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On the effect of δ -doping in self-switching diodes

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Lowering the carrier concentration is presented as a way to considerably improve the performance of self-switching diode (SSD) detectors. A physics-based theoretical model was used to derive an expression for the responsivity of SSDs as a function of carrier concentration, mobility, and design parameters. Monte Carlo simulations confirmed the modeled effect of varying carrier concentration and channel width. SSDs were fabricated in InAs heterostructures with different δ -doping levels. Radio frequency (RF) characterization at 50 GHz reproduced the modeled trends. By reducing the carrier concentration in InAs SSDs with 40 nm wide channels from $2.7 \times 10^{12} \text{ cm}^{-2}$ to $1.5 \times 10^{12} \text{ cm}^{-2}$ (–44%), the noise equivalent power (NEP) improved from $130 \text{ pW/Hz}^{1/2}$ to $87 \text{ pW/Hz}^{1/2}$ (–33%). © 2014 AIP Publishing LLC. [<http://dx.doi.org/10.1063/1.4894806>]

Self-switching diodes (SSDs) are semiconductor devices where the current in nanometer-sized channels is modulated by a field-effect.¹ The nonlinear I-V relationship of the SSDs can be used for detection of millimeter-wave signals.² SSDs have been utilized in mixers,³ however mainly as direct detectors, both with^{2,4} and without bias.^{5,6} The latter option is preferred when a low $1/f$ noise⁷ is required, an important property for direct detection. Zero-bias detection at 1.5 THz has been reported with GaAs SSDs.² Previously, we demonstrated InAs SSDs with a responsivity of 34 V/W and a noise-equivalent power (NEP) of $65 \text{ pW/Hz}^{1/2}$ at 50 GHz.⁶ In this study, we have investigated the influence of the δ -doping level in InAs SSDs.

In most semiconductor devices, the doping level is a parameter that is fundamental to the device behavior. The influence of δ -doping level on the performance of SSD detectors in terms of responsivity and NEP has not been reported, neither experimentally, nor theoretically, nor in device simulations. The effect of δ -doping level in SSDs has only been studied in simulations, without experimental verification, and only with regard to I-V characteristics.^{8,9} In this study, InAs SSDs are fabricated in InAs/Al₈₀Ga₂₀Sb heterostructures with different δ -doping levels and electrically characterized. The δ -doping mainly affects the sheet carrier concentration n_s in the two-dimensional electron gas (2DEG) of the heterostructure. By modeling the SSD as a side-gated field-effect transistor (FET),¹⁰ a theoretical relationship between n_s , design and detector performance is derived. It is shown that reduction of the δ -doping and thereby n_s , is beneficial for the performance of the InAs SSD detectors, both in terms of responsivity and NEP. Monte Carlo (MC) simulations and measurements confirm the model.

The design of an SSD channel is illustrated in Fig. 1. In this study, the number of channels in parallel were $N = 43$. The channels were defined by trenches etched slightly below the two-dimensional electron gas (2DEG) of the

heterostructure.¹¹ The δ -doping level and the channel width W were the only studied design parameters. Other geometrical parameters were, as defined in Fig. 1: trench widths $W_h = W_v = 100 \text{ nm}$, channel length $L = 1000 \text{ nm}$, and channel separation $S = 350 \text{ nm}$. The 2DEG had a thickness $Z = 15 \text{ nm}$.

Fig. 1 also shows a simplified equivalent device circuit (extrinsic reactive elements were excluded) of the SSD. All electrical non-linearity in the SSD is represented by the intrinsic non-linear resistance R_i , which is modulated by the drain-connected flanges surrounding the channel.¹ Other resistances defined in Fig. 1 constitute a parasitic linear resistance $R_{s,\text{tot}} = R_{s2} + R_{sa} + R_{da}$.

