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# Experimental and modelling studies of the shape memory properties of amorphous polymer network composites

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**Abstract.** Shape memory polymer composites (SMPCs) have become an important leverage to improve the development of shape memory polymers (SMPs) applications. An amorphous SMP matrix has been filled with different types of reinforcements in this study. An experimental set of results is presented and then compared to 3D finite element simulations. Thermomechanical shape memory cycles were performed in uniaxial tension. The fillers effect was studied in stress-free and constrained-strain recoveries. Experimental observations indicate complete shape recovery and put in evidence the increased sensitivity of constrained length stress recoveries to the heating ramp on the tested composites. The simulations reproduced a simplified periodic reinforced composite and use a model for the matrix material that has been previously tested on regular SMPs. The latter combines viscoelasticity at finite strain and time-temperature superposition. The simulations permit to represent the recovery properties of a reinforced SMP easily.

## 1. Introduction

For the past decade, shape memory polymers (SMPs) have drawn significant attention due to their ability to store a temporary shape and to recover a permanent shape under external stimuli. These materials have shown to be attractive due to their low weight, low processing cost, high deformability and the easy tailoring of the shape transition temperature. In order to broaden their potential applications, SMPs have been reinforced to enable athermal shape recovery stimuli and to increase their mechanical properties. The literature presents shape memory polymer composites (SMPCs) reinforced by fibres (Ohki et al. 2004, Lan et al. 2009, Ivens et al. 2011, Cuevas et al. 2012), carbon nanotubes (Miaudet et al. 2007, Lu et al. 2010, Ding et al. 2013, Li et al. 2013), nanoclay particles (Cao and Jana 2007), silicium carbide nanoparticles (Gall et al. 2002, Liu et al. 2004), fabrics (Zhang and Ni 2007, Ivens et al. 2011), etc. One may find more references in reviews on stimulus methods and applications for SMPCs (Leng et al. 2011, Meng and Li 2013, Liu et al. 2014).

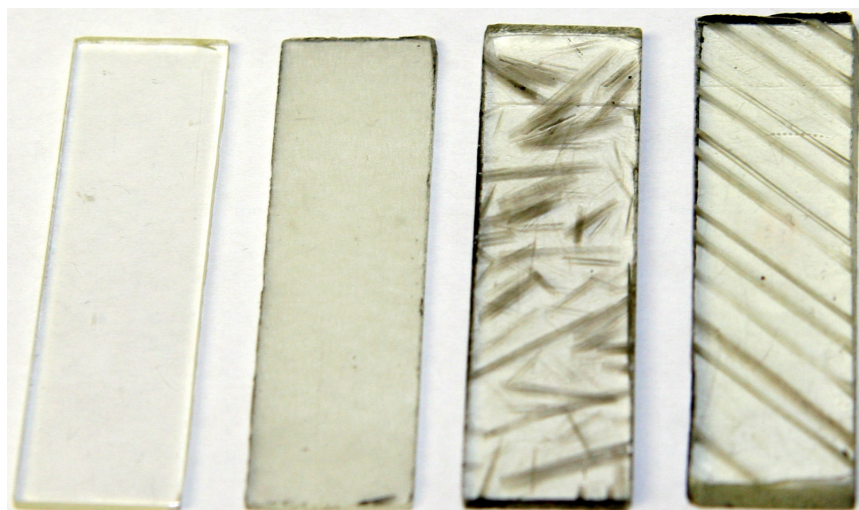
Several studies have focused on the development of athermal recovery stimuli (for instance Razzaq et al. 2007, Lu et al., 2010, Kumar et al. 2012, Leng et al. 2009), other studies have tested the shape recovery ability of SMPCs, in a qualitative way (Zhang and Ni 2007, Lan et al. 2009, Lu et al. 2010 among others) or a in quantitative one (Liu et al. 2004, Cao and Jana 2007, Miaudet et al. 2007, Ivens et al. 2011, Cuevas et al. 2012, Li et al. 2013). Few works report on stress recovery during strain-constrained heating (Gall et al. 2002, Fejos et al. 2012, Li et al. 2013), which may be of interest for actuator applications or for strain-constrained stress recovery applications. Albeit it would be interesting to be able to predict the recovery properties of SMPCs from the properties of the SMP matrix, few studies have compared the recovery kinetics of SMPCs to the recovery kinetics of their plain SMP matrices. Last, only Alexander et al. (2014) have proposed a model to estimate SMPC recovery properties from the recovery properties of the polymer matrix. The model consists of a 2D finite element representation of a periodic cell containing the cross-section of an infinite cylinder embedded in the thermo-viscoelastic polymer matrix. Their model presents interesting features but unfortunately it has not been compared to actual experimental data.

