



# Reduction of a RRTTT machine tool geometric model by combinatorial analysis to improve volumetric accuracy

F Viprey, S Lavernhe, H Nouira, Christophe Tournier

## ► To cite this version:

F Viprey, S Lavernhe, H Nouira, Christophe Tournier. Reduction of a RRTTT machine tool geometric model by combinatorial analysis to improve volumetric accuracy. *Laser Metrology and Machine Performance (LAM DAMAP)* 2015, Mar 2015, Huddersfield, United Kingdom. hal-01122531

**HAL Id: hal-01122531**

**<https://hal.science/hal-01122531>**

Submitted on 4 Mar 2015

**HAL** is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers.

L'archive ouverte pluridisciplinaire **HAL**, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d'enseignement et de recherche français ou étrangers, des laboratoires publics ou privés.

# **Reduction of a RRTTT machine tool geometric model by combinatorial analysis to improve volumetric accuracy**

F.VIPREY<sup>1,2</sup>, S.LAVERNHE<sup>2</sup>, C.TOURNIER<sup>2</sup>, H.NOUIRA<sup>1</sup>

*1. Laboratoire National de Métrologie et d'Essais (LNE)*

*1, rue Gaston Boissier, F-75015 Paris, France*

*2. LURPA, ENS Cachan, Univ Paris-Sud*

*61, avenue du Président Wilson, F-94235 Cachan, France*

## **Abstract**

To significantly improve manufacturing processes, the intrinsic geometric deviations of machine tool must be optimized. Despite the international standard ISO 230-1, many geometric errors model are developed in the literature. In this paper, the modeling of a RRTTT five-axis machine tool including geometric error related to the international standard is carried out. The reduction and determination of model parameters is based on a combinatorial analysis coupled with rank analysis. The goal is to find all groups of position and orientation axes errors to model the volumetric accuracy actually measured. This task is performed by probing a datum sphere with a touch probe integrated in the machine tool. Finally, a combination of optimal parameters is determined in order to better map volumetric accuracy.

**Keywords:** Machine tool calibration; volumetric accuracy; geometric errors model; combinatorial analysis; indirect measurement.

## **1. Introduction**

5-axis machine tools are multi-axis structural loops with a large number of types of structures [1, 2], currently considered as common manufacturing system. In this paper, structural loops with three linear axes and two rotary axes are considered.

The main function of this loop is to maintain the relative position and orientation between the tool and the workpiece. Between both, a relative deviation, namely volumetric accuracy ( $V_{xyz}$ ) in ISO 230-1 [3], is principally generated by geometric errors [4]. To significantly improve the manufacturing process, it is necessary to minimize  $V_{xyz}$ . This goal may be achieved through identification and compensation of geometric errors.

Assuming infinite rigid bodies hypothesis, each axis of the structural loop is composed of two solids constituting a link with one degree of freedom biased by geometric errors, called motion errors. According to ISO 230-1 [3], the six motion errors of linear axis are: one linear positioning motion error along the

direction of motion, two straightness motion errors in two orthogonal directions of motion, and three angular motion errors (i.e. roll, pitch and yaw in the case of horizontal axis). According to ISO 230-7 [5], the six motion errors of rotary axis are: one angular positioning motion error around the direction of motion, two tilt motion errors in two orthogonal directions of motion, one axial error motion along the direction of rotary axis and two radial motion errors in orthogonal directions.

Structural loop is made up of axes which are composed of solids. Due to manufacturing and assembly errors, geometric deviation appears between nominal and real motion direction of the structure. ISO 230 defines the sufficient position and orientation errors of straight line and average line respectively in the case of linear and rotary axis. There are two orientation errors for one straight line (e.g.  $E_{A0Z}$  et  $E_{B0Z}$  in Figure 1) and four position and orientation errors of average line (e.g.  $E_{X0C}$ ,  $E_{Y0C}$  et  $E_{A0C}$ ,  $E_{B0C}$  in Figure 1). Moreover, one zero position error is defined for each axis (i.e.  $E_{Z0Z}$  and  $E_{C0C}$  in Figure 1).

