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# Effects of climate variations and global warming on the durability of RC structures subjected to carbonation

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Carbonation affects the performance, serviceability and safety of reinforced concrete (RC) structures when they are placed in environments with important CO<sub>2</sub> concentrations. Since the kinetics of carbonation depends on parameters that could be affected by climate change (temperature, atmospheric CO<sub>2</sub> pressure and relative humidity (RH)), this study aims at quantifying the effect of climate change on the durability of RC structures subjected to carbonation risks. This work couples a carbonation finite element model with a comprehensive reliability approach to consider the uncertainties inherent to the deterioration process. The proposed methodology is applied to the probabilistic assessment of carbonation effects for several cities in France under various climate change scenarios. It was found that climate change and local RH have a significant impact on corrosion initiation risks.

**Keywords:** carbonation; reinforced concrete; corrosion; reliability; climate change

## 1. Introduction

The performance, serviceability and safety of reinforced concrete (RC) structures are affected by corrosion-induced deterioration when they are placed in environments with important CO<sub>2</sub> concentrations. Carbonation is a chemical evolution of the cementitious materials, induced by the reactive diffusion of CO<sub>2</sub> in the porous media. Indeed, atmospheric CO<sub>2</sub> reacts with cement hydrates, dissolves portlandite and forms calcite. The main consequence of this chemical reaction is a significant decrease in pH in the porous solution that induces corrosion of the reinforcing steel. The kinetics of this degradation depends on temperature, atmospheric CO<sub>2</sub> pressure and relative humidity (RH), all parameters related with time and climate change.

Natural and anthropogenic actions will increase environmental CO<sub>2</sub> concentrations in the future and produce changes in temperature and humidity. For instance, following the current patterns, an increase in CO<sub>2</sub> concentration from 379 ppm in 2005 over 1000 ppm by the year 2100 is expected (IPCC 2007). Therefore, these new environmental conditions will modify the kinematics of carbonation by increasing or reducing the consequences of corrosion-induced damage. Besides climate change, there are other uncertainties related to the carbonation process. Consequently,

probabilistic approaches are suitable tools for assessing structural risk and reliability for this problem.

Various studies have focused on the effect of climate change on the durability of corroded RC structures. Bastidas-Arteaga et al. (2010) proposed a stochastic approach to study the influence of global warming on chloride ingress for RC structures. They found that chloride ingress could induce reductions of the corrosion initiation stage varying from 2% to 18%. Concerning corrosion propagation until failure, Bastidas-Arteaga et al. (2013) found that global warming could reduce the time to failure by up to 31% for RC structures subject to chloride ingress. Recent work also focused on the assessment of climate change on the durability of concrete structures in specific locations. Stewart, Wang, and Nguyen (2011) found that the temporal and spatial effects of a changing climate can increase current predictions of carbonation-induced damage risks by more than 16% which means that one in six structures will experience additional and costly corrosion damage by 2100 in Australia and presumably elsewhere. Wang, Stewart, and Nguyen (2012) studied the impact of climatic change on corrosion-induced damage in Australia. They proposed a probabilistic approach to assess corrosion damage taking into account the influence of climate change on areas characterised by different geographical conditions. Talukdar et al. (2012) estimated the effects of climate change on carbonation in Canadian cities (Toronto and Vancouver). They found potential increases in carbonation depths over 100 years of approximately 45%. However, this work did not consider the uncertainties related to climate, materials and models.

This study uses a probabilistic approach to compare and quantify the effect of different climate change scenarios on the structural safety of an RC structure exposed to a risk of corrosion induced by the cement paste carbonation. In comparison with previous studies, this paper integrated a relevant carbonation finite element model that takes into account all these climate evolutions (Section 3). Probabilistic assessment using this finite element model requires a significant computational effort. Therefore, Section 4 presents the adopted reliability approach that is used in this work. Finally, Section 5 presents an application to the assessment of climate change effects to RC structures placed in various cities in France.

