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► **To cite this version:**

Mohamed Benbouzid, Brice Beltran, Yassine Amirat, Gang Yao, Jingang Han, et al.. Second-Order Sliding Mode Control for DFIG-Based Wind Turbines Fault Ride-Through Capability Enhancement. ISA Transactions, 2014, 53 (3), pp.827-833. hal-01020027

HAL Id: hal-01020027

<https://hal.science/hal-01020027v1>

Submitted on 7 Jul 2014

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Second-Order Sliding Mode Control for DFIG-Based Wind Turbines Fault Ride-Through Capability Enhancement

Mohamed Benbouzid, Brice Beltran, Yassine Amirat, Gang Yao, Jingang Han and Hervé Mangel

Abstract—This paper deals with the fault ride-through capability assessment of a doubly-fed induction generator-based wind turbine using a high-order sliding mode control. Indeed, it has been recently suggested that sliding mode control is a solution of choice to the fault ride-through problem. In this context, this paper proposes a second-order sliding mode as an improved solution that handle the classical sliding mode chattering problem. Indeed, the main and attractive features of high-order sliding modes are robustness against external disturbances, the grids faults in particular, and chattering-free behavior (no extra mechanical stress on the wind turbine drive train).

Simulations using the NREL FAST code on a 1.5-MW wind turbine are carried-out to evaluate ride-through performance of the proposed high-order sliding mode control strategy in case of grid frequency variations and unbalanced voltage sags.

Index Terms—Wind turbine, doubly-fed induction generator, fault-ride through, second-order sliding mode.

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Nomenclature

WT	=	Wind Turbine;
DFIG	=	Doubly-Fed Induction Generator;
FRT	=	Fault Ride-Through;
LVRT	=	Low-Voltage Ride-Through;
HOSM	=	High-Order Sliding Mode;
SOSM	=	Second-Order Sliding Mode;
MPPT	=	Maximum Power Point Tracking;
v	=	Wind speed (m/sec);
ρ	=	Air density (kg/m^3);
R	=	Rotor radius (m);
P_a	=	Aerodynamic power (W);
T_a	=	Aerodynamic torque (Nm);
λ	=	Tip speed ratio;
$C_p(\lambda)$	=	Power coefficient;
ω	=	Wind turbine rotor speed (rad/sec);
T_g	=	Generator electromagnetic torque (Nm);
J	=	Turbine total inertia (kg m^2);
K	=	Turbine total external damping (Nm/rad sec);
d, q	=	Synchronous reference frame index;
$s, (r)$	=	Stator (rotor) index;
$V(I)$	=	Voltage (Current);
$P(Q)$	=	Active (Reactive) power;
ϕ	=	Flux;
T_{em}	=	Electromagnetic torque;
R	=	Resistance;
$L(M)$	=	Inductance (Mutual inductance);
σ	=	Leakage coefficient, $\sigma = 1 - M^2/L_s L_r$;
θ_r	=	Rotor position;
$\omega_r (\omega_s)$	=	Angular speed (Synchronous speed);
s	=	Slip;
p	=	Pole pair number.

1. Introduction

An increasing number of power system operators have implemented technical standards known as *grid codes* that wind turbines must meet when connecting to the grid [1-2]. Generally, these grid codes requirements cover many topics such as, voltage operating range, power factor regulation, frequency operating range, grid support capability, and low fault ride-through capability. Indeed, grid codes dictate FRT requirements. LVRT capability is considered to be the biggest challenge in wind turbines design and manufacturing technology [3]. LVRT requires wind turbines to remain connected to the grid in presence of grid voltage sags.

The DFIG is one of the most frequently deployed large grid-connected wind turbines. Indeed, when compared with the full-scale power converter WT concept, the DFIG offers some advantages, such as reduced inverter and output filter costs due to low rotor- and grid-side power conversion ratings (25%–30%) [4]. However, DFIG-based WTs are very sensitive to grid disturbances, especially to voltage dips [5].

In this context, this paper proposes to address the FRT problems using a so-called active method achieving FRT with no additional devices. The goal is to control rotor voltages and currents, to reduce the rotor overvoltages and/or overcurrents, and therefore avoid the crowbar use/activation in order to keep full DFIG control at all times to meet the FRT requirements. The implementation of classical flux-oriented vector control techniques (PI controllers) has been proven to work well for the accomplishment of the initial grid code requirements [6-9]. But, this kind of control could be easily saturated when dealing with substantial sag. Moreover, it is sensitive to the generator parameters and other phenomena such as disturbances and unmodeled dynamics [10-11]. In particular, [10] gives a critical review of control methods for LVRT compliance with DFIG. This state-of-the-art review suggests the need of robust and nonlinear controller. A robust one have been proposed in [12], claiming full control in all LVRT cases. However, this was achieved with an oversized converter to accommodate rotor overvoltages and full rotor current control. It is therefore suggested that sliding mode control is a solution of choice to the FRT problem [13].

Therefore and in this particular context, this paper proposes the use of high-order sliding mode control as an improved solution that handles the classical sliding mode chattering problem and particularly avoids using additional devices and converter oversizing. Indeed, the main and attractive features of HOSMs are robustness against external disturbances (grid faults) and chattering-free behavior (no extra mechanical stress on the drive train) [14-16]. The proposed control strategy combines an MPPT using a second-order sliding mode for the DFIG control [17-18]. The proposed work is based on [17-18] philosophy (high-order sliding mode). In the case of [18], the control is on the turbine with a specific controller. In the case of [17],

the control is on the DFIG as in this paper. However, this paper contribution is on the design of the second-order sliding mode controller based on the supertwisting algorithm that takes into account grid disturbances, in addition to the optimal power extraction [19]. This strategy presents attractive features such as chattering-free behavior, finite reaching time, robustness and unmodeled dynamics (generator and turbine). To check the overall control strategy ride-through performance, simulations using the NREL FAST code on a 1.5-MW wind turbine are carried-out in case of grid frequency variations and unbalanced voltage sags.

