pi\alpha t} dt, \quad (8)$$

with $R_x^*(t, \tau) = E[x(t + \tau/2)x(t - \tau/2)]$, and the corresponding SCF called *conjugate spectral correlation function* is

$$S_{x^*}^\alpha(f) = \int_{-\infty}^{\infty} R_{x^*}^\alpha(\tau) e^{-j2\pi f \tau} d\tau. \quad (9)$$

For a noncyclostationary signal, $R_x^\alpha(\tau) = R_{x^*}^\alpha(\tau) = S_x^\alpha(f) = S_{x^*}^\alpha(f) = 0$ for all $\alpha \neq 0$, and for a cyclostationary signal, any nonzero value of the frequency parameter α , for which the nonconjugate and conjugate CAFs and SCFs differ from zero is called a *cycle frequency*. Both nonconjugate and conjugate CAFs and SCFs are discrete functions of the cycle frequency α and are continuous in the lag parameter τ and frequency parameter f , respectively.

3. LPTV System

LPTV is a special case of linear almost-periodically time-variant (LAPTV), which is introduced in [7]. A linear time-variant system with input $x(t)$, output $y(t)$, impulse response function $h(t, u)$, and input-output relation

$$y(t) = \int_R h(t, u) x(u) du, \quad (10)$$

is said to be LPTV if the impulse response function admits the Fourier series expansion:

$$h(t, u) = \sum_{\sigma \in G} h_\sigma(t - u) e^{j2\pi\sigma u}, \quad (11)$$

where G is a countable set.

By substituting (11) into (10) the output $y(t)$ can be expressed in the two equivalent forms

$$y(t) = \sum_{\sigma \in G} h_\sigma(t) \otimes [x(t) e^{j2\pi\sigma t}], \quad (12)$$

$$y(t) = \sum_{\sigma \in G} [g_\sigma(t) \otimes x(t)] e^{j2\pi\sigma t}, \quad (13)$$

where “ \otimes ” denotes convolution operation, and

$$g_\sigma(t) = h_\sigma(t) e^{-j2\pi\sigma t}. \quad (14)$$

From (12) it follows that a LPTV system performs a linear time-invariant filtering of frequency-shifted version of the input signal. For this reason LPTV is also referred to as *frequency-shift* filtering. Equivalently, from (13) it follows that a LPTV system performs a frequency shift of linear time-invariant filtered versions of the input.

In the special case for which $G \equiv \{k/T_0\}_{k \in \mathbb{Z}}$ for some period T_0 , the system becomes the linear periodically time-variant (LPTV).

LPTV transformation is defined as follows [8]:

$$y(t) = \int_{-\infty}^{\infty} \hat{\mathbf{h}}(t, u) \hat{\mathbf{x}}(u) du, \quad (15)$$

where $\hat{\mathbf{x}}$ is a L -element column vector input (L is any non-zero positive integer) and $y(t)$ is a scalar response. $\hat{\mathbf{h}}(t, u) = \hat{\mathbf{h}}(t + T_0, u + T_0)$ is the periodically time-variant (L -element row vector) of impulse response functions that specify the transformation. The function $\hat{\mathbf{h}}(t + \tau, t)$ is periodic in t with a period T_0 for each τ represented by the Fourier series

$$\hat{\mathbf{h}}(t + \tau, t) = \sum_{n=-\infty}^{\infty} \hat{\mathbf{g}}_n(\tau) e^{j2\pi n t / T_0}, \quad (16)$$

where

$$\hat{\mathbf{g}}_n(\tau) = \frac{1}{T_0} \int_{-T_0/2}^{T_0/2} \hat{\mathbf{h}}(t + \tau, t) e^{-j2\pi n t / T_0} dt. \quad (17)$$

The Fourier transform of function $\hat{\mathbf{h}}(t + \tau, t)$ is defined as a system function:

$$\hat{\mathbf{G}}(t, f) = \int_{-\infty}^{\infty} \hat{\mathbf{h}}(t, t - \tau) e^{-j2\pi f \tau} d\tau, \quad (18)$$

which can be also represented by a Fourier series:

$$\hat{\mathbf{G}}(t, f) = \sum_{n=-\infty}^{\infty} \hat{\mathbf{G}}_n\left(f + \frac{n}{T_0}\right) e^{j2\pi n t / T_0}, \quad (19)$$

where

$$\hat{\mathbf{G}}_n(f) = \int_{-\infty}^{\infty} \hat{\mathbf{g}}_n(\tau) e^{-j2\pi f \tau} d\tau. \quad (20)$$

By substitution of (15) and (16) into the definition of (3) and (4), it can be shown that the nonconjugate cyclic autocorrelation and cyclic spectrum of the input $\hat{\mathbf{x}}(t)$ and output $y(t)$ of the LPTV system are related by the formulas

$$R_y^\alpha(\tau) = \sum_{n, m=-\infty}^{\infty} \text{trace} \left\{ \left[\hat{\mathbf{R}}_x^{\alpha-(n-m)/T_0}(\tau) \cdot e^{-j\pi(n+m)\tau/T_0} \right] \otimes \hat{\mathbf{R}}_{nm}^\alpha(-\tau) \right\}, \quad (21)$$

$$S_y^\alpha(f) = \sum_{n, m=-\infty}^{\infty} \hat{\mathbf{G}}_n\left(f + \frac{\alpha}{2}\right) \hat{\mathbf{S}}_x^{\alpha-(n-m)/T_0}\left(f - \frac{[n+m]}{2T_0}\right) \cdot \hat{\mathbf{G}}_m^T\left(f - \frac{\alpha}{2}\right)^*, \quad (22)$$

where “ \otimes ” denotes convolution operation, the superscript symbol “ T ” denotes matrix transposition, and “ $*$ ” denotes conjugation. $\hat{\mathbf{R}}_x^\beta$ is the matrix of cyclic cross-correlation of the elements of the vector $\hat{\mathbf{x}}(t)$

$$\hat{\mathbf{R}}_x^\beta(\tau) = \lim_{T \rightarrow \infty} \frac{1}{T} \int_{-T/2}^{T/2} \hat{\mathbf{x}}^* \left(t + \frac{\tau}{2} \right) \hat{\mathbf{x}}^T \left(t - \frac{\tau}{2} \right) e^{-j2\pi\beta t} dt, \quad (23)$$

and $\hat{\mathbf{r}}_{nm}^\alpha$ is the matrix of finite cyclic cross correlation

$$\hat{\mathbf{r}}_{nm}^\alpha(\tau) = \int_{-\infty}^{\infty} \hat{\mathbf{g}}_n^T \left(t + \frac{\tau}{2} \right) \hat{\mathbf{g}}_m^* \left(t - \frac{\tau}{2} \right) e^{-j2\pi\alpha t} dt. \quad (24)$$

Formulas (21) and (22) reveal that the cyclic autocorrelation and spectra of a modulated signal are each self-determinant characteristics under an LPTV transformation.

The conjugate cyclic autocorrelation and cyclic spectrum of the input $\hat{\mathbf{x}}(t)$ and output $y(t)$ of the LPTV system are obtained similarly:

$$R_{y^*}^\alpha(\tau) = \sum_{n,m=-\infty}^{\infty} \text{trace} \left\{ \left[\hat{\mathbf{R}}_{x^*}^{\alpha-(n+m)/T_0}(\tau) \cdot e^{-j\pi(n-m)\tau/T_0} \right] \otimes_{nm}^\alpha(-\tau) \right\}, \quad (25)$$

$$S_{y^*}^\alpha(f) = \sum_{n,m=-\infty}^{\infty} \hat{\mathbf{G}}_n \left(f + \frac{\alpha}{2} \right) \hat{\mathbf{S}}_{x^*}^{\alpha-(n+m)/T_0} \left(f - \frac{[n-m]}{2T_0} \right) \cdot \hat{\mathbf{G}}_m^T \left(f - \frac{\alpha}{2} \right), \quad (26)$$

$$\hat{\mathbf{R}}_{x^*}^\beta(\tau) = \lim_{T \rightarrow \infty} \frac{1}{T} \int_{-T/2}^{T/2} \hat{\mathbf{x}} \left(t + \frac{\tau}{2} \right) \hat{\mathbf{x}}^T \left(t - \frac{\tau}{2} \right) e^{-j2\pi\beta t} dt, \quad (27)$$

$$\hat{\mathbf{r}}_{nm}^\alpha(\tau) = \int_{-\infty}^{\infty} \hat{\mathbf{g}}_n^T \left(t + \frac{\tau}{2} \right) \hat{\mathbf{g}}_m \left(t - \frac{\tau}{2} \right) e^{-j2\pi\alpha t} dt. \quad (28)$$

4. Spectral Correlation of MCM Signals

Generally, the carrier modulated passband MCM signal $c(t)$ can be expressed as

$$c(t) = \text{Re} \left\{ y(t) e^{j2\pi f_c t} \right\}, \quad (29)$$

where Re denotes the real part of $\{\cdot\}$, $y(t)$ is the baseband envelope of the actual transmitted MCM signal, and f_c is the carrier frequency.