## **2. Climate change effects**

### **2.1. Increase in carbon dioxide emissions**

Following the current patterns, studies have estimated that environmental CO<sub>2</sub> concentration could increase from 379 ppm in 2005 over 1000 ppm by the year 2100 (IPCC 2007). Consequently, the long-term management of RC structures should consider the effect of atmospheric CO<sub>2</sub> concentration change and global warming. The increase in atmospheric CO<sub>2</sub> concentration is difficult to estimate because it depends on several socio-technical and political factors. These factors have been considered by the Intergovernmental Panel on Climate Change (IPCC 2007) that defined four scenarios families of global warming (i.e. A1, A2, B1 and B2). These scenarios integrate different assumptions in terms of population growth, economical development, transfer of clean technologies, etc. The A1 scenario describes a future world of very rapid economic growth, global population that peaks in mid-century and declines thereafter, and the rapid introduction of new and more efficient technologies. This scenario family is divided into three groups distinguished by different technological emphasis: fossil-intensive (A1FI), non-fossil energy sources (A1T) or a balance across all sources (A1B). The A2 scenario describes a very heterogeneous world with continuously increasing population. The economic development is primarily regionally oriented and technological change more fragmented and slower. The B1 scenario is similar to the A1 scenario with respect to population growth, but with rapid change in economic structures towards a service and information economy, with reductions in material intensity and the introduction of clean and

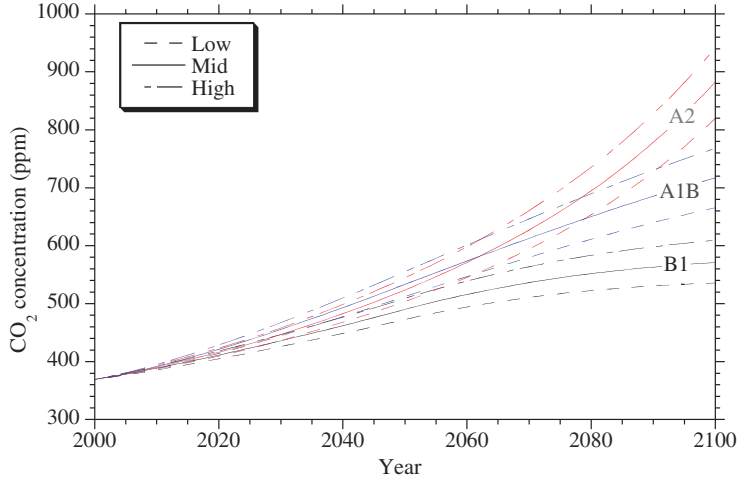


Figure 1. CO<sub>2</sub> emissions for the studied scenarios.

resource-efficient technologies. The B2 scenario describes a world in which the emphasis is on local solutions to economic, social and environmental sustainability. The population growth pattern is similar to the scenario A2 but with a lower rate. It also includes more diverse technological solutions. Figure 1 presents a projection from 2000 of environmental CO<sub>2</sub> concentrations the A2, A1B and B1 global warming scenarios. These scenarios were selected in this study because they represent pessimistic, medium and optimistic climate change effects on climate, respectively (Section 2.2). These values were computed using the MAGICC software (Model for Assessment of Greenhouse-gas Induced Climate Change) (Wigley, Richels, and Edmonds 1996). Every scenario includes three versions for the CO<sub>2</sub> emissions: a lower one, a medium one and a higher one. For this study, it has been decided to take into account only the medium one (assessing the higher the CO<sub>2</sub> pressure, the faster the carbonation). Taking into account the description of the scenarios presented previously, the highest projections for CO<sub>2</sub> concentration for 2100 correspond to the A2 scenario.