2. Grid-Code Requirements

Grid-code requirements typically refer to large wind farms connected to the transmission system, rather than smaller stations connected to the distribution network. These new grid codes stipulate that wind farms should contribute to power system control (frequency and also voltage), much as the conventional power stations, and emphasize wind farm behavior in case of abnormal operating conditions of the network (such as in case of voltage dips). The most common requirements include FRT capability, extended system voltage and frequency variation limits, active power regulation, and frequency control, as well as reactive power/power factor and voltage regulation capabilities [1-2]. Grid codes main requirements regarding the addressed faults are given below.

2.1. Frequency Operating Range

Wind power plants are required to run continuously within typical grid frequency variations between 49.5 Hz and 50.5 Hz. Figure 1 gives an example of frequency-grid voltage variations [1].

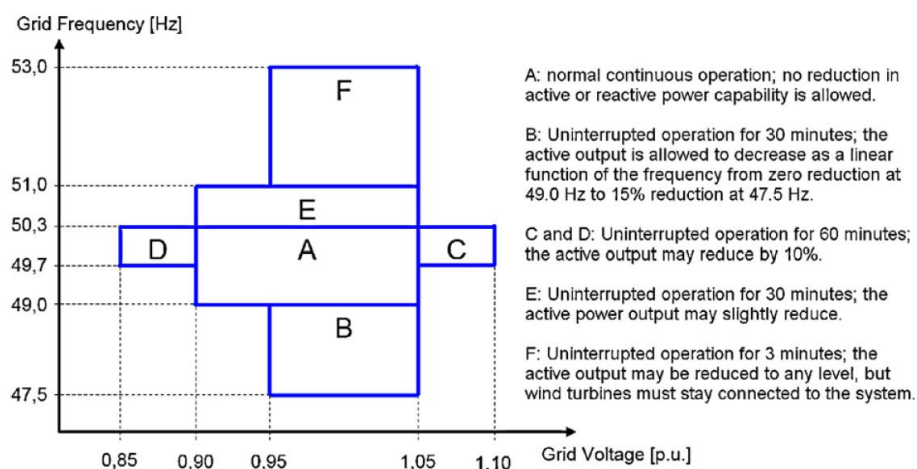


Fig. 1. Frequency-voltage variations ranges [© Nordel] [1].

2.2. Low Voltage Ride-Through

Grid codes invariably require that large wind farms must withstand voltage sags down to a certain percentage of the nominal voltage and for a specified duration. Such constraints are known as LVRT requirements. They are described by a voltage versus time characteristic, denoting the minimum required immunity of the wind power station to the system voltage sags (Fig. 2) [1].

3. Wind Turbine Modeling

The wind turbine modeling is inspired from [17]. In the following, the wind turbine components models are briefly described.

3.1. Turbine Model

In this case, the aerodynamic power captured by the wind turbine is given by

$$P_a = \frac{1}{2} \pi \rho R^2 C_p(\lambda) v^3 \quad (1)$$

where $\lambda = \frac{R\omega}{v}$ (2)

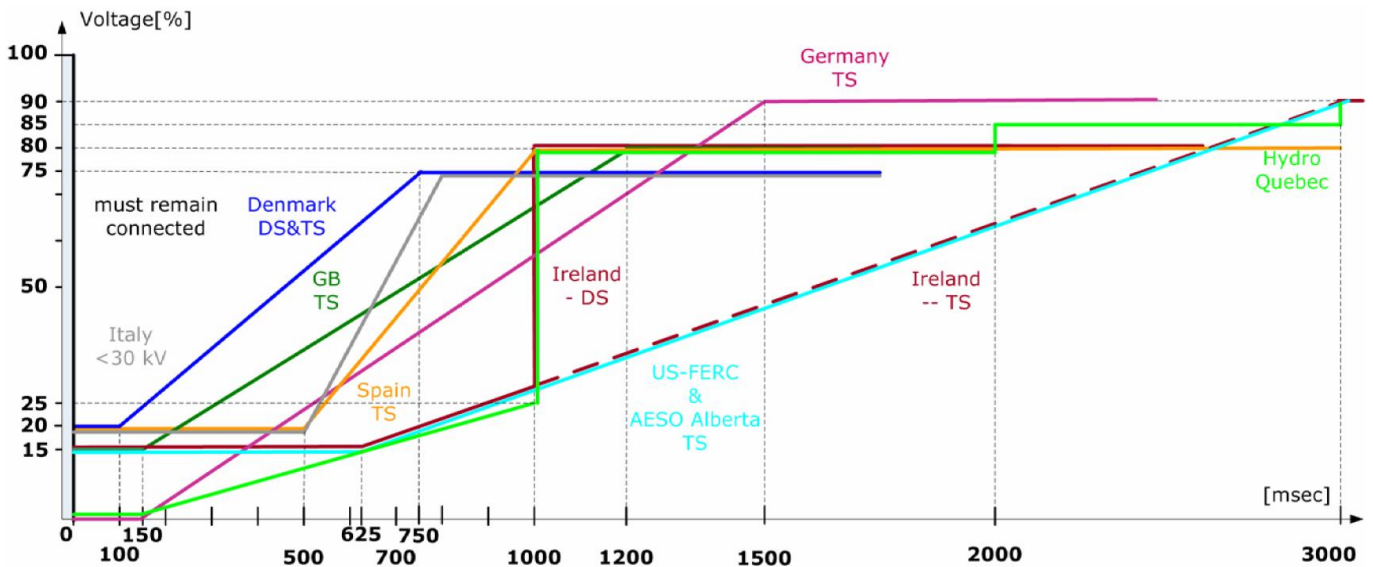


Fig. 2. LVRT requirements for different countries [1].