The non-linearity of the SSD I-V translates directly into a detector responsivity. Considering V_D as the voltage across R_i , the intrinsic I-V curvature can be defined as $\gamma_i = (d^2 I_D / dV_D^2) / (dI_D / dV_D)$. The voltage responsivity with lossless optimum radio frequency (RF) match, β_{opt} , is then found as¹²

$$\beta_{\text{opt}} = \frac{1}{2} R_i \gamma_i \times \frac{R_i}{R_i + R_{s,\text{tot}}}. \quad (1)$$

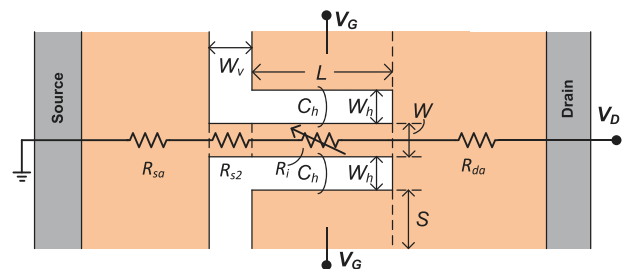


FIG. 1. Schematic top view of the geometry of one SSD channel, and an equivalent circuit. White fields depict etched trenches, reaching through the 2DEG. The fictional V_G terminals are used in the analysis of the intrinsic SSD as a side-gated field-effect transistor.

As seen from (1), a high R_i increases β_{opt} . However, power transfer from an RF source with limited impedance to an SSD detector with large R_i may become narrowband and lossy. To illustrate this trade-off, it is relevant to study the responsivity when the SSD is fed from a lower impedance, here $50\ \Omega$, which is found as $\beta_{50\Omega} = \beta_{opt}(1 - |\Gamma|^2)$, where Γ is the reflection coefficient from the source into the SSD detector.

The noise voltage across diode terminals at zero bias is the Johnson noise voltage $V_n = \sqrt{4kT(R_i + R_{s,tot})}$ where k is Boltzmann's constant and the physical temperature $T = 290\ \text{K}$, making the NEP with optimum power match

$$NEP_{opt} = \sqrt{4kT(R_i + R_{s,tot})}/\beta_{opt}. \quad (2)$$

The NEP with a $50\ \Omega$ source can be found as $NEP_{50\Omega} = \sqrt{4kT(R_i + R_{s,tot})}/\beta_{50\Omega}$. A model for how δ -doping and design affects the device performance can be derived by extending the direct current (DC) analysis of the intrinsic SSD as a double side-gated transistor.^{1,10} Referring to Fig. 1, the intrinsic SSD consists of R_i and the two flanges acting as gates with potential V_G . The gates couple to the channel with the capacitance $2C_h$ per unit channel length. It is assumed that no surface charge is present at the channel sidewalls, that the long channel approximation is valid and that the electron mobility μ_n is field-independent ($V_{D_i} \approx 0\ \text{V}$). Further, the SSD is assumed to be in depletion mode, i.e., $V_{D_i} > V_T$, where V_T is a threshold voltage. Defining V_G as the voltage of the flanges surrounding the channel, the drain current becomes¹⁰

$$I_D = NK \left[\left(\frac{qn_s W}{2C_h} + V_G \right) V_{D_i} - \frac{V_{D_i}^2}{2} \right], \quad (3)$$

where q is the elementary charge and $K = 2\mu_n C_h/L$. By setting $V_G = V_{D_i}$ and defining the threshold voltage as $V_T = -qn_s W/2C_h$, (3) transforms into

$$I_D = NK \left(\frac{V_{D_i}}{2} - V_T \right) V_{D_i}, \quad (4)$$

from which R_i can be calculated as

$$R_i = \left(\frac{dI_D}{dV_{D_i}} \right)^{-1} = \frac{1}{NK(V_{D_i} - V_T)} \quad (5)$$

and the curvature as

$$\gamma_i = \frac{d^2 I_D / dV_{D_i}^2}{dI_D / dV_{D_i}} = \frac{1}{V_{D_i} - V_T}. \quad (6)$$

Simplifying (1) by considering $R_{s,tot} \ll R_i$, the zero-bias β_{opt} is found as

$$\beta_{opt} = \frac{1}{2} R_i \gamma_i = \frac{1}{2NK(V_{D_i} - V_T)^2}. \quad (7)$$

The major observation from (2)–(7) is how n_s affects R_i , γ_i , and β_{opt} in a zero-bias ($V_{D_i} = 0\ \text{V}$) SSD with $R_{s,tot} = 0\ \Omega$. First, $R_i \propto 1/n_s$, and the same relationship holds for γ_i ,

resulting in $\beta_{opt} \propto 1/n_s^2$. Similarly, $NEP_{opt} \propto 1/n_s^{3/2}$. If the SSD is severely mismatched to the source ($R_i \gg 50\ \Omega$), $\beta_{50\Omega} \propto 1/n_s$, and $NEP_{50\Omega} \propto n_s^{3/2}$. Notably, (2)–(7) predict the same relationships for W as for n_s , assuming C_h is independent of W .