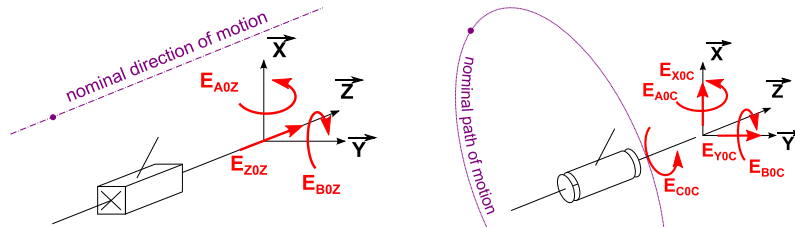


Figure 1: Position and orientation errors of linear Z-axis and rotary C-axis.

Table 1. Sufficient geometric errors on five-axis machine tool ([3], [5])

Type of axis	Motion errors per axis	Zero position error per axis	Position and orientation errors per axis	Number of axes	Total of errors
Linear	6	1	2	3	27
Rotary	6	1	4	2	22
					49

Hence, for a RRTTT structural loop, without considering errors of the tool spindle, the total number of sufficient geometric errors is equal to forty-nine (Table 1). These errors are not all required to characterize the volumetric accuracy. Indeed, due to the selection of reference position and orientation of machine coordinate system, and the possibility to set to zero the zero positions, the international standard ISO230-1 [3] gives the minimum of eight position and orientation error parameters, in addition to the thirty motion errors, to fully characterize a five-axis machine tool. The reduction of model to drop the position and orientation errors from nineteen to eight is not clearly justified. Reduction may be difficult to understand, and very difficult to be applied to any

architecture of machine tool. Therefore, there is a requirement to analyze the reduction methods of geometric error models.

Abbaszadeh-Mir et al. [6], develop a geometric model with position and orientation axes errors. Six parameters are defined between each axis, and six parameters describe tool deviations as well as six for the workpiece deviations (mounting errors). Reduction is done thanks to the rank study of the jacobian matrix given by the inverse geometric model. A method based on the mathematical analysis of singularities of linear systems is used to assist in selecting a minimal set of twenty parameters for the calibration of a five axis machine tool. Identification is performed by telescoping magnetic ball-bar measurement.

Yu et al. [7], define a high efficiency computable model with clear physical meanings. The model is reduced and a combination of twenty groups of parameters including motion errors as well as position and orientation errors is proposed.

Bohez et al. [8] adopt a model with nine position and orientation errors, found by minimum number of rigid bars to form a single rigid body. A reduction is performed by a linear dependencies study. Identification of parameters is done by measurement of a machined test part on Coordinate Measuring Machine (CMM).

Lei and Hsu. [9, 10] build a model with sixty-one geometric parameters including thirty motion errors, thirteen position and orientation errors, eighteen mounting errors associated respectively with the spindle block and the Z-slide, with the spindle-tool interface, and with turntable and workpiece. An identification of fifty-nine parameters is done with probe-ball measurement and 5D laser interferometer.

Tsutsumi and Saito [11] assess an identification of eight rotary axis parameters of thirteen position and orientation errors of axes in the 5-axis machine tool. Identification is carried out by using telescoping magnetic ball-bar.

Lin and Shen [12] propose a geometric model based on motion errors and seven squareness parameters. A matrix summation approach is performed to simplify the homogenous matrix transform approach and provides a clearer physical interpretation.

Table 2. Papers comparison of geometric errors modelisation and identification on 5-axis machine tool

References	Motion errors	Position and orientation errors	Mounting errors	Independent errors
ISO230 [3, 5]	30	19	0	38
Abbaszadeh-Mir et al. [6]	0	30	12	20
Yu et al. [7]	30	30	0	20
Bohez et al. [8]	30	9	0	32
Lei and Hsu. [9, 10]	30	19	12	59
Tsutsumi and Saito [11]	0	30	0	13
Lin and Shen [12]	30	7	0	-

From this literature review (Table 2), when motion errors are taken into account, the number of geometric parameters is the same (i.e. thirty geometric parameters). Indeed, motion errors depend on the axis position and cannot be reduced. It is not the case for the position and orientation errors. The reduction of these errors is often made without clear justification. Thus the number of independent errors which have a different effect on volumetric accuracy needs to be clarified.

