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Strain-induced crystallization of carbon black-filled natural rubber during fatigue measured by in situ synchrotron X-ray diffraction

S. Beurrot-Borgarino, B. Huneau*, E. Verron, P. Rublon

LUNAM Université, Ecole Centrale de Nantes, GeM, UMR CNRS 6183, BP 92101, 44321 Nantes cedex 3, France

Natural rubber (NR) exhibits great fatigue properties which are usually explained by its ability to crystallize under strain. Nevertheless, strain-induced crystallization of NR in fatigue has never been investigated. We perform original in situ fatigue tests during which the degree of crystallinity, and the number and volume of crystallites are measured by synchrotron wide angle X-ray diffraction. For all loading conditions, the number of crystallites is constant. The evolution of their volume depends on the minimum stretch ratio achieved at each cycle. The results show that cyclic loading conditions modify the macromolecular structure of the material, in particular of its amorphous phase. Keywords: Rubber Experimental technique Strain-induced crystallization Synchrotron WAXD

1. Introduction

Natural rubber (NR, cis-1,4-polyisoprene) vulcanizates have the ability to crystallize under strain at room temperature. Strain-induced crystallization (SIC) of NR has been discovered by Katz in 1925 with the help of X-ray diffraction [1]. This technique has since permitted to obtain the crystallographic data of NR [2,3], to exhibit the existence of stretch ratio thresholds of crystallization and melting of the crystallites [4,5], to relate SIC to the mechanical hysteresis of the stress–strain response [6,4], and to put into light the effect of fillers such as carbon black [7]. For more details on the use of X-ray diffraction for SIC in NR, the reader can refer to the recent review of Huneau [8].

The great majority of the studies on SIC of NR focus on uniaxial quasi-static cycles and relaxation tests. Here, the expression "quasi-static" stands for low strain rates compared to crystallization rate. But NR is often used in engineering applications for its great properties in fatigue such as long fatigue life, even at large strain [9–11]. The mechanical properties of NR have been thoroughly studied [12–14]; but studies on the evolution of SIC during fatigue testing of NR are very rare, though it is often accepted that the remarkable fatigue properties are closely related to SIC. This is mainly because the typical frequencies of fatigue tests (1 Hz or more) are not compatible with the long time acquisition required by X-ray diffraction measurements (from a few seconds to an hour). Nevertheless, Kawai succeeded in measuring SIC during fatigue by using a stroboscopic technique to accumulate the weak intensity of the

diffracted beam over a large number of cycles [15]. He studied only one set of loading conditions for which both minimum and maximum stretch ratios achieved are 3.5 and 4.5, respectively. In this case, he observed an increase in the degree of crystallinity with the number of cycles. Furthermore, Rouvière et al. recently measured the evolution of crystallinity along fatigue life for different uniaxial loading conditions by performing interrupted fatigue tests [16]. Nevertheless, this method does not allow to separate SIC induced by fatigue from SIC induced by constant stretching during the 45-min acquisition of the X-ray diffractogram.

The aim of the present study is to measure the evolution of the strain-induced crystallinity during fatigue of carbon black-filled NR and to determine the mechanisms that drive this evolution. For this purpose, we developed an innovative experimental method which allows to measure SIC in real time during a fatigue experiment. In-situ wide angle X-ray diffraction (WAXD) measurements are performed with a very short exposure time achieved thanks to synchrotron radiation. Thanks to the results obtained, we highlight the key role of the melting stretch ratio and we propose two mechanisms of SIC in NR fatigue depending on loading conditions.

2. Experimental method

2.1. Material and samples

The material used in this study is a carbon black-filled natural rubber, cross-linked with 1.2 phr (per hundred of rubber) of sulphur and CBS accelerator. It also contains ZnO (5 phr) and stearic acid (2 phr) and is filled with 50 phr of N330 carbon black. The

^{*} Corresponding author. Tel.: +33 2 40 37 68 82; fax: +33 2 40 37 25 66. *E-mail address*: bertrand.huneau@ec-nantes.fr (B. Huneau).

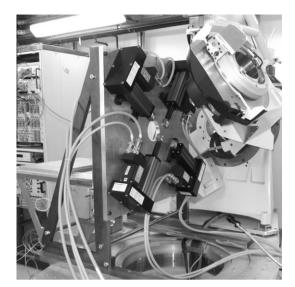


Fig. 1. Uniaxial fatigue machine in DiffAbs beamline.

samples are classical flat dumbbell specimen with a 10 mm gauge length and a 2×4 mm 2 section.