Equations (2)–(7) are consistent with design dependencies that have been observed previously: Enhancing C_h , for example, by reducing W_h , can be expected to increase γ_i and thus β_{opt} , which has been confirmed by MC simulations.¹³ It has further been reported that β_{opt} in SSDs is enhanced when W is decreased.^{5,6} The model derived above quantifies this effect.

The n_s - and W -dependence suggested by (5)–(7) was compared to MC simulations. These simulations were carried out with a two-dimensional representation of an InAs SSD.^{14–16} The SSD design used in MC simulations was with $L = 900\ \text{nm}$, $W = 35\ \text{nm}$, and $n_s = 1.5 \times 10^{10}\ \text{cm}^{-2}$. W and n_s were then varied independently. A single channel was simulated, and the resulting current was scaled to $Z = 15\ \text{nm}$ and multiplied by $N = 43$ to obtain I_D . A uniform carrier concentration of $N_D = n_s/Z$ were used. No surface charge was placed on the channel sidewalls. $R_{s,tot}$ was calculated at low V_D , and used to derive $V_{D_i} = V_D - I_D$. For every n_s and W , the I-V curve was simulated for $V_D \in [-0.15, 0.15]\ \text{V}$. By fitting a 5th order polynomial to the simulated $I_D - V_{D_i}$ relationship, the intrinsic β_{opt} at $V_D = 0\ \text{V}$ was calculated according to (7). For the modeled data, the same parameters were used as for simulations, with the addition of $\mu_n = 28\ 000\ \text{cm}^2/\text{Vs}$, as found from MC simulations.¹⁷ C_h was found as $C_h = \epsilon_0 Z/W_h$, where ϵ_0 is the permittivity of vacuum.

Fig. 2 shows β_{opt} as acquired from MC simulations and the model in (4)–(7) for different n_s . The inset demonstrates a plot of R_i and γ_i as extracted from MC simulations compared to modeled values. The model accurately predicts the variation of β_{opt} . Also R_i and γ_i are modeled accurately. The W -dependence of β_{opt} , R_i , and γ_i is presented in Fig. 3, again comparing results from MC simulations to the model. Also for W , the modeled dependencies match the simulated data. Thus, the MC simulations confirm the SSD model in (7) for the intrinsic β_{opt} .

To experimentally investigate the influence of doping, InAs/Al₈₀Ga₂₀Sb heterostructures with different δ -doping

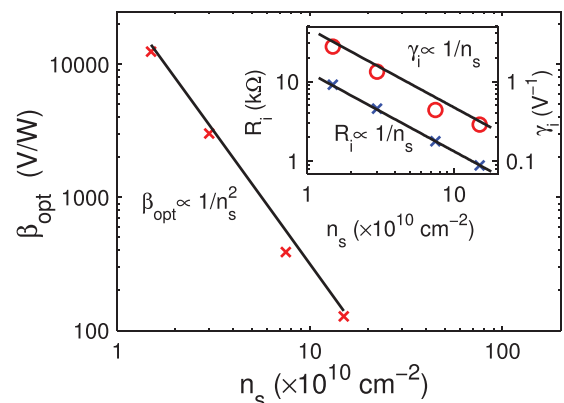


FIG. 2. Intrinsic β_{opt} as derived from Monte Carlo simulations (crosses) and the model (solid line) as a function of n_s . The inset shows simulated R_i (crosses) and γ_i (circles), and the modeled counterparts (solid lines).