The current study aims at testing and modelling the kinetics of the strain and stress recoveries of an amorphous acrylate network reinforced by various types of fillers. The plain acrylate and the composites were prepared in our lab. Fillers include micrometric glass bead, short and long glass fibres. Materials were submitted to stress-free strain recovery and strain-constrained stress recovery thermomechanical cycles in uniaxial tension. A relatively complete set of experimental data is reported, providing a better understanding of the effect of fillers on the behavior and the thermal kinetics of recovery of the SMPCs. Based on satisfactory modelling of the shape memory properties of the acrylate network reported by Arrieta et al. (2014a), finite element simulations of the glass bead reinforced acrylate were run in order to explore the interest of such simulations for predictive purpose in design applications. The composite is defined by a 3D periodic cell containing a spherical rigid bead surrounded by the viscoelastic acrylate satisfying to the time-temperature superposition property.

## **2. Materials and experiments**

### *2.1. Materials*

The amorphous acrylate network was obtained by photopolymerization of benzyl methacrylate (BMA) added with 550 g/mol molar weight poly(ethylene glycol) dimethacrylate (PEGDMA) and 0.5% of 2-dimethoxy-2-phenylacetophenone (DMPA) used as photoinitiator following the protocol described in Safransky and Gall (2008). The composition was set to 90% moles of BMA and 10% moles of PEGDMA. The plain amorphous polymer network presents a glass transition at 46°C when measured by DSC with a 10°C/min heating ramp. Fillers were added to the polymer mix before the UV thermo activated polymerization (50 minutes in a UVP CL-100 oven). Three different



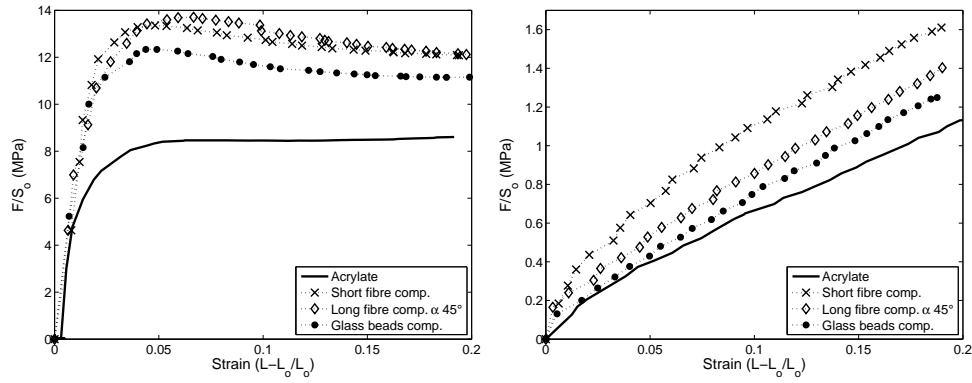
**Figure 1.** Material samples, from left to right: plain amorphous acrylate network, acrylate reinforced by glass bead, short glass fibres, and long glass fibres at 45°.

types of fillers were selected: polydisperse hollow glass bead of 55  $\mu\text{m}$  average diameter (Glasscell 25 from Sicomin), short glass fibres and continuous long glass fibres disposed at 45°. The various composites contain a mass fraction of  $\sim 2\%$  of glass bead,  $\sim 5\%$  of short glass fibres and  $\sim 2\%$  of continuous glass fibres respectively. Final products are rectangular plates of 1.3 to 2.1 mm thickness, which are then cut in rectangular samples for mechanical tests and analysis (figure 1).