## 2.2. Effects of climate change on temperature and relative humidity

The effect of climate change on weather will change depending on the geographical and meteorological characteristics of the studied location. The impact of climate change on the future weather

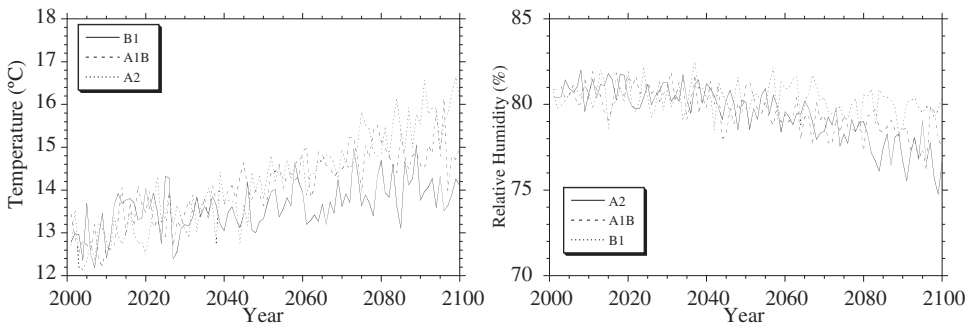


Figure 2. Temperature and RH projections for Nantes.

of the selected locations was estimated by using data computed by the French general circulation model SCRATCH-ARPEGE-V4-RETIC (Déqué et al. 1994). This model was selected because it is able to account for climate projections at a regional scale with a 8 km grid. For instance, Figure 2 presents the yearly projections of temperature and RH for the city of Nantes and the selected climate change scenarios. It is noted that climate change projections announce a temperature increase and RH decrease for all scenarios. The most important changes in temperature and RH are related to the larger emission scenarios described in the previous section. Concerning consequences on climate change, it is possible to define A2 as a pessimistic scenario, A1B as a medium impact scenario and B1 as an optimistic scenario.

### 3. Carbonation model

This section presents the model used herein for describing the coupled drying and carbonation of concrete, which is detailed in de Larrard et al. (2013a). This is a simplified version of the model proposed in Bary and Sellier (2004), which assumes that the main phenomena involved in the carbonation are the water migration through the connected porosity, and the diffusion of carbon dioxide in the gaseous phase and its subsequent interactions with the hydrated phases initially present to produce calcium carbonate (calcite). Accordingly, it is governed by two coupled mass conservation equations for water (Equation (1)) and carbon dioxide in gas phase (Equation (2)):

$$\frac{\partial(\rho_l \phi S_r)}{\partial t} = \nabla \left[ K(\phi) \frac{\rho_l}{\eta} k_r(S_r) \nabla(P_1) \right] + W_{\text{H}_2\text{O}}, \quad (1)$$

$$\frac{\partial((1 - S_r)\phi P_c)}{\partial t} = \nabla [f(\phi, S_r) D_c \nabla(P_c)] + W_{\text{CO}_2}. \quad (2)$$

Equation (1) implicitly assumes that the main transport process for moisture results from gradients of partial pressure of water in the liquid phase  $P_1$  (permeation), i.e. the migration of vapour in gas phase is neglected (Mainguy, Coussy, and Baroghel-Bouny 2001; Bary and Sellier 2004). Moreover, the pressure of the gas phase is neglected with respect to the liquid phase, such that  $P_c \approx -P_1$ , where  $P_c$  is the capillary pressure. Equation (1) is also driven by  $P_c$  in the desorption isotherm that accounts for the relationships between the saturation degree  $S_r$  and  $P_c$  (van Genuchten 1980):

$$S_r = \left[ 1 + (P_c/P_0)^{1/(1-m)} \right]^{-m}, \quad (3)$$

where  $P_0$  and  $m$  are calibration parameters. Other parameters involved in Equation (1) are  $K(\phi)$  is the intrinsic permeability coefficient that depends on the initial porosity  $\phi$  and the initial intrinsic permeability  $K_0$  (van Genuchten 1980);  $\rho_l$  and  $\eta$  are the density and dynamic viscosity of water, respectively;  $k_r(S_r)$  is the relative permeability for liquid that depends on the saturation degree  $S_r$  (van Genuchten 1980) and  $W_{\text{H}_2\text{O}}$  is the rate of water formation.