The rotor power (aerodynamic power) is also defined by

$$P_a = \omega T_a \quad (3)$$

The following simplified model is adopted for the turbine (drive train) for control purposes.

$$J \dot{\omega} = T_a - K \omega - T_g \quad (4)$$

3.2. DFIG Model

The control system is usually defined in the synchronous d - q frame fixed to either the stator voltage or the stator flux. For the proposed control strategy, the generator dynamic model written in a synchronously rotating frame d - q is given by

$$\begin{cases} V_{sd} = R_s I_{sd} + \frac{d\phi_{sd}}{dt} - \omega_s \phi_{sq} \\ V_{sq} = R_s I_{sq} + \frac{d\phi_{sq}}{dt} + \omega_s \phi_{sd} \\ V_{rd} = R_r I_{rd} + \frac{d\phi_{rd}}{dt} - \omega_r \phi_{rq} \\ V_{rq} = R_r I_{rq} + \frac{d\phi_{rq}}{dt} + \omega_r \phi_{rd} \\ \phi_{sd} = L_s I_{sd} + M I_{rd} \\ \phi_{sq} = L_s I_{sq} + M I_{rq} \\ \phi_{rd} = L_r I_{rd} + M I_{sd} \\ \phi_{rq} = L_r I_{rq} + M I_{sq} \\ T_{em} = pM (I_{rd} I_{sq} - I_{rq} I_{sd}) \end{cases} \quad (5)$$

For simplification purposes, the q -axis is aligned with the stator voltage and the stator resistance is neglected. These will lead to

$$\begin{cases} \frac{dI_{rd}}{dt} = \frac{1}{\sigma L_r} \left(V_{rd} - R_r I_{rd} + s\omega_s \sigma L_r I_{rq} - \frac{M}{L_s} \frac{d\phi_{sd}}{dt} \right) \\ \frac{dI_{rq}}{dt} = \frac{1}{\sigma L_r} \left(V_{rq} - R_r I_{rq} - s\omega_s \sigma L_r I_{rd} - s\omega_s \frac{M}{L_s} \phi_{sd} \right) \\ T_{em} = -p \frac{M}{L_s} \phi_{sd} I_{rq} \end{cases} \quad (6)$$

4. DFIG-Based Wind Turbine Control

4.1. MPPT Strategy

The control objective is to optimize the capture wind energy by tracking the optimal torque T_{opt} .

$$T_{opt} = k\omega^2, \text{ with } k = \frac{1}{2}\pi\rho R^5 \frac{C_{p\max}}{\lambda_{opt}^3} \quad (7)$$

Details about the adopted strategy are given in [17].

4.2. HOSM Control Strategy

The DFIG-based WT control objective is to optimize the extracted power by tracking the optimal torque T_{opt} (7). The control is a compromise between conversion efficiency and torque oscillation smoothing.

The reactive power is expressed as follows.

$$Q_s = V_{sq} I_{sd} - V_{sd} I_{sq} \quad (8)$$

Adapting (8) to our hypotheses, it comes then

$$Q_s = \frac{V_s \phi_s}{L_s} - \frac{V_s M}{L_s} I_{rd} \quad (9)$$

As the stator reactive power reference is zero, then

$$\phi_s = \frac{V_s}{\omega_s} \rightarrow I_{rd_ref} = \frac{V_s}{\omega_s M} \quad (10)$$

Let us consider the following tracking errors.

$$\begin{cases} e_{I_{rd}} = I_{rd} - I_{rd_ref} \\ e_{T_{em}} = T_{em} - T_{ref} \end{cases} \quad (11)$$

Then we will have

$$\begin{cases} \dot{e}_{I_{rd}} = \frac{1}{\sigma L_r} \left(V_{rd} - R_r I_{rd} + g \omega_s L_r \sigma I_{rq} - \frac{M}{L_s} \frac{d\phi_{sd}}{dt} \right) - \dot{I}_{rd_ref} \\ \dot{e}_{T_{em}} = -p \frac{M}{\sigma L_s L_r} \phi_s \begin{pmatrix} V_{rq} - R_r I_{rq} - g \omega_s L_r \sigma i_{rd} \\ -g \omega_s \frac{M}{L_s} \phi_{sd} \end{pmatrix} - \dot{T}_{ref} \end{cases} \quad (12)$$

If we define the G_1 and G_2 functions as follows.

$$\begin{cases} G_1 = \frac{1}{\sigma L_r} \left(g \omega_s \sigma L_r I_{rq} - \frac{M}{L_s} \frac{d\phi_{sd}}{dt} \right) - \dot{I}_{rd_ref} \\ G_2 = -p \frac{M}{\sigma L_s L_r} \phi_s \left(-g \omega_s \sigma L_r I_{rd} - g \omega_s \frac{M}{L_s} \phi_{sd} \right) - \dot{T}_{ref} \end{cases}$$