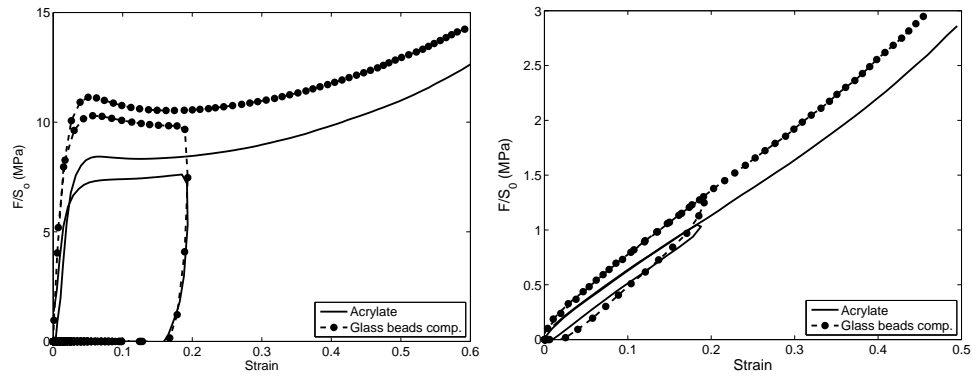
## 2.2. Mechanical characterization

**2.2.1. Uniaxial tension tests** Uniaxial tension tests were performed in order to characterize the material stress-strain properties at various temperatures, to evaluate the filler reinforcement, and to estimate possible damage during loading. Tests were performed on an Instron 5881 testing machine equipped with a thermal chamber and local strain video extensometry. Crosshead speed was set to 10 mm/min for all tests. Tests were run at 45°C, which corresponds to a temperature within the glass transition, and at 65°C (above the glass transition). At 45°C the material should present high viscoelasticity while at 65°C the material is in the rubbery state and should present low viscoelasticity. Figure 2 presents the uniaxial stress-strain responses of the materials at 45°C and 65°C. One notices the filler reinforcement at both temperatures.

Cyclic tests were run to detect possible damage during stretching. For this purpose, the materials were stretched up to 20%, then unloaded and allowed recovering completely from the first stretch before reloading until break. The fibre glass composites were unable to stand a second loading phase, breaking systematically during the reloading step, evidencing serious damage at first stretch. To the contrary, the glass bead composite presented no appreciable damage as the initial modulus remained unchanged during the second loading (figure 3). It is to be noted that complete strain recoveries were obtained



