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High negative genetic correlations between growth traits and wood properties suggest incorporating multiple traits selection including economic weights for the future Scots pine breeding programs

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Abstract

- **Context** The development of multiple trait selection indices for solid (structure) wood production in the Scots pine (*Pinus sylvestris* L.) breeding program requires genetic variances and covariances estimated among wood quality traits including stiffness.
- **Aims** Genetic control and relationships among Scots pine growth, fiber, and wood quality traits were assessed by estimating heritability, phenotypic and genetic correlation using a Scots pine full-sib family trial.
- **Method** Wood quality traits including clearwood and dynamic acoustic stiffness were measured using SilviScan and Hitman in a 40-year-old progeny trial and by sampling increment cores of 778 trees of 120 families. Genetic parameters were estimated using the mixed model by the ASReml software.
- **Results** Heritability ranged from 0.147 to 0.306 for growth, earlywood, transition wood and latewood proportion traits and from 0.260 to 0.524 for fiber dimension, wood density, MFA

and stiffness traits. The highly unfavorable genetic correlation between diameter and whole core density (−0.479) and clearwood stiffness (−0.506) and dynamic acoustic stiffness (−0.382) was observed in this study.

- **Conclusion** The unfavorable genetic correlations between growth traits and stiffness indicate that multiple traits selection using optimal economic weights and optimal breeding strategies are recommended for the advanced Scots pine breeding program.

Keywords Heritability · Correlation · Genetic gain · Wood quality traits · Scots pine

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Contributions of the co-authors Zhou Hong's contribution includes field data collection, data analysis and the writing of the manuscript. Anders Fries coordinated the experiment design, data collection and contributed to the writing of the manuscript. Harry X. Wu initiated the project, designed sampling strategy and contributed to the writing of the manuscript. All authors read and approved the final manuscript.

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1 Introduction

Scots pine (*Pinus sylvestris* L.) is the most widely distributed pine, native to Europe and northwestern Asia, ranging from Scotland, Ireland and Portugal in the west to Siberia and the Caucasus Mountains in the east and to far north as the Arctic Circle in Scandinavia countries (York and Littlefield 1942). Scots pine and Norway spruce (*Picea abies* (L.) Karst.) are the two most important commercial species for Swedish forestry. The Swedish Scots pine breeding program has implemented two cycles of selective breeding and established a third cycle of seed orchards with large genetic gains for growth-related traits (Rosvall 2011). The general objectives of the Swedish Scots pine breeding program are to balance efficient improvement of high-valued economic traits and adequate genetic variation. Open-pollinated seed orchards are widely implemented for deployment purpose, and breeding values for vitality, growth and wood quality traits are predicted for selection purposes (Berlin 2009).

Wood quality traits (e.g. wood density, stiffness) were not included as the selection criteria and breeding objective traits

in the first two cycles of selective breeding program for Scots pine. As Scots pine breeding program progresses further, improvement of wood quality traits is becoming an important issue due to highly negative genetic correlations between growth and wood density observed in the species and breeding experience in other pine species (Fries and Ericsson 2006; Hannrup et al. 2000). Wood density has been regarded as one of the most important factors affecting wood properties such as stiffness, strength and shrinkage behavior and was used by many breeding programs as an initial wood quality trait for improvement. However, it has been shown both experimentally and theoretically (Cave 1976) that microfibril angle (MFA) is at least as important as density for the prediction of the strength and stiffness of solid wood. To include MFA and stiffness in the breeding program, a rapid, cost-effective method to measure a large number of sample trees from progeny tests is required. SilviScan has become a commonly used technique for detailed measurement of radial variations in wood density and MFA and the estimation of stiffness (e.g. modulus of elasticity—MOE) using increment cores (Evans 2006), and genetic parameters were estimated using SilviScan data in many conifer species including radiata pine (*Pinus radiata*, Baltunis et al. 2007), Douglas fir (*Pseudotsuga menziesii*, Lachenbruch et al. 2010; Vikram et al. 2011) and white spruce (*Picea glauca*, Lenz et al. 2010, 2011).

To include wood quality traits into selection and breeding program, genetic variance and covariance are required for breeding value prediction and for designing optimal breeding strategy (mating and selection strategy). Genetic parameters for growth and wood properties have been estimated for Scots pine. The heritability for stem diameter ($h^2=0.10\text{--}0.30$) is usually lower than that for tree height ($h^2=0.25\text{--}0.32$) in Scots pine (Hannrup and Ekberg 1998; Hannrup et al. 2000, 2001). For wood properties, the main focus has so far been on wood density (Fries and Ericsson 2009) with a few estimates on tracheid length and heartwood properties. Heritability for wood density was estimated relatively high based on the whole core ($h^2=0.57$, Velling 1974) and slightly lower based on separate annual rings or annual ring components (earlywood or latewood) (Fries and Ericsson 2006, 2009; Hannrup and Ekberg 1998; Hannrup et al. 2000) or estimated by the pilodyn method ($h^2=0.10\text{--}0.50$, Haapanen et al. 1997). Furthermore, heritability from 0.30 to 0.50 was estimated for fiber length, fiber width and fiber angle for Scots pine (Ericsson and Fries 2004; Hallingbäck 2010; Hannrup and Ekberg 1998). Nearly all estimated genetic correlations between growth traits and wood density were negative $r_A=-0.14$ to -0.4 for height and wood density (Fries and Ericsson 2006, 2009; Hannrup et al. 2000) and $r_A=-0.42$ to -0.5 for stem diameter and wood density (Fries and Ericsson 2006, 2009). Fiber length was also negatively correlated with growth traits $r_A=-0.12$ for height and $r_A=-0.63$ for stem diameter, respectively (Ericsson and Fries 2004). In contrast, fiber width was