Thus we have

$$\begin{cases} \ddot{e}_{I_{rd}} = \frac{1}{\sigma L_r} \dot{V}_{rd} + \dot{G}_1 - \frac{1}{\sigma L_r} R_r \dot{I}_{rd} \\ \ddot{e}_{T_{em}} = -p \frac{M}{\sigma L_s L_r} \phi_s \dot{V}_{rq} + \dot{G}_2 + p \frac{M}{\sigma L_s L_r} \phi_s R_r \dot{I}_{rq} \end{cases} \quad (13)$$

Now, lets us consider the following second-order sliding mode controller based on the supertwisting algorithm [17-19].

$$\begin{cases} V_{rq} = y_1 + B_1 \left| e_{T_{em}} \right|^{\frac{1}{2}} Sgn(e_{T_{em}}) + \frac{1}{\sigma L_r} R_r I_{rd} \\ \dot{y}_1 = +B_2 Sgn(e_{T_{em}}) \\ V_{rd} = y_2 - B_3 \left| e_{I_{rd}} \right|^{\frac{1}{2}} Sgn(e_{I_{rd}}) - p \frac{M}{\sigma L_s L_r} \phi_s R_r I_{rq} \\ \dot{y}_2 = -B_4 Sgn(e_{I_{rd}}) \end{cases} \quad (14)$$

Where y_1 and y_2 are intermediate variables and represent the control error integral.

To ensure the sliding manifolds convergence to zero in finite times, the gains B_1 , B_2 , B_3 , and B_4 can be chosen as follows [19-20]

$$\begin{cases} |\dot{G}_1| < \Phi_1 \\ B_1 > p \frac{M}{\sigma L_s L_r} \phi_s \Phi_1, B_2^2 \geq \frac{4\Phi_1 (B_1 + \Phi_1)}{\sigma^2 L_r^2 (B_1 - \Phi_1)} \\ |\dot{G}_2| < \Phi_2 \\ B_3 > \frac{\Phi_2}{\sigma L_r}, B_4^2 \geq \frac{4\Phi_2 (B_3 + \Phi_2)}{\sigma^2 L_r^2 (B_3 - \Phi_2)} \end{cases} \quad (15)$$

In this context, it can be asserted that there exist finite times t_{Tem} and t_{Ird} leading to (16). This means that the control objective is achieved.

$$\begin{cases} I_{rd_ref} = I_{rd}, \quad \forall t > t_{Ird} \\ T_{ref} = T_{em}, \quad \forall t > t_{Tem} \end{cases} \quad (16)$$

The above proposed second-order sliding mode control strategy for a DFIG-based WT is illustrated by Fig. 3.

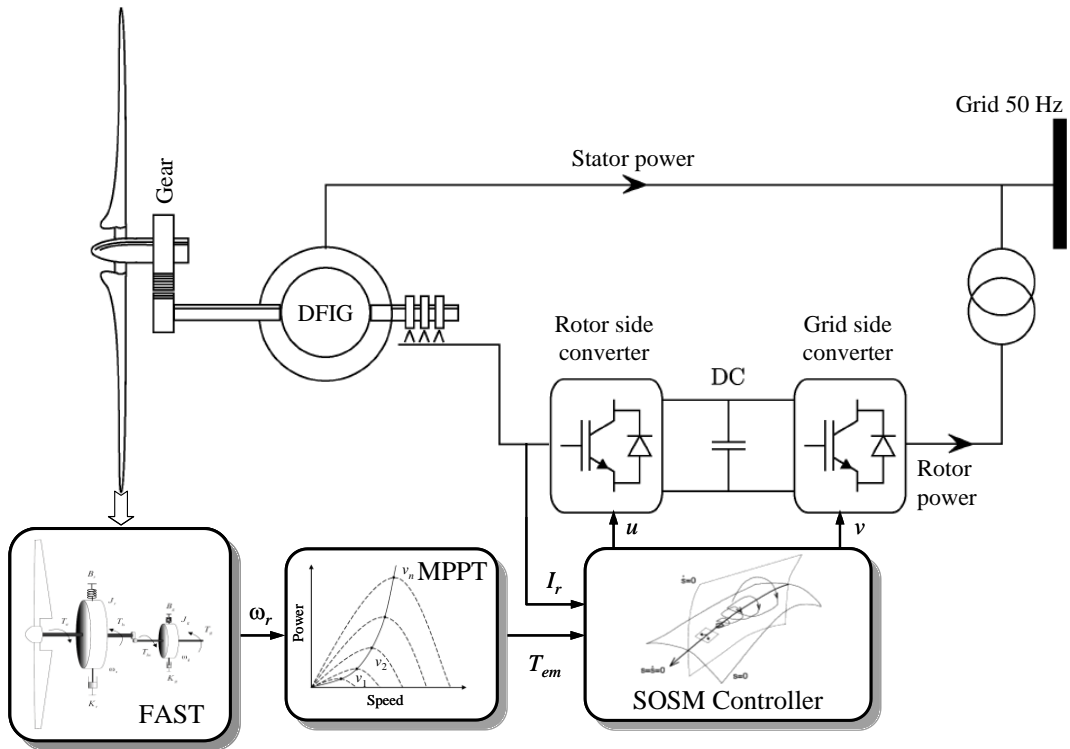


Fig. 3. The proposed FRT control structure.

5. Simulations using FAST Code

Simulation using FAST with Matlab-Simulink[®] have been carried out on the NREL WP 1.5-MW wind turbine (Fig. 4) using turbulent FAST wind data shown by Fig. 5 [21]. The wind turbine, the DFIG ratings, and control parameters are given in the Appendix.