**Figure 2.** Uniaxial tension stress–strain responses measured at 45°C and at 65°C.

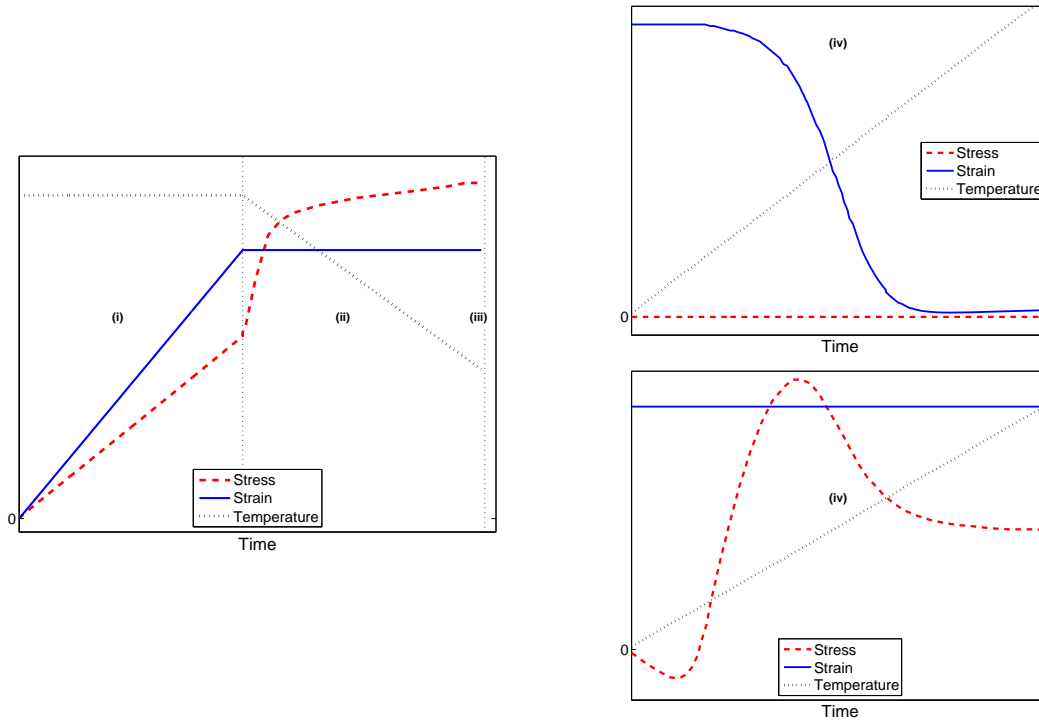


**Figure 3.** Load–unload–reload test for the glass bead composite and the plain acrylate at 45°C (left) and at 65°C (right).

at 45°C and 65°C but within very different durations, since two hours were needed for full recovery at 45°C when instantaneous recovery was observed at 65°C. This feature is a signature of the temperature dependence of the polymer viscoelasticity.

### 2.3. Shape recovery tests

Free and constrained length recovery tests were performed in uniaxial tension, using an Instron 5881 machine. Shape recovery tests consist in: (i) applying 20% strain in uniaxial tension at 45°C, (ii) maintaining the strain while cooling down the samples to room temperature, (iii) releasing stress to zero, and (iv) heating at a constant temperature rate of 1°C/min or 5°C/min in free or constrained length conditions. A graphic representation of the tests is shown in figure 4. It may be observed that stress–free length recovery and constrained–length stress recovery differ only at the last step, where either the strain is recorded in stress-free conditions or the stress is recorded in constrained–length conditions with respect to temperature. The temperature was measured accurately with a thermocouple placed close to the samples. The temperature of 45°C was chosen to apply strain since, the acrylate exhibits full strain recovery and high stress recovery at such a temperature (Arrieta et al. 2014b).



**Figure 4.** Thermomechanical recovery tests. Left: (i) uniaxial pre-stretching, (ii) cooling down to room temperature at constant strain, (iii) stress release. Right: (iv) stress-free length recovery (above) or constrained-length stress recovery (below), while heating the sample.

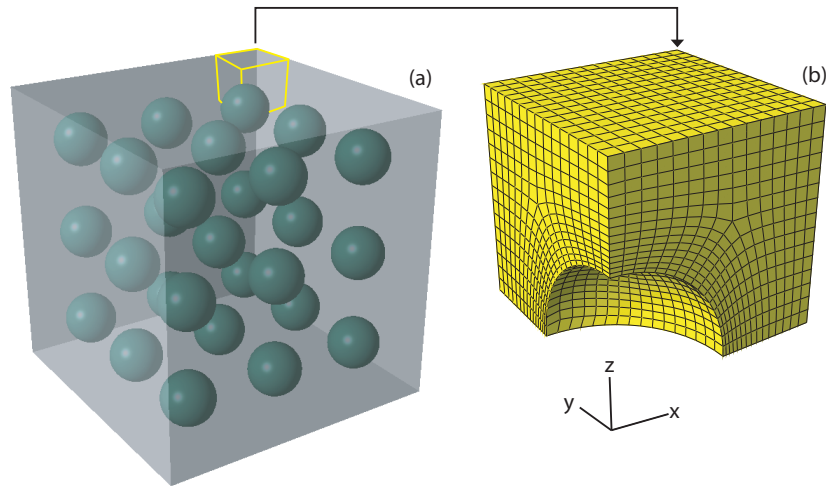
### 3. Modelling

#### 3.1. Thermomechanical behaviour of amorphous networks

The shape memory property of amorphous polymer networks is due to the material viscoelasticity and to its time-temperature superposition property (Diani et al. 2012). The free-length strain recovery and the constrained-length stress recovery exhibited by the acrylate network have been successfully modelled (Arrieta et al. 2014a) by constitutive equations combining the finite strain viscoelastic model of Simo (1987), for which the relaxation times and the associated moduli of the generalized Maxwell viscoelastic model are extracted from standard small strain dynamic mechanical analysis tests, and by the WLF (Williams et al. 1955) equation to describe the time-temperature superposition. The acrylate network model parameters are reported in (Arrieta et al. 2014a). Since the constitutive equations were implemented in Abaqus (Abaqus/Standard 2010), a large spectrum of loading conditions and thermal histories were easily tested and confronted to experimental data.

