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Subsampling and homogenization to investigate variability of composite material mechanical properties

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A B S T R A C T

This paper presents an innovative homogenization sampling technique applied to multiscale modelling of composite materials. The goal is to build efficiently statistical variability of mechanical properties at mesoscopic scale from the heterogeneous media analysis at microscopic scale. It is applied to the transverse elastic properties of a unidirectional Long Fibres Reinforced Composite (LFRC). A large representative part of the ply – the cell – is modelled from a micrography and studied at microscopic scale with the Finite Element Analysis (FEA) under 2D plane strain hypothesis. The study consists in estimating the effective elastic properties of subcells, subparts of the previous cell, thanks to a specifically developed numerical procedure.

A unique calculation is computed on the entire ply reduced to three basic loading cases is applied to the cell. Subsamples taken into the simulation cell are homogenized at post-processing level of strain and stress fields. A standard mechanics approach was considered. Various subsampling schemes are performed with various size and spatial distribution to generate variability functions of effective elastic properties at mesoscopic scale. A statistical inference is highlighted: the variability parameters vary with the way of sampling. Dispersion functions are finally obtained and discussed.

Keywords:

Structural composites
Elastic properties
Finite Element Analysis (FEA)
Multiscale modeling
Probabilistic methods

1. Introduction

1.1. Working context

The objective of this work is to develop an efficient way to obtain and characterise the variability of the mechanical properties at intermediate scale between microscopic and mesoscopic scale taking into account the variability of the mechanical properties at od constituents; the microscopic to mesoscopic variability transport, see Fig. 1(c), is particularly adressed in this paper. As explored in [5], the approach can be transposed from the mesoscale to the macroscale. Then, knowing the variability at different scale through distributions functions, the authors are furtherly interested by performing reliable analysis. The present paper focuses on investigations concerning linear elastic properties variability with the view to work laterly on stresses, damage, failure singularities and non linear behaviour. The starting point is a morphological analysis realized on a micrography of a unidirectional long fibre ply microstructure extracted from a stratified LFRC. A FE mesh of the microstructure representative of a real material configuration is then realised. A FEA is applied to compute strongly heterogeneous strain and stress fields.

Many authors developed homogenization techniques to get the effective properties of heterogeneous materials. Most of the time, the Representative Volume Element (RVE) concept is considered [15,10,11]: studying a large enough part of the material gives a global estimation of a given effective property. In [1], homogenization is performed under RVE size and depicts variability of behaviour. To get suitable elastic properties, two criteria have to be verified: the inter scales energy equivalence depicted by the so-called Hill lemma [7,17] and the convergence of effective properties depending on the size of homogenized volume. The energy criterion is verified for smaller volumes than these needed for properties convergence [19]. Other authors [18,4] worked on cells smaller than the RVE – that are called here subcells – and developed statistical approaches to obtain global effective properties from the effective properties of a large population of subcells.

The RVE or the statistical subcells are usually exploited with FEM models [8,3,16]. Various homogenization techniques are numerically performed to obtain bounds or statistical moments of effective properties, at least average values. Kinematic Uniform Boundary Conditions (KUBC), Stress Uniform Boundary Conditions (SUBC) or Mixed Boundary Conditions (MBC) are the easiest to compute. Periodic Boundary Conditions give a better accuracy on the effective properties and can advantageously be applied regardless on the geometry of the medium but are not trivial to implement in a FEA tool. All boundary conditions applied in works cited before lead to energetically accurate estimation of effective properties; in

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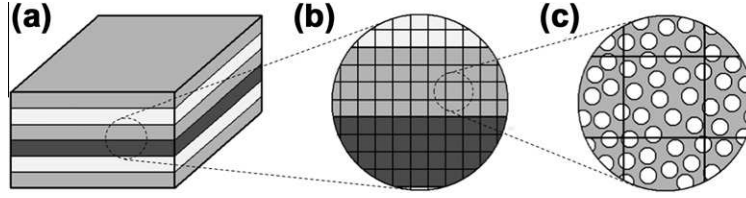


Fig. 1. (a) Laminate composite, (b) detail of a ply meshing at mesoscopic scale with homogeneous elements and (c) detail of heterogeneous microstructure with fibres and matrix.

case of non periodic loading conditions, some precautions have to be taken to ensure the estimation validity.

