



Optimized off-diagonal GMI-based magnetometer

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Optimized off-diagonal GMI-based magnetometer

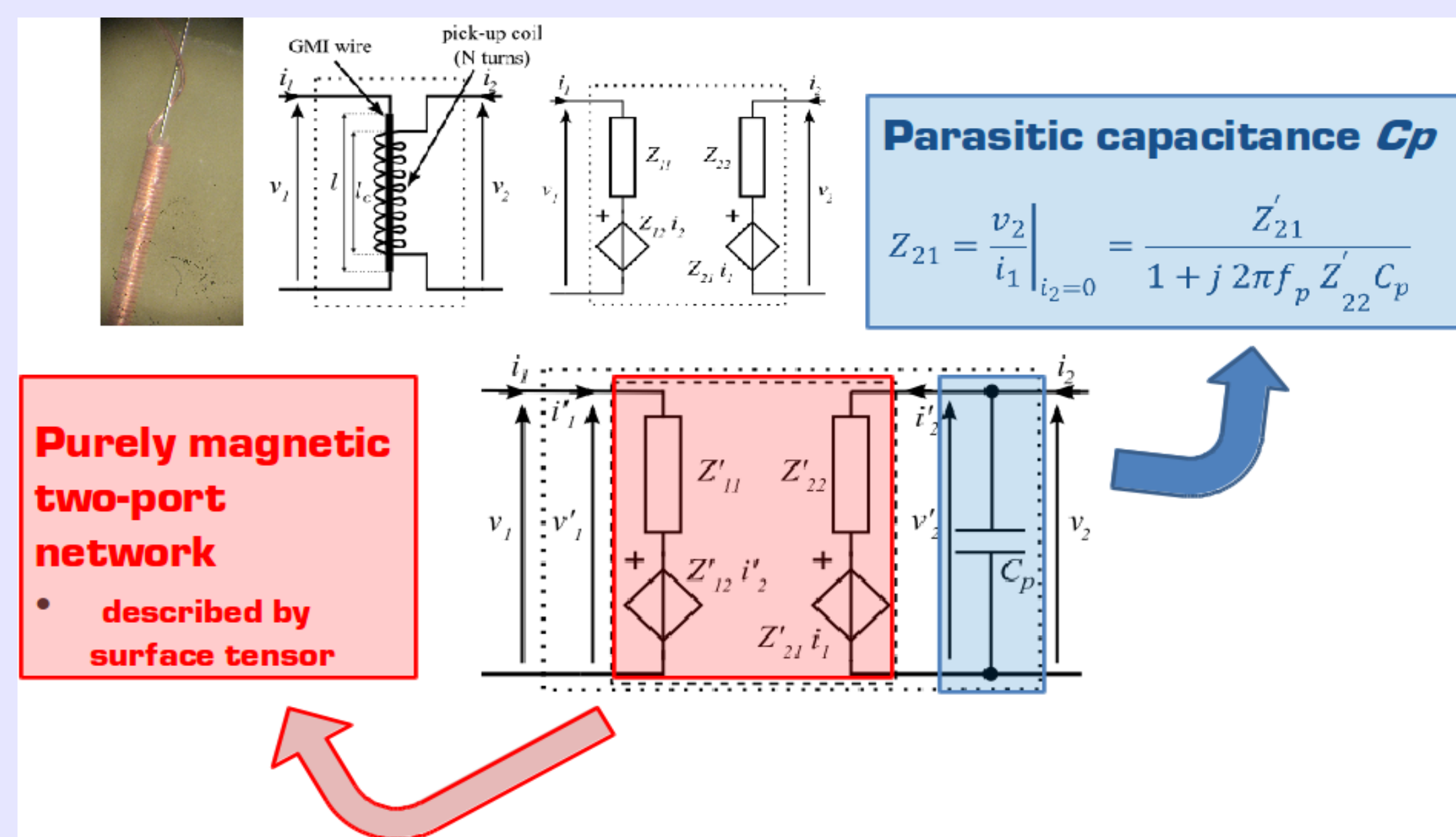
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GMI-coil modelisation



$$\begin{pmatrix} e_\varphi \\ e_z \end{pmatrix} = \begin{bmatrix} \zeta_{\varphi z} & \zeta_{\varphi\varphi} \\ \zeta_{zz} & \zeta_{z\varphi} \end{bmatrix} \begin{pmatrix} h_\varphi \\ h_z \end{pmatrix}$$

$$\begin{cases} v'_1 = l e_z \\ i'_1 = 2\pi a h_\varphi \end{cases} \quad \begin{cases} i'_2 = \frac{l}{N} h_z \\ v'_2 = -2\pi a N e_\varphi \end{cases}$$

$$\begin{pmatrix} Z_{11} & Z_{12} \\ Z_{21} & Z_{22} \end{pmatrix} = \begin{pmatrix} \frac{l}{2\pi a} (Z_M \cos^2 \theta_M + Z_N \sin^2 \theta_M) - \frac{j N (Z_N - Z_M) \sin \theta_M \cos \theta_M}{1 + j \frac{2\pi a N^2}{l} (Z_M \sin^2 \theta_M + Z_N \cos^2 \theta_M) C_p \omega_p} & \frac{N (Z_N - Z_M) \sin \theta_M \cos \theta_M}{1 + j \frac{2\pi a N^2}{l} (Z_M \sin^2 \theta_M + Z_N \cos^2 \theta_M) C_p \omega_p} \\ \frac{N (Z_N - Z_M) \sin \theta_M \cos \theta_M}{1 + j \frac{2\pi a N^2}{l} (Z_M \sin^2 \theta_M + Z_N \cos^2 \theta_M) C_p \omega_p} & \frac{2\pi a N^2 (Z_M \sin^2 \theta_M + Z_N \cos^2 \theta_M)}{1 + j \frac{2\pi a N^2}{l} (Z_M \sin^2 \theta_M + Z_N \cos^2 \theta_M) C_p \omega_p} \end{pmatrix}$$

$$Z_M = k_M \rho \frac{j_0(k_M a)}{J_1(k_M a)} \quad Z_N = k_N \rho \frac{j_0(k_N a)}{J_1(k_N a)}$$