#### 3.2. Finite element simulations

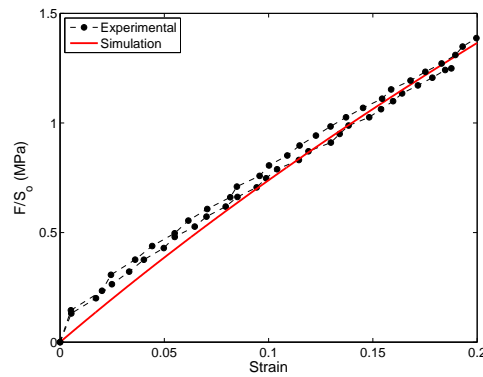
The glass bead reinforced acrylate is modelled as an infinite periodic medium, with a cubic lattice of glass bead, as illustrated in figure 5a. Due to periodicity and to the



**Figure 5.** (a) Partial view of the infinite periodic medium used to represent the glass bead reinforced acrylate. (b) Meshed volume used in the simulations where uniaxial tension is applied along the  $z$  axis.

symmetry of the elementary cubic cell (where a bead is located at the center), a sufficient volume to study when uniaxial tension is applied parallel to a lattice axis is one eighth of the cubic cell. The 3D finite element mesh used for the matrix part is shown in figure 5b (4463 hexahedric C3D8H elements). The volume fraction of beads was chosen to 8% in order to well reproduce the observed experimental reinforcement (figure 6). Perfect adhesion between the glass bead and the matrix has been assumed. This assumption was motivated by the observed absence of damage noticed during experimental cyclic tests. Note that assuming poor adhesion at the matrix–bead interface almost cancels the reinforcement effect, therefore this assumption has been discarded. Consequently, keeping the nodes located on the spherical cap in figure 5b fixed is sufficient to model perfect adhesion to a rigid bead, and this is why no bead is shown in figure 5b. Standard symmetry boundary conditions are applied on the bottom, left, and front faces of the mesh. A uniform vertical displacement is prescribed to the nodes of the upper face, letting their  $x$  and  $y$  displacements free, in order to apply uniaxial tension. The right and back faces of the mesh are free to translate along the  $x$  and  $y$  axes, respectively, to model the lateral free surfaces of the specimen. Their nodes are left free to move in the plane of the face they belong to, which ensures periodicity. For simulations of the free–length and constrained–length recovery tests, every step from (i) to (iv) is simulated in order to correctly account for the whole loading history. Temperature is uniform over the whole mesh and the same history is applied as measured in the experiments.





**Figure 6.** Comparison between the stress-strain behaviours at 65°C of the finite element simulation using representation Figure 5 and of the actual glass bead reinforced acrylate.

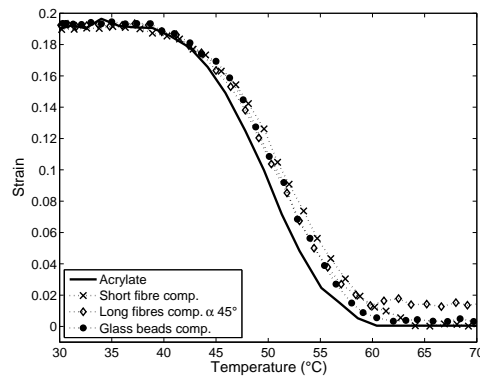
## 4. Results and discussion

### 4.1. Experimental recovery tests

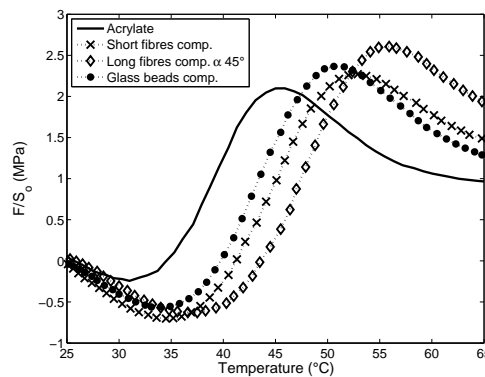
*4.1.1. Free and constrained length recovery of SMP composites: first results* In this section, the plain acrylate and the SMPCs are submitted to the storage of 20% uniaxial strain applied at 45°C. The free-length and constrained-length recoveries are recorded while heating the samples at 5°C/min from room temperature to 65°C. For free-length recovery tests, SMPCs and the plain acrylate showed full recovery. The recovery kinetics were similar, but with a slight shift toward higher temperatures for SMPCs (figure 7). Full strain or shape recovery for SMPCs has been reported already (Ivens et al. 2011, Fejos et al. 2012), and Liu et al. (2004) whose results show similar kinetics when comparing the free recoveries of a SiC reinforced epoxy and plain epoxy heated at 5°C/min. Therefore, knowing the recovery property of the polymer matrix may be enough to predict the shape recovery of the SMPCs, since it is likely to be close.