If the baseband envelope signal $y(t)$ is cyclostationary, the spectral correlation function of its corresponding carrier modulated signal $c(t)$ can be expressed as [13]

$$S_c^\alpha(f) = \frac{1}{4} \left[S_y^\alpha(f - f_c) + S_y^\alpha(f + f_c) + S_{y^*}^{\alpha-2f_c}(f - f_c) + S_{y^*}^{\alpha+2f_c}(f + f_c) \right], \quad (30)$$

where $S_y^\alpha(s)$ and $S_{y^*}^\alpha(s)$ are the nonconjugate and conjugate spectral correlation function of the complex envelope $y(t)$,

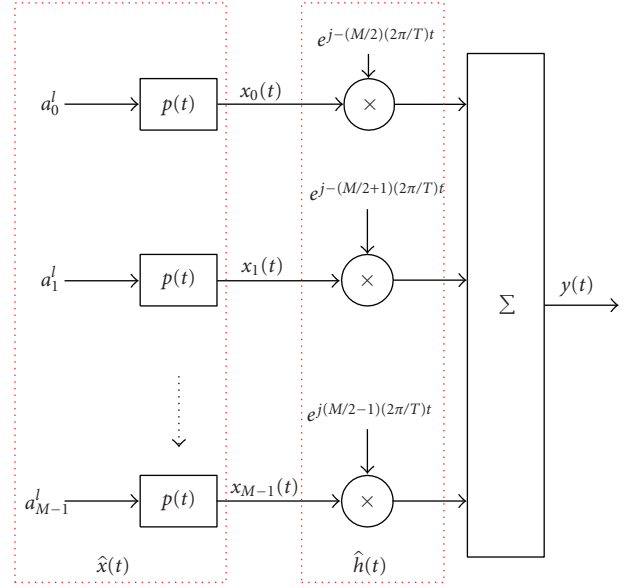


FIGURE 1: Baseband OFDM transmitter.

respectively. We can observe that the spectral correlation of the carrier modulated signal $c(t)$ is determined by the nonconjugate and conjugate spectral correlation of the complex envelope signal $y(t)$ and is related to the double carrier frequency, so the problem of spectral analysis correlation analysis of passband carrier modulated signal can be reduced to the spectral correlation analysis of the complex baseband signal.

The spectral correlation analysis of MCM signals is the theoretical basis for further signal processing. In this section, we investigate two typical MCM signals: OFDM and FBMC signals. Other MCM signals share similar spectral correlation properties with these two signals.

4.1. Spectral Correlation of OFDM Signal Using LPTV.

Figure 1 shows a filter bank based schematic baseband equivalent of transmultiplexer system, based on the LPTV theory M parallel complex data streams are passed to M subcarrier transmission filters. OFDM system is special filter bank based multicarrier system with the rectangular pulse filters. The baseband OFDM signal can be expressed as a sum of M single carrier signals like (15)

$$\begin{aligned} y(t) &= \sum_{k=0}^{M-1} \sum_{l=-\infty}^{\infty} a_k^l p(t - lT_s) \cdot e^{jk(2\pi t/T_0)} \cdot e^{-jM(\pi/T_0)t} \\ &= \sum_{k=0}^{M-1} x_k(t) h_k(t), \end{aligned} \quad (31)$$

where $x_k(t)$ is the element of the input vector of LPTV system and $h_k(t)$ is the element of impulse response of LPTV:

$$\begin{aligned} x_k(t) &= \sum_{l=-\infty}^{\infty} a_k(lT_s) p(t - lT_s), \quad k = 0, 1, \dots, M-1, \\ h_k(t) &= e^{j(k-M/2)(2\pi t/T_0)}, \quad k = 0, 1, \dots, M-1, \end{aligned} \quad (32)$$

for which a_k is the purely stationary data, $T_s = T_0 + T_g$ is one OFDM symbol duration, where T_0 is the useful symbol duration and T_g is the length of the guard interval where the OFDM signal is extended cyclically. $p(t)$ is the rectangular pulse function, and $h_k(t)$ can be regarded as the periodic function in t with the period T_0 for $k = 0, 1, \dots, M-1$.

Element of input vector $x_k(t)$ can also be regarded as an inherent LPTV transformation of data a_k with the time-invariant filters $p(t)$:

$$x_k(t) = a_0(t) \otimes p(t), \quad (33)$$

where

$$a_0(t) = \sum_{l=-\infty}^{\infty} a_k(lT_s) \delta(t - lT_s). \quad (34)$$

Assuming $E[a_{l,k} a_{l,k}^*] = \sigma^2$, each entity of matrix $\hat{\mathbf{R}}_x^\alpha(\tau)$ and $\hat{\mathbf{S}}_x^\alpha(f)$ in (21) and (22) reduce to

$$\begin{aligned} R_{x_k}^\alpha(\tau) &= R_{a_0}^\alpha(\tau) \otimes r_p^\alpha(\tau), \\ S_{x_k}^\alpha(f) &= S_{a_0}^\alpha(f) \cdot S_p^\alpha(f), \end{aligned} \quad (35)$$

where $S_p^\alpha(f)$ is the Fourier transform of $r_p^\alpha(\tau)$ and

$$\begin{aligned} r_p^\alpha(\tau) &= \int_{-\infty}^{\infty} p\left(t + \frac{\tau}{2}\right) p\left(t - \frac{\tau}{2}\right) e^{-j2\pi\alpha t} dt, \\ R_{a_0}^\alpha(\tau) &= \frac{\sigma^2}{T_s} \cdot \delta(\tau), \quad \alpha = \frac{\text{integer}}{T_s}, \\ S_{a_0}^\alpha(f) &= \frac{\sigma^2}{T_s}, \quad \alpha = \frac{\text{integer}}{T_s}. \end{aligned} \quad (36)$$

Other terms corresponding to the LPTV system can be similarly calculated:

$$\begin{aligned} \hat{\mathbf{h}}(t, u) &= \left[e^{j(-M/2)(2\pi t/T_0)} \delta(t - u), \right. \\ &\quad e^{j(1-M/2)(2\pi t/T_0)} \delta(t - u), \dots, \\ &\quad \left. e^{j(M/2-1)(2\pi t/T_0)} \delta(t - u) \right], \\ \hat{\mathbf{G}}(t, f) &= \left[e^{j(-M/2)(2\pi t/T_0)}, e^{j(1-M/2)(2\pi t/T_0)}, \dots, \right. \\ &\quad \left. e^{j(M/2-1)(2\pi t/T_0)} \right], \\ \hat{\mathbf{g}}_n(\tau) &= \begin{bmatrix} g_n^0 \\ \vdots \\ g_n^{M-1} \end{bmatrix} = \begin{bmatrix} \delta(\tau) & \dots & 0 \\ \vdots & \delta(\tau) & \vdots \\ 0 & \dots & \delta(\tau) \end{bmatrix}, \\ \hat{\mathbf{G}}_n(f) &= \begin{bmatrix} G_n^0 \\ \vdots \\ G_n^{M-1} \end{bmatrix} = \begin{bmatrix} 1 & \dots & 0 \\ \vdots & 1 & \vdots \\ 0 & \dots & 1 \end{bmatrix}, \\ n &= -\frac{M}{2}, \dots, \frac{M}{2} - 1 \text{ for } M = 8, 16, \dots \end{aligned} \quad (37)$$

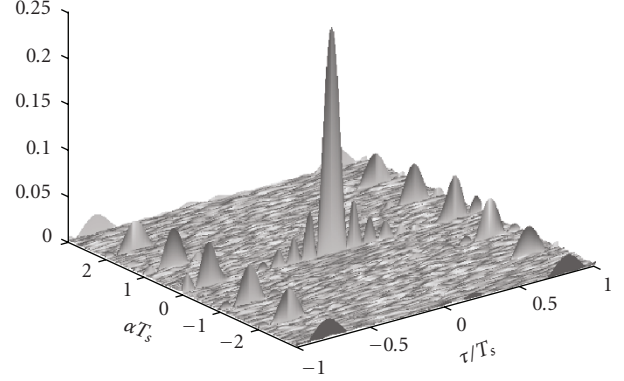


FIGURE 2: 8-channel nonconjugate cyclic autocorrelation of OFDM signal.

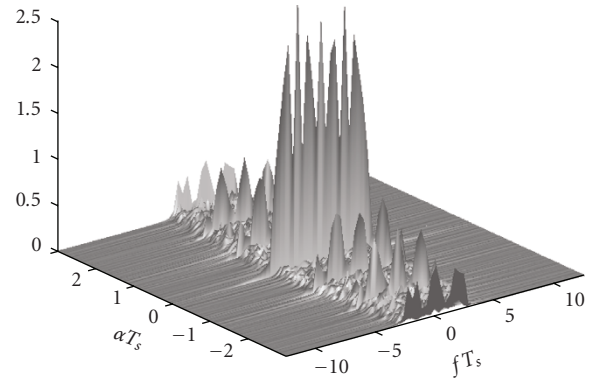


FIGURE 3: 8-channel nonconjugate spectral correlation function of OFDM signal.