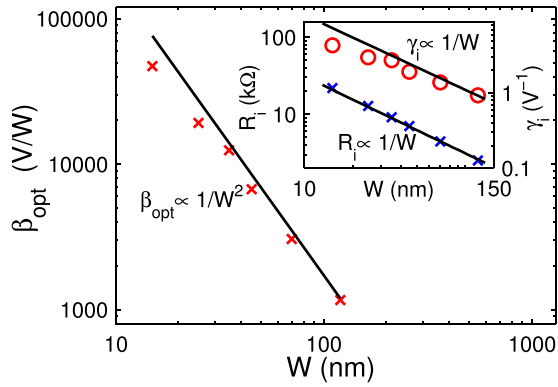


FIG. 3. Intrinsic β_{opt} as derived from Monte Carlo simulations (crosses) and the model (solid line) as a function of W . The inset shows simulated R_i (crosses) and γ_i (circles), and the modeled counterparts (solid lines).

were grown by molecular beam epitaxy.⁶ Similar structures have been used in InAs/AlSb high-electron-mobility transistors.¹⁸ An AlSb metamorphic buffer was grown on a GaAs substrate. On top of the buffer, a 15 nm thick InAs/Al₈₀Ga₂₀Sb quantum well was formed. The doping was placed in the Al₈₀Ga₂₀Sb barrier, 50 Å above the InAs channel. To allow formation of low-resistivity ohmic contacts in subsequent device processing, a highly doped InAs cap layer was grown on top of the structure. In the active area, i.e., the area of the trenches, the cap layer was etched away. After the trench etch, the devices were passivated with silicon nitride using plasma enhanced chemical vapor deposition carried out at room temperature. Details in the fabrication process have been given elsewhere.¹¹

Two samples with different δ -doping were used in SSD fabrication, one low-doped (i.e., non-intentionally doped, $\delta = 0 \text{ cm}^{-2}$) and one high-doped ($\delta = 1 \times 10^{12} \text{ cm}^{-2}$). Hall measurements are shown in Table I, both for unprocessed samples and samples where the cap was etched and the surface passivated (similar to the active area of the SSDs). The etched Hall structure was processed on the same chip used in SSD fabrication. The low-doped sample showed a significant n_s , in line with what have been reported for similar structures.¹⁹ n_s was higher in the etched than in the as-grown structures, especially in the low-doped sample where n_s went from 0.61×10^{12} to $1.5 \times 10^{12} \text{ cm}^{-2}$. As expected, the low-doped sample showed a higher μ_n than the high-doped sample.²⁰

In Figs. 4–6, RF measurements of the InAs SSD detectors are compared to modeled counterparts. Zero-bias RF measurements of β_{opt} were performed on-wafer at 50 GHz.⁶ NEP_{opt} and $NEP_{50\Omega}$ was found from (2) using DC measurements of $R_i + R_{s,\text{tot}}$.⁶ The measurements on the low-doped

TABLE I. Sheet resistance (R_{sh}), carrier concentration (n_s), and mobility (μ_n) from Hall measurements for the low- and high-doped samples used for InAs SSD fabrication.

δ -doping		R_{sh} (Ω/sq)	n_s ($\times 10^{12} \text{ cm}^{-2}$)	μ_n ($\text{cm}^2/\text{V s}$)
0 cm^{-2}	As-grown	435	0.61	23 400
	Etched and passivated	164	1.5	26 000
$1 \times 10^{12} \text{ cm}^{-2}$	As-grown	156	2.2	18 300
	Etched and passivated	136	2.7	17 000

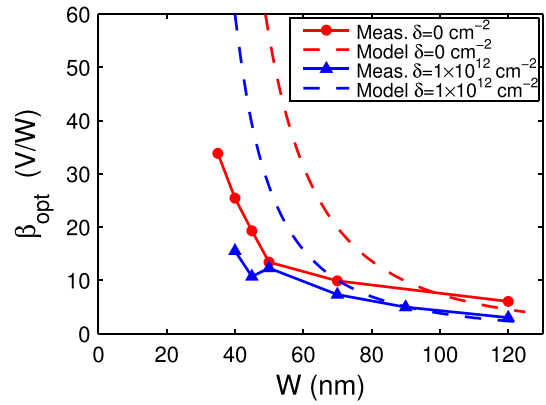


FIG. 4. Measured β_{opt} in low-doped and high-doped samples compared to modeled values.