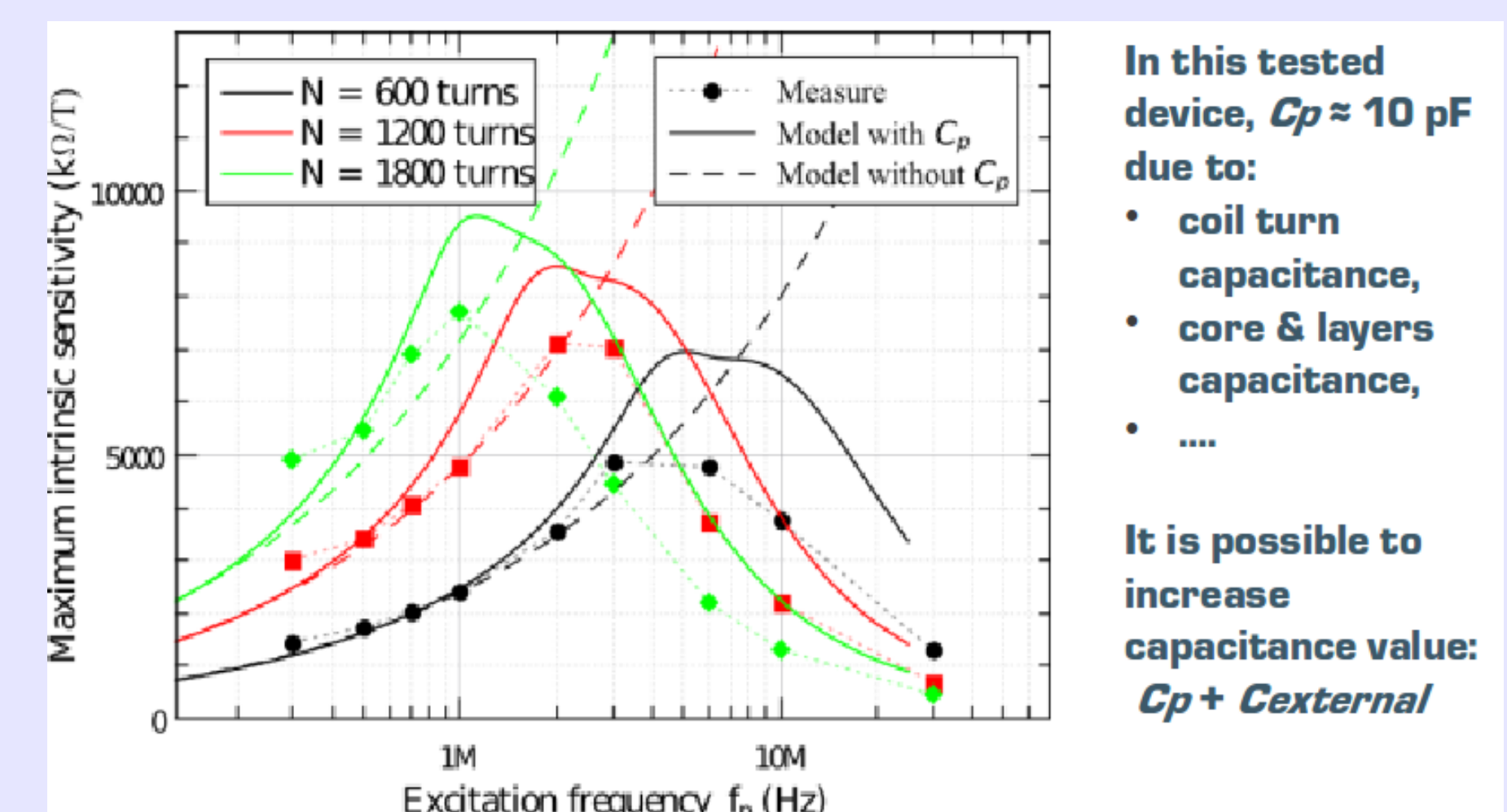
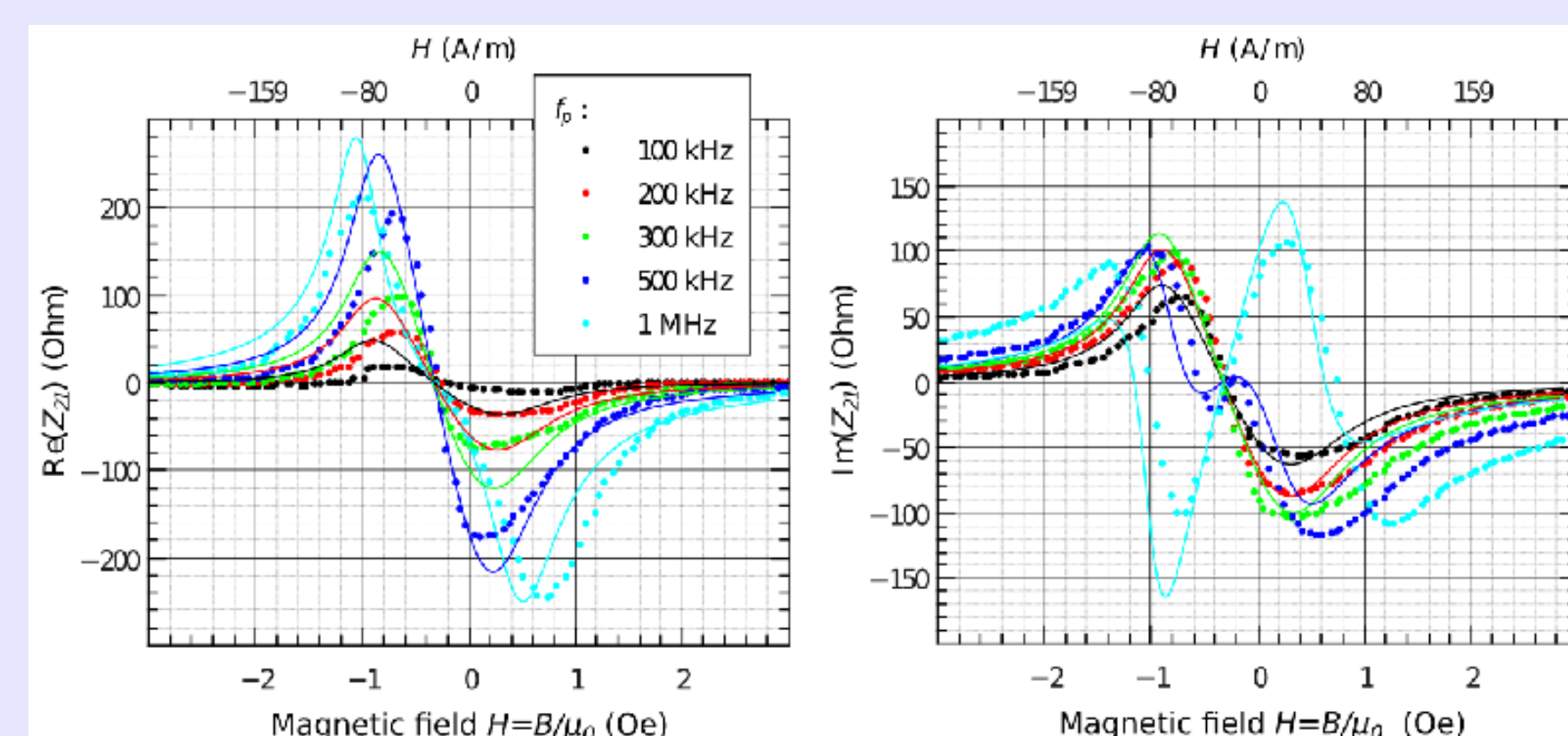
$$\begin{cases} k_M = k_N \sqrt{\frac{\mu_M}{\mu_0}} \\ k_N = 1 - j \frac{\delta_N}{\delta_M} \end{cases} \quad \delta_N = \sqrt{\frac{2\rho}{\omega_p \mu_0}}$$