Substituting (31)~(37) into (21) and (22), the nonconjugate cyclic autocorrelated and cyclic spectra of OFDM signal are transformed into

$$R_{\text{ofdm}}^\alpha(\tau) = \begin{cases} \frac{\sigma^2}{T_s} \cdot \frac{\sin[\pi\alpha(T_s - |\tau|)]}{\pi\alpha} \\ \cdot \frac{\sin(\pi M\tau/T_0)}{\sin(\pi\tau/T_0)}, & \alpha = \frac{\text{integer}}{T_s}, |\tau| < T_s, \\ 0, & \alpha \neq \frac{\text{integer}}{T_s}, \end{cases} \quad (38)$$

$$S_{\text{ofdm}}^\alpha(f) = \begin{cases} \frac{\sigma^2}{T_s} \sum_{n=-M/2}^{M/2-1} P\left(f + \frac{\alpha}{2} - \frac{n}{T_0}\right) \\ \cdot P^*\left(f - \frac{\alpha}{2} - \frac{n}{T_0}\right), & \alpha = \frac{\text{integer}}{T_s}, \\ 0, & \alpha \neq \frac{\text{integer}}{T_s}, \end{cases} \quad (39)$$

where T_s is the time length of one OFDM symbol, $P(f)$ is the Fourier transform of $p(t)$. The magnitudes of nonconjugate CAF and SCF of OFDM signal are drawn in graphical terms as the heights of surfaces above a bifrequency plane in Figures 2 and 3.

For the conjugate case, according to (25) and (26), the conjugate cyclic autocorrelation and cyclic spectra of OFDM signal are transformed into

$$R_{\text{ofdm}^*}^{\alpha}(\tau) = \begin{cases} \frac{1}{T_s} \sum_{n=-M/2}^{M/2-1} r_p^{\alpha-(2n/T_0)}(\tau) \\ \quad \cdot E[a_{l,k} a_{l,k}^*], \quad \alpha = \frac{\text{integer}}{T_s}, \quad |\tau| < T_s, \\ 0, \quad \alpha \neq \frac{\text{integer}}{T_s}, \end{cases} \quad (40)$$

$$S_{\text{ofdm}^*}^{\alpha}(f) = \begin{cases} \frac{1}{T_s} \sum_{n=-M/2}^{M/2-1} P\left(f + \frac{\alpha}{2} - \frac{n}{T_0}\right) \times P^*\left(f - \frac{\alpha}{2} + \frac{n}{T_0}\right) \\ \quad \cdot E[a_{l,k} a_{l,k}^*], \quad \alpha = \frac{\text{integer}}{T_s}, \\ 0, \quad \alpha \neq \frac{\text{integer}}{T_s}. \end{cases} \quad (41)$$

Consequently, the explicit spectral correlation function of the carrier modulated OFDM signal can be derived by substituting (39) and (41) into (30):

$$S_{\text{ofdm}}^{\alpha}(f) = \begin{cases} \sum_{n=-M/2}^{M/2-1} \left\{ \frac{\sigma^2}{T_s} P\left(f - f_c + \frac{\alpha}{2} - \frac{n}{T_0}\right) \right. \\ \quad \times P^*\left(f - f_c - \frac{\alpha}{2} - \frac{n}{T_0}\right) \\ \quad + \frac{\sigma^2}{T_s} P\left(f + f_c + \frac{\alpha}{2} - \frac{n}{T_0}\right) \\ \quad \times P^*\left(f + f_c - \frac{\alpha}{2} - \frac{n}{T_0}\right) \\ \quad + \frac{A}{T_s} P\left(f - f_c + \frac{\alpha - 2f_c}{2} - \frac{n}{T_0}\right) \\ \quad \times P^*\left(f - f_c - \frac{\alpha - 2f_c}{2} + \frac{n}{T_0}\right) \\ \quad + \frac{A}{T_s} P\left(f + f_c + \frac{\alpha + 2f_c}{2} - \frac{n}{T_0}\right) \\ \quad \times P^*\left(f + f_c - \frac{\alpha + 2f_c}{2} + \frac{n}{T_0}\right) \left. \right\}, \\ \quad \alpha = \frac{\text{integer}}{T_s}, \\ 0, \quad \alpha \neq \frac{\text{integer}}{T_s}, \end{cases} \quad (42)$$

where $A = E[a_{l,k} a_{l,k}^*]$. Since $E[a_{l,k} a_{l,k}^*] = 0$ for MPSK ($M \neq 2$) or QAM modulation types, given that $a_{l,k}$ is centered and i.i.d.. According to (41), it can be seen that the OFDM signal does not exhibit conjugate cyclostationarity, that is $R_{\text{ofdm}^*}^{\alpha}(\tau) = S_{\text{ofdm}^*}^{\alpha}(f) = 0$, for all α, τ, f . The spectral

correlation function of the carrier-modulated signal for MPSK ($M \neq 2$) or QAM modulation can be simplified as

$$S_{\text{ofdm}}^{\alpha}(f) = \begin{cases} \frac{\sigma^2}{T_s} \sum_{n=-M/2}^{M/2-1} \left\{ P\left(f - f_c + \frac{\alpha}{2} - \frac{n}{T_0}\right) \right. \\ \quad \times P^*\left(f - f_c - \frac{\alpha}{2} - \frac{n}{T_0}\right) \\ \quad + P\left(f + f_c + \frac{\alpha}{2} - \frac{n}{T_0}\right) \\ \quad \times P^*\left(f + f_c - \frac{\alpha}{2} - \frac{n}{T_0}\right) \left. \right\}, \\ \quad \alpha = \frac{\text{integer}}{T_s}, \\ 0, \quad \alpha \neq \frac{\text{integer}}{T_s}. \end{cases} \quad (43)$$

4.2. Spectral Correlation of FBMC Signal Using LPTV. An efficient FBMC scheme based on offset quadrature amplitude modulation (OQAM) system has been developed [14–19]. OQAM in [15] can achieve smaller intersymbol interference (ISI) and interchannel interference (ICI) without using the cyclic prefix by utilizing well designed pulse shapes. Saltzberg in [16] showed that by designing a transmit pulse-shape in a multichannel QAM system, and by introducing a half symbol space delay between the in-phase and quadrature components of QAM symbols, it is possible to achieve a baud-rate spacing between adjacent subcarrier channels and still recover the information symbol free of ISI and ICI. Further development was made by Hirosaki [17], who showed that the transmitter and receiver part of this modulation method could be implemented efficiently in a polyphase Discrete Fourier Transform (DFT) structure. Some new progress about OQAM system can be found in [18, 19].

The principle of OQAM multicarrier modulation system is to divide the transmission into M independent transmissions using M subcarriers. Instead of a Fast Fourier Transform (rectangular shape filters), a more normal filter bank $p(t)$ is used. Subcarrier bands are spaced by the symbol rate $1/T_0$ (T_0 is one OQAM symbol period). An introduced orthogonality condition between subcarriers guarantees that the transmitted symbols arrive at the receiver free of ISI and ICI, which is achieved through time staggering the in-phase and quadrature components of the subcarrier symbols by half a symbol period $T_0/2$. The typical baseband OQAM transmitter system is shown in Figure 4.

Supposing the complex input symbols of OQAM system are

$$x_k^l = a_k^l + j b_k^l, \quad (44)$$

where a_k^l and b_k^l are, respectively, the real and imaginary parts of the k th subcarrier of the l th symbol. The complex-valued baseband OQAM signal is defined as

$$y(t) = \sum_{k=0}^{M-1} \sum_{l=-\infty}^{\infty} \left[a_k^l p(t - lT_0) + j b_k^l p\left(t - lT_0 - \frac{T_0}{2}\right) \right] \cdot e^{j(k-M/2)(2\pi t/T_0 + \pi/2)}. \quad (45)$$

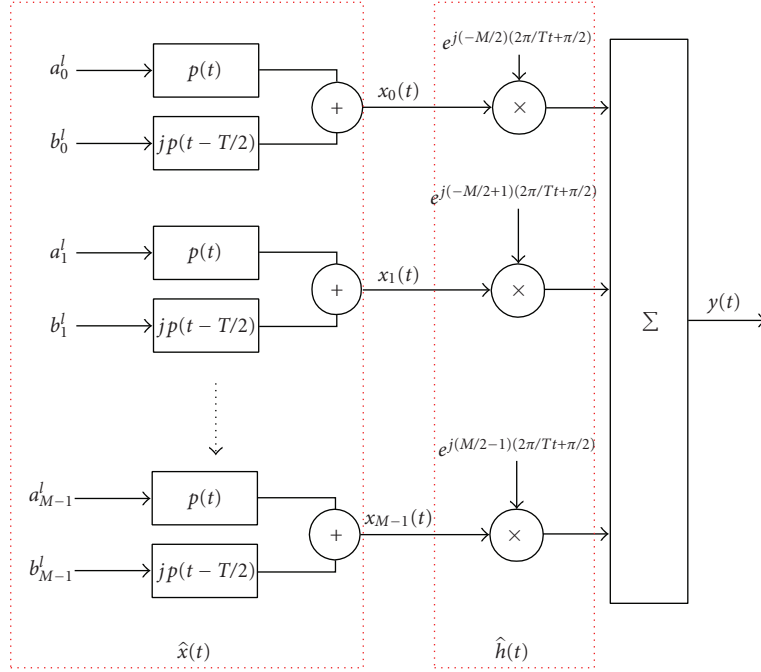


FIGURE 4: Baseband OQAM transmitter.