In order to get the variability of elastic properties at mesoscopic scale for a scale length inferior to the RVE size, a statistical approach on subcells is realized. One FEM simulation is usually performed on each subcell [4]. It leads to unreasonable computing times as huge number of subcells is required to assess the first statistical moments. To reduce the amount of FEA calculations, a sampling procedure performed at post-processing level and including standard homogenization on non-periodic geometry is developed in this work. It is inspired from morphological analysis of random heterogeneous media [12,13] and has been performed in [1] with only regular spatial repartition. Distribution functions of effective elastic properties are obtained and discussed depending on the subsampling scheme for a statistical inference issue, historically explored in geostatistics [14].

1.2. Investigation method

The starting point is a micrograph of a LFRC transverse section ply. Under invariance hypothesis in fibre direction, the study can be restricted to a 2D plane strain analysis. On this micrograph, a random organisation of carbon fibres in epoxy matrix is observed. This micrograph is considered representative of the material microstructure. It is transformed into a FE mesh which defines the so-called cell.

The final point is to obtain the statistical distributions describing the dispersion of the effective elastic properties of smaller zones taken in the ply, the subcells, selected through a subsampling procedure. Their size correspond to a predefined discretization of the ply and consequently the cell, for example a mesoscopic FE mesh as seen Fig. 1(c).

The micrograph is digitized and a threshold is performed on grey levels to generate a FEM mesh of the microstructure. Only three basic loading cases are performed under 2D plane strain hypothesis for the whole work, Section 2. The subsampling procedure is achieved at post processor level on FE strain and stress computed before. A numerical nonperiodic homogenization is performed on subcells following random or organized sampling schemes, Section 3.

Subsampling presents many advantages compared to studies involving virtual material and Monte Carlo procedure. The potential number of subcells to be characterised is wide and directly linked to the resolution of the starting micrograph. Moreover subcells don't need to be virtually generated as they are various parts of the meshed simulation cell: they are morphologically representative of the microstructure of the ply.

2. Hill-Mandell numerical homogenization on nonperiodic geometry

2.1. Standard mechanics approach

The following formalism describes the standard mechanics to obtain effective properties of an heterogeneous medium. It is inspired from [10,9].

Considering a subcell Ω taken in the heterogeneous medium, an average operator $\langle \cdot \rangle^\Omega$ or $\bar{\cdot}$ is applied to any spatial function defined on the domain, most particularly to stress and strain fields in mechanical applications. Using the Voigt indices contraction convention, stress σ and strain ϵ are written as column matrices and behaviour operators C or S as square matrices. The goal is to estimate the effective stiffness C_{eff} defined Eq. (1).

$$\bar{\sigma}^\Omega = C_{eff}^\Omega \bar{\epsilon}^\Omega \quad (1)$$

The strain and stress fields are decomposed in their average part and a second part called here the perturbation field; for example strain field is decomposed Eq. (2).

$$\epsilon = \bar{\epsilon}^\Omega + \tilde{\epsilon}^\Omega \quad (2)$$

A microstructure localization tensor M^Ω is introduced Eq. (3) to link the perturbation and average strain fields, adapted from literature [9].

$$\tilde{\epsilon}^\Omega = M^\Omega \bar{\epsilon}^\Omega \quad (3)$$

The localization tensor is injected in the local behaviour equation. The average of behaviour relation gives an explicit expression of the effective stiffness explained Eq. (4).

$$C_{eff}^\Omega = \langle C + CM^\Omega \rangle^\Omega \quad (4)$$

It is highlighted that the localization tensor can present minor symmetries $M_{ijkl} = M_{jikl} = M_{ijlk}$ in agreement with Voigt convention, but not generally major symmetry $M_{ijkl} = M_{klij}$. Consequently, the symmetry of behaviour tensor C_{eff}^Ω can be affected as evoked in [9], in conflict with the definition of thermodynamic potentials in the elastic behaviour.

The same method being applied to stress fields, defining the concentration operator L^Ω , the effective compliance S_{eff}^Ω is explained Eq. (5).

$$S_{eff}^\Omega = \langle S + SL^\Omega \rangle^\Omega \quad (5)$$

The effective properties tensor could be directly obtained from average strain and stress fields, inverting the local behaviour relation. But the calculation of localization and concentration tensors allows to compute the effective properties through various ways and to verify the relevance of numerical results.

2.2. Energy balance: Hill lemma

The advantage of the general approach is that it can be applied regardless of any hypothesis on fields' properties or scale decoupling, the effective operators depending on the average values of fields. Both of them should conform to the scale energy balance characterized by the Hill lemma explained in Eq. (6). Using Voigt convention, the elastic strain energy volume density is half the scalar product of strain and stress columns. The reference to cell Ω is not used laterly to simplify mathematical notations.

$$\langle \sigma \cdot \epsilon \rangle = \bar{\sigma} \cdot \bar{\epsilon} \quad (6)$$

' \cdot ' defining the scalar product.