Abstract

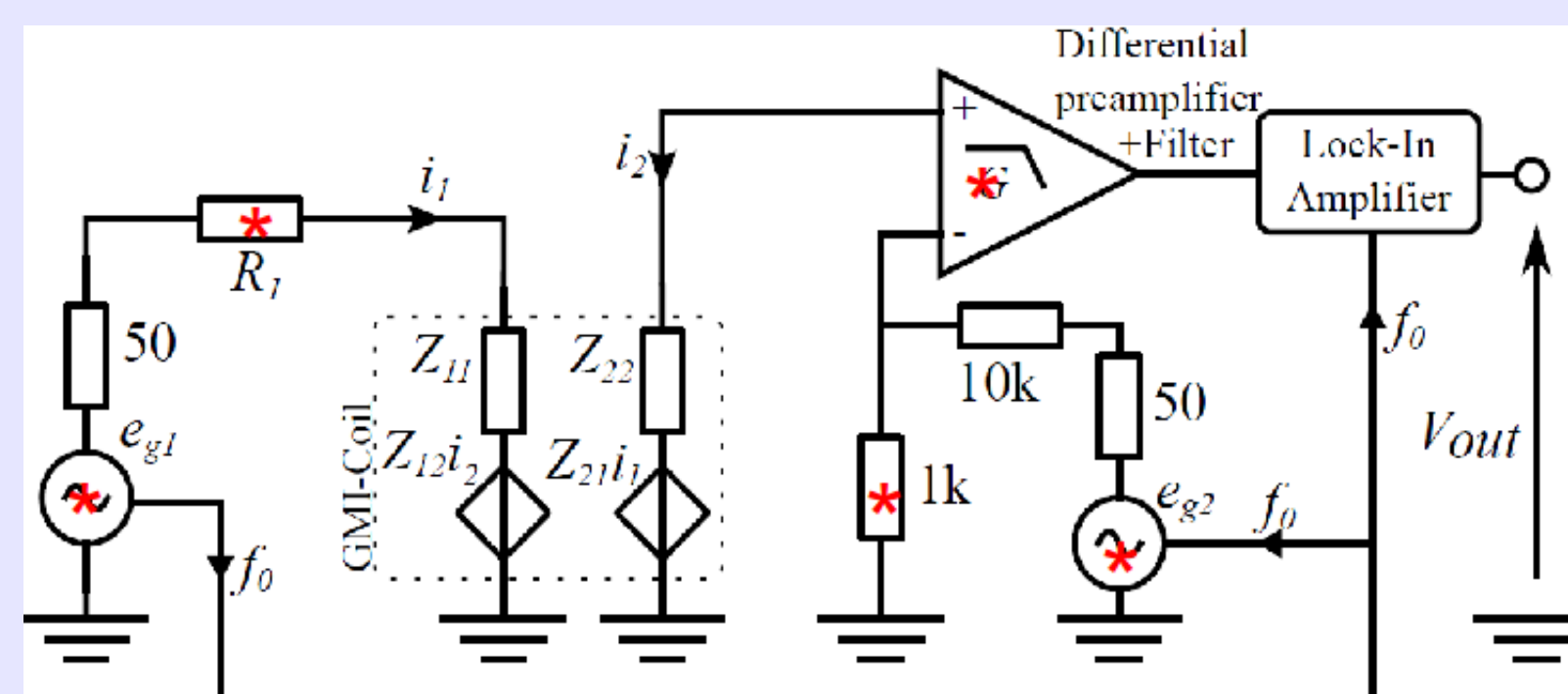
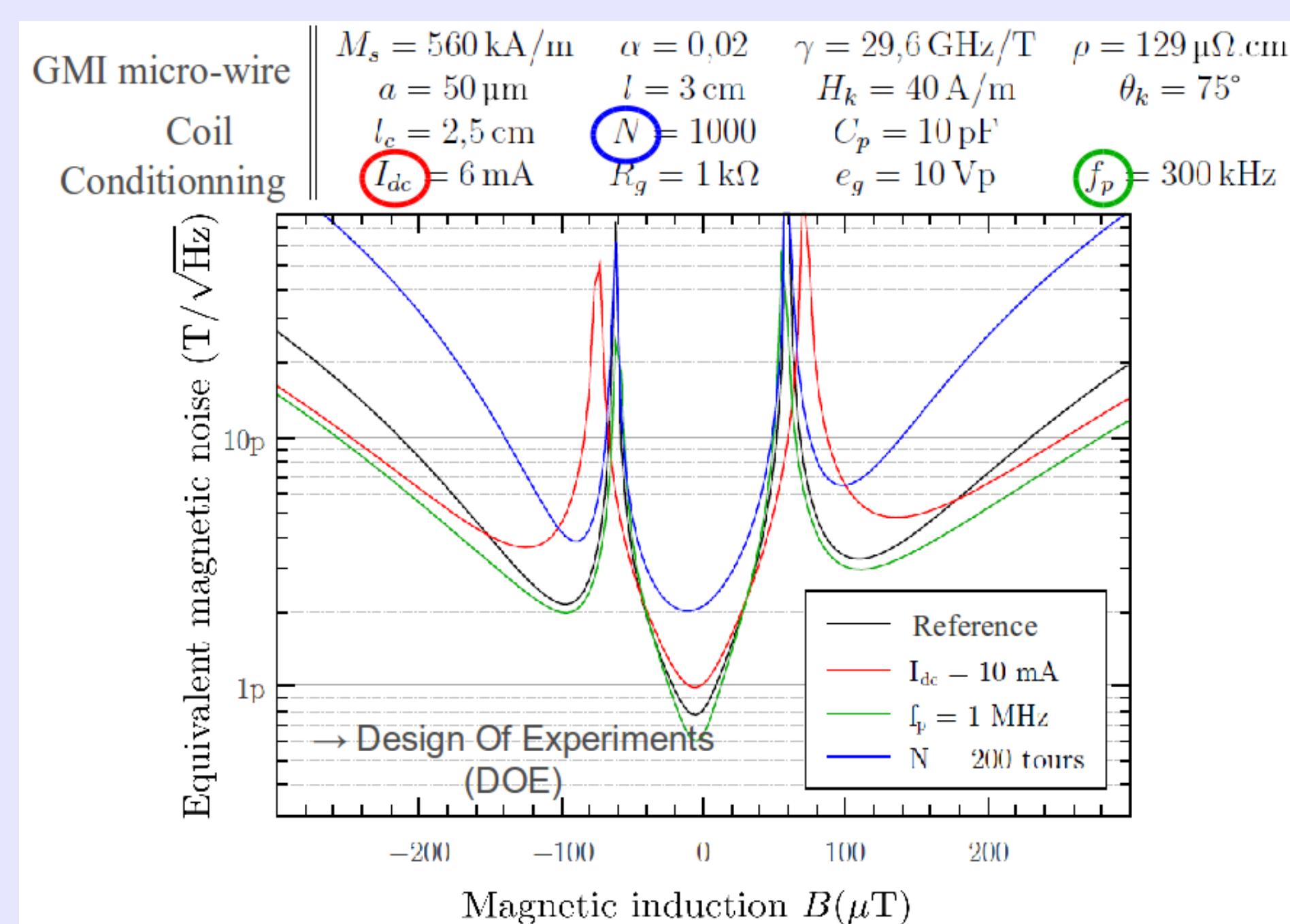
An optimized giant magneto-impedance effect magnetometer has been developed, based upon an overall analysis of the measurement chain, including physical material properties, associated detection coil parameters, and equivalent magnetic noise performances. The field response model for the sensing element and the noise model yield good agreement with experimental results. The noise performance of the magnetometer, approximately 1.7 pT/√Hz in the white noise region, with a band-pass of about 70 kHz, is competitive with that of other technologies. Present limitations are clearly established, leaving room for further improvements.

Index Terms—Giant magneto-impedance (GMI), magnetometer, noise.