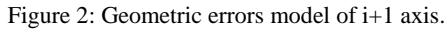
This paper aims at building a geometric errors model consistent with ISO 230, in order to perform compensation on a RRTTT 5-axis machine tool. This model is made up of a sufficient number of geometric parameters which have independent effects on volumetric accuracy. The proposed approach consists in performing a model reduction. Thus, an analysis of functional combinations of parameters is carried out to minimize volumetric accuracy previously measured. Therefore, the paper is organized as follows: Section 2 presents the geometric model of a five-axis machine tool based on international standard; Section 3 deals with the volumetric accuracy simulation and physical procedure for parameters identification; Section 4 is dedicated to the reduction of this model by combinatorial analysis to find the best combinations of functional geometric parameters.

## **2. Geometric errors model**

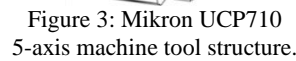
Geometric model is based on infinite rigid body assumption. Each degree of freedom between two successive bodies  $S_i$  and  $S_{i+1}$ , respectively attached with  $R_i$  and  $R_{i+1}$  frames, constitutes the  $i+1$  axis.

Sufficient geometric parameters are introduced between two consecutive bodies. The non-ideal  $i+1$  axis model are defined and calculated by homogenous transformation matrices without first order simplification. In other words, all rotation matrix are completely defined. The non-ideal  $i+1$  axis model is depicted in Equation 1 and in Figure 2 with:

- $T_N$  is the nominal geometry of  $S_i$ ;
- $T_{POE}$  represents the position and orientation error between nominal axis and straight or average line : three or five parameters for linear or rotary axis respectively;
- $T_M$  is the nominal motion joint;
- $T_{ME}$  depicts the six motion errors of axis: linear positioning motion errors, straightness errors, roll, pitch and yaw in the case of linear axis.



$$R_{nom\ 2}^{R_i T_{axis\ i+1}} = R_{nom\ 1}^{R_i T_N} \cdot \frac{R_{nom\ 1}^{T_{POE}}}{R_{mean}^{T_{POE}}} \cdot \frac{R_{mean}^{T_M}}{R_m^{T_M}} \cdot \frac{R_m^{T_{ME}}}{R_{real}^{T_{ME}}} \cdot \frac{R_{real}^{T_{POE}}}{R_{nom\ 2}^{T_{POE}}}$$



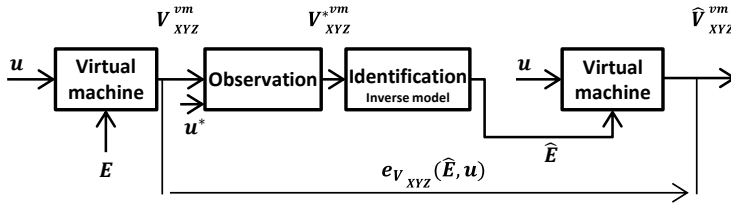


Figure 4: Procedure of volumetric accuracy modelling by virtual machine.

The inputs are one vector  $E$  of geometric parameters and a vector of excitement  $u$  (Figure 4). A restricted excitement vector  $u^*$  can be chosen. It corresponds with particular joint configurations of  $u$ . A mapping of the resulting observed volumetric accuracy  $V_{XYZ}^{*vm}$  for this restricted excitement vector  $u^*$  allows the identification of one vector of  $\hat{E}$ -parameters. Therefore these parameters are estimated. This vector is the combination of sufficient parameters to depict volumetric accuracy ( $V_{XYZ}^{*vm}$ ). With the identified parameters, it is possible to map the identified volumetric accuracy  $\hat{V}_{XYZ}^{vm}$  everywhere in the workspace. The second model of virtual machine (Figure 4) is different from the first model. Indeed, the inputs are different. The first model uses imposed  $E$ -vector (i.e. imposed geometric parameters), whereas the second uses identified  $\hat{E}$ -vector. Then, the goal is to assess the pertinence of this second model to a broader set of excitation vectors (covering most points of the workspace). The pertinence can be evaluated with an error. The error of calculation  $e_{V_{XYZ}}(\hat{E}, u)$  can be defined between these models (Equation 2). This error allows testing and verifying the robustness of the estimation procedure (i.e. the identification).