An interface has been developed between FAST and Matlab-Simulink[®] enabling users to implement advanced turbine controls in Simulink convenient block diagram form (Fig. 6). Hence, electrical model (DFIG, grid, control system, etc.) designed in the Simulink environment is simulated while making use of the complete nonlinear aerodynamic wind turbine motion equations available in FAST (Fig. 7).



Fig. 4. 1.5-MW wind turbine illustration.

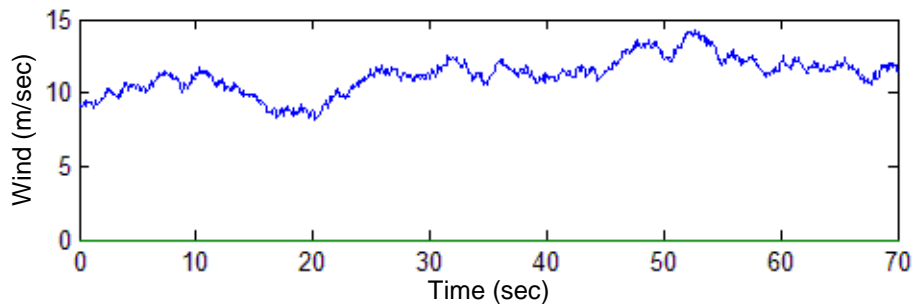


Fig. 5. Wind speed profile.

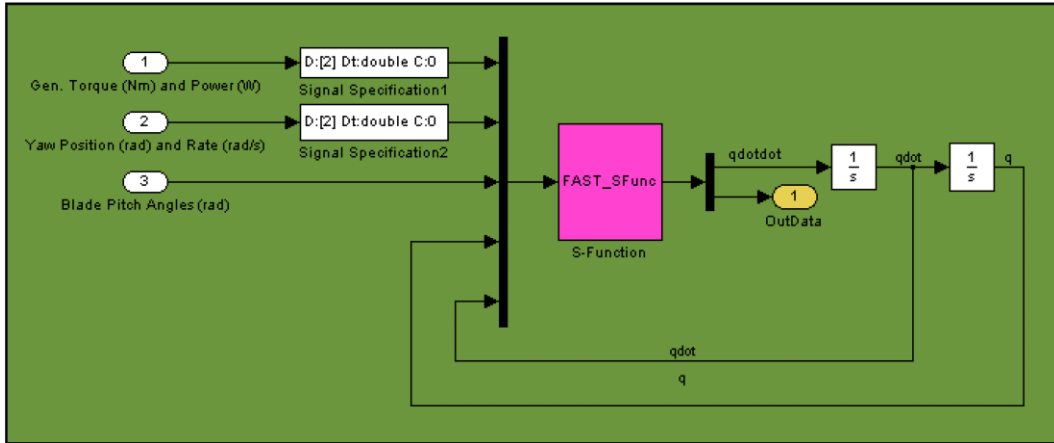


Fig. 6. FAST wind turbine block.

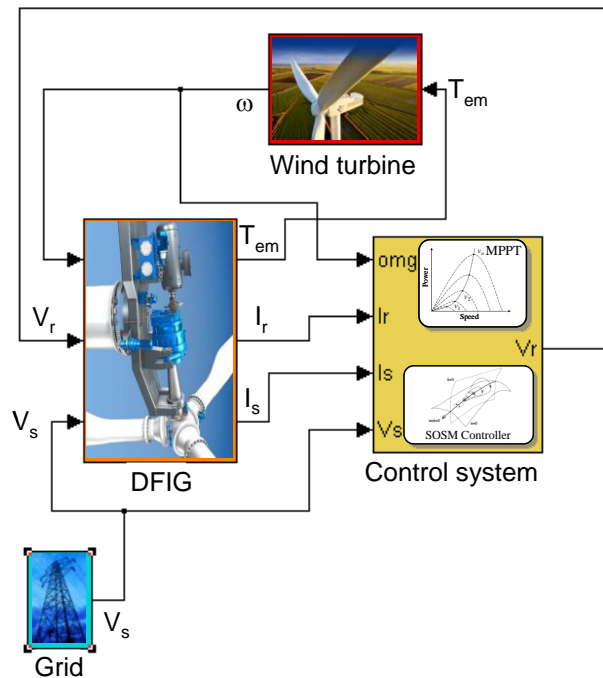


Fig. 7. Simulink model.

5.1. Frequency Variation

The proposed SOSM-based FRT strategy will be first tested regarding a frequency variation. Indeed, the studied case is a frequency fall from 50 to 48 Hz as illustrated by Fig. 8. This case corresponds to a power generation loss that could lead to a rapid decrease of the grid frequency.

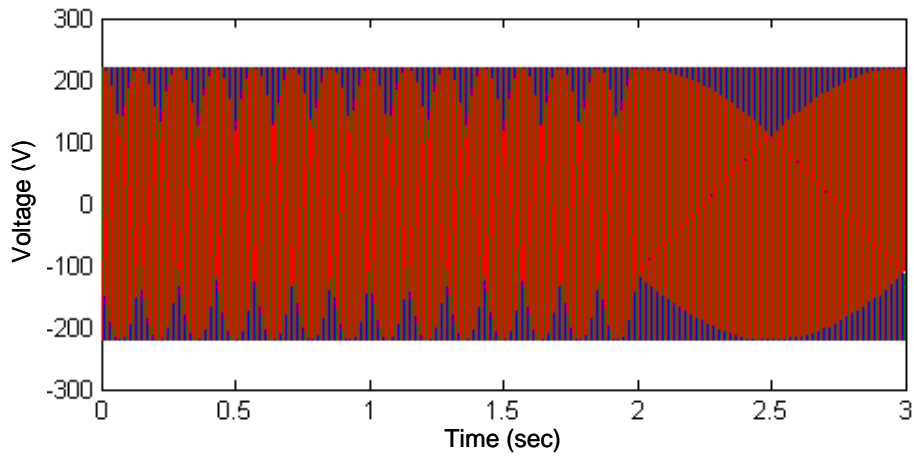


Fig. 8. Grid voltage.