positively correlated with growth ($r_A=0.56$ for height and $r_A=0.90$ for stem diameter, respectively).

In this paper, genetic parameters for wood quality related traits, e.g., fiber dimension, wood density, earlywood and latewood proportion as well as for MFA, clearwood stiffness and dynamic acoustic stiffness of the standing trees are estimated for Swedish Scots pine. The objectives in this study were to (1) estimate genetic variation and heritability for growth, fiber and wood quality traits including stiffness; (2) estimate the genetic correlations between these growth, fiber and wood quality traits; (3) evaluate the possibility to use nondestructive acoustic testing techniques to predict stiffness of clearwood for Scots pine; and (4) estimate genetic gain for volume and stiffness from simple mass selection.

2 Material and method

2.1 The field test

The study was undertaken using a full-sib diallel progeny test located at 100-km northwest of Örnsköldsvik in Northern Sweden (Skogforsk S23F711261 Grundtjärn, latitude 63°33' N; Longitude 17°25' E; altitude 320 m.a.s.l.). The trial was planted on an undulated sandy moraine with gradual sloping facing west in September 1971. A single tree plot at 2.2-m square spacing with 179 full-sib families, generated from a partial diallel mating of 40 plus trees was planted on a 3.5-ha block. A completely randomized design with 40 trees each family was used. The 40 plus trees were selected from the first generation parents. In September 2011, the trees were 40 years old, and about 43 % of the planted trees had left after the first thinning and mortality. Approximately five trees from 120 families and two trees from the remaining families were sampled giving a total of 778 sample trees for the study.

2.2 Growth data

The 778 sample trees were measured for tree height (HGT) and breast height diameter (DBH) at 40 years of tree age. Stem volume (VOL, dm³) was calculated as a function of diameter at breast height (DBH, cm) and height (HGT, m) according to the following equations for trees >5 cm in diameter (Brandel 1990): $VOL = \exp[-2.7841 + 1.9474 \cdot \ln(DBH) - 0.05947 \cdot \ln(DBH + 20) + 1.40958 \cdot \ln(HGT) - 0.4581 \cdot \ln(HGT - 1.3)]$.

2.3 Hitman ST300 predicted modulus of elasticity (MOE_{tor})

Standing-tree acoustic velocity was measured by hammering two sensor probes (transmitting and receiving probes) around breast height (1.3 m from the ground) into the stem. A stress wave was induced by striking the transmitting probe with a steel hammer, and the time-of-flight (TOF) was recorded. The

Hitman ST300 measurements were taken on the southeast side of the tree, and two series of eight hits gave two values of which the average was used. Distance between the measurement points was 0.7–1.3 m (distances below 0.8 m were not very common). If the two velocities differed more than 0.1 m/ms, additional series were taken to get a satisfactory precision. The standing tree time-of-flight technique provided an acoustic wave velocity for the stem. Modulus of elasticity using time-of-flight (MOE_{tof}) was related to the acoustic velocity of the wood according to the following equation: $MOE_{tof} = V^2 \times D / 10^9$, where, V = Velocity (m/s) ($V = 1/T$; T = time-of-flight (s)), D = Green density (kg/m^3) (Bucur 2006).

2.4 SilviScan analysis for wood and fiber traits

Increment cores at breast height were taken from 778 trees for SilviScan measurement. The SilviScan instrument (Innventia AB, Stockholm, Sweden) is an instrument designed to analyze wood and fiber traits in radial strip samples measuring 2-mm thick and 7-mm high. The sampled strips for this study were prepared from increment cores (diameter 10 mm) taken through the stem from bark to bark with a normal increment borer run by an electric boring machine. Each sample was soaked in clean acetone to remove extractives to avoiding disturbances of the measurement. The specimens were conditioned in the laboratory at approximately 23 °C and 43 % relative humidity and then scanned from pith-to-bark for wood and fiber traits using X-ray densitometry and X-ray diffractometry. From the obtained data, wood properties such as fiber wall thickness (FWT), fiber width in the radial direction (FRW) and in the tangential direction (FTW), fiber coarseness (FMC), microfibril angle (MFA) and clearwood modulus of elasticity (MOE_s) are estimated (Evans 2006). Earlywood was then defined as the first part of the ring with wood density changing from the minimum up to 20 % variation from the minimum within the ring. Latewood was defined as the part of ring with the highest density with 20 % of the variation, and transition wood was defined as the middle of the ring occupying 60 % variation (e.g., from 20 to 80 % of range in variation). Proportion of earlywood (EWP), transition wood (TWP) and latewood width (LWP) and wood density of earlywood (EWD), transition wood (TWD) and latewood (LWD) were also calculated.