Equation (2) is driven by the partial pressure of  $\text{CO}_2$  in the gaseous phase denoted as  $P_c$ .  $f(\phi, S_r)$  and  $D_c$  are the reduction factor (Millington 1959) and the diffusion coefficient of  $\text{CO}_2$  in gas phase, respectively, such that their product can be considered as the effective diffusion coefficient of  $\text{CO}_2$  through the porous material and  $W_{\text{CO}_2}$  is the rate of  $\text{CO}_2$  dissolution. The coupling between Equations (1) and (2) appears through (i) the saturation degree  $S_r$ , and (ii) the rates of water formation and carbon dioxide dissolution. These rates,  $W_{\text{H}_2\text{O}}$  and  $W_{\text{CO}_2}$ , respectively, derive from the molar formation rate of calcite ( $\dot{N}_{\text{cal}}$ , Equation (4)), and the molar dissolution rate of portlandite ( $\dot{N}_{\text{por}}$ , Equation (5)) and of other hydrates ( $\dot{N}_{\text{CSH}}$ , Equation (6)), mainly C-S-H. We have indeed considered separately the dissolution-precipitation processes of portlandite and of

the other hydrates, due to the higher reactivity of portlandite (Bary and Sellier 2004; Thiery et al. 2007).

$$\dot{N}_{\text{cal}} = \dot{N}_{\text{por}} + \dot{N}_{\text{CSH}}, \quad (4)$$

$$\dot{N}_{\text{por}} = k_{\text{sl}}(S_r) k_{\text{H}} \tilde{k}_{\text{p}}(V_{\text{p}}) P_{\text{c}}, \quad (5)$$

$$\dot{N}_{\text{CSH}} = k_{\text{sl}}(S_r) k_{\text{H}} \tilde{k}_{\text{CSH}}(C_{\text{cal}}) P_{\text{c}}, \quad (6)$$

where  $k_{\text{sl}}(S_r)$  is a function introduced by Bazant and Najjar (1972) to describe at a macroscopic scale the influence of the saturation degree on the chemical reaction processes (i.e. the reduction of water in the pores leads to decrease the reactions);  $k_{\text{H}}$  is the Henry constant for carbon dioxide; and the functions  $\tilde{k}_{\text{p}}(V_{\text{p}})$  and  $\tilde{k}_{\text{CSH}}(C_{\text{cal}})$  are kinetic coefficients depending on the current volume fraction of portlandite  $V_{\text{p}}$  and concentration of calcium in solid phase  $C_{\text{cal}}$ , respectively. It should be stressed that the simplified chemical reactions relative to the hydrate dissolution–calcite precipitation as expressed by these equations correspond to first-order kinetic law with respect to the  $\text{CO}_2$  pressure. The kinetic coefficient for the calcite formation from portlandite  $\tilde{k}_{\text{p}}$  is assumed to evolve as proposed in Thiery et al. (2007), i.e. the calcite is supposed to form a growing layer surrounding the portlandite crystals during the dissolution process. The consequence is that this layer progressively reduces the corresponding chemical reactions kinetics, which are driven by the diffusive phenomena through the calcite layer. The kinetic coefficient for the other hydrates is assumed to evolve linearly with the calcium concentration.

The main simplification of this numerical model in comparison with the previous version (Bary and Sellier 2004) concerns the calcium concentration calculation. In the present approach, no diffusion of calcium is considered and it is instead replaced by a local chemical equilibrium of calcium, meaning that the calcium dissolved from portlandite and the other hydrates is locally transformed into calcite. Formally, this is equivalent to considering that the whole calcite formation process (including  $\text{CO}_2$  diffusion) is faster than calcium migration through the solution. de Larrard et al. (2013a) numerically demonstrated that this simplification has a very weak influence on the results in the case of accelerated carbonation. Further investigations, which are beyond the scope of this paper, would be necessary to analyse its effects in atmospheric carbonation conditions.