Figure 8 presents the stress vs. temperature history recorded during constrained-length stress recovery tests. One notices that experimental results vary according to the material. The four materials exhibit the same curve shapes, but the curves are shifted significantly toward higher temperatures when fillers are added. Like Fejos et al. (2011) and Gall et al. (2002), one also observes an increase in the stress overshoot for reinforced polymers. Therefore, reinforcing SMPs may have a favorable impact for actuator applications, since it renders the material capable of generating larger forces. Figure 8 displays another interesting feature that has not been reported in the literature yet: the maximum compressive stress may be increased when adding fillers.

The change of recovery kinetics displayed by composites in figure 8 has not been observed by Gall et al. (2002). In order to better understand this result, further tests were run lowering the heating rate to 1°C/min or adding a step of stress relaxation at 45°C after stretching the material. These test conditions were applied to the plain acrylate and to the glass bead reinforced acrylate only, since the experimental results



**Figure 7.** Stress-free length recovery comparison for samples pre-stretched 20% at 45°C heated at 5°C/min.

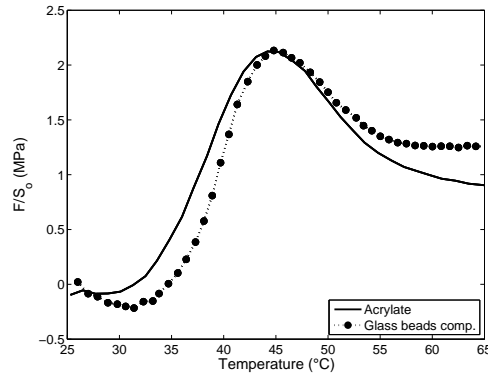


**Figure 8.** Constrained-length stress recovery comparison for samples pre-stretched 20% at 45°C and heated at 5°C/min.

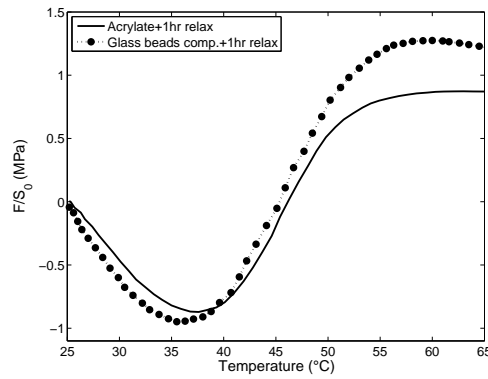
obtained for these materials could be compared to the finite element simulations.

*4.1.2. Glass bead reinforced SMP: additional results* Figure 9 shows the comparison of the stress recovery measured on the plain acrylate and on the glass bead SMPC while heating the samples at 1°C/min. Contrary to previous results obtained at 5°C/min and plotted in figure 8, the stress recoveries exhibited by both materials are very similar but to the higher stress exhibited by the SMPC at high temperatures. This result is in good accordance with Gall et al. (2002). In general, an increase of the stress overshoot and the shift of the recovery curve toward higher temperatures have been observed for SMPs when the temperature heating rate is increased (Qi et al. 2008, Castro et al. 2010). This effect seems to be strengthened for the glass bead composite, where the recovery curve is even more shifted to higher temperatures and both the compression and tensile peaks are enhanced.