2.5 Area-weighted average data

The variation of wood quality trait was analyzed at whole core level and for each annual ring component (earlywood, transition wood and latewood, respectively). Area-weighted values were calculated and utilized in the study since area-weighted average was more accurate to represent the average properties of the wood in a log (Gräns et al.

2009). The area-weighted values of the cores and the segments were calculated as

$$AB = \sum (ai \times di) / \sum ai$$

where AB was the ring area-weighted value, ai was the cross-sectional area of the i th annual ring assuming that each ring was circular and di is the value of the i th annual ring (Hannrup et al. 2000).

2.6 Statistical analysis

Data analyses for Swedish trials were usually conducted using post-blocking for the completely randomly design in the past and using spatial analyses of the adjustment in the recent. However, due to irregular distribution of sampled trees after thinning in the current study, these adjustments are not efficient (Fries and Ericsson 2006); therefore, the data were analyzed using the following model by the ASReml statistical software package (Gilmour et al. 2009) for individual and multivariate traits:

$$y_{ijk} = \mu + G_i + G_j + S_{ij} + E_{ijk}$$

where, y_{ijk} is the k th observation for the i th cross; μ is the overall mean; G_i , G_j is the random general combining ability (GCA) effect of the i th female or the j th male ~normally, independently distributed (NID) ($0, \sigma^2_G$), $i, j = 1$ to p and $i < j$; S_{ij} is the random specific combining ability (SCA) effect of the i th and the j th parents ($i \neq j$) ~NID ($0, \sigma^2_S$); E_{ijk} is the random error term ~NID ($0, \sigma^2_E$).

Estimates of heritability were obtained for each trait using the variance components from the GCA and SCA model. Standard errors were estimated using Taylor expansion as described in ASReml package.

Individual-tree narrow-sense heritability $h^2 = \frac{\sigma^2_A}{\sigma^2_p} = \frac{4\sigma^2_G}{2\sigma^2_G + \sigma^2_s + \sigma^2_e}$ where σ^2_A : additive genetic variance; σ^2_p : phenotypic variance; σ^2_G : general combining ability variance; σ^2_s : specific combining ability variance; σ^2_e : residual variance.

Variances are not independent of the scale and the mean of the respective traits (Sokal and Rohlf 1995). Therefore, to relatively compare phenotypic and additive genetic variation of the different traits, a parameter measuring the coefficient of variation was calculated using variance and mean (CV_A and CV_p , respectively).

Genetic correlations between traits x and y were obtained from the estimated additive genetic covariance and variance components (using the individual tree model) as

$$r_A = \frac{\sigma_{A_x A_y}}{\sigma_{A_x} \sigma_{A_y}}$$

where $\sigma_{A_x A_y}$ is the additive genetic covariance component between traits x and y and $\sigma_{A_x}^2$, and $\sigma_{A_y}^2$ is the additive genetic variance component for traits x and y , respectively.

In the Swedish Scots pine program, volume and stem-wood quality (stiffness) are two important breeding objective traits (Berlin 2009; Fries 2012). Genetic gains were calculated to improve these two traits (VOL, MOE_s or MOE_{tof}) by direct selection and indirect selection using correlated traits. The genetic gain expressed as the percentage of the mean in direct selection for trait i was estimated as

$$\Delta G_i = \frac{i \times h_i^2 \times \sigma_p(i)}{Mv_i} \times 100$$

where i is the selection intensity, h_i^2 is the individual-tree narrow-sense heritability, $\sigma_p(i)$ is the phenotypic standard deviation and Mv_i is the mean value of trait (Falconer and Mackay 1996). The genetic gain of target trait t from indirect selection of correlated trait i was estimated using

$$\Delta G_t = \frac{i h_i h_t r_A \sigma_{pt}}{Mv_t} \times 100$$

where h_t is the square root of heritability for target trait, r_A is the additive genetic correlation between selection trait i and target trait t and σ_{pt} is the phenotypic standard deviation for target trait t .

3 Result

3.1 Mean values and the size of variation for growth, fiber and wood quality traits

The average, minimum and maximum value, genetic and phenotypic standard deviation and coefficients of variation for growth, fiber and wood quality traits were presented in Table 1. The average of DBH was 19.6 cm for 40 years Scots pine, translating into about 0.5 cm per year growth rate. On average, earlywood had the highest proportion (55.2 %), and latewood had the least proportion (15.3 %). Scots pine has a relatively high wood density (447 kg/m³) and with a low earlywood density (331 kg/m³) and a high latewood density (763 kg/m³). The average MFA of Scots pine was also relatively low at 17.3°.