The FRT performances are illustrated by Fig. 9. It clearly shows that the frequency fall has practically no effect on the torque. This is confirmed by the quadratic error shown by Fig. 10. Obviously, a good tolerance is achieved for this type of fault.

To assess the FRT capability enhancement of the proposed SOSM control approach, it has been compared to a classical PI control approach [22-23]. The achieved results as shown by Figs 11 and 12 clearly confirm the superiority of a high-order sliding mode approach over more classical control approaches. It should be noticed that the SOSM control approach achieves the same quadratic error as a classical first-order sliding mode control.

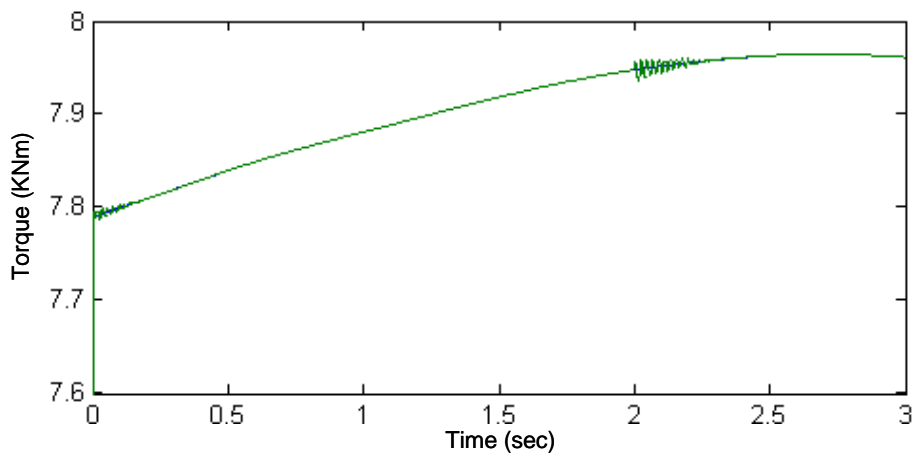


Fig. 9. Torque tracking performance during frequency variation: Reference (green) and real (blue).

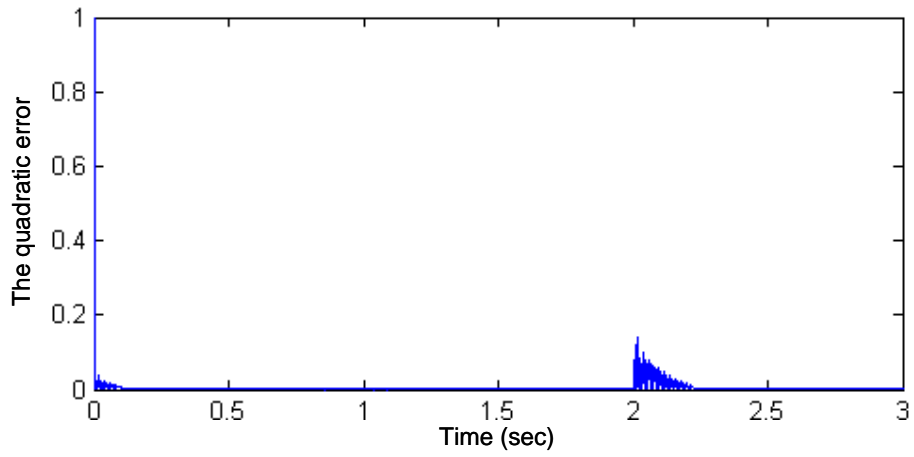


Fig. 10. Quadratic error between the reference torque and the SOSM control-based one (frequency variation).

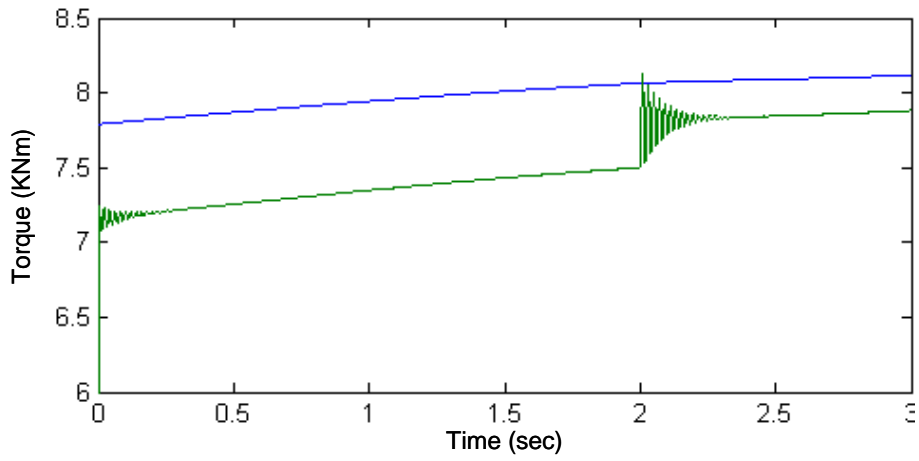


Fig. 11. Torque: Reference (green) and real (blue).