From (45) and Figure 4 we can see that OQAM signal is a special model with M -input $\hat{\mathbf{x}}(t)$ transformed by LPTV transformation $\hat{\mathbf{h}}(t)$ and one scalar output $y(t)$. The baseband OQAM signal (45) can also be expressed as a sum of M single carrier signals like (15)

$$y(t) = \sum_{k=0}^{M-1} x_k(t) h_k(t), \quad (46)$$

where $x_k(t)$ is the element of the input vector of LPTV system and $h_k(t)$ is the element of impulse response of LPTV

$$x_k(t) = \sum_{l=-\infty}^{\infty} \left\{ a_k(lT_0) p(t - lT_0) + j b_k(lT_0) p\left(t - lT_0 - \frac{T_0}{2}\right) \right\},$$

$$k = 0, 1, \dots, M-1,$$

$$h_k(t) = e^{j(k-M/2)(2\pi t/T_0 + \pi/2)}, \quad k = 0, 1, \dots, M-1, \quad (47)$$

for which a_k and b_k are the purely stationary data, T_0 is one OQAM symbol duration, $p(t)$ is the prototype filter bank pulse function, and $h_k(t)$ can be regarded as the periodic function in t with the period T_0 for $k = 0, 1, \dots, M-1$.

$x_k(t)$ also can be regarded as a two-element vector LPTV transformation of input data a_k and b_k with the time-invariant filters $p(t)$ and $p(t - T_0/2)$:

$$x_k(t) = a_0(t) \otimes p(t) + b_0(t) \otimes p\left(t - \frac{T_0}{2}\right), \quad (48)$$

where

$$a_0(t) = \sum_{l=-\infty}^{\infty} a_k(lT_0) \delta(t - lT_0),$$

$$b_0(t) = \sum_{l=-\infty}^{\infty} j b_k(lT_0) \delta(t - lT_0). \quad (49)$$

Assuming $E[a_{l,k} a_{l,k}^*] = E[b_{l,k} b_{l,k}^*] = \sigma^2$, each entity of matrices $\hat{\mathbf{R}}_x^\alpha(\tau)$ and $\hat{\mathbf{S}}_x^\alpha(f)$ in (21) and (22) reduces to

$$R_{x_k}^\alpha(\tau) = \frac{\sigma^2}{T_0} \cdot [\delta(\tau) \otimes r_{p1}^\alpha(\tau) + \delta(\tau) \otimes r_{p2}^\alpha(\tau)]$$

$$= \frac{\sigma^2}{T_0} \cdot r_{p1}^\alpha(\tau) (1 + e^{-j\pi\alpha T_0}), \quad \alpha = \frac{\text{integer}}{T_0},$$

$$S_{x_k}^\alpha(f) = \frac{\sigma^2}{T_0} \cdot [S_{p1}^\alpha(f) + S_{p2}^\alpha(f)]$$

$$= \frac{\sigma^2}{T_0} \cdot S_{p1}^\alpha(f) (1 + e^{-j\pi\alpha T_0}), \quad \alpha = \frac{\text{integer}}{T_0}, \quad (50)$$

where $S_{p1}^\alpha(f)$ is the Fourier Transform of $r_{p1}^\alpha(\tau)$ and

$$r_{p1}^\alpha(\tau) = \int_{-\infty}^{\infty} p\left(t + \frac{\tau}{2}\right) p\left(t - \frac{\tau}{2}\right) e^{-j2\pi\alpha t} dt,$$

$$r_{p2}^\alpha(\tau) = \int_{-\infty}^{\infty} p\left(t + \frac{\tau}{2} - \frac{T_0}{2}\right) p\left(t - \frac{\tau}{2} - \frac{T_0}{2}\right) e^{-j2\pi\alpha t} dt$$

$$= r_{p1}^\alpha(\tau) e^{-j\pi\alpha T_0}. \quad (51)$$

Other terms corresponding to the LPTV system can be similarly calculated:

$$\begin{aligned}\hat{\mathbf{h}}(t, u) &= \left[e^{j(-(M/2)((2\pi t/T_0)+(\pi/2))} \delta(t-u), \right. \\ &\quad e^{j(1-(M/2)((2\pi t/T_0)+(\pi/2))} \\ &\quad \cdot \delta(t-u), \dots, \\ &\quad \left. e^{j((M/2)-1)((2\pi t/T_0)+(\pi/2))} \delta(t-u) \right], \\ \hat{\mathbf{G}}(t, f) &= \left[e^{j(-(M/2)((2\pi t/T_0)+(\pi/2))}, \right. \\ &\quad e^{j(1-(M/2)((2\pi t/T_0)+(\pi/2))}, \dots, \\ &\quad \left. e^{j((M/2)-1)((2\pi t/T_0)+(\pi/2))} \right], \\ \hat{\mathbf{g}}_n(\tau) &= \begin{bmatrix} g_n^0 \\ \vdots \\ g_n^{M-1} \end{bmatrix} = \begin{bmatrix} \delta(\tau) & \dots & 0 \\ \vdots & e^{j(\pi/2)k} \delta(\tau) & \vdots \\ 0 & \dots & e^{j(\pi/2)(M-1)} \delta(\tau) \end{bmatrix}, \\ \hat{\mathbf{G}}_n(f) &= \begin{bmatrix} G_n^0 \\ \vdots \\ G_n^{M-1} \end{bmatrix} = \begin{bmatrix} 1 & \dots & 0 \\ \vdots & e^{j(\pi/2)k} & \vdots \\ 0 & \dots & e^{j(\pi/2)(M-1)} \end{bmatrix}, \\ n &= -\frac{M}{2}, \dots, \frac{M}{2} - 1 \quad \text{for } M = 8, 16, \dots\end{aligned}\quad (52)$$

By the substitution of (46)~(52) into (21) and (22), the nonconjugate cyclic autocorrelation and cyclic spectra of OQAM signal are transformed into

$$R_{\text{oqam}}^\alpha(\tau) = \begin{cases} \frac{2\sigma^2}{T_0} \cdot r_{p1}^\alpha(\tau) \cdot \frac{\sin(\pi M \tau / T_0)}{\sin(\pi \tau / T_0)}, \\ \alpha = \frac{2 \cdot \text{integer}}{T_0}, \quad |\tau| < K T_0, \\ 0, \quad \alpha \neq \frac{2 \cdot \text{integer}}{T_0}, \end{cases} \quad (53)$$

$$S_{\text{oqam}}^\alpha(f) = \begin{cases} \frac{2\sigma^2}{T_0} \sum_{n=-M/2}^{M/2-1} P\left(f + \frac{\alpha}{2} - \frac{n}{T_0}\right) P^*\left(f - \frac{\alpha}{2} - \frac{n}{T_0}\right) \\ \alpha = \frac{2 \cdot \text{integer}}{T_0}, \\ 0, \quad \alpha \neq \frac{2 \cdot \text{integer}}{T_0}, \end{cases} \quad (54)$$

where $K T_0$ is the time length of the prototype filter bank, $P(f)$ is the Fourier transform of $p(t)$ and $r_{p1}^\alpha(\tau)$ is described as (51). The magnitudes of nonconjugate CAF and SCF of OQAM signal are shown in Figures 5 and 6. We unfortunately found that OQAM signal has very poor

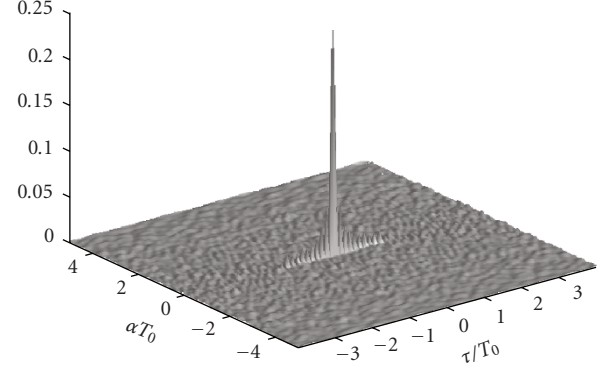


FIGURE 5: 8-channel nonconjugate cyclic autocorrelation of OQAM signal.