The model presented above has been modified to take into account the influence of temperature variations on carbonation. The modifications of the carbonation model to take into account temperature effects are detailed in de Larrard et al. (2013b), based upon the studies proposed in de Larrard et al. (2012). These modifications include the influence on the following thermo-activated parameters/phenomena: (i) the  $\text{CO}_2$  diffusion coefficient, (ii) the dissolution of portlandite, as well as other hydrates and (iii) the constant of Henry (Equation (5)), and (iv) the sorption–desorption isotherms. The dependency of temperature of all these parameters/phenomena is modelled with Arrhenius functions. According to Yuan and Jiang (2011), we assume that the temperature inside concrete is constant and equal to the atmospheric temperature. It is to be noted that the effective temperature of RC elements exposed to solar radiation may differ from the ambient temperature, but it is assumed that the time steps used for numerical simulations are large enough to work with a mean value for the temperature and the difference (as the kinetics for the heat transfer is important with regards to these for the aggressive species diffusion) involved by this assumption are neglected. This will be the subject for a future study, beyond the scope of the present paper.

This carbonation model was implemented in the finite element code Cast3M ([www-cast3m.cea.fr](http://www-cast3m.cea.fr)), and the equations solved successively and iteratively with a fully implicit numerical scheme. To conclude, the present model turns out to provide results in terms of calcite and portlandite concentration profiles very close to the ones obtained with a previous and more complex version of the model. Furthermore, the phenolphthalein carbonation depths calculated in the case of an accelerated test appear in very good agreement with both experimental and

numerical results (de Larrard et al. 2013a). We then consider that the model is relevant and suitable for the probabilistic simulations required to determine the reliability index of RC structures under the combined action of climate change and carbonation.

#### 4. Reliability analysis

A common practical measure of the structural reliability is the Hasofer–Lind’s reliability index denoted  $\beta$  (Hasofer and Lind 1971). This index is defined in the standardised space of reduced normal and independent variables as the minimum distance from the origin to a point of the failure surface, the so-called design point  $P^*$ . The determination of  $\beta$  is a constrained optimisation problem (Hasofer and Lind 1971; Rackwitz and Fiessler 1979). The function to be minimised is the Euclidean distance  $\|u\|$  in the standardised space under the constraint  $G(u) = 0$ , where  $G$  is the limit-state function. If  $u^*$  is the solution of the optimisation with  $\beta = \|OP^*\| = \|u^*\|$ , then:

$$u^* = \arg \min(\|u\|)_{G(u)=0}. \quad (7)$$

As the carbonation depth is not directly accessible numerically, the failure function for the carbonation model presented in this paper is based on the quantity of portlandite dissolved at the steel/concrete interface. The carbonation depth, as defined by the widely used phenolphthalein test, is simply estimated from the portlandite profile for a threshold value of dissolution. For instance, if the remaining volume fraction of portlandite is less than 33% of the initial value after dissolution at the cover depth, it is considered that corrosion starts. This threshold is among the values reported by Chang and Chen (2006), de Larrard et al. (2013a) and Park (2008). Thus, for this threshold value, the limit-state function becomes

$$G(u) = V_p(u, c_t(u), t_{\text{fin}}) - 0.33 \times V_p(u, c_t(u), t_0), \quad (8)$$

where  $V_p$  is the volume fraction of portlandite, depending on  $c_t$ , which is the concrete cover thickness from the exposed face, and the time.  $V_p$  is calculated with the FE model presented above.  $t_{\text{fin}}$  is the final time of the simulations (100 years) and  $t_0$  is the initial time (0 year). It is clear that the choice of the dissolved portlandite threshold will affect the assessment of reliability index. However, for a comparative study of climate change effects on various climates, the global trends will be the same for all the studied cases if the threshold is fixed.

According to design codes,  $G(u)$  defines a limit-state function, which is expected to be continuous, at least in the neighbourhood of the design point  $P^*$ . Most part of optimisation algorithms used in structural reliability are useful for differentiable constraint functions. However, in the carbonation model considered in this study, the limit-state function  $G$  is computed by using the finite element method. Therefore, the reliability index is computed according to the gradient projection algorithm in the standardised space (Duprat et al. 2010). The result of the reliability analysis could therefore provide  $\beta$  over the lifetime  $t_{\text{fin}}$ .