2.2. Testing machine

Experiments have been conducted with the homemade stretching machine shown in Fig. 1. It is composed of four electrical actuators, but only two opposite ones were used in this study. Their movements are synchronized, in order to keep the centre of the specimen fixed during the fatigue tests. Their loading capacity is ±500 N and their stroke is 75 mm each.

2.3. Procedures

2.3.1. Accommodation

In order to lower the residual stretch ratio of the sample due to Mullins effect and viscoelasticity, all the samples are pre-cycled just before testing: 5 cycles at a higher strain level than during fatigue tests for Mullins effect (maximum displacement of the clamps is 45 mm, except for fatigue test No. 4 described hereafter, before which the maximum displacement is 50 mm); additional 50 cycles for viscous effect (at the same displacements of the clamps than during the fatigue tests).

2.3.2. Preliminary quasi-static experiment

A quasi-static test is beforehand conducted to determine (i) the relation between the stretch ratio λ and the displacements of clamps which will be used in all other experiments and (ii) the stretch ratio thresholds of crystallization λ_C and melting λ_M of the material at room temperature and low strain rate (similarly as in [17]). During these experiments, the sample is elongated of 90 mm at the speed 0.012 mm s⁻¹, the total duration of the cycle being about 2 h. A scattering pattern is recorded every 98 s. The local stretch ratio λ at the centre of the sample is *a posteriori* measured continuously by video extensometry. Finally, this experiment is a quasi-static test from λ = 1 to λ = 4 at λ = 1.1 × 10⁻³ s⁻¹, and it leads to λ_C = 2.36 on the loading path and λ_M = 1.80 on the unloading path.

2.3.3. Fatigue experiments

The fatigue tests are conducted by prescribing triangular displacements of the clamps. They are performed at conventional frequencies for rubber, i.e. around 1 Hz, which limit self-heating

Table 1 Fatigue loading conditions.

Test No.	d_{\min} (mm)	d_{\max} (mm)	λ_{\min}	λ_{max}	f (Hz)
1	0	20	1.00	2.90	2.5
2	4	33.2	1.44	3.66	0.8
3	9.3	33.2	1.98	3.66	1
4	25	45	3.18	4.02	1.5

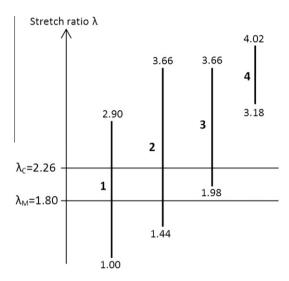


Fig. 2. Minimum and maximum stretch ratios reached during fatigue tests and threshold stretch ratios for crystallization λ_C and melting λ_M . Bold numbers stand for the fatigue tests numbers.

to about 3° only [18]. As the minimum exposure time to record a diffraction pattern is 1 s (about the duration of a full cycle), it is not possible to record the diffraction patterns while the actuators are in motion. Therefore, to measure the evolution of SIC during fatigue testing, the tests are paused at maximum displacement every 250 cycles to record a complete diffraction pattern. As the fatigue machine is triggered by the monitoring system of the X-ray beam, the duration of the pause is less than 1.5 s. The first scattering pattern is recorded during the first cycle of the test.

Four different fatigue tests have been performed. Table 1 presents the corresponding minimum and maximum displacements of the clamps d_{\min} and d_{\max} , the corresponding minimum and maximum stretch ratios λ_{\min} and λ_{\max} and the loading frequency f. To summarize the fatigue tests, Fig. 2 presents the loading conditions in terms of stretch ratios, and compares them to the thresholds of crystallization λ_C and melting λ_M (measured during the preliminary experiment).

2.3.4. Relaxation experiments

The relaxation tests consist in quickly stretching a sample to a given stretch ratio and then maintaining the same stretch level. They last 28 min and scattering patterns are recorded every 2 min. Table 2 presents the stretch ratios at which the three relaxation experiments are conducted. The stretch rate λ of the loading path is between 5.6 and 6.0 for the three tests.

Table 2Relaxation loading conditions.