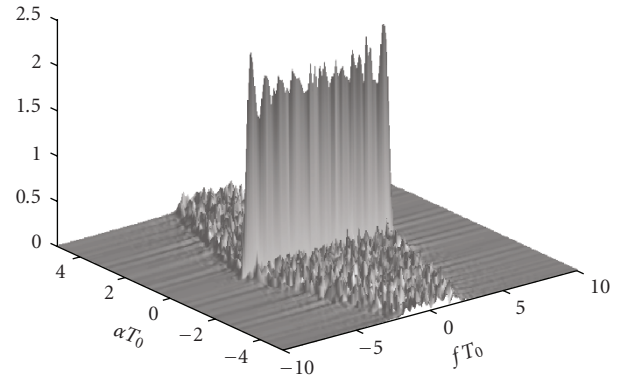


FIGURE 6: 8-channel nonconjugate spectral correlation function of OQAM signal.

inherent cyclostationary property when the cyclic frequency is not equal to zero, which can be interpreted by (54), where the value of cross product “ $P(f + \alpha/2)P^*(f - \alpha/2)$ ” tends to zero when “ $\alpha = 2 \cdot \text{integer}/T_0$ ” due to the low sidelobes property of OQAM prototype function.

For the conjugate situation, assuming $E[a_{l,k}a_{l,k}] = E[b_{l,k}b_{l,k}] = \sigma^2$, in the same way we can get each entity of matrices $\hat{\mathbf{R}}_{x^*}^\alpha(\tau)$ and $\hat{\mathbf{S}}_{x^*}^\alpha(f)$ in (25) and (26):

$$\begin{aligned}R_{x_k^*}^\alpha(\tau) &= \frac{\sigma^2}{T_0} \cdot [\delta(\tau) \otimes r_{p1}^\alpha(\tau) - \delta(\tau) \otimes r_{p2}^\alpha(\tau)] \\ &= \frac{\sigma^2}{T_0} \cdot r_{p1}^\alpha(\tau) (1 - e^{-j\pi\alpha T_0}), \quad \alpha = \frac{\text{integer}}{T_0},\end{aligned} \quad (55)$$

$$\begin{aligned}S_{x_k^*}^\alpha(f) &= \frac{\sigma^2}{T_0} \cdot [S_{p1}^\alpha(f) - S_{p2}^\alpha(f)] \\ &= \frac{\sigma^2}{T_0} \cdot S_{p1}^\alpha(f) (1 - e^{-j\pi\alpha T_0}), \quad \alpha = \frac{\text{integer}}{T_0}.\end{aligned} \quad (56)$$

Substitution of (52), (55), and (56) into (25) and (26), the conjugate cyclic autocorrelation and cyclic spectra of OQAM signal is transformed into

$$R_{\text{oqam}}^{\alpha}(\tau) = \begin{cases} \frac{2\sigma^2}{T_0} \sum_{n=-M/2}^{M/2-1} r_{p1}^{\alpha-2n/T_0}(\tau)(-1)^n, \\ \alpha = \frac{2 \cdot \text{integer} - 1}{T_0}, |\tau| < KT_0, \\ 0, & \alpha \neq \frac{2 \cdot \text{integer} - 1}{T_0}, \end{cases} \quad (57)$$

$$S_{\text{oqam}}^{\alpha}(f) = \begin{cases} \frac{2\sigma^2}{T_0} \sum_{n=-M/2}^{M/2-1} P\left(f + \frac{\alpha}{2} - \frac{n}{T_0}\right) \\ \quad \times P^*\left(f - \frac{\alpha}{2} + \frac{n}{T_0}\right)(-1)^n, \\ \alpha = \frac{2 \cdot \text{integer} - 1}{T_0}, \\ 0, & \alpha \neq \frac{2 \cdot \text{integer} - 1}{T_0}. \end{cases} \quad (58)$$

As same as OFDM signal (except BPSK), OQAM signal does not exhibit conjugate cyclostationarity, either. This property can be exactly interpreted by (58), where the value of cross product " $P(f + \alpha/2 - n/T_0)P^*(f - \alpha/2 + n/T_0)(-1)^n$ " equals to zero due to neighbored offset effect. The explicit spectral correlation function of the carrier modulated FBMC signal can be obtained by substituting (54) into (30):

$$S_{\text{fbmc}}^{\alpha}(f) = \begin{cases} \frac{2\sigma^2}{T_0} \sum_{n=-M/2}^{M/2-1} \left\{ P\left(f - f_c + \frac{\alpha}{2} - \frac{n}{T_0}\right) \right. \\ \quad \times P^*\left(f - f_c - \frac{\alpha}{2} - \frac{n}{T_0}\right) \\ \quad + P\left(f + f_c + \frac{\alpha}{2} - \frac{n}{T_0}\right) \\ \quad \times P^*\left(f + f_c - \frac{\alpha}{2} - \frac{n}{T_0}\right) \Big\}, \\ \alpha = \frac{2 \cdot \text{integer}}{T_0}, \\ 0, & \alpha \neq \frac{2 \cdot \text{integer}}{T_0}. \end{cases} \quad (59)$$

5. Cyclostationary Signature for MCM Signal

The poor inherent cyclostationarity is unsuitable for practically applications in the context of cognitive radio. Even for OFDM signals which contain inherent cyclostationary features due to the underlying periodicities properties

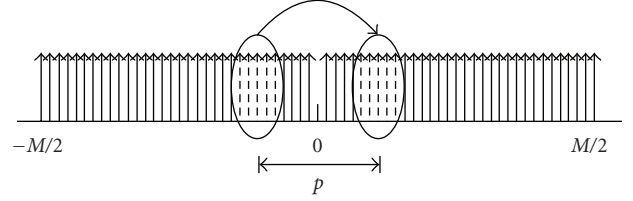


FIGURE 7: Generation of cyclostationary signatures by repeated transmitting MCM subcarrier symbols.

(Figure 3), as the power of inherent OFDM features are relative low to the power of signal, reliable detection of these features requires complex architecture and long observation time.

In this paper we study the detection problem of MCM signals considering the AWGN and Rayleigh fading environment by using an induced cyclostationary scheme [20], which is realized by intentionally embedding some cyclostationary signatures. Cyclostationarity-inducing method enables the recognition among primary system and secondary system or among multiple secondary systems competing for the same space spectrum, which is important as it may facilitate the setting of advanced spectrum policy such as multilevel priority or advanced access control [12]. Cyclostationary signature has been shown to be a powerful tool in overcoming the challenge of the distributed coordination of operating frequencies and bandwidths between co-existing systems [10]. A cyclostationary signature is a feature, intentionally embedded in the physical properties of a digital communication signal. CSs are effectively applied to overcome the limitations associated with the use of inherent cyclostationary features for signal detection and analysis with minimal additional complexity for existing transmitter architectures. Detection and analysis of CS may be also achieved using low-complexity receiver architectures and short observation durations. CS provides a robust mechanism for signal detection, network identification and signal frequency acquisition.

As illustrated in Figure 7, CSs are easily created by mapping a set of subcarriers onto a second set as

$$\gamma_{n,l} = \gamma_{n+p,l} \quad n \in N, \quad (60)$$

where $\gamma_{n,l}$ is the l th independent and identically distributed message at n th subcarrier frequency, N is the set of subcarrier values to be mapped and p is the number of subcarriers between mapped subcarriers. So a correlation pattern is created and a cyclostationary feature is embedded in the signal by redundantly transmitting message symbols.

In order to avoid redundant theoretical analysis, herein we just discuss the cyclostationary signature for FBMC signal. According to (21), (22), (53), (54), and (60), we can rewrite the nonconjugate cyclic autocorrelation and spectral

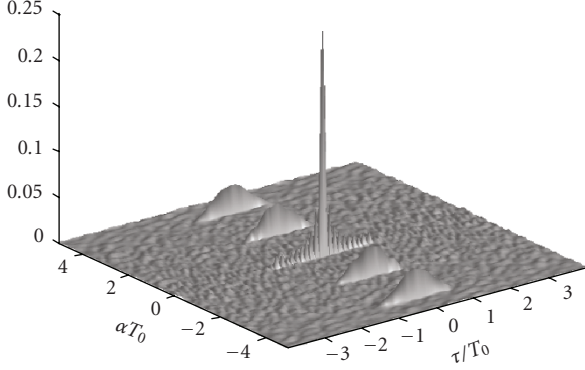


FIGURE 8: Nonconjugate Cyclic Autocorrelation Function for FBMC signal with cyclostationary features at cyclic frequencies $\alpha = \pm 2/T_0$ and $\alpha = \pm 4/T_0$.