#### 5. Numerical example: application to RC structures placed in France

##### 5.1. Problem description

The objective of this example is to estimate the effects of several scenario of climate change on the carbonation of an RC structure placed in several cities in France. The material considered is a CEM I concrete with a water/cement ratio equal to 0.42% and 68% aggregate volume fraction.

Table 1. Statistical parameters of the random variables (de Larrard et al. 2010, 2013a).

Variable	Unit	Distribution	Mean	COV (%)
Concrete cover, $c_t$	cm	Normal	2	5
Initial porosity, $\varphi_0$	%	Normal	30	5
Intrinsic permeability, $K_0$	m <sup>2</sup>	Normal	$1.8 \times 10^{-22}$	5
Parameter, $m$ (Equation (3))		Normal	0.532	5
Diffusion coefficient, $D_{\xi}$	m <sup>2</sup> /s	Normal	$1.9 \times 10^{-8}$	5

The material is initially set to saturation degree corresponding to the year before 2000, and exposed to drying, carbonation and temperature variations according to climate change scenarios for each city. It is also supposed that carbonation takes place in one dimension. The material properties as well as the model parameters were chosen equivalent to those proposed in de Larrard et al. (2013a).

Table 1 presents the five random variables considered in this study. Concrete cover corresponds to a global structural uncertainty related to a variability introduced by the building process. The initial porosity of the cement paste has a significant influence on the kinetics of the diffusion processes studied here, as it appears in every term of the governing equations. Two other variables concern the drying process: the intrinsic permeability  $K_0$  and the  $m$  parameter from the van Genuchten model, which govern the desorption isotherm. The last random variable is the diffusion coefficient for CO<sub>2</sub>. These four last parameters are materials properties. Their ‘randomness’ stands for the natural uncertainty and spatial variability of the materials properties, even for the same concrete formulation. These random variables follow independent normal distributions with a coefficient of variation (COV) equal to 5%. These means and COVs are among the values observed for a given concrete formulation (de Larrard et al. 2010, 2013a). It is to be noted that the choice of a normal distribution may not be the most relevant, even though it is in good accordance with the data observed in de Larrard et al. (2013). Besides, these values for the COVs are within the lower values experimentally observed. The COVs depend on the mix design and the implementation process of the concrete. However, this study aims mainly at comparing the different scenarios for different locations; therefore it is mostly important to keep the same hypothesis for all cases.

This work focused on the study of the effects of climate change on specific locations in France: Marseille, Paris, Toulouse, Strasbourg, Clermont-Fd. and Nantes (Figure 3). These cities correspond to different types of climate: Nantes is close to the Atlantic Ocean in the Northern part of the country and has a temperate oceanic climate; Toulouse is in the South and its climate has continental, oceanic and Mediterranean influences; Marseille in the South-East on the Mediterranean coast and has a Mediterranean climate rather hot and dry; Strasbourg in the North-East, close to the German frontier with a northern continental climate; Paris is more in the centre of the country with an intermediate continental climate; and Clermont-Fd. is in the mountains of ‘Massif Central’, in elevated South-Central France and has rather a continental climate.

## 5.2. Results and discussions

As mentioned in Section 2, climate change effects on weather will be different for each location. By using the outputs of the French atmosphere model, Table 2 describes the mean temperature and RH for the first decade of the study (2001–2010). It is observed that Marseille is the most hot and dry city, Strasbourg is the most cold and Nantes is the most humid. Tables 3 and 4 summarise the effects of climate change by comparing the mean values of the first (2001–2010) and the last decade (2091–2111) for each climate change scenario. Figure 2 presents an example of evolution of T and RH for one of the studied locations, whereas Tables 3 and 4 summarise these evolutions for the different cities and for various periods through the elevation of their mean values. Table 3





Figure 3. Studied locations in France.

Table 2. Mean temperature and RH over the period 2001–2010.

Scenario	Marseille	Paris	Toulouse	Strasbourg	Clermont-Fd.	Nantes
Temperature	14.75	13.04	14.08	11.53	11.66	12.76
RH	68.78	74.22	77.36	77.02	75.44	80.65

Table 3. Change in temperature (in °C) over the period 2001–2100.