Equation 2: error of calculation.

$$e_{V_{XYZ}}(\hat{E}, u) = \hat{V}_{XYZ}^{vm}(\hat{E}, u) - V_{XYZ}^{vm}(E, u)$$

### 3.2. Measurement of volumetric accuracy $V_{XYZ}^{*mr}$

Within an industrial context, it is important to implement a rapid procedure both on the setting and the measurement to minimize the downtime of the machine tool. It is also essential to perform a raw measurement of joint coordinates, thus avoiding to affect the measurements by the unwanted treatments and compensations of the industrial CNC.

This process requires the integration of a 3D touch probe, and the collection of raw data on linear and rotary encoders. Moreover, it is necessary to synchronize in real time the control of the machine tool and the external measurement. This process includes several tasks which are:

- Procedure to acquire the machine zero point by counting distance-coded reference marks;
- Absolute machine coordinate collection (X, Y, Z, A, C) in real time ( $f = 33\text{kHz}$ ) and directly on Heidenhain encoders;

- Collection of trigger signal directly on Renishaw RMP600 touch probe ( $U_{(k=2)} = 0,25\mu\text{m}$  with feedrate of 240mm/min);
- Synchronized recording of coordinates with trigger signal;
- Fetch stored data on dSpace hardware.

The components of position of volumetric accuracy  $V_{XYZ}^{*mr}$  are measured thanks to the probing of a datum sphere directly clamped on the rotary table. The volumetric accuracy is equal to the difference between actual position of the datum sphere and the ideal position. Fifty different joint configurations are used to maximize the motion along of the travel range axes, as depicted in Figure 5. They are uniformly distributed along the path of the A-axis and for nine turns of the C-axis.  $V_{XYZ}^{*mr}(u^*)$  is shown in Figure 6. It is a vector with one hundred and fifty components (i.e. three components of position multiplied by fifty joint configurations).

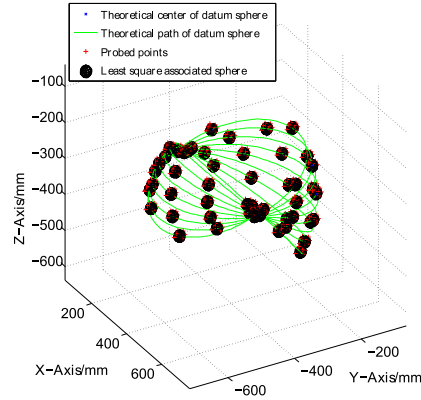


Figure 5: Location of datum sphere in machine workspace.

The measurement of the datum sphere in fifty joint configurations allows mapping the position components of the measured volumetric accuracy (Figure 6). The influence of position and orientation errors of axis is clearly observable in Figure 6. Indeed, the nine oscillations correspond to the nine turns of rotary table.

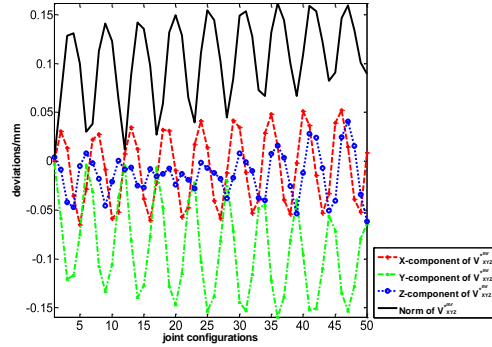


Figure 6: Norm and components of  $V_{XYZ}^{*mr}$  for each of the fifty configurations.



#### 4. Model reduction and identification

In the next step a focus is made on geometric errors parameters without taking into account motion errors. Combinations of position and orientation errors of axis as well as mounting errors of tool and workpiece will be identified. However, the proposed measurement process with a datum sphere does not allow the identification of the orientation component of tool and workpiece mounting errors.

From the nominal links and joint parameters of the structural loop, the sensitivity Jacobian matrix  $J$  is obtained using the little displacement theory which is based on first order approximation [6]. It is built to propagate the effect of errors on the position of center location of tool (i.e. centre of tool frame) for the fifty joint configurations. These errors are the nineteen position and orientation errors of axis and the six mounting errors of tool and workpiece. So  $J$  is a  $150 \times 25$  matrix (Equation 3).