Parasitic capacitance effect



Noise modelisation

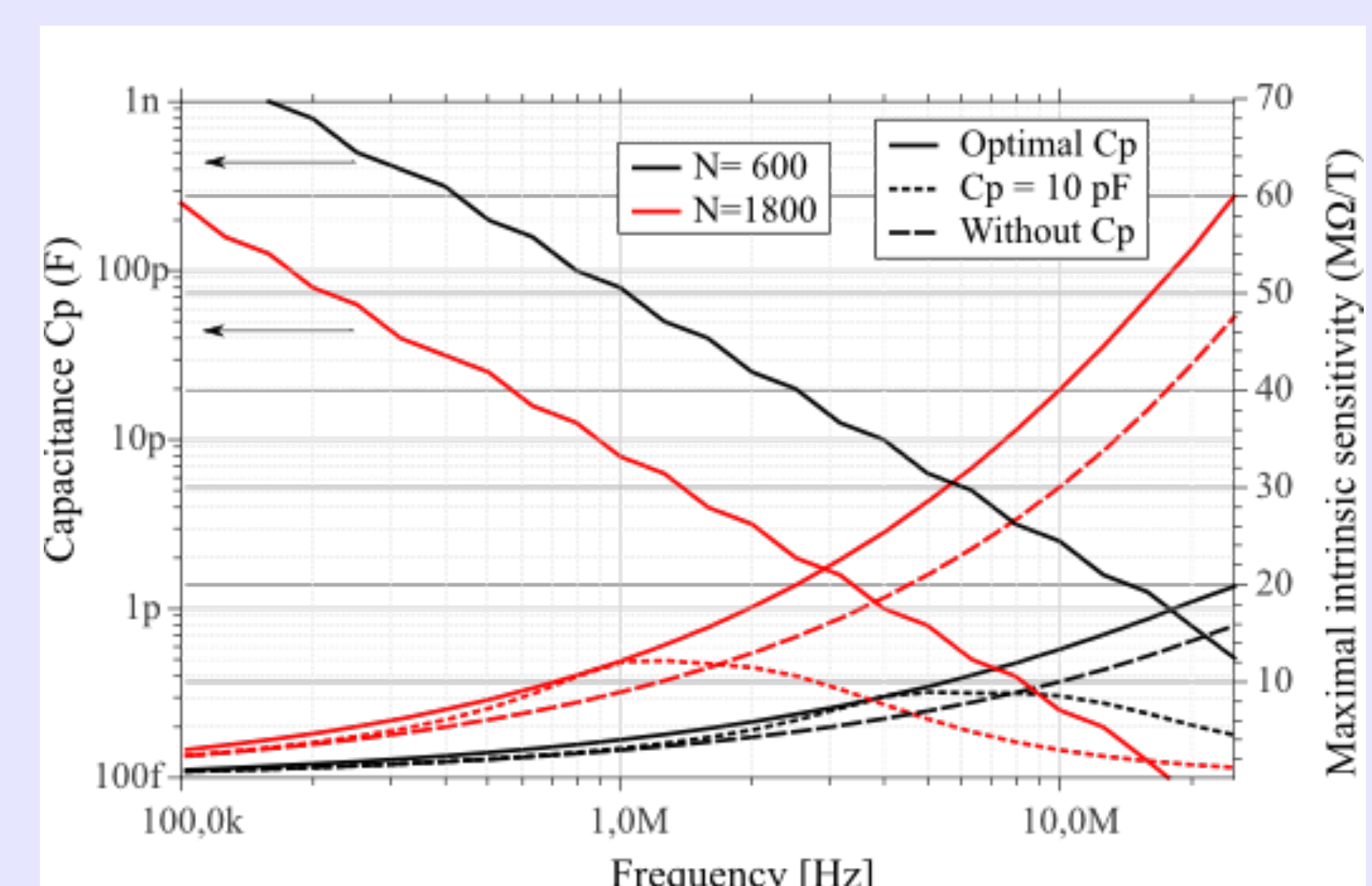


$$h_{nB}^2 \approx \frac{1}{2} \frac{d^2}{d\omega_p^2} \left\{ \frac{G_{buff}^2}{R_{buff}^2} \left[\frac{N (Z_N - Z_M) \sin \theta_M \cos \theta_M}{1 + j \frac{2\pi a N^2}{l} (Z_M \sin^2 \theta_M + Z_N \cos^2 \theta_M) C_p \omega_p} \right]^2 + 4k_B T_{comp} (R_g || R_{bias}) \right\} + \left[\frac{I_{dc}}{2\pi a} (Z_M \cos^2 \theta_M + Z_N \sin^2 \theta_M) - \frac{j N (Z_N - Z_M) \sin \theta_M \cos \theta_M}{1 + j \frac{2\pi a N^2}{l} (Z_M \sin^2 \theta_M + Z_N \cos^2 \theta_M) C_p \omega_p} \right]^2 \left[2 \left(\frac{V_g / \sqrt{2}}{10^{-3} \cdot 708} \right)^2 + 4k_B T_{comp} (R_g || R_{bias}) \right] + \left[\frac{2\pi a N^2 (Z_M \sin^2 \theta_M + Z_N \cos^2 \theta_M)}{1 + j \frac{2\pi a N^2}{l} (Z_M \sin^2 \theta_M + Z_N \cos^2 \theta_M) C_p \omega_p} - \frac{j N (Z_N - Z_M) \sin \theta_M \cos \theta_M}{1 + j \frac{2\pi a N^2}{l} (Z_M \sin^2 \theta_M + Z_N \cos^2 \theta_M) C_p \omega_p} \right]^2 \left[\frac{2\pi a N^2 (Z_M \sin^2 \theta_M + Z_N \cos^2 \theta_M)}{1 + j \frac{2\pi a N^2}{l} (Z_M \sin^2 \theta_M + Z_N \cos^2 \theta_M) C_p \omega_p} \right]^2 + 4k_B T_{comp} R_{buff} + e_{buff}^2 + R_{buff}^2 \frac{d^2}{d\omega_p^2} \left\{ \frac{2\pi a N^2 (Z_M \sin^2 \theta_M + Z_N \cos^2 \theta_M)}{1 + j \frac{2\pi a N^2}{l} (Z_M \sin^2 \theta_M + Z_N \cos^2 \theta_M) C_p \omega_p} \right\}$$