Scenario	Marseille	Paris	Toulouse	Strasbourg	Clermont-Fd.	Nantes
A2	+3.04	+3.59	+3.23	+3.63	+3.43	+3.22
A1B	+2.21	+2.56	+2.29	+2.58	+2.39	+2.23
B1	+1.16	+1.33	+1.18	+1.40	+1.28	+1.14

indicates that temperature could increase from 1.14 °C up to 3.63 °C with respect to current values for all the locations over the period 2001–2100. It is noted that Strasbourg could be more affected by climate change. Table 4 shows that climate change could reduce the current RH by  $-0.21\%$  up to  $-4.92\%$  with respect to current RH. The major changes could be expected for Paris. It is also confirmed that the A2 scenario is the most pessimistic with larger temperature increases and RH decreases. The B1 scenario predicts lower changes in temperature and RH and the A1B scenario is intermediate between A2 and B1.

Table 5 presents the reliability indexes for these climate change scenarios over a period of 100 years. It is observed that there is a large variation of the reliability index from  $\beta < 0$  to  $\beta > 8$ .

Table 4. Change in RH (in %) over the period 2001–2100.

Scenario	Marseille	Paris	Toulouse	Strasbourg	Clermont-Fd.	Nantes
A2	-2.61	-4.92	-4.79	-4.64	-4.59	-3.96
A1B	-1.10	-3.44	-2.79	-2.87	-2.33	-2.75
B1	-0.21	-1.14	-0.93	-1.11	-0.79	-0.59

Table 5. Reliability indexes for the different climate change scenarios.

City	A2	A1B	B1
Marseille	< 0	< 0	< 0
Paris	1.70	3.68	6.55
Toulouse	2.09	3.90	6.91
Strasbourg	7.51	> 8	> 8
Clermont-Fd.	> 8	> 8	> 8
Nantes	> 8	> 8	> 8

Let us specify here that a reliability index negative refers to a situation where the probability of corrosion initiation is higher than 50%. This implies a larger difference in the safety issues for the extreme cases. This larger variability is due to the fact that the same material has been tested for cities with different climates (Table 2). For instance, the climate is very different in Nantes and Marseille. Since the exposure conditions are not the same, we should design a specific formulation for a concrete or select a different concrete cover adapted for each city. Considering that the same concrete mix design for such different exposure conditions was required only for the needs of the comparison within the framework of this study. The reliability index for Marseille was  $\beta < 0$ , indicating that the probability of corrosion initiation is very high in a period of 100 years. The lower values of  $\beta$  for Marseille are explained, on the one hand, because the temperature is more important and carbonation is thermo-activated. On the other hand, RH varies between 65% and 70% by accelerating carbonation. These results could justify the implementation of an adaptation measure for this type of climate that could consist of increasing the concrete cover or the strength grade (Bastidas and Stewart 2013; Stewart et al. 2014).

On the opposite, corrosion initiation risks are very low for the cities of Strasbourg, Clermont-Fd. and Nantes. Even considering the effects of climate change, the lower temperatures and higher RH for these cities decelerate the carbonation process. For example, RH in Nantes remains between 80% and 85% which corresponds to a ‘retarding effect’, modelled by the function presented in Equation (2) (Millington 1959): when RH is larger ( $RH > 80\%$ ), there is not enough gaseous phase in the pores for the diffusion process to occur efficiently. This ‘natural safety’ due to a higher RH appears mainly because only carbonation is studied here, but the opposite effect would appear if the corrosion process was considered instead (because its kinetics is driven by water saturation).

Climate change could have important effects on structures placed in Paris and Toulouse. Although Paris has lower temperatures than southern cities, the value of RH for the decade 2001–2010 is within the optimal interval for accelerating carbonation (Table 2). Climate changes also accelerate carbonation in Paris by a significant decrease in RH (Table 3). Toulouse has a similar behaviour to that of Paris. On the one hand, the higher temperature in Toulouse accelerates the carbonation effects; on the other hand, the larger RH reduces them. It is therefore possible to conclude that, for the studied locations, carbonation is more sensitive to RH than temperature. It is to be noted that, except for Marseille, the reliability index is higher than the 1.5 value given for a serviceability limit state in Eurocode 0. The reliability index calculated here only takes

Table 6. Design point coordinates in the standardised space for A1B scenario.