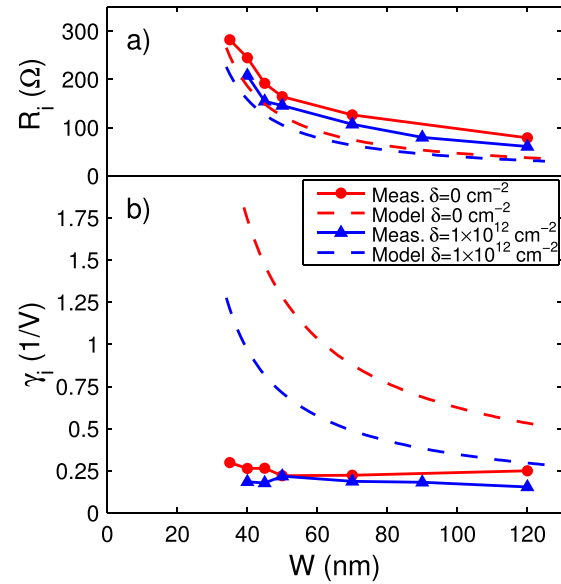


FIG. 5. (a) Measured R_i and (b) γ_i in the low-doped and high-doped samples compared to modeled counterparts.

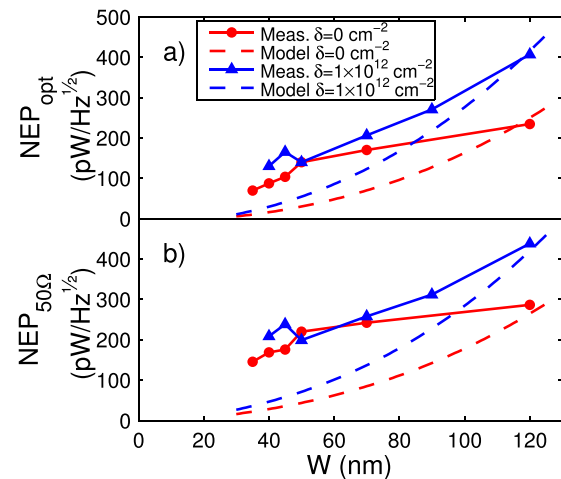


FIG. 6. (a) Estimated NEP_{opt} and (b) $NEP_{50\Omega}$ at 50 GHz for the low-doped and high-doped samples compared to modeled counterparts.

sample has been published partly elsewhere.⁶ Modeled values were derived from (1)–(6) using measured μ_n and n_s , with the following considerations: $R_{s,\text{tot}}$ was found by

recognizing that $R_{s2} = R_i W_v / L$. Further, $R_{sa} + R_{da}$ was measured to 40Ω and 27Ω for the low- and high-doped samples, respectively, in structures without trenches (ignoring possible current-crowding effects at channel entrances). $2C_h$ was calculated from the capacitance to ground in a coplanar transmission line with the dimensions W , W_h , and L and the relative dielectric constant of AlSb $\epsilon_{AlSb} = 10.9$.^{21,22} The only adjustment of the model to measurements was that W was replaced with an efficient channel width $W_{eff} = W - 20 \text{ nm}$ to reproduce the measured W -dependence of R_i .⁵ Consequently, W_h was replaced with an efficient trench width $W_{h,eff} = W_h + 20 \text{ nm}$.

In Fig. 4, β_{opt} versus W for the two samples is presented. As has been reported previously,^{5,6} reducing W increases β_{opt} . More importantly, Fig. 4 shows that the low-doped sample demonstrates a higher β_{opt} than the high-doped samples. For $W = 40 \text{ nm}$, the smallest W for which SSDs from both samples are available, the measurements exhibit a factor of $1.6 \times$ difference in β_{opt} between the low- and high-doped sample, while the model predicts a factor of $2 \times$ difference. The model also overestimates β_{opt} for small W . However, the model captures the relative dependencies well for both n_s and W .