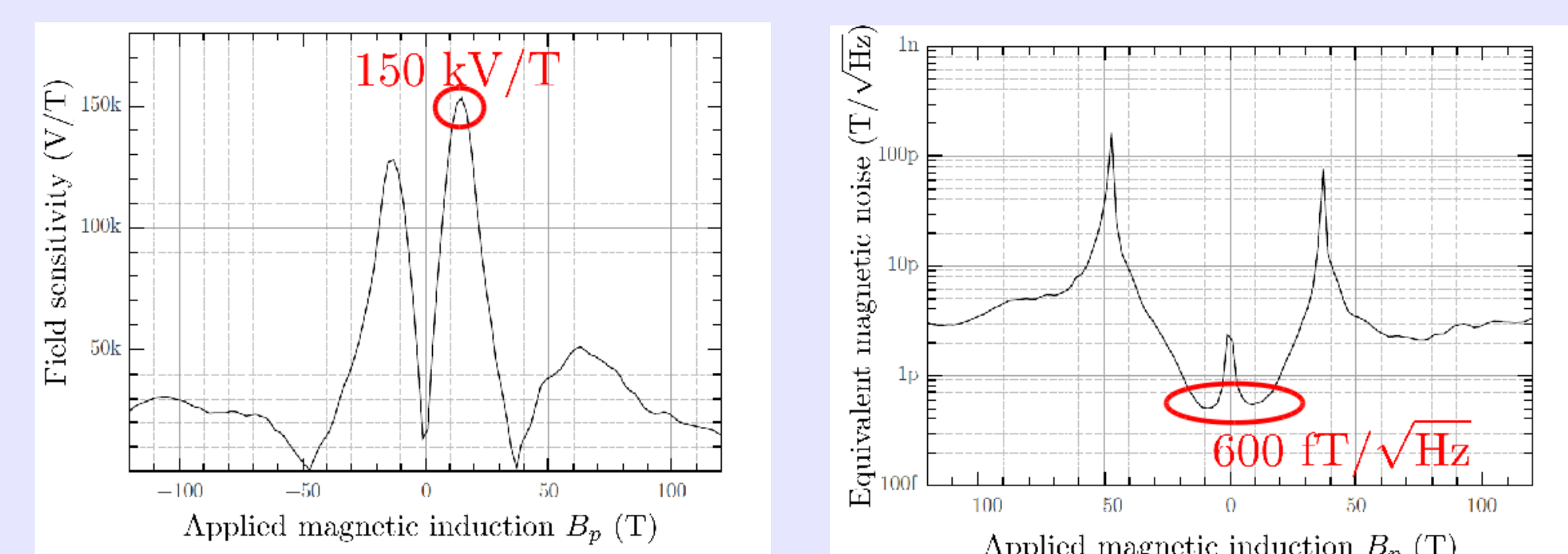
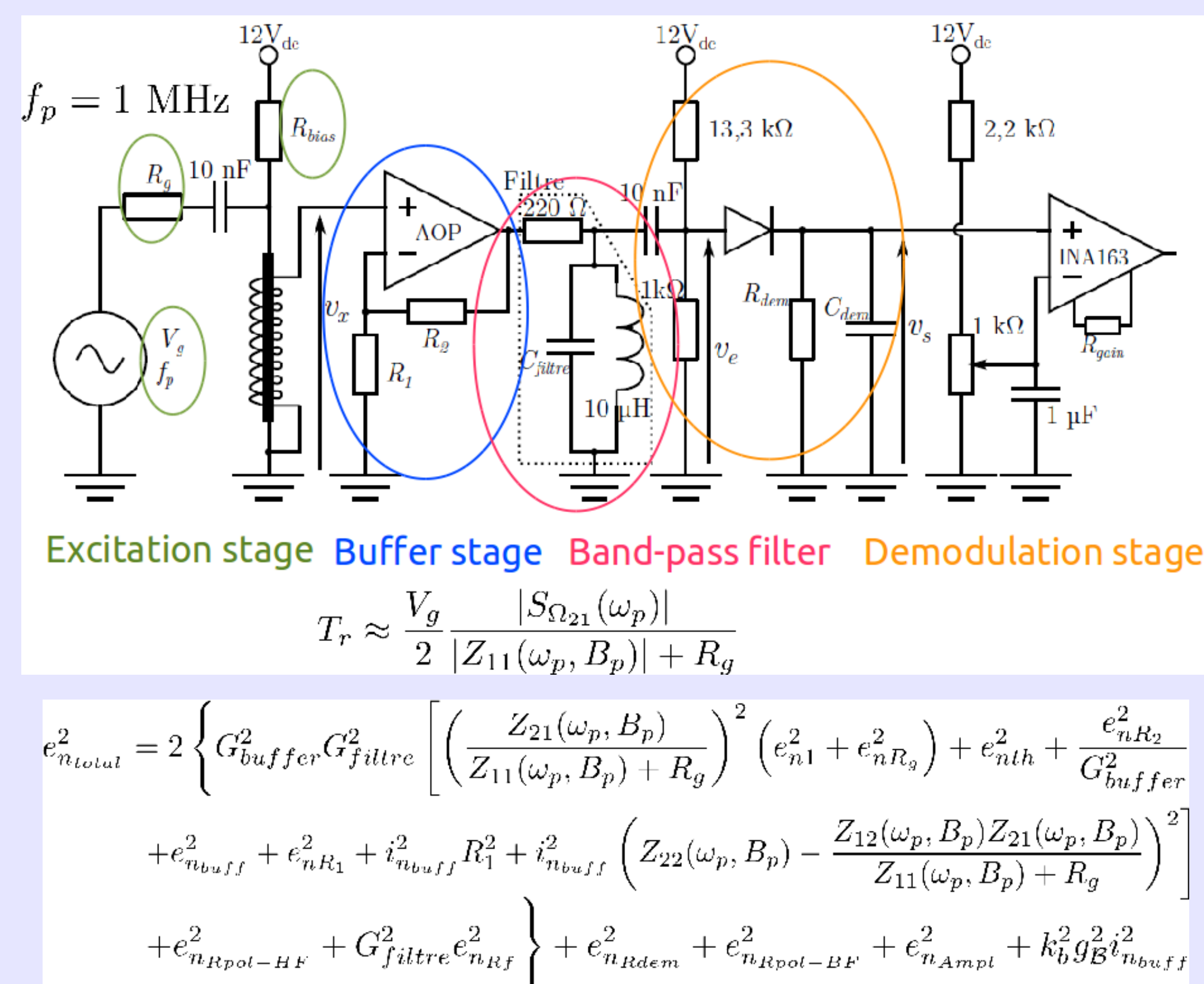
. GMI wire . Detection coil (C_p , N) . Electronic conditioning (excitation, detection, ...)