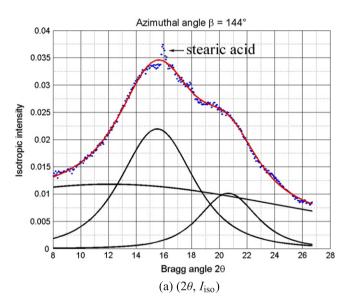
Test No.	λ
5	2.41
6	2.90
7	3.66

2.4. Synchrotron

The synchrotron measurements have been carried out at the DiffAbs beamline in the French national synchrotron facility SOL-EIL. The wavelength used is 1.319 Å and the beam size is 0.3 mm in diameter at half-maximum. The 2D WAXD patterns are recorded by a MAR 345 CCD X-ray detector. The exposure time is 1 s (minimum time to record a workable scattering pattern) for the fatigue and relaxation tests. For the low strain rate cycle test, it is set to 2 s in order to enhance the accuracy of the measurements. A PIN-diode beam stop was used in order to make an accurate correction of air scattering.

2.5. Scattering pattern analysis

In this study, we consider large angle scattering: the range of diffraction angles is $2\theta \in [8^{\circ}, 26.7^{\circ}]$. We used the (012) reflections of Cr_2O_3 powder placed on each side of a specimen to calibrate the diffraction angles 2θ (a = 4.9590 Å and c = 1.3596 Å). Moreover, we follow the well-established correction method of Ran et al. [19]: an



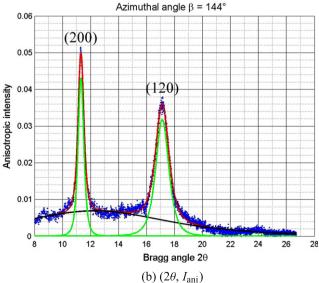


Fig. 3. Examples of deconvolution of diffraction diagrams fitted by series of Pearson functions.

air scattering pattern (without sample) was first collected and has been used to correct the patterns, and the change in thickness of the sample under extension and the change in intensity of the incident photons have also been considered. Once the corrections performed, the intensity of photons diffracted by the isotropic phases in the material $I_{iso}(2\theta)$ is extracted from the diffraction patterns by considering the minimum intensity along the azimuthal angle β for each Bragg angle 2θ . Then, the intensity of photons diffracted by the anisotropic material $I_{ani}(2\theta,\beta)$ is calculated as the difference between the total intensity of photons diffracted $I_{\text{total}}(2\theta, \beta)$ and $I_{\rm iso}(2\theta)$. The diffraction diagrams extracted from $I_{\rm ani}(2\theta,\beta)$ and $I_{\rm iso}(2\theta)$ are classically fitted by series of Pearson functions [20,17,21,4]. Figs. 3a and b present examples of fitting and deconvolution of diffraction diagrams $(2\theta, I_{iso})$ and $(2\theta, I_{ani})$ respectively. With these quantities, it is possible to calculate: an index of crystallinity, an index of the mean volume of crystallites, and an index of number of crystallites.

2.5.1. Crystallinity

The index of mass crystallinity χ is calculated as follow:

$$\chi = \frac{\mathcal{I}_{\text{cryst}}}{\mathcal{I}_{\text{cryst}} + \mathcal{I}_{\text{amorph}}} \tag{1}$$

where $\mathcal{I}_{\text{cryst}}$ is the integrated intensity of the (120) and (200) Bragg reflections of NR measured on one diffraction diagram $(2\theta, I_{\text{ani}})$ and $\mathcal{I}_{\text{amorph}}$ is the integrated intensity of the amorphous halo at the same diffraction angle, assumed equal to the integrated intensity I_{iso} .

2.5.2. Mean volume of crystallites

An index of the mean volume of the crystallites $\overline{V}_{\text{cryst}}$ is calculated from the crystallites size in three different directions:

$$\overline{V}_{\text{cryst}} = l_{200} \cdot l_{120} \cdot l_{201} \tag{2}$$

where the mean crystallites size l_{hkl} is deduced from the Scherrer formula [22]:

$$l_{hkl} = \frac{K\lambda}{\text{FWHM}_{2\theta}\cos\theta} \tag{3}$$

in which I_{hkl} is the crystallites size in the direction normal to the hkl diffraction plane, K is a scalar which depends on the shape of the crystallites (here we adopt 0.78 as in [17]), λ is the radiation wavelength, θ is the Bragg angle and FWHM $_{2\theta}$ is the full width at half-maximum of the peak hkl in a diffraction diagram $(2\theta, I_{ani})$.