Equation 3: Model for identification.

$$J_{[150 \times 25]} \times E_{[25 \times 1]} = V_{XYZ}^{*mr}$$

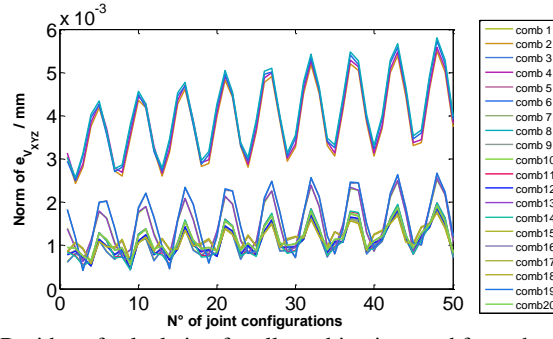
Combinatorial analysis of possible combinations of fourteen geometric errors is carried out. Then,  $J$  is reduced to effects of combinations (i.e.  $J_{[150 \times 14]}$ ) and a rank analysis is performed. Thanks to these studies, it is possible to minimize  $E$  according to the Equation 4.

Equation 4: Minimization of  $E$ .

$$\hat{E} = \operatorname{argmin}_{\mathbb{R}^n} (\|J \times E - V_{XYZ}^{*mr}\|_2)$$

The  $E$ -vector is composed of fourteen components. It is the concatenation of eight errors among nineteen of structural loop and six position components of mounting error.

Among the  $C_8^{19} = 78\,582$  possible combinations of geometric parameters, only twenty allow to resolve the Equation 4. The combinations which appear in ISO 230 and in [6], are included among the twenty combinations. It was proved that whatever the size of the vector  $V_{XYZ}^{*mr}$  the number and the composition of combinations are the same. In other words, if just the components of position or all components (i.e. position and orientation) of  $V_{XYZ}^{*mr}$  are used in Equation 4, combinations of eight geometric errors of the structural loop are the same. This result was demonstrated by using the previous virtual machine and the study of  $e_{V_{xyz}}(\hat{E})$ . Moreover, this study shows that combinations don't have the same performance on calculation error minimization and consequently on the compensation of simulated volumetric accuracy. An analysis of the error  $e_{V_{xyz}}(\hat{E})$  for a  $E$ -vector of parameters and in the particular case of  $u = u^*$  is highlighted in Figure 7.


 Figure 7: Residue of calculation for all combinations and for a chosen  $E$ -vector.

After identification of parameters (Figure 8), the residue of estimation can be calculated (Equation 5).

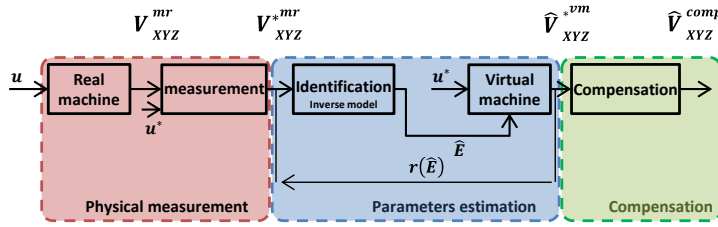


Figure 8: Identification procedure.

This residue is the difference between the measured volumetric accuracy for a chosen vector of excitement  $u^*$  (i.e. fifty joint configurations) and simulated volumetric accuracy  $\hat{V}_{XYZ}^{*vm}(u^*)$  from virtual machine and estimated parameters.

Equation 5: Residue of estimation.

$$r(\hat{E}) = V_{XYZ}^{*mr}(u^*) - \hat{V}_{XYZ}^{*vm}(\hat{E}, u^*)$$

To improve manufacturing process, the focus is on volumetric accuracy  $V_{XYZ}^{mr}(u)$  in the workspace. It is necessary to carry out correction of  $V_{XYZ}^{mr}(u)$  by compensation of identified geometric errors  $\hat{E}$ . The Figure 9 depicts the residue  $r(\hat{E})$  for the twenty combinations. All combinations characterise the volumetric accuracy in the same way because all twenty curves are superimposed. The residue may be explained by the presence of motion errors, thermal effects and terms of second order or higher order, and due to measurement.

This study demonstrates that there are twenty potential combinations of sufficient parameters. They produce the same residue of estimation but few of them exhibit a lower sensitivity to calculation approximations. A priori, few characterize better volumetric accuracy of the actual machine.