- Increase the number of turns allows to increase the sensitivity
however the parasitic capacitance is the main limiting factor.

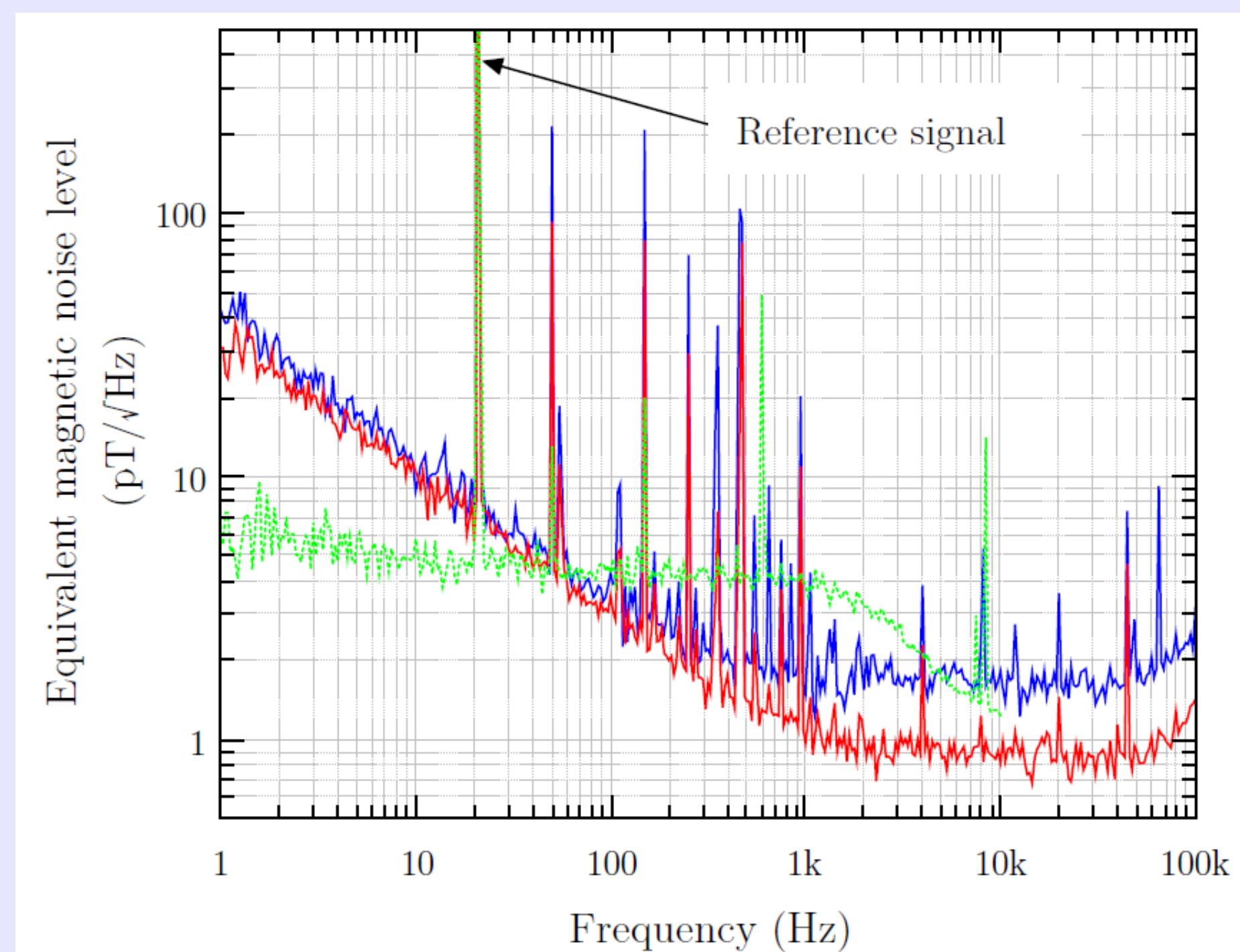
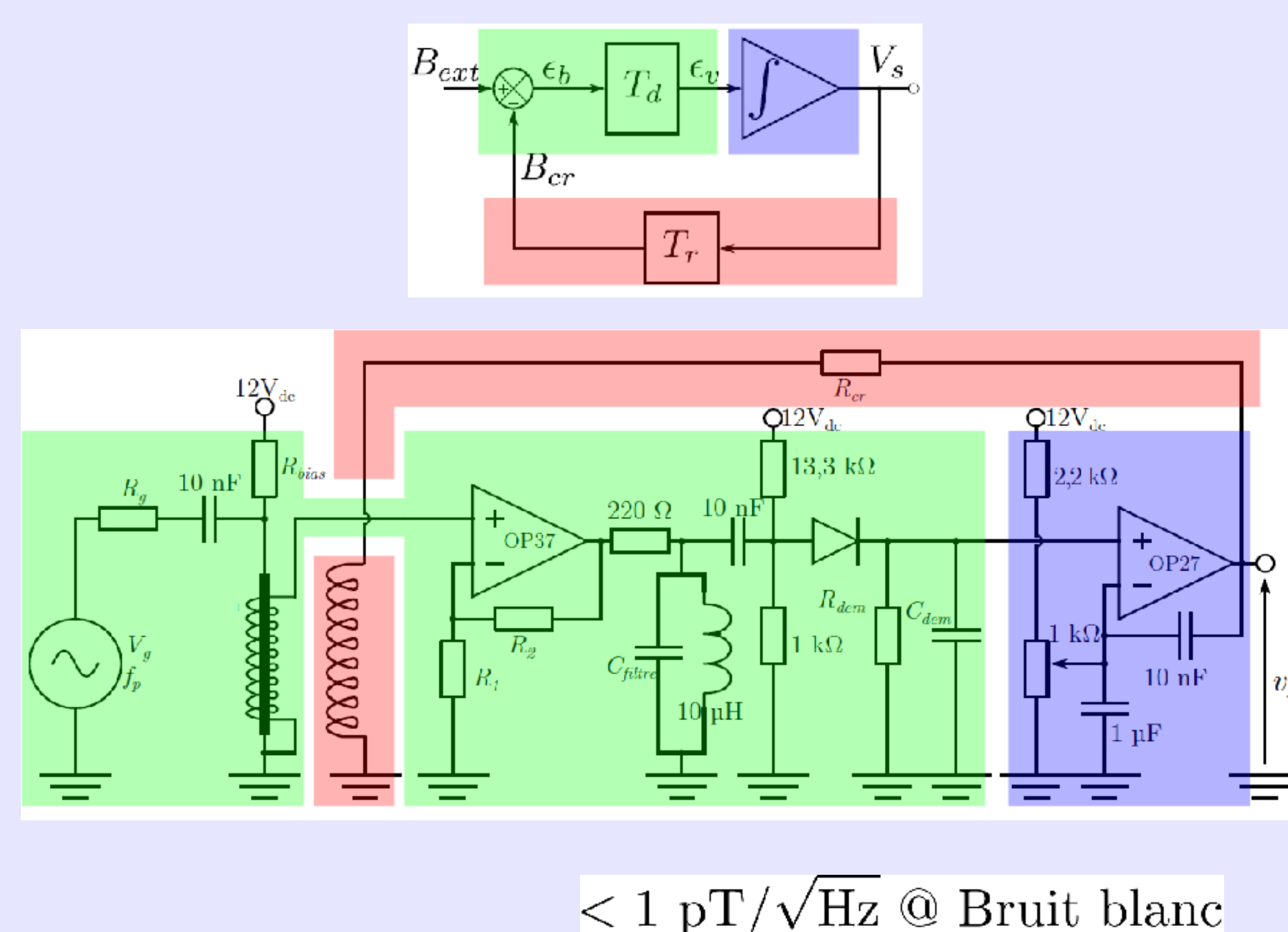
- Adapt the excitation frequency (or to tune the parasitic capacitance)
- Optimum between $\nearrow N$ and $\searrow C_p$



Optimized open loop



Optimized Magnetometers (field feedback loop)



Magnetometer	Sensitivity	Band-pass	Noise at 1 Hz	White noise	Maximum excursion	Dimension
	kV/T	Hz	pT/√Hz	pT/√Hz	μT	Length x diameter (mm)
GMI External feedback coil	490	DC to 90 kHz	35	0.9	±20	50×40
GMI re-use of detection coil	100	DC to 70 kHz	35	1.6	±100	25×3
Flux-Gate Bartington (Mag-03)	143	DC to 3 kHz	4	4	±70	30×8

- Model of the whole measurement chain
From physical properties to noise performance

Noise performance:

- < 1 pT/√Hz in white noise range
Well competitive compared to other main challengers such as Flux-Gate

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[2] L. G. C. Melo, D. Ménard, A. Yelon, L. Ding, S. Saez, and C. Dolabdjian, J. Appl. Phys. 103, 033903, 2008

[3] Characterization of an optimized off-diagonal GMI-based magnetometer. B. Dufay, S. Saez, C. Dolabdjian, A. Yelon, D. Menard, IEEE Sensors Journal (12) 2012, DOI: 10.1109/JSEN.2012.2216521)