2.5.3. Number of crystallites

Assuming the incompressibility of the material and that the volume crystallinity is equal to the mass crystallinity, we calculate an index of number of crystallites per unit of undeformed volume N_{cryst} :

$$N_{\rm cryst} = \frac{\chi}{\overline{V}_{\rm cryst}} V_{\rm irradiated} = \frac{\chi}{\overline{V}_{\rm cryst}} \frac{\pi R^2 t_0}{\sqrt{\lambda}} \tag{4}$$

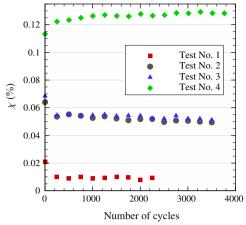
where $V_{\text{irradiated}}$ is the volume irradiated by the X-ray beam, R is the radius at half-maximum of the beam, t_0 is the thickness of the sample in the undeformed state and λ is the stretch ratio.

3. Results and discussion

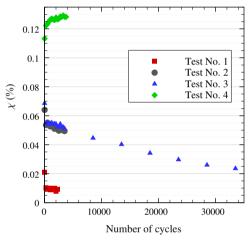
3.1. Evolution of crystallinity during fatigue tests

The evolution of the index of crystallinity (measured at maximum deformation) during fatigue tests for different strain levels is shown in Fig. 4.

As expected, larger is the strain, higher is the crystallinity. During the three fatigue tests with the lowest minimum and



(a) During the first 4,000 cycles.

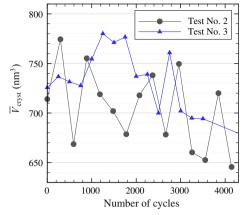


(b) During the first 35,000 cycles of test No. 3.

Fig. 4. Evolution of the crystallinity index during fatigue tests.

maximum strain levels (tests No. 1, 2 and 3), the index of crystal-linity decreases (of 15–50%) during the first 250 cycles, and then continues to decrease at a lower but constant rate until the end of the tests. During fatigue test No. 4, which minimum and maximum strain levels are much higher (see Fig. 2), the evolution of the index of crystallinity is very different: χ increases with the number of cycles (of about 13% during the first 4000 cycles). This result is in agreement with those of Kawai [15] obtained during a fatigue test at $\lambda_{\rm min}=3.5$ and $\lambda_{\rm max}=4.5$. It is to note that the results shown in Fig. 4a only correspond to the first 4000 cycles, but fatigue test No. 3 was performed during 35,000 cycles as shown in Fig. 4b and we observe that χ decreases at a constant rate during the whole test, down to about $\chi=2\%$ in comparison with $\chi=7\%$ at the beginning of the test.

As mentioned above, the fatigue tests were performed by prescribing constant maximum and minimum displacements of the clamps. As the material is cycled, the strain level reached at a given displacement of each cycle decreases, because the reference length of the sample at zero-stress increases with the number of cycles due to Mullins and viscous effects. This phenomenon is reduced by the accommodation of the material, but it cannot be completely suppressed. Thus, all results of the fatigue tests are obtained for a constant maximum displacement which corresponds to a decreasing maximum strain level. As shown in Fig. 2, fatigue tests No. 1 and 2 are performed with minimum stretch ratios lower than λ_M .



(a) Volume of the crystallites

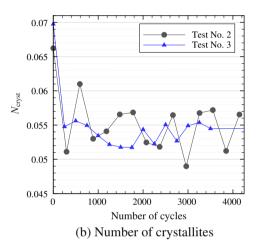


Fig. 5. Evolution of the crystallites during fatigue tests No. 2 and 3.

Moreover, even if the initial minimum stretch ratio in the fatigue test No. 3 is slightly higher than λ_M , it becomes lower after a few cycles only. So, for these three tests, the same phenomenon takes place during each cycle: all the crystallites melt when the minimum displacement is reached, and new crystallites nucleate when the sample is stretched again; and χ decreases with the number of cycles. For fatigue test No. 4, the minimum stretch ratio reached at each cycle decreases with the number of cycles as well, but it is always greatly larger than the threshold of crystallization λ_C , and then than the threshold of melting λ_M .

Finally, three cases can be highlighted:

- The maximum stretch ratio in one cycle λ_{max} is lower than the threshold of crystallization $\lambda_{C}: \chi$ remains equal to 0.
- λ_{max} is higher than λ_{C} and the minimum stretch ratio in one cycle λ_{min} is lower than the threshold of melting λ_{M} : all crystallites melt at each cycle and the maximum crystallinity index decreases with the number of cycles. This is the case of tests No. 1, 2 and 3.
- λ_{\max} is higher than λ_C and λ_{\min} is higher than λ_M . During the cycles, some crystallites never melt: the maximum crystallinity index reached in each cycle increases with the number of cycles. This is the case of the test No. 4.