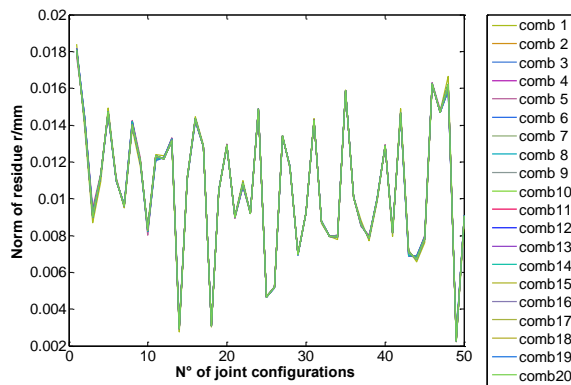


Figure 9: Residue of estimation  $r(\hat{E})$  for twenty combinations

## Conclusion

In this paper, a geometric errors modeling based on international standard of a 5-axis machine tool was developed. The generic property of this geometric modeling and the parameter identification can be applied on another type of structure (e.g. robot, CMM). The determination of the necessary and sufficient parameters to optimally map volumetric accuracy was carried out by combinatorial analysis. A measurement with touch probe and datum sphere is used to identify the parameters' values of a potential combination.

The use of such a model for compensation should decrease drastically the volumetric accuracy in the machine workspace. Further works will complete the identification of the motion errors and provide a criterion to define and choose the best compensation strategy.

**Acknowledgments:** The authors sincerely thank the EMRP organization. The EMRP is jointly funded by the EMRP participating countries within EURAMET and the European Union (IND62: JRP-TIM).

## References

- [1] Moriwaki T 2008 Multi-functional machine tool, *CIRP Annals - Manufacturing Technology* vol. 57, no. 2, pp 736-749
- [2] Bohez E.L 2002 Five-axis milling machine tool kinematic chain design and analysis, *Int J Mach Tool Manu* vol. 42, no. 4, pp. 505-520.
- [3] ISO. 230-1 2012 Test code for machine tools - Part 1: Geometric accuracy of machines operating under no-load or quasi-static conditions
- [4] Ramesh R, Mannan M and Poo A 2000 Error compensation in machine tools - a review: Part I: geometric, cutting-force induced and fixture-dependent errors, *Int J Mach Tool Manu*, vol. 40, no. 9, pp. 1235-1256
- [5] ISO. 230-7 2007 Test code for machine tools - Part 7: Geometric accuracy of axes of rotation
- [6] Abbaszadeh-Mir Y, J. R. R. Mayer J.R.R, Cloutier G and Fortin Cn 2002 Theory and simulation for the identification of the link geometric errors for a five-axis machine tool using a telescoping magnetic ball-bar, *Int J Prod Res*, vol. 40, no. 18, pp. 4781-4797
- [7] Yu Z, Tiemin L and Xiaoqiang T 2011 Geometric Error Modeling of Machine Tools Based on

Screw Theory, *Procedia Engineering* , vol. 24, no. 0, pp. 845-849

- [8] Bohez E.L, Ariyajunya B, Sinlapeecheewa C, Shein T.M.M, Lap D.T and Belforte G 2007 Systematic geometric rigid body error identification of 5-axis milling machines, *Comput Aid D*, vol. 39, no. 4, pp. 229-244,
- [9] Lei W and Hsu Y 2002 Accuracy test of five-axis CNC machine tool with 3D probe-ball. Part I: design and modeling, *International Journal of Machine Tools and Manufacture* , vol. 42, no. 10, pp. 1153-1162
- [10] Lei W and Hsu Y 2002 Accuracy test of five-axis CNC machine tool with 3D probe-ball. Part II: errors estimation, *Int J Mach Tool Manu*, vol. 42, no. 10, pp. 1163-1170
- [11] Tsutsumi M and Saito A 2003 Identification and compensation of systematic deviations particular to 5-axis machining centers, *Int J Mach Tool Manu*, vol. 43, no. 8, pp. 771-780
- [12] Lin Y and Shen Y 2003 Modelling of Five-Axis Machine Tool Metrology Models Using the Matrix Summation Approach," *Int J Adv Manuf Tech*, vol. 21, no. 4, pp. 243-248
- [13] Mekid S and Ogedengbe T A review of machine tool accuracy enhancement through error compensation in serial and parallel kinematic machines, *Int J Prec Tech*, vol. Vol 1, p. 35