Genetic coefficients of variation (CV_A) varied between 2.34 and 16.6 %, with the highest coefficients for volume of individual tree. Among the three wood proportion traits, the latewood proportion had the largest CV_A (7.25 %) even though it had the lowest average of 15.3 %. All other wood quality traits had low CV_A from 2.34 to 5.71 % with three exceptions (e.g. MFA 12.5 %, MOE_s 11.1 % and MOE_{tof} 13.6 %). The average clearwood stiffness from SilviScan (MOE_s) is significantly higher than the acoustic MOE_{tof} for the population.

3.2 Heritability of growth, fiber and wood quality traits

Heritability for the growth traits (DBH, HGT and VOL) was between 0.238 and 0.273, and for wood proportion traits, it was slightly lower with an exception of a higher heritability of 0.306 for the latewood proportion (Table 1). The heritability for the wood and fiber quality traits was higher than growth traits, ranging from 0.260 (FTW) to 0.524 (FMC) and was around 0.400 for most of the wood quality traits.

3.3 Correlations among growth traits

Earlywood proportion was positively additive genetic correlated with all three growth traits (0.427, 0.320 and 0.295 for DBH, HGT and VOL, respectively), while transition and latewood proportion were negatively additive genetic correlated with these same growth traits (Table 2). As expected, correlations among the wood proportion percentage are all negative (for example, genetic correlation was −0.514 between EWP and LWP).

3.4 Correlations among fiber and wood quality traits

Genetic correlations were high among the four wood density traits ($r_A \geq 0.764$) but high to low with the fiber dimension traits ($0.909 \geq r_A \geq -0.0701$, Table 3). Two fiber dimension traits (FRW and FTW) had low and non-significant genetic correlations with wood density traits ($0.125 \geq r_A \geq -0.248$), while fiber wall thickness and coarseness had high and positive correlations with wood density traits ($0.909 \geq r_A \geq 0.544$) reflecting fiber wall thickness contributing to the overall wood density. This indicates that it is the fiber cell wall thickness rather than the size of the fiber cell contributing to wood density. MFA was highly but negatively correlated with all wood density traits as expected ($-0.522 \geq r_A \geq -0.781$), while MFA had negative but non-significant genetic correlations with the two fiber dimension traits (Table 3). As expected, genetic correlation between two stiffness measurements (MOE_s and MOE_{tof}) was very high (0.945), and stiffness had high and positive genetic correlations with all wood density traits ($0.904 \geq r_A \geq 0.760$) and with FWT and FMC. Similarly, stiffness had high negative genetic correlation with MFA as expected (−0.911 and −0.831 for MOE_s and MOE_{tof}, respectively) but had low and non-significant correlations with two fiber dimension traits. The phenotypic correlations for among-trait groups and within-trait group are similar to genetic correlations but usually slightly lower than the genetic correlations.

3.5 Correlation between growth, fiber and wood quality traits

Growth traits (DBH, HGT and VOL) all had negative genetic correlations with the four wood density traits (DEN, EWD,

Table 1 The average, range, genetic (σ_a) and phenotypic (σ_p) standard deviations, genetic (CV_A) and phenotypic (CV_P) coefficients of variation, and narrow-sense heritability (h^2) for the six growth, fiber, and 11 wood quality traits (standard errors for h^2 presented within the parenthesis)

Trait	Min	Max	Mean	σ_a	CV_A (%)	σ_p	CV_P (%)	h^2
Wood quantity traits								
DBH (mm)	82.0	314	196	15.0	7.65	30.8	15.7	0.238 (0.0791)
HGT (dm)	102	196	162	7.07	4.36	13.5	8.33	0.273 (0.0883)
VOL (dm ³)	46.0	746	332	55.1	16.6	112	33.8	0.243 (0.0844)
EWP (%)	36.1	67.2	55.2	1.85	3.35	4.43	8.02	0.174 (0.0572)
TWP (%)	18.2	45.3	29.5	1.60	5.42	4.17	14.1	0.147 (0.0653)
LWP (%)	9.21	22.8	15.3	1.11	7.25	2.01	13.1	0.306 (0.0954)
Wood and fiber quality traits								
DEN (kg/m ³)	364	597	447	20.1	4.50	31.2	6.98	0.417 (0.100)
EWD (kg/m ³)	280	410	331	12.8	3.87	20.4	6.16	0.399 (0.101)
TWD (kg/m ³)	376	660	497	21.9	4.41	34.1	6.86	0.417 (0.102)
LWD (kg/m ³)	590	905	763	33.6	4.40	50.1	6.57	0.449 (0.101)
FRW (μ m)	16.9	38.4	33.4	1.08	3.23	1.62	4.85	0.449 (0.111)
FTW (μ m)	14.0	35.5	28.6	0.67	2.34	1.31	4.58	0.260 (0.0891)
FWT (μ m)	1.22	3.36	2.45	0.13	5.31	0.191	7.80	0.438 (0.110)
FMC (μ g/m)	202	522	405	23.1	5.71	32.0	7.90	0.524 (0.117)
MFA (°)	7.77	36.7	17.3	2.17	12.5	4.22	24.4	0.264 (0.0791)
MOE _s (Gpa)	2.77	15.9	10.2	1.14	11.1	1.86	18.2	0.377 (0.101)
MOE _{tof} (Gpa)	3.44	11.2	6.68	0.91	13.6	1.36	20.3	0.447 (0.104)