As the change in crystallinity can be induced by the change in the mean number of crystallites and/or the change in the mean volume of crystallites, the two latter aforementioned cases will be analyzed in terms of these quantities.

3.2. $\lambda_{max} > \lambda_C$ and $\lambda_{min} < \lambda_M$: Tests No. 2 and 3

In this section, only tests No. 2 and 3 are considered because the diffraction diagrams for test No. 1 are too noisy to be analyzed due to a very small degree of crystallinity. Similarly, only the first 14,000 cycles of test No. 3 are considered. The evolution of the mean volume of the crystallites and of the number of crystallites is shown in Fig. 5a and b respectively. It shows that the mean volume of crystallites decreases continuously with the number of cycles. Their number decreases during the first 250 cycles, and is then constant. We observe the same evolution of both quantities for higher number of cycles as illustrated by the results for fatigue test No. 3 given in Fig. 6. Thus, the decrease in crystallinity shown in Fig. 4 is due to the simultaneous decrease in volume and number of crystallites at the beginning of the tests (250 cycles), and only to the decrease in size for further cycles. Recalling that all crystallites melt at the end of each cycle, it means that at each cycle the newly nucleated crystallites are smaller than the ones nucleated and melted during the previous cycle. It is to note that the decrease of \overline{V}_{cryst} with the number of cycles is not explained by the decrease of λ_{max} . Indeed, during quasi-static tests the lower the strain, the higher the size of the crystallites as shown in [17,23–26]; similar results have been obtained for strain rates similar to those of the present fatigue tests [27]. Moreover, results are the same for tests No. 2 and 3 which are performed at the same maximum stretch ratio $\lambda_{\max} > \lambda_C$ but two different minimum stretch ratios $\lambda_{\min} < \lambda_M$. Then, it suggests that when the minimum stretch ratio is smaller than the threshold of melting, the value of this minimum stretch ratio does not influence how the material crystallizes at minimum deformation.

As a summary: (i) \overline{V}_{cryst} and χ depend on the number of cycles and (ii) N_{cryst} , \overline{V}_{cryst} and χ at λ_{max} do not depend on λ_{min} when inferior to λ_{M} . These observations can be interpreted in the following way:

- The mechanical loading history has no effect on the material for strain smaller than λ_M .
- The mechanical loading history modifies the material for strain larger than λ_C . Indeed, as the crystallites evolve in time for the same loading conditions, it indicates that the macromolecular structure of the material changes from one cycle to another.
- Our experiments show that the crystalline phase of NR is different from one cycle to another, eventhough the mechanical conditions are similar; at each cycle, the crystalline phase totally

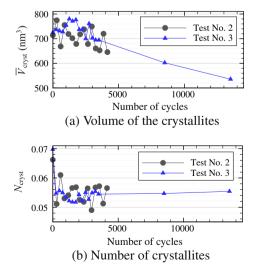


Fig. 6. Evolution of the crystallites during fatigue test No. 2 and the 14,000 first cycles of fatigue test No. 3.

melts and reappears differently at the next cycle. Thus, it suggests that the amorphous macromolecular structure of the material changes along fatigue testing.

3.3. $\lambda_{\text{max}} > \lambda_C$ and $\lambda_{\text{min}} > \lambda_M$: Test No. 4

During fatigue test No. 4, for which the stretch ratio always remains greater than λ_C , the crystallinity index increases with the

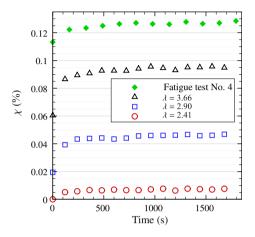
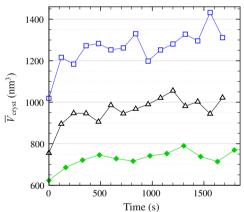


Fig. 7. Evolution of the crystallinity index χ with time during fatigue test No. 4 and relaxation tests. The stretch ratios λ at which the relaxation tests are performed are given in the legend.



(a) Volume of crystallites (see (b) for legend).