Finally, both materials were submitted to stress relaxation at fixed length during one hour at 45°C after stretching. Then, they were submitted to the same thermomechanical history, cooled down to room temperature at constant length, stress released, and constrained-length heating at 5°C/min. Stress recoveries with respect to



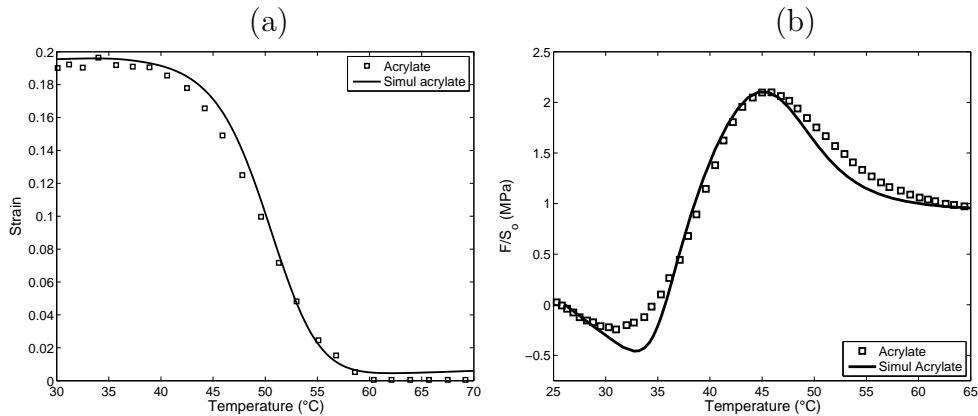
**Figure 9.** Constrained-length stress recovery comparison of the plain material and glass bead filled material pre-stretched 20% at 45°C and heated at 1°C/min.



**Figure 10.** Constrained-length stress recovery for plain material and glass bead filled material after one hour of stress relaxation at fixed length at 45°C for samples pre-stretched at 45°C and heated at 5°C/min.

temperature are plotted in figure 10. The comparison of figure 8 and figure 10 shows the effects of a stress relaxation at high temperature on the stress recovery: a loss of stress overshoot, a larger compressive stress, and a shift of the recovery toward higher temperatures. Such effects have already been reported for plain SMPs (Nguyen et al. 2008, Castro et al. 2010, Arrieta et al. 2014b). Figure 10 extends them to SMPCs. Finally, stress relaxation at high temperature leads to similar stress recovery kinetics for SMPC and plain SMP. As a conclusion for the experimental data reported in the current study, one notices that:

- It is possible to reinforce SMP with various kinds of fillers and to keep their memory property,
- The shape recovery kinetics of reinforced SMPCs is very similar to the shape recovery of their SMP matrix material,
- The stress recovery exhibited by SMPCs may differ from the SMP matrix material according to the thermomechanical conditions,
- Slow heating and stress relaxation at high temperature after applying the temporary shape are in favor of obtaining the same recovery kinetics for SMPC and SMP.



**Figure 11.** Comparison between model and experiments for plain acrylate pre-stretched 20% at 45°C and recovered in (a) stress-free length conditions at 5°C/min, and (b) constrained-length conditions at 5°C/min.

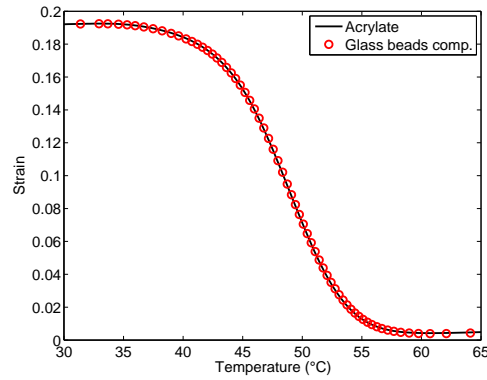
## 4.2. Simulations

**4.2.1. Plain acrylate** Figure 11 compares the model predictions and the experimental thermal recoveries for the plain acrylate network when heated at 5°C/min. Good agreements between the model and the experiments are displayed. More results in Arrieta et al (2014a) assessed the prediction ability of the model for thermal recovery properties. Nonetheless, simulations and experiments have shown that constrained-length stress recoveries are more sensitive to the thermal history, and therefore are more difficult to model accurately than stress-free length recoveries.