DBH diameter at breast height, HGT tree height, VOL stem volume of individual tree, EWP earlywood width proportion, TWP transition wood width proportion, LWP latewood width proportion, DEN area-weighted mean wood density, EWD area-weighted earlywood density, TWD area-weighted transition wood density, LWD area-weighted latewood density (densities from SilviScan measurements), FRW fiber width in the radial direction in the stem, FTW fiber width in the tangential direction in the stem, FWT fiber wall thickness, FMC fiber coarseness, MFA microfibril angle, MOE_s modulus of elasticity estimated using SilviScan-3, MOE_{tof} modulus of elasticity estimated using VEL and DEN

TWD and LWD), fiber wall thickness (FWT), fiber coarseness (FMC) and the two stiffness traits (Table 4). However, negative correlations between growth traits and whole core and earlywood density and stiffness were moderately strong ($-0.235 \geq r_A \geq -0.524$), while negative correlations between growth traits and transition and latewood density, fiber wall thickness and fiber coarseness were generally low ($-0.0801 \geq r_A \geq -0.356$). Genetic correlations between the ring width proportion traits (EWP, TWP and LWP) and their corresponding

densities (EWD, TWD and LWD) were all positive with an increasing trend from earlywood to latewood (e.g. from 0.102 to 0.615). Earlywood proportion had low and non-significant genetic correlations with three wood densities (DEN, TWD and LWD), while transition wood had slightly higher but negative genetic correlation with three other wood densities (DEN, EWD and LWD). However, latewood proportion had higher and positive genetic correlation with all four wood densities ($0.615 \geq r_A \geq 0.274$). Growth traits (DBH, HGT and

Table 2 Additive genetic (above diagonal) and phenotypic (below diagonal) correlations between growth traits (standard errors within the parenthesis)

	Growth traits			Ring width traits		
	DBH	HGT	VOL	EWP	TWP	LWP
DBH	1	0.620 (0.155)	0.980 (0.00843)	0.427 (0.249)	-0.0621 (0.290)	-0.631 (0.170)
HGT	0.557 (0.0301)	1	0.681 (0.0841)	0.320 (0.263)	-0.133 (0.292)	-0.366 (0.224)
VOL	0.876 (0.00815)	0.450 (0.0271)	1	0.295 (0.142)	-0.0831 (0.131)	-0.487 (0.117)
EWP	0.024 (0.0412)	-0.0221 (0.0458)	-0.0322 (0.0278)	1	-0.798 (0.102)	-0.514 (0.209)
TWP	0.100 (0.0443)	0.0558 (0.0454)	0.0411 (0.0248)	-0.894 (0.00921)	1	-0.396 (0.0651)
LWP	-0.262 (0.0421)	-0.0721 (0.0482)	-0.170 (0.0309)	-0.355 (0.0401)	-0.103 (0.045)	1

Table 3 Additive genetic (above diagonal) and phenotypic (below diagonal) correlations between wood and fiber quality traits (standard errors within the parenthesis)

	Wood density traits				Fiber dimension traits					Stiffness traits	
	DEN	EWD	TWD	LWD	FRW	FTW	FWT	MFC	MFA	MOE _s	MOE _{tof}
DEN	1	0.856 (−0.0591)	0.931 (0.0282)	0.923 (0.0368)	0.121 (0.205)	−0.183 (0.229)	0.773 (0.123)	0.585 (0.127)	−0.556 (0.170)	0.843 (0.0778)	0.872 (0.0644)
EWD	0.843 (0.0168)	1	0.764 (0.0848)	0.836 (0.0681)	0.0342 (0.214)	−0.248 (0.226)	0.771 (0.0889)	0.544 (0.142)	−0.781 (0.134)	0.862 (0.0545)	0.904 (0.0591)
TWD	0.820 (0.0161)	0.693 (0.0268)	1	0.930 (0.0301)	0.0334 (0.208)	−0.0701 (0.232)	0.909 (0.0445)	0.659 (0.109)	−0.593 (0.160)	0.805 (0.0856)	0.816 (0.0801)
LWD	0.650 (0.0241)	0.544 (0.0319)	0.703 (0.0218)	1	0.125 (0.182)	−0.213 (0.199)	0.893 (0.0522)	0.646 (0.109)	−0.522 (0.146)	0.760 (0.0845)	0.848 (0.0645)
FRW	0.269 (0.0532)	−0.258 (0.0528)	−0.189 (0.0548)	−0.100 (0.0552)	1	0.407 (0.199)	0.264 (0.201)	0.647 (0.122)	−0.169 (0.224)	0.0733 (0.215)	0.0111 (0.210)
FTW	−0.152 (0.0465)	−0.199 (0.0461)	−0.104 (0.0447)	−0.103 (0.0462)	0.492 (0.0401)	1	0.157 (0.233)	0.523 (0.165)	−0.0556 (0.254)	−0.0811 (0.238)	−0.292 (0.222)
FWT	0.663 (0.0139)	0.740 (0.0239)	0.749 (0.0191)	0.609 (0.0285)	0.139 (0.0552)	0.273 (0.0478)	1	0.886 (0.0444)	−0.600 (0.170)	0.614 (0.0933)	0.770 (0.0971)
MFC	0.493 (0.0419)	0.439 (0.0441)	0.453 (0.0409)	0.378 (0.0431)	0.468 (0.0431)	0.507 (0.0378)	0.789 (0.0122)	1	−0.515 (0.181)	0.614 (0.143)	0.543 (0.150)
MFA	−0.207 (0.0458)	−0.255 (0.0432)	−0.276 (0.0424)	−0.382 (0.0378)	0.0789 (0.0511)	0.0256 (0.0467)	−0.181 (0.0478)	−0.299 (0.0522)	1	−0.911 (0.0411)	−0.831 (0.0863)
MOE _s	0.552 (0.0330)	0.541 (0.0341)	0.527 (0.0323)	0.517 (0.0248)	−0.202 (0.0544)	−0.125 (0.0494)	0.481 (0.0389)	0.283 (0.0504)	−0.891 (0.00891)	1	0.945 (0.0354)
MOE _{tof}	0.629 (0.0301)	0.619 (0.0311)	0.566 (0.0332)	0.596 (0.03109)	−0.213 (0.0551)	−0.105 (0.0511)	0.565 (0.0356)	0.356 (0.0489)	−0.780 (0.0311)	0.755 (0.0211)	1