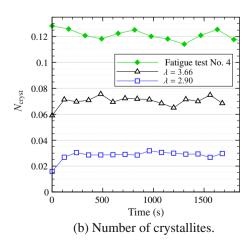
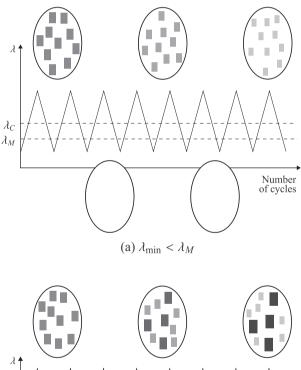


Fig. 8. Evolution of the crystallites during fatigue test No. 4 and relaxation tests. Legends of (a) and (b) are the same and only given in (b) for clarity. The stretch ratios λ at which the relaxation tests are performed are given in the legend.

number of cycles. Yet, it is well-established that crystallinity increases as well during relaxation experiments when the stretch ratio is higher than λ_{C} [28,29]. One can wonder whether the increase of crystallinity during fatigue is related to its evolution during relaxation, and in which ways. On this purpose the relaxation experiments described in Section 2.3.4 are conducted. Fig. 7 presents the evolution of the index of crystallinity in time for the fatigue test No. 4 and relaxation experiments. As expected, χ increases during relaxation because the stretch ratio is maintained higher than the threshold of crystallization λ_{C} and the equilibrium state is very long to achieve.

Fig. 8 presents the evolution of the volume of the crystallites and their number for both test No. 4 and two relaxation tests. Quantitatively, both volumes and numbers highly differ from one test to another. These differences are due to the values of $\lambda_{\rm max}$ for each test: the higher the stretch ratio, the smaller and the more numerous the crystallites, as exhibited in [23,25]. For all the tests, the volume increases in time, and this increase is higher during relaxation than during fatigue (about +20% for fatigue test and +33% for both relaxation tests). Moreover, the number of



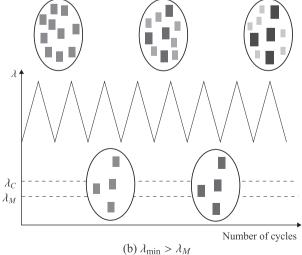


Fig. 9. Scenario of crystallization under different fatigue loading conditions. The ovals stand for a unit volume of material. The ones at the top of the figures represent the material at maximum strain whereas the ones at the bottom represent the material at minimum strain. The grey rectangles stand for the crystallites and the larger the crystallite, the larger and darker the rectangle.

crystallites seems to be constant for the fatigue test whereas it slightly increases at the beginning of the relaxation tests then remains constant.

During the fatigue test No. 4, because the stretch ratio is always larger than λ_M we think that the most probable scenario is as follow. Two families of crystallites coexist, and at each cycle:

- some crystallites do not melt. They evolve during the whole fatigue test as crystallites in NR subjected to relaxation: their volume increases in time,
- the other crystallites disappear; new ones will nucleate during the next cycle. Those crystallites behave as during fatigue tests No. 2 and 3: their volume decreases from one cycle to another.

The sum of the number of crystallites of both families is constant. As shown in Figs. 5 and 8 the increase in volume during relaxation is higher of more than one decade than the decrease in volume during fatigue tests No. 2 and 3. Assuming that the change in crystallites volume of each family follows the same trend as for relaxation and fatigue tests No. 2 and 3, respectively, the mean volume of crystallites increases during fatigue test No. 4 and then it explains the increase of crystallinity during this test. It must be noted that as in fatigue tests No. 2 and 3, the macromolecular structure of the material (including of the amorphous phase) is modified in time during test No. 4 and then some crystallites which did not melt during a large number of cycles may eventually melt because of the evolution of the mechanical state of the neighbouring macromolecules. Similarly, some crystallites may nucleate after a large number of cycles and not melt afterwards.

4. Conclusion

In this study, we developed an original experimental method to measure in real time the evolution of strain-induced crystallization of NR during fatigue by in situ synchrotron WAXD. The main results are twofold. First, the number of crystallites per unit volume measured at maximum strain is constant during fatigue. Second, the minimum stretch ratio reached at each cycle λ_{\min} as compared to the threshold of melting λ_M drives the evolution of the mean volume of crystallites and therefore of the degree of crystallinity: if $\lambda_{\min} < \lambda_M$ the mean volume and the crystallinity decrease with the number of cycles, whereas if $\lambda_{\min} > \lambda_M$ they increase.

To explain those results, we propose the crystallization scenario detailed in Section 3; a simplified scenario, which shows only the main phenomena occurring during fatigue, is summarized in Fig. 9. We believe that this unexpected behaviour may be due to a modification of the macromolecular structure of the material, and especially of its amorphous phase, induced by cyclic loading conditions. The origin of this modification is not clarified yet: does the strain-induced crystallization change the macromolecular structure of the amorphous phase? If yes, does it explain the great fatigue strength of crystallizable elastomers [9,30,10,31]?

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