correlation formulas of FBMC signal with cyclostationary signatures:

$$R_{\text{fbmc-cs}}^{\alpha}(\tau) = \begin{cases} \frac{2\sigma^2}{T_0} \cdot r_{p1}^{\alpha}(\tau) \cdot \frac{\sin(\pi M \tau / T_0)}{\sin(\pi \tau / T_0)}, \\ \alpha = \frac{2 \cdot \text{integer}}{T_0}, 2 \cdot \text{integer} \neq -p, |\tau| < K T_0, \\ \frac{2\sigma^2}{T_0} \cdot r_{p1}^0(\tau) \cdot \sum_{n \in N} e^{-j\pi(2n+p)\tau/T_0}, \\ \alpha = -\frac{p}{T_0}, |\tau| < K T_0, \\ 0, \alpha \neq \frac{2 \cdot \text{integer}}{T_0}, \alpha \neq -\frac{p}{T_0}, \end{cases} \quad (61)$$

$$S_{\text{fbmc-cs}}^{\alpha}(f) = \begin{cases} \frac{2\sigma^2}{T_0} \sum_{n=-M/2}^{M/2-1} P\left(f + \frac{\alpha}{2} - \frac{n}{T_0}\right) P^*\left(f - \frac{\alpha}{2} - \frac{n}{T_0}\right), \\ \alpha = \frac{2 \cdot \text{integer}}{T_0}, 2 \cdot \text{integer} \neq -p, \\ \frac{2\sigma^2}{T_0} \sum_{n \in N} P\left(f + \frac{\alpha}{2} - \frac{n}{T_0}\right) P^*\left(f - \frac{\alpha}{2} - \frac{n+p}{T_0}\right), \\ \alpha = -\frac{p}{T_0}, \\ 0, \alpha \neq \frac{2 \cdot \text{integer}}{T_0}, \alpha \neq -\frac{p}{T_0}, \end{cases} \quad (62)$$

where N is the set of subcarriers to be mapped and $p \in P$ ($P = \pm 2i$, $i = 1, 2, 3, 4, \dots$).

The magnitudes of nonconjugate CAF and SCF of FBMC signal with CS are drawn in Figures 8 and 9, where four cyclostationary signatures are embedded corresponding to two different values of p (choosing $p = 2$ and $p = 4$), and a reference filter bank is designed using the method given in [21]. We can see that for the FBMC signal with CS the

strong cyclostationary features appear at the cyclic frequency “ $\alpha = \pm 2/T_0$ ” and “ $\alpha = \pm 4/T_0$ ”.

OFDM and FBMC signals detection utilizing CSs by nonconjugate operation are already investigated in [10, 14], respectively. They both exhibit good performances, but the experiments using CSs by conjugate operation are still an open topic. In the following, we will insert the CSs by conjugate operation aiming at generating cyclostationary features on some predefined cyclic frequency, which is feasible based on the fact that most of MCM signals and noise don't display cyclostationarity under the conjugate operation for all the cyclic frequencies. (Herein the noise is assumed to be circularly symmetric.) Therefore, a simple cyclostationarity detector for the presence of conjugate cyclostationarity over the predefined cyclic frequency can be given to detect MCM signal and noise or detect two different MCM signals. (Recognition is feasible between the MCM signal embedded by CS and the other MCM signal without CS at a predetermined cyclic frequency.)

Contrary to the nonconjugate operation, a CS is created by mapping the conjugate formation of a set of subcarriers onto a second set as

$$\gamma_{n,l} = \gamma_{n+p,l}^* \quad n \in N \quad (63)$$

by which a correlation pattern is created and a cyclostationary feature is embedded in the signal.

According to (25), (26), (57), (58), and (63), we can rewrite the conjugate cyclic autocorrelation and spectral correlation formulas of FBMC signal with cyclostationary signatures

$$R_{\text{fbmc-cs}}^{\alpha}(\tau) = \begin{cases} \frac{2\sigma^2}{T_0} \sum_{n=-M/2}^{M/2-1} r_{p1}^{\alpha-2n/T_0}(\tau) (-1)^n, \\ \alpha = \frac{2 \cdot \text{integer} - 1}{T_0}, 2 \cdot \text{integer} - 1 \neq 2n + p, \\ |\tau| < K T_0, \\ \frac{2\sigma^2}{T_0} \cdot e^{j\pi p \tau / T_0} \cdot r_{p1}^0(\tau), \quad \alpha = \frac{2n+p}{T_0}, |\tau| < K T_0, \\ 0, \alpha \neq \frac{2 \cdot \text{integer} - 1}{T_0}, \alpha \neq \frac{2n+p}{T_0}, \end{cases} \quad (64)$$

$$S_{\text{fbmc-cs}}^{\alpha}(f) = \begin{cases} \frac{2\sigma^2}{T_0} \sum_{n=-M/2}^{M/2-1} P\left(f + \frac{\alpha}{2} - \frac{n}{T_0}\right) P^*\left(f - \frac{\alpha}{2} + \frac{n}{T_0}\right) (-1)^n, \\ \alpha = \frac{2 \cdot \text{integer} - 1}{T_0}, 2 \cdot \text{integer} - 1 \neq 2n + p, \\ \frac{2\sigma^2}{T_0} \sum_{n \in N} P\left(f + \frac{\alpha}{2} - \frac{n}{T_0}\right) P^*\left(f - \frac{\alpha}{2} + \frac{n+p}{T_0}\right), \\ \alpha = \frac{2n+p}{T_0}, \\ 0, \alpha \neq \frac{2 \cdot \text{integer} - 1}{T_0}, \alpha \neq \frac{2n+p}{T_0}, \end{cases} \quad (65)$$

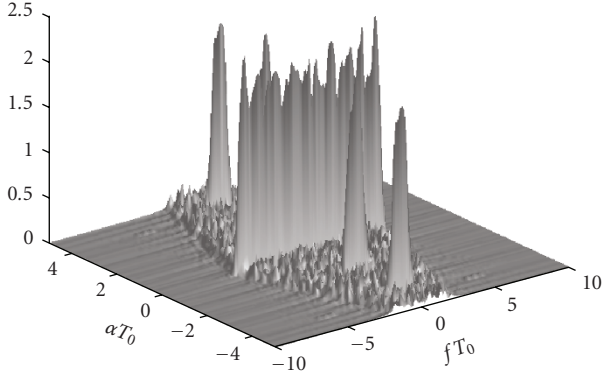


FIGURE 9: Nonconjugate Spectral Correlation Function for FBMC signal with four CSs at cyclic frequencies $\alpha = \pm 2/T_0$ and $\alpha = \pm 4/T_0$.

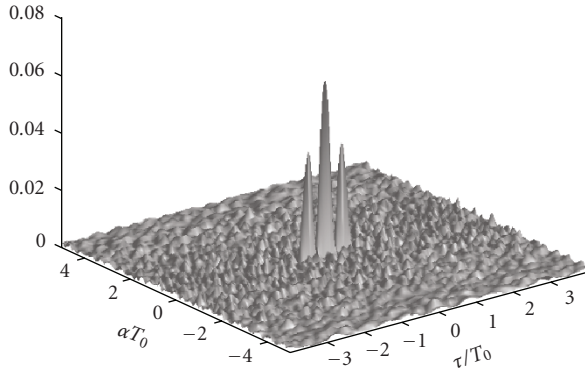


FIGURE 10: Conjugate Cyclic Autocorrelation Function for FBMC signal with cyclostationary features at cyclic frequencies $\alpha = 0$.

where N is the set of subcarriers to be mapped and $p \in P (P = \pm 2i, i = 1, 2, 3, 4, \dots)$. From (65) we can embed the CSs at zero cyclic frequency by setting a group of mapping subcarriers according to (63) under the condition “ $2n + p = 0$ ”. The magnitudes of conjugate CAF and SCF of FBMC signal with CS are drawn in Figures 10 and 11, where two subcarriers are repeated transmitted at the value of $p = 2$. We can see that the strong cyclostationary features appear at the cyclic frequency “ $\alpha = 0$ ”.

6. Signature Detector

Since complex noise does not exhibit nonconjugate (conjugate) cyclostationarity, the presence of the MCM signal under noise and interference is equivalent to the detection of the presence of nonconjugate (conjugate) cyclostationarity in the received composite signal $x(t) = s(t) + n(t)$ on the pre-determined cyclic frequency, where $n(t)$ is the contribution from noise.

The signature detector in [10] can be used for efficient FBMC signal detection. Cyclostationary features generated by subcarriers set mapping can be successfully detected using spectral resolution (subcarrier spacing Δf). So the low-complexity signature detector can be designed by sliding a

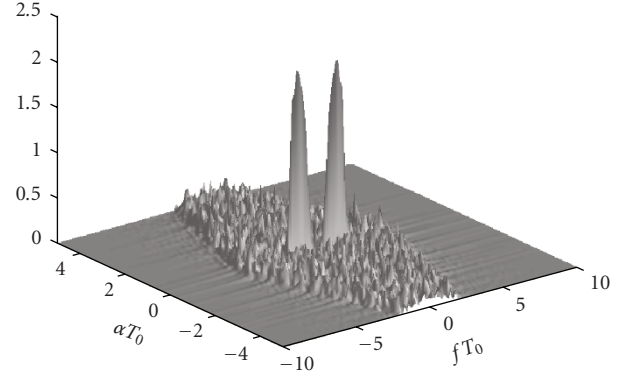


FIGURE 11: Conjugate Spectral Correlation Function for FBMC signal with two CSs at cyclic frequencies $\alpha = 0$.

window W with the width $N_s \cdot \Delta f$ (N_s is the number of subcarriers in the mapped set) around estimated nonconjugate (conjugate) SCF at the cyclic frequency α_0 :

$$T_{x^{(*)}} = \max_m \sum_n \hat{S}_{x^{(*)}}^{\alpha_0}(n) W(m - n), \quad (66)$$

where $\hat{S}_{x^{(*)}}^{\alpha_0}$ is estimated using a time-smoothed cyclic cross periodogram [8].