To further analyze how β_{opt} is affected by n_s , R_i , and γ_i are plotted in Fig. 5. R_i was derived from DC measurements and γ_i from β_{opt} using (1). R_i is fairly similar in both samples. The low-doped sample shows a slightly higher R_i than the high-doped sample. The same trend was seen for R_{sh} in Table I, where R_{sh} was similar for all etched samples. From (5), $R_i \propto 1/\mu_n n_s$ is expected. While n_s is lower in the low-doped sample, μ_n is higher, making R_{sh} and thus also R_i similar in both samples. The model which uses measured n_s and μ_n reproduces R_i fairly accurately.

While both samples exhibit similar R_i , the low-doped sample shows a significantly higher γ_i . This is explained by (6), where $\gamma_i \propto 1/n_s$, and independent of variations in μ_n . Thus, a larger difference in γ_i than R_i between samples could be expected. From the model and measured n_s , a factor $1.8 \times$ greater γ_i could be expected in the low-doped sample than in the high-doped sample, for all W . In Fig. 5(b), for $W = 40 \text{ nm}$, the difference in γ_i is a factor $1.4 \times$, in good agreement with the model. The model shows considerably stronger W -dependence of γ_i than measurements, and overestimates γ_i which led to also β_{opt} being overestimated for small W in Fig. 4. Measurements exhibit the predicted trend qualitatively: InAs SSDs from the low- and high-doped samples with $W = 35 \text{ nm}$ and $W = 40 \text{ nm}$, respectively, showed 20% higher γ_i compared to devices with $W = 120 \text{ nm}$.

Fig. 6 demonstrates the effect on NEP_{opt} and $NEP_{50\Omega}$ for varying δ -doping. As has been shown elsewhere,⁶ NEP_{opt} and $NEP_{50\Omega}$ decrease when reducing W . Further, the low-doped sample exhibited both a lower NEP_{opt} and $NEP_{50\Omega}$ than the high-doped sample. The model underestimates both NEP_{opt} and $NEP_{50\Omega}$ for small W due to the overestimated β_{opt} . However, the difference in NEP related to δ -doping is well described by the model, which predicts a 46% lower NEP_{opt} in the low-doped sample than in the high-doped sample. Comparing the low- and high-doped sample for $W = 40 \text{ nm}$, the former shows an NEP_{opt} reduced with 33% ($130 \text{ pW/Hz}^{1/2}$ and $87 \text{ pW/Hz}^{1/2}$, respectively) whereas the model predicts a 46% reduction.

It was found from measurements of fabricated devices, model and MC simulations that lowering the δ -doping is beneficial for SSD direct detector performance with respect to responsivity and NEP. Reducing n_s increases γ_i , but also R_i , provided μ_n is constant. High R_i requires a more complex matching network and as shown in (2), R_i contributes to noise, while γ_i does not. Increasing γ_i will therefore always improve both responsivity and NEP.

Published SSDs have shown $\beta_{50\Omega} < 200 \text{ V/W}$.^{2,4-6} Since $\beta_{50\Omega} = 100\gamma_i$ for $R_i \gg 50 \Omega$, all published SSDs have $\gamma_i < 2 \text{ V}^{-1}$. Zero-biased Schottky diodes reaches γ_i close to their theoretical limit of 39.6 V^{-1} .⁷ There is thus a large potential in increasing γ_i in SSDs. As shown in Figs. 2–6, lowering the δ -doping and thus n_s is a powerful way to enhance γ_i .

We have studied how the level of δ -doping in the InAs/Al₈₀Ga₂₀Sb heterostructure affects the SSD direct detector performance. By treating the SSD as a double side-gated transistor, responsivity and NEP of the detector could be expressed as a function of design and material parameters μ_n and n_s . The voltage responsivity with an optimal power match was theoretically found to be proportional to $1/n_s^2$. A similar relationship was found for the channel width. Monte Carlo simulations of InAs SSDs confirmed the model. When comparing to measurements of fabricated devices, the model reproduced the main features of both β_{opt} , NEP_{opt} and $NEP_{50\Omega}$. The n_s -dependence showed good agreement between model and measurements. By a combination of theory, simulations, and measurements, it was shown that lowering the δ -doping improves the performance of SSD direct detectors.

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