VOL) had positive and low genetic correlations with two fiber dimension traits (FRW and FTW) and MFA but negative correlations with other two fiber dimension traits (FWT and FMC).

Among genetic correlations between ring width proportion traits and fiber dimension traits, two correlations (e.g. 0.482 between EWP and FRW and 0.544 between LWP and FWT) are moderate to high. It also seems that stiffness traits are more

Table 4 Genetic correlation between growth, fiber and wood quality traits (standard errors within the parenthesis)

		Density trait				Fiber dimensions trait					Stiffness trait	
		DEN	EWD	TWD	LWD	FRW	FTW	FWT	MFC	MFA	MOE _s	MOE _{tof}
Growth traits	DBH	−0.479 (0.190)	−0.524 (0.074)	−0.248 (0.217)	−0.237 (0.193)	0.111 (0.228)	0.235 (0.252)	−0.353 (0.216)	−0.177 (0.220)	0.340 (0.221)	−0.506 (0.181)	−0.382 (0.196)
	HGT	−0.378 (0.208)	−0.430 (0.202)	−0.178 (0.224)	−0.310 (0.188)	0.0178 (0.235)	0.290 (0.250)	−0.292 (0.205)	−0.204 (0.219)	0.310 (0.229)	−0.448 (0.200)	−0.323 (0.210)
	VOL	−0.395 (0.116)	−0.355 (0.115)	−0.111 (0.110)	−0.126 (0.105)	0.0967 (0.230)	0.182 (0.244)	−0.356 (0.216)	−0.0801 (0.114)	0.239 (0.220)	−0.370 (0.178)	−0.235 (0.192)
Ring width traits	EWP	−0.211 (0.233)	0.102 (0.251)	0.0444 (0.242)	0.0889 (0.209)	0.482 (0.0251)	0.103 (0.278)	−0.0338 (0.253)	0.165 (0.242)	−0.249 (0.244)	0.0301 (0.248)	0.00398 (0.243)
	TWP	−0.218 (0.252)	−0.307 (0.251)	0.469 (0.208)	−0.379 (0.188)	−0.244 (0.264)	−0.097 (0.297)	−0.334 (0.254)	−0.366 (0.239)	0.372 (0.237)	−0.305 (0.238)	−0.259 (0.242)
	LWP	0.575 (0.128)	0.274 (0.208)	0.612 (0.144)	0.615 (0.164)	−0.264 (0.0481)	−0.0281 (0.253)	0.544 (0.163)	0.263 (0.198)	−0.118 (0.236)	0.392 (0.189)	0.376 (0.189)

positively correlated with latewood proportion (0.392 and 0.376, respectively with MOE_s and MOE_{tof}).

3.6 Genetic gain

The genetic gains from the direct selection on three breeding objective traits (VOL, MOE_s and MOE_{tof}) and correlated genetic gains from the indirect selection based on other 14 growth, fiber dimension and wood quality traits are presented in Table 5 with a 10 % selection intensity. There were relatively moderate genetic gains from the direct selection (e.g. $\Delta G_{MOE_{tof}} = 16.0$ %, $\Delta G_{VOL} = 14.2$ % and $\Delta G_{MOE_s} = 12.1$ %, respectively). Relatively high correlated gains for volume are observed if selection was based on DBH and tree height. However, positive selection based on ring width proportion and wood quality traits (but lower MFA) will generate negative gains for volume except for EWP.