7. Simulations

Instead of discussing the detection applications of various MCM signals, in this section only the performance of the conjugate cyclostationarity detector between FBMC signal inserted by CS and noise signal is investigated. A 512-subcarrier FBMC signal is chosen and the following assumptions are made.

- (1) Cognitive radio system with a bandwidth of 5 MHz, and assuming signals are transmitted at carrier frequency $f_c = 2.4$ GHz.
- (2) The Additive White Gaussian Noise (AWGN) and Rayleigh fading channel are considered, respectively. A typical urban channel [22] is used with a maximum spread delay $\tau \approx 2.2 \mu s$ and a Doppler frequencies $f_d = 240$ Hz, which corresponds to a moving speed 30 m/s.
- (3) Subcarriers are modulated using OQAM. 6, 12, 18 and 24 subcarriers are respectively used as the mapping subcarrier sets at zero cyclic frequency.
- (4) Using the detector (66), the entry $\hat{S}_{x^{(*)}}^{\alpha_0}$ is estimated using time-smoothed cyclic periodogram, where a Hamming window is used. For simplicity, a rectangular sliding window W is chosen.
- (5) For comparison, the traditional energy detector proposed by Urkowitz [9] is applied under the assumption of noise uncertainty indicated by U , which is defined in [23].

Receiver operating characteristic (ROC) curves are drawn in Figures 12–15 by averaging 500 Monte Carlo

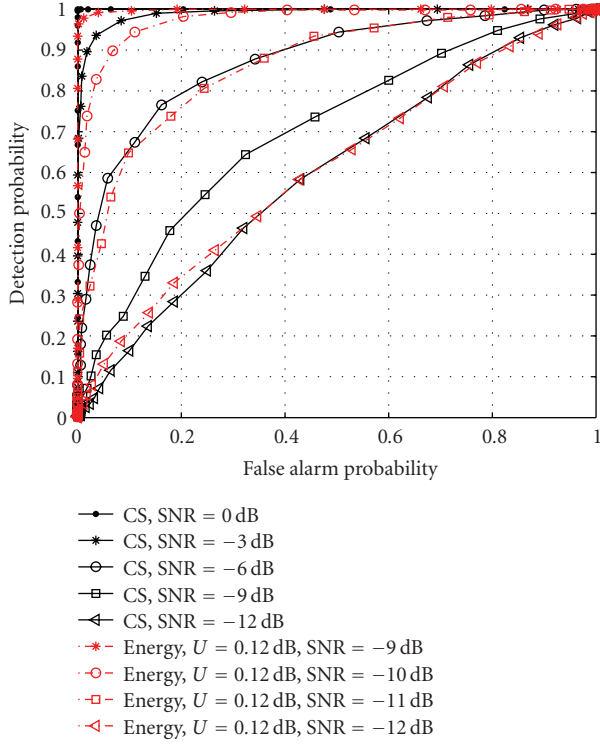


FIGURE 12: Receiver Operating Characteristic performance for AWGN channel with $N = 6$ subcarriers mapping set and an observation time $T = 1$ ms.

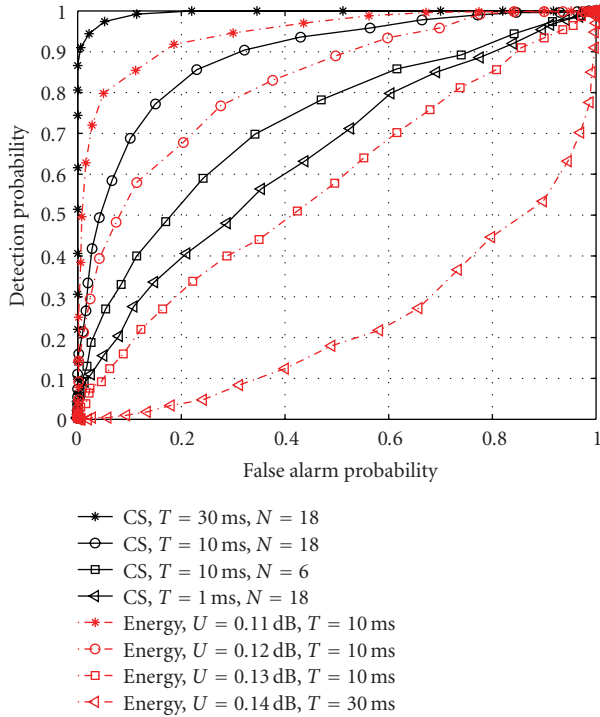


FIGURE 13: Receiver Operating Characteristic performance for AWGN channel with a fixed SNR = -12 dB.

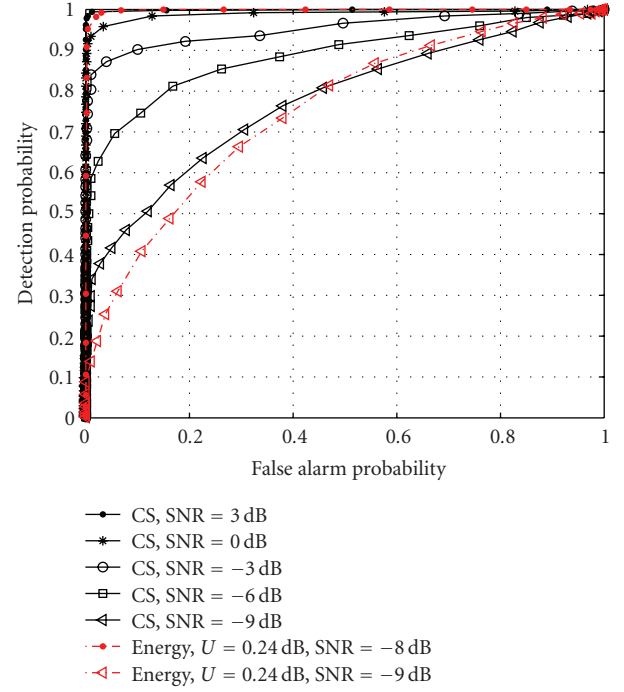


FIGURE 14: Receiver Operating Characteristic performance for Rayleigh fading channel with $N = 12$ subcarriers mapping set and an observation time $T = 3$ ms.

simulations for AWGN channel and Rayleigh fading channel, respectively. Figure 12 gives the experimental results for an AWGN channel at different SNR levels (0 dB, -3 dB, -6 dB, -9 dB, and -12 dB) with 6 subcarriers mapping set and an observation time $T = 1$ ms (10 FBMC symbols). As a comparison, the energy detector proposed in [9] with a noise uncertainty $U = 0.12$ dB is used. It can be seen that desired detection performance can be achieved for CS detector at the low SNR level, and almost 100% detection rate can be achieved when the SNR level is more than 0 dB. We can also observe that the energy detector significantly outperforms the CS detector when the noise power is well estimated. Effects of observation time and mapping set are shown in Figure 13 at a fixed SNR = -12 dB, where the ROC curves show that the performance of the CS detector improves when longer observation time and larger mapping set are applied. In addition, energy detector performance for different noise uncertainty values is depicted in Figure 13, which verifies that energy detector is very susceptible to noise uncertainty at low SNR level. Due to the noise uncertainty, the performance of energy detector does not improve even if the observation time increases. This behavior is predicted by the so called “SNR wall” in [24]. Namely, the energy detector can’t distinguish the weak received signal from slightly higher noise power below some SNR level.