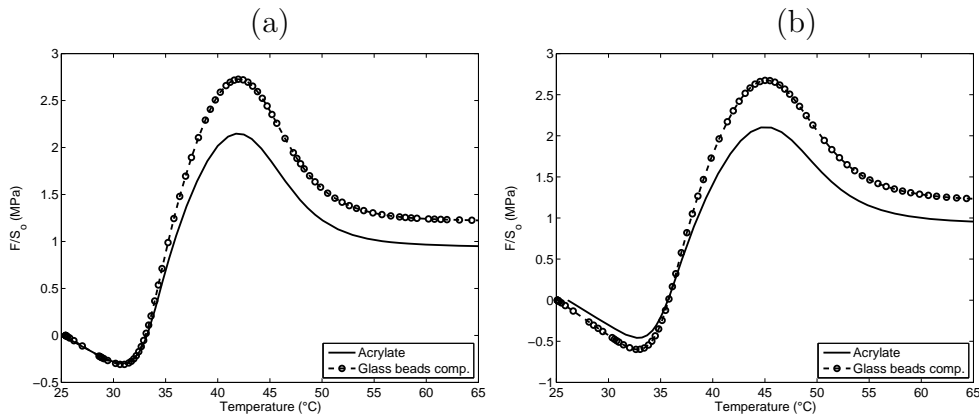
**4.2.2. Glass bead filled acrylate** In order to study the results provided by the modelled SMPC, its recovery properties are compared to those of the modelled plain SMP. Figure 12 presents the theoretical stress-free length thermal recoveries of the SMP and the SMPC when heated at 5°C/min. One notes that both recoveries superimpose perfectly. Therefore, finite element simulations with perfect adhesion of reinforced polymer will predict identical stress-free shape recoveries for the SMP and the SMPC. Analogous results were obtained by Alexander et al. (2013) when comparing theoretical stress-free strain recoveries obtained by 2D finite element simulations.

Figure 13 compares the simulations of constrained-length stress recoveries at 1°C/min and 5°C/min. At 1°C/min, when comparing figure 9 and figure 13(a), it is to be noted that simulations are capable of reproducing the recovery kinetics observed experimentally, but to the fact that simulations predict a larger stress overshoot. This contrasts with the 5°C/min heating ramp (figure 13(b) and figure 8), where the stress peak is well reproduced, with no shift to higher temperatures though.

Therefore, simulations were unable to represent the experimental results showed in figure 8, which may be due to the too simple assumptions of a monodisperse and periodic distribution of fillers.



**Figure 12.** Stress-free length recovery simulations for the plain acrylate and glass bead filled composite for 20% pre-stretching at 45°C and recovered at 1°C/min.



**Figure 13.** Constrained-length stress recovery simulations for samples pre-stretched 20% at 45°C and heated at (a) 1°C/min and at (b) 5°C/min.

## 5. Conclusions

Recently, SMPs have been reinforced into SMPCs in order to circumvent some of their drawbacks, and to extend the development of these smart materials to new devices and applications. Reinforcements may produce stiffer and tougher materials in service and may also generate larger forces for actuator applications. In order to better characterize the effect of adding fillers on the recovery properties of SMPs, SMPCs were fabricated and tested in lab. It was shown that SMPCs can show excellent strain recovery properties. Moreover, the kinetics of stress-free length recovery displayed by the SMPCs is very similar to the recovery kinetics of their matrix material. Therefore, knowing the shape recovery properties of the polymer matrix allows predicting the shape recovery property of the SMPCs directly.

In SMPs, constrained-length stress recoveries have been known to be more sensitive to the thermal and loading histories, than stress-free recoveries. Experimental results show that this recovery feature is enhanced in SMPCs. The latter display a significant dependence of the constrained-length stress recovery with respect to the heating ramp.

Nevertheless, it was shown that an SMPC and its polymer matrix material could show similar kinetics of stress recoveries when the parameters of the thermomechanical cycle were carefully chosen.

SMPCs are good candidates for finite element modelling. Based on the representation of the polymer matrix behaviour by viscoelastic finite strain constitutive equations combined with time-temperature superposition, and on the representation of the composite microstructure by a 3D periodic cell, the recovery properties of the glass bead reinforced SMPCs were simulated. It was observed that such a modelling leads to similar recovery properties for the SMPC and the SMP matrix for any thermomechanical loading conditions, which shows the limit of such a modelling.

## Acknowledgment

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