As expected, positive selection for growth traits generated negative gains for stiffness traits but positive selection for all ring width proportion traits, and wood quality traits (but lower MFA) generated positive gain for stiffness traits except for TWP and FTW. Indirect selection for stiffness traits based on wood quality traits had slightly smaller but still considerable gains (about 10 and 13 % for MOE_s and MOE_{tof} , respectively) than the direct selection for stiffness traits. The negative genetic correlation and gains between volume and stiffness in Scots pine indicated that appropriate economic weights for growth and wood quality traits are required for balancing the gain for both volume and stiffness.

It was also observed that the indirect selection from acoustic stiffness (MOE_{tof}) will generate more gain for clearwood stiffness MOE_s than the direct selection based on MOE_s . This is due to the higher heritability observed in MOE_{tof} than in MOE_s and the high genetic correlation between the two stiffness traits. Indirect selection using wood quality traits for clearwood and acoustic stiffness was also observed generating gains that were about 20 % less than the gain from the direct selection for the stiffness traits.

4 Discussion

4.1 Experimental design

The completely randomized design (CRD) experiment was used for this site and other Swedish tree progeny trials in the last several decades. The potential consequence of CRD design is that residual variance could be increased due to the confounding effect of replicates and true randomly environmental errors if the significant replicates were not separated from the error term in the experiment. This would reduce heritability estimates. To overcome such potential shortage, post-blocking was usually recommended to reduce residual error variance as

Table 5 Genetic gain and correlated genetic responses for three breeding target traits with 10 % selection intensity. **Bold**, genetic gain; normal, genetic response

		Target traits		
		VOL	MOE_s	MOE_{tof}
Selection traits	DBH	13.9	−4.91	−4.45
	HGT	10.2	−4.60	−3.97
	VOL	14.2	−3.56	−2.81
	EWP	3.59	0.241	0.101
	TWP	−0.902	−2.36	−2.41
	LWP	−7.92	4.27	5.06
	DEN	−7.52	10.7	13.4
	EWD	−6.61	10.6	13.6
	TWD	−2.04	10.1	12.5
	LWD	−2.53	10.0	13.7
	FRW	1.95	0.921	0.182
	FTW	2.66	−0.801	−3.56
	FWT	−6.93	7.95	12.2
	FMC	−1.67	8.64	9.36
	MFA	3.55	−9.12	−10.1
	MOE_s	−6.62	12.1	13.9
	MOE_{tof}	−4.67	12.46	16.0

much as possible and to increase heritability (Ericsson 1997). The CRD was used due to its simplicity of field implementation of planting in Sweden's tree breeding program. It was estimated that the loss associated with using CRD is much less than the benefit gained by using an uncomplicated, less expensive design (Ericsson 1999). There was a continued debate within tree-breeding community in Sweden whether the CRD should be used in future experiments with post-blocking or spatial analyses or using replicated and more complicated design. To answer this debated question, one study project was set up recently to compare the overall efficiency between the CRD and other replicated design using both statistical and economic measures. For this particular site in this study, the post-blocking was previously used for the analyses (Fries and Ericsson 2006, 2009), and it was found that the post-blocking was not significant. Thus, analyses based on CRD would not significantly affect the estimates of genetic variances and heritability.

There was only one site used in this study. If there was potential genotype by site (G by E) interaction among several sites, genetic parameters such as heritability would be inflated if estimated based on a single site. For growth traits, the G by E was found not to play a great role in Swedish Scots pine trials as long as the progeny testing was aimed at one climate region (or breeding zone) (Zhelev et al. 2003; Kroon et al. 2011). For wood quality traits such as wood density and stiffness, the G by E was usually non-significant (Baltunis et al. 2010) or small (Zobel and Talbert 1984; Gapare et al. 2010) in many studies.

These may indicate that estimate of heritability for wood quality traits would have less bias than for growth and survival traits (Eriksson 2008).

4.2 Trait means and variation

The average height and diameter for the trial were also measured in 2001 before the thinning. In the last 10 years, average tree height increased 5.10 m and DBH increased 4.25 cm. However, both genetic and phenotypic coefficients of variation for height decreased (e.g., from 5.4 to 4.4 % for CV_A and from 11.3 to 8.3 % for CV_P for tree height) (Fries and Ericsson 2006, 2009; Kroon et al. 2008). The reduction of both CV_A and CV_P may be caused by the thinning process that removed smaller depressed trees unproportionally.

The average value of whole core wood density (447 kg/m^3) was comparable with the average densities reported in other Scots pine studies. The separation of earlywood density (331 kg/m^3) and latewood density (763 kg/m^3) using a transition wood made the difference of wood density between the earlywood and latewood larger than the previous comparison between the earlywood and latewood when the delineation of a transition zone was not implemented (Fries and Ericsson 2006, 2009). The proportion of the latewood was recognized as one of the most important factors influencing the whole core density (Louzada and Fonseca 2002). Also, the latewood proportion is usually increased as cambial age increases, with a consequence of an increased overall wood density. Wood stiffness is one of the most important properties of structural wood products, and Scots pine is known for its strong, stiff and dense wood. Mean values for MOE_s and MOE_{tof} were 10.2 and 6.68 Gpa, respectively. The difference between these two estimates was due to the different methods used for the measurements. SilviScan is calibrated using sonic resonance on dry wood and acoustic dynamic measurement used on green wood, and green wood is less stiff than the dry wood. Such difference was observed in radiata pine (*Pinus radiata*) (Gapare et al. 2009), Douglas fir (*Pseudotsuga menziesii*) (Lachenbruch et al. 2010) and loblolly pine (*Pinus taeda*) (Isik et al. 2011).