City	$c_t$	$\phi_0$	$K_0$	$D_{\bar{c}}$	$m$
Marseille	3.05	-1.58	-0.28	-1.62	-4.49
Paris	-3.09	0.72	0.38	0.91	1.58
Toulouse	-3.48	0.87	0.38	1.03	1.07
Strasbourg	-8.26	1.29	0.76	1.64	2.37
Clermont-Fd.	-10.68	1.46	0.69	1.73	2.55
Nantes	-14.29	1.26	0.63	1.53	1.81

into account the carbonation process, and not the oxygen transfer for instance which is linked to the corrosion process kinetics. Therefore, no conclusion concerning actions required on the RC elements considered here can be drawn directly from these results.

Concerning the effects of different climate change scenarios, it appears that the reliability index decreases when temperature increases and RH decreases. The impact of the scenario is significant for Paris and Toulouse. For instance in Paris, according to B1-scenario, the reliability index is close to 6.6, which corresponds to a rather safe area, but according to A2-scenario, it is reduced to 1.7. This means that, under A2-scenario, the RC structures should be surveyed with care or adaptation measures implemented, because the risk of carbonation around the steel rebar (and corrosion initiation) is significant.

This discussion will end with some comments about the coordinates of the design point in the standardised space. These coordinates are presented in Table 6 for the A1B (intermediate scenario). These coordinates indicate how many standard deviations separate the design point from the origin of the standardised space (being the mean value for each input parameter). A high value for a coordinate indicates that the design point is located in the distribution tail for the considered parameter. Therefore, it implies that this parameter has a significant influence on whether the mean point is in the security domain or in the failure area.

These results indicate that the most influent random variable on the reliability analysis is the concrete cover thickness. The other random variables have a similar order of importance. One can also discuss the physical sense of these coordinates. It is obvious that increasing cover thickness increases the structural reliability as it lengthens the path from the external environment to the steel rebar. A reduction of the coefficient of diffusion or the permeability, as well as the porosity, decreases the transfer ability of the porous material (either for CO<sub>2</sub> or water or even both). The last parameter is the  $m$  factor from the desorption isotherm (Equation (3)). A decrease in this parameter rises the desorption isotherm curve in a (RH;  $S_r$ ) plot, meaning that for the same hydric state (governed by the water pressure, and therefore the RH), the saturation degree  $S_r$  is higher. This reduces the gaseous phase in the pores, where the CO<sub>2</sub> diffuses, and thus decelerates the carbonation process.

## 6. Conclusions and perspectives

In this paper, we proposed a probabilistic finite element model for carbonation under variable conditions of temperature, RH and CO<sub>2</sub> concentration. This model allows us to determine the reliability index of RC structures exposed to a risk of corrosion induced by the cement paste carbonation and climate change. We calculated this reliability index for six cities in France corresponding to different kinds of climate (oceanic, Mediterranean and continental) according to several scenarios of climatic changes.

This study has shown that carbonation is very sensitive to local climate. There are locations with a large carbonation risk for which current environmental conditions could accelerate corrosion

initiation (Marseille). A specific design improvement and/or adaptation strategy should be considered for these climates. There are also other climates for which carbonation risks are lower for an optimistic climate change scenario but could be significantly increased for the most pessimistic scenario (Paris and Toulouse). These results highlight the importance of considering the climate evolution in lifetime assessment to predict, as precisely as possible, carbonation risks. This study has also shown that in first approach, the most influent parameter on the structural safety remained the concrete cover thickness, more than materials properties (such as porosity, permeability, diffusion coefficient or desorption isotherm). This work appeals in-depth studies about a comprehensive characterisation of the probability distributions of the random variables. Also the correlations between the materials properties involved in the degradation processes could be considered. Another final improvement is the selection of a threshold defining the carbonation depth and its relationship with effective corrosion initiation.

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