The results deteriorate when more realistic time variant Rayleigh fading channels are considered. As shown in Figure 14, effects of SNR are illustrated at different SNR levels (3 dB, 0 dB, -3 dB, -6 dB, and -9 dB) with 12 subcarriers mapping set and an

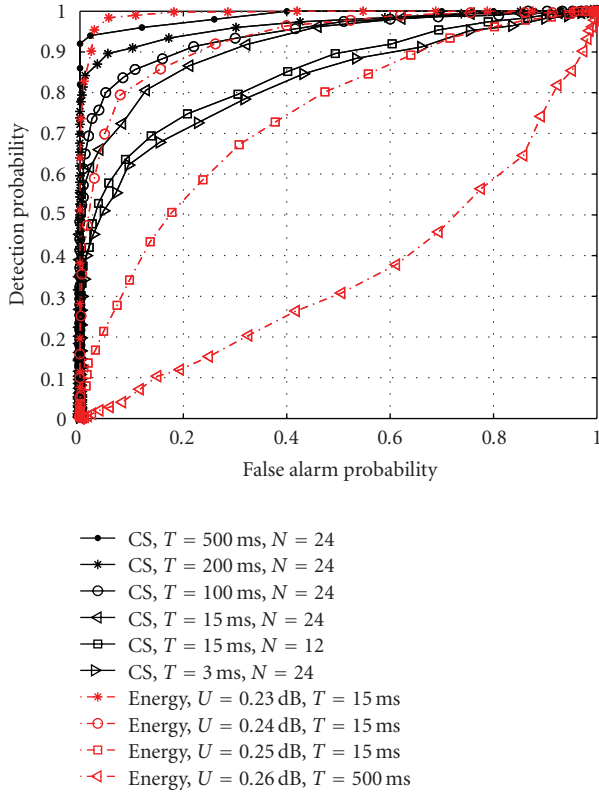


FIGURE 15: Receiver Operating Characteristic performance for Rayleigh fading channel with a fixed SNR = -9 dB.

observation time $T = 3$ ms (30 FBMC symbols). Compared with Figure 12, it can be seen that Rayleigh fading channel affects detection performance significantly. The energy detector with noise uncertainty $U = 0.24$ dB is compared with CS detector in Figure 14, which once again shows the advantage of energy detector when the SNR level is below the SNR wall. In order to achieve higher detection reliability for CS detector, longer observation time or more mapping subcarriers are needed as shown in Figure 15. It can be noted that from Figures 13 and 15 at a low SNR level ($\text{SNR} \leq -9$ dB) energy detector is not robust under the condition of a noise uncertainty $U \geq 0.13$ dB.

Simulations show that the energy detector is very susceptible to noise uncertainties and its performance is dictated by the accuracy of the noise power estimate. Moreover, energy detector can't differentiate different modulated signals, noise and interference. Conversely, good performance can be achieved for CS detector with a short observation time. Detection reliability can be seriously impacted by time-variant Rayleigh fading channel, which can be overcome through the use of longer observation time and more mapping subcarriers. Besides, CS detector is not susceptible to noise uncertainty and can distinguish different modulated signals by inserting CSs at different frequency positions.

8. Conclusion

This paper firstly analyzes the cyclic spectral correlation of both OFDM and FBMC signals. By utilizing an LPTV

model, we have derived the explicit formulas of nonconjugate and conjugate cyclic autocorrelation and spectral correlation functions for OFDM and FBMC signals, which provide the theoretical basis for further signal detection.

Secondly, a strategy for the detection of MCM signals by embedding cyclostationary signature at the predefined cyclic frequency is investigated. Because of the LPTV structure of the FBMC signal, the explicit formulas of nonconjugate and conjugate CAF and SCF with CS for FBMC signal are derived and CS can be accordingly easily inserted into the FBMC signal at some predetermined frequency position. During the simulation, a low-complexity conjugate detector is applied for detecting FBMC signal by embedding the CS at zero cyclic frequency in the AWGN and Rayleigh fading situations, respectively. All the cyclic operations at zero cyclic frequency are actually the conventional correlation and power spectral operations, which in some way reduce the computation complexity. Experimental results show that CS is an effective and robust tool for signal detection in cognitive radio network. We can improve the performance with increased subcarriers mapping size, but this causes a reduction in overall data rate because of the increased overhead. Via flexible CS position design for different MCM signals (different CR networks), identification among different modulated signals can be implemented in the same way.

Future work will be undertaken to examine the uses of pilots for generating cyclostationary signatures. In addition, further applications of CSs will be carried out in a practical cognitive radio platform.

References

- [1] W. A. Gardner, "Spectral correlation of modulated signal—part I: analog modulation," *IEEE Transactions on Communications*, vol. 35, no. 6, pp. 584–594, 1987.
- [2] W. A. Gardner, W. A. Brown, and C.-K. Chen, "Spectral correlation of modulated signals—part II: digital modulation," *IEEE Transactions on Communications*, vol. 35, no. 6, pp. 595–601, 1987.
- [3] M. Öner and F. Jondral, "On the extraction of the channel allocation information in spectrum pooling systems," *IEEE Journal on Selected Areas in Communications*, vol. 25, no. 3, pp. 558–565, 2007.
- [4] D. Vučić, M. Obradović, and D. Obradović, "Spectral correlation of OFDM signals related to their PLC applications," in *Proceedings of the 6th International Symposium on Power-Line Communications and Its Applications (ISMPLC '02)*, 2002.
- [5] H. Bölcskei, "Blind estimation of symbol timing and carrier frequency offset in wireless OFDM systems," *IEEE Transactions on Communications*, vol. 49, no. 6, pp. 988–999, June 2001.
- [6] P. Ciblat and E. Serpedin, "A fine blind frequency offset estimator for OFDM/OQAM systems," *IEEE Transactions on Signal Processing*, vol. 52, no. 1, pp. 291–296, 2004.
- [7] W. A. Gardner, A. Napolitano, and L. Paura, "Cyclostationarity: half a century of research," *Signal Processing*, vol. 86, no. 4, pp. 639–697, 2006.
- [8] W. A. Gardner, "The spectral correlation theory of cyclostationary time-series," *Signal Processing*, vol. 11, no. 1, pp. 13–36, 1986.

- [9] H. Urkowitz, "Energy detection of unknown deterministic signals," *Proceeding of the IEEE*, vol. 55, no. 4, pp. 523–531, 1967.
- [10] P. D. Sutton, K. E. Nolan, and L. E. Doyle, "Cyclostationary signatures in practical cognitive radio applications," *IEEE Journal on Selected Areas in Communications*, vol. 26, no. 1, pp. 13–24, 2008.
- [11] A. Chevreuil, E. Serpedin, P. Loubaton, and G. Giannakis, "Blind channel identification and equalization using non-redundant periodic modulation precoders: performance analysis," *IEEE Transactions on Signal Processing*, vol. 48, no. 6, pp. 1570–1586, 2000.
- [12] K. Maeda, A. Benjebbour, T. Asai, T. Furuno, and T. Ohya, "Cyclostationarity-inducing transmission methods for recognition among OFDM-Based systems," *EURASIP Journal on Wireless Communications and Networking*, vol. 2008, Article ID 586172, 14 pages, 2008.
- [13] D. Vučić and M. Obradović, "Matrix-based stochastic method for the spectral correlation characterization of digital modulation," *Facta Universitatis, Series: Electronics and Energetics*, vol. 11, no. 3, pp. 271–284, 1998.
- [14] H. Zhang, D. Le Ruyet, and M. Terre, "Signal detection for OFDM/OQAM system using cyclostationary signatures," in *Proceedings of the IEEE International Symposium on Personal, Indoor and Mobile Radio Communications (PIMRC '08)*, pp. 1–5, September 2008.
- [15] R. W. Chang, "Synthesis of band-limited orthogonal signals for multicarrier data transmission," *Bell System Technical Journal*, vol. 45, pp. 1775–1796, 1966.
- [16] B. R. Saltzberg, "Performance of an efficient parallel data transmission system," *IEEE Transactions on Communication Technology*, vol. 15, no. 6, pp. 805–811, 1967.
- [17] B. Hirosaki, "An orthogonally multiplexed QAM system using the discrete Fourier transform," *IEEE transactions on communications systems*, vol. 29, no. 7, pp. 982–989, 1981.
- [18] H. Bolcskei, P. Duhamel, and R. Hleiss, "Orthogonalization of OFDM/OQAM pulse shaping filters using the discrete Zak transform," *Signal Processing*, vol. 83, no. 7, pp. 1379–1391, 2003.
- [19] P. Siohan, C. Siclet, and N. Lacaille, "Analysis and design of OFDM/OQAM systems based on filterbank theory," *IEEE Transactions on Signal Processing*, vol. 50, no. 5, pp. 1170–1183, 2002.
- [20] M. K. Tsatsanis and G. B. Giannakis, "Transmitter induced cyclostationarity for blind channel equalization," *IEEE Transactions on Signal Processing*, vol. 45, no. 7, pp. 1785–1794, 1997.
- [21] M. G. Bellanger, "Specification and design of a prototype filter for filter bank based multicarrier transmission," in *Proceedings of the IEEE International Conference on Acoustics, Speech, and Signal Processing (ICASSP '01)*, vol. 4, pp. 2417–2420, 2001.
- [22] 3GPP, "ARIB TR-T12-25.943 V4.2.0 Deployment aspects (Release 4)," 3GPP, June 2002.
- [23] A. Sonnenschein and P. M. Fishman, "Radiometric detection of spread-spectrum signals in noise of uncertain power," *IEEE Transactions on Aerospace and Electronic Systems*, vol. 28, no. 3, pp. 654–660, 1992.
- [24] R. Tandra and A. Sahai, "SNR walls for signal detection," *IEEE Journal on Selected Topics in Signal Processing*, vol. 2, no. 1, pp. 4–17, 2008.