4.3 Genetic variation and heritability

The coefficient of additive genetic variation (CV_A) for density was about 4 % which was similar to the previous estimates of CV_A in Scots pine (Ericsson and Fries 2004; Fries and Ericsson 2006, 2009 and Fries 2012). CV_A for MFA, MOE_s and MOE_{tof} was 12.5, 11.1 and 13.6 %, which were about three times of the estimates for density. Much higher CV_A for MOE than wood density indicate that there will be more scope for improving MOE than for its component trait of wood density. Higher CV_A for MOE than for wood density was also found in

radiata pine (Gapare et al. 2009) and Norway spruce (Gräns et al. 2009).

Heritability is an important parameter in the prediction of genetic gain and for developing breeding strategies (Falconer and Mackay 1996). Heritability for density, stiffness and fiber dimension traits in this study was moderate, generally around or above 0.4, while heritability for growth traits, proportions of earlywood, transition wood and latewood types was lower (0.147–0.306). The heritability for growth traits and wood density was similar to the previous estimates in Scots pine (Ericsson and Fries 2004; Fries and Ericsson 2006, 2009; Kroon et al. 2008) and black (*Picea mariana*), white (*Picea glauca*) (Lenz et al. 2010, 2011) and Norway spruce (Hyllen 1999; Park et al. 2012; Zhang and Jiang 1998) and maritime pine (*Pinus pinaster*) (Louzada and Fonseca 2002). Relative higher genetic variation ($CV_A=7.25\%$), moderate heritability ($h^2=0.306$) and lower mean value (15.3 %) for the latewood percentage were interesting observations. The latewood percentage was also highly correlated with whole core density and stiffness. Therefore, improvement of latewood percentage seems highly desirable and potential for improving overall wood density and stiffness of Scots pine (Gryc et al. 2011).

The low heritability for MFA in this study ($h^2=0.264$) is comparable with the estimates in Norway spruce (around 0.30, Hannrup et al. 2004) but lower than in radiata pine (average $h^2_i=0.63$, Wu et al. 2008). Higher MOE increases the recovery rate of the structural and appearance grade products, which give a higher economic return. MOE was under moderate genetic control with heritability around 0.4 in this study. This was higher than for Douglas fir ($h^2=0.33$, Vikram et al. 2011) and loblolly pine ($h^2=0.30$, Isik et al. 2011) but lower than in radiata pine (average $h^2=0.50$, Wu et al. 2008).

4.4 Genetic correlations between traits

Generally, genetic correlations among the growth traits and among the wood quality traits are favorable, but genetic correlations between the growth and wood quality traits are unfavorable in Scots pine. The negative correlation between growth traits and wood quality traits could be genetic cause or environmental causes (Auty and Achim 2008; Louzada and Fonseca 2002; Lenz et al. 2013). Highly unfavorable genetic correlation between DBH and whole core density (-0.479), clearwood MOE (-0.506) and dynamic acoustic MOE (-0.382) was observed in this study. Such adverse genetic correlations between growth and wood quality traits were observed in a previous Scots pine study (Fries and Ericsson 2009) and in many other conifers (Wu et al. 2008).

In advanced generation tree breeding programs, tree breeders are becoming increasingly concerned with the negative genetic correlation between growth and wood quality traits (Wu and Sanchez 2011). Stiffness is usually a breeding objective trait to increase recovery rate for sawn timber, and

the negative genetic correlation between growth traits and stiffness (MOE) indicates proper economic values that should be estimated in the future (Ivković et al. 2006).

4.5 Genetic gains

Genetic gain is often used as a measure of the increase in performance after direct or indirect selection. Tree volume was one of the most important selection criteria in the Swedish Scots pine breeding program (Fries 2012). Direct selection for volume had the highest genetic gain of 14.2 %. Selection based on DBH and height also had high genetic gain (13.9 and 10.2 %, respectively for volume), but selection for volume, DBH and height generated negative genetic gain for stiffness. Similarly, selection based on stiffness and wood density traits produced negative gain for volume. The negative correlated response between growth, and wood density traits were obvious in previous studies of Scots pine (Fries 2012; Hannrup et al. 2000) and other pines and spruces (Gräns et al. 2009; Wu et al. 2008). For sawn timber of Scots pine should 4.4–4.9 % of the stiffness be lost if selection was based on DBH alone. Such negative genetic gain reinforces that multiple trait selection using optimal economic weights (Ivković et al. 2006) and optimal breeding strategies (Wu and Sanchez 2011) is recommended for the advanced Scots pine and other conifer breeding programs.

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