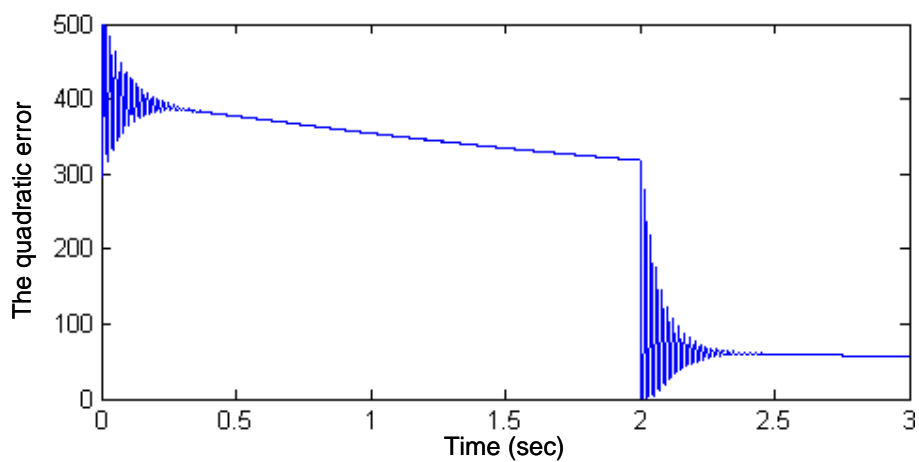


Fig. 12. Quadratic error between the reference torque and the PI control-based one (frequency variation).

5.2. Unbalanced Voltage Sags

When unbalanced sags occur (Fig. 13), very high current, torque, and power oscillations appear at double of the electrical frequency, forcing a disconnection.

The LVRT performances are illustrated by Fig. 14 where an almost constant torque is achieved. Good tracking performances are also achieved in terms of DFIG rotor current (Fig. 15). Fault-tolerance performances are also confirmed by the quadratic error shown by Fig. 16.

To assess the LVRT capability enhancement of the proposed SOSM control approach, it has also been compared to the same classical PI control approach. The achieved results are illustrated by Fig. 17. This figure clearly shows that PI control achieves poorer LVRT performances.

If the FRT performances were similar in case of frequency variation, Fig. 18 shows the superiority of a high-order mode control over a first-order in case of unbalanced voltage sags.

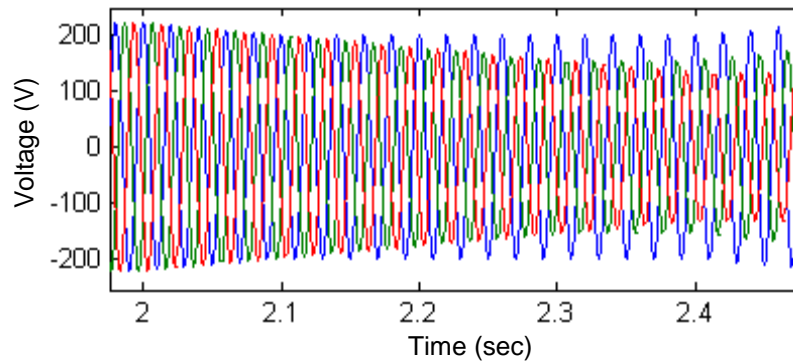


Fig. 13. Grid voltage.

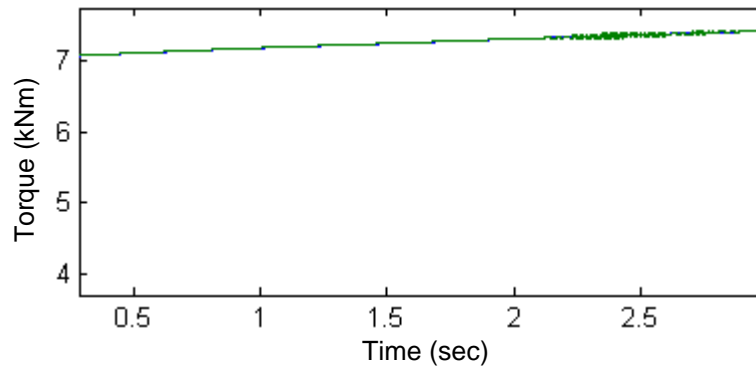


Fig. 14. Torque tracking performance during unbalanced voltage sags: Reference (blue) and real (green).

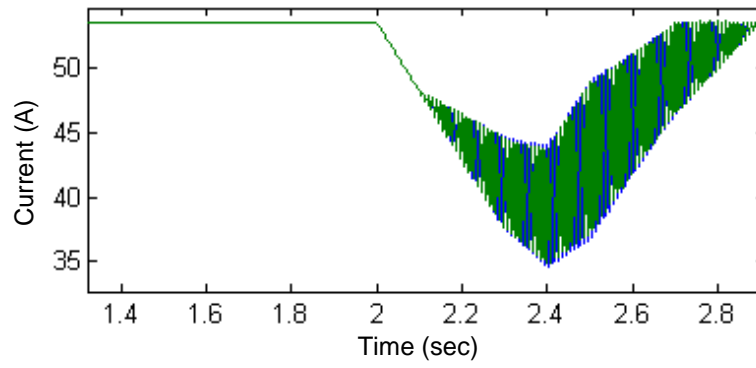


Fig. 15. Current I_{rd} tracking performance during unbalanced voltage sags: Reference (blue) and real (green).

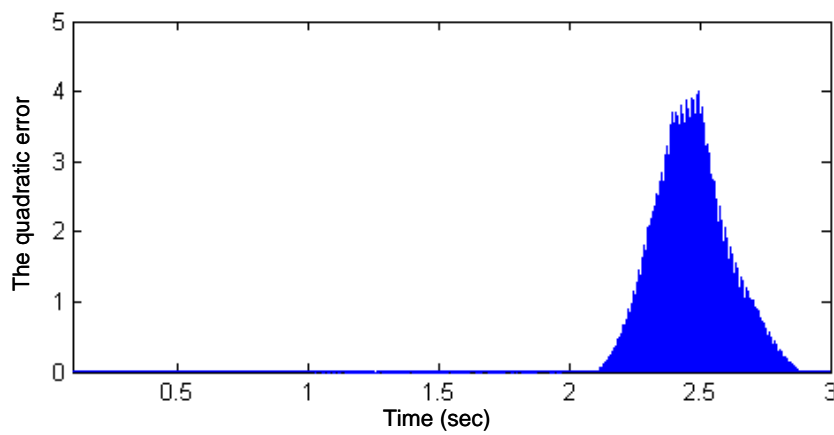


Fig. 16. Quadratic error between the reference torque and the SOSM control-based one (voltage sags).

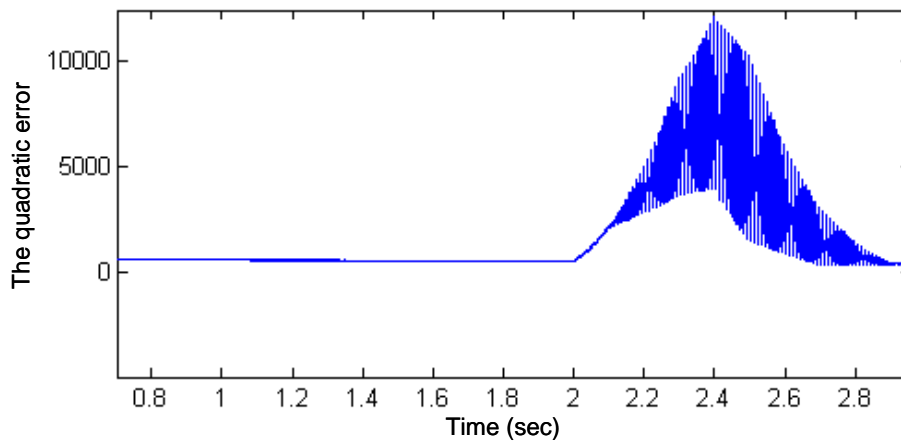


Fig. 17. Quadratic error between the reference torque and the PI control-based one (voltage sags).

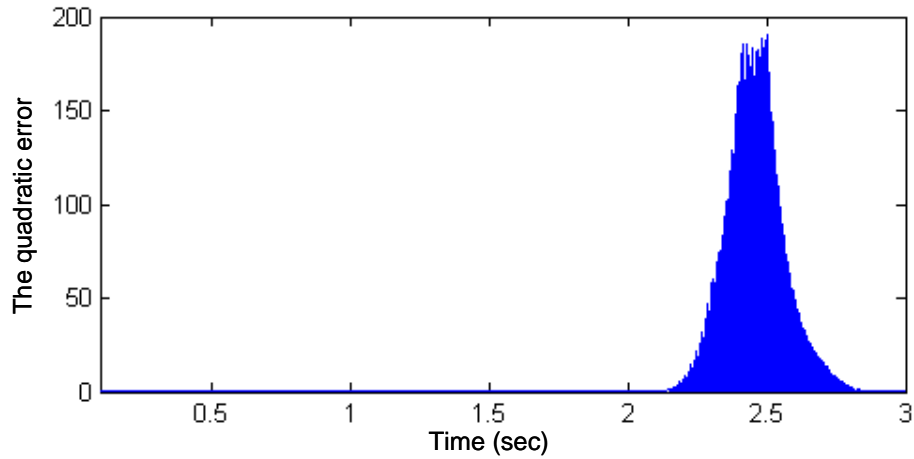


Fig. 18. Quadratic error between the reference torque and the first-order sliding mode control-based one (voltage sags).

6. Conclusion

This paper dealt with a second-order sliding mode control of a doubly-fed induction-based wind turbine for fault ride through. The SOSM-based FRT strategy has been tested regarding grid frequency variations and unbalanced voltage sags on a 1.5-MW three-blade wind turbine using the NREL wind turbine simulator FAST.

The achieved results show promising successful ride-through performances over well-known PI-based control and even over classical sliding mode control (first-order). It should be particularly mentioned that the proposed SOSM control approach does not need any specific adjustments to fault ride-through purposes.

Appendix

Simulated Wind Turbine Characteristics

Number of blades	3
Rotor diameter	70 m
Hub height	84.3 m
Rated power	1.5 MW
Turbine total inertia	$4.4532 \times 10^5 \text{ kg m}^2$

Simulated DFIG Parameters

$$R_s = 0.005 \, \Omega, L_s = 0.407 \, \text{mH}, R_r = 0.0089 \, \Omega, L_r = 0.299 \, \text{mH}, M = 0.0016 \, \text{mH}, p = 2$$

Control Parameters

$$B_1 = 10, B_2 = 20000, B_3 = 7, B_4 = 500$$

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