In our case, it is easily proved that the averages of perturbation fields are equal to zero. The average energy on the cell is then developed, simplified and expressed Eq. (7).

$$\langle \sigma \cdot \epsilon \rangle = \bar{\sigma} \cdot \bar{\epsilon} + \langle \tilde{\sigma} \cdot \tilde{\epsilon} \rangle \quad (7)$$

In standard homogenization techniques, the average of perturbation elastic strain energy is null, given the uniform or periodic boundary conditions or fields analytical conformation. In our case, there are no guaranties that it is true. The subsampling conditions are investigated to verify the energy balance. An energy error indicator is defined Eq. (8). It is simply the ratio between perturbations product and averages product. The energy balance is considered verified when the error energy is small enough.

$$eR = \frac{\langle \tilde{\sigma} \cdot \tilde{\epsilon} \rangle}{\bar{\sigma} \cdot \bar{\epsilon}} \quad (8)$$

2.3. Numerical procedure

Basic triangle elements with linear interpolation are used for the FEA. They are not very accurate for strain and stress field calculation but are consequently the easiest to develop our post-processing tools. A mesh refinement naturally increases the quality of FE analysis without penalizing the numerical procedure. The FE simulations are realized under (\vec{e}_1, \vec{e}_2) plane strain hypothesis which suggest geometry invariance along the fibres direction. Strain and stress tensors are 3×1 columns and stiffness, compliance, localization and concentration tensors 3×3 matrices. For example, the strain is given Eq. (9).

$$\epsilon = \begin{bmatrix} \epsilon_{11} \\ \epsilon_{22} \\ \epsilon_{12} \end{bmatrix} = \begin{bmatrix} \epsilon_1 \\ \epsilon_2 \\ \epsilon_6 \end{bmatrix} \quad (9)$$

For a given subcell Ω , the mesh is tested to identify the elements inside or intersecting the domain, as shown Fig. 2. Considering each selected element E_i^Ω , its intersected surface $S_i^\Omega(E_i^\Omega)$ is calculated through basic geometric operations.

The average estimation on subcell Ω for any spatial functions is expressed with a discrete weighted sum. For instance the average strain is given Eq. (10) and contains only surfaces and integration point values.

$$\bar{\epsilon}^\omega = \frac{1}{\sum_{E_i^\Omega \cap S_i^\Omega(E_i^\Omega)} \sum_{E_i^\Omega} S_i^\Omega(E_i^\Omega) \epsilon(E_i^\Omega)} \quad (10)$$

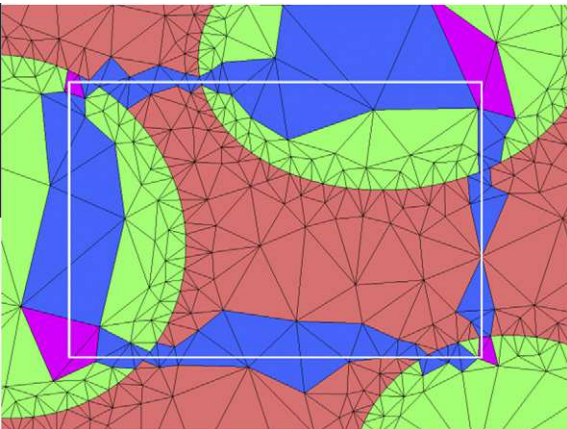


Fig. 2. Detail of heterogeneous meshing of fibres (green) and matrix (red) and identification of intersecting elements with one single boundary (blue) or a corner (purple). (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)

Perturbation fields are then computed.

The effective stiffness tensor is assessed with a discrete sum on cell Ω , as expressed in Eq. (11).

$$C_{eff}^\Omega = \frac{1}{|\Omega|} \sum_{\Omega} C(E_i^\Omega) + C(E_i^\Omega) M_i^\Omega \quad (11)$$

With the same method applied to stress fields and concentration tensors we obtain the effective compliance. In the two cases, we need to know the local tensors to explain the effective properties.

Three unit loading cases subscripted *I*, *II* and *III* are applied to the heterogeneous cell by kinematic conditions on the boundaries: (i) traction along \vec{e}_1 direction with global strain E^I , (ii) traction along \vec{e}_2 with global strain E^{II} and (iii) a plane shearing with global strain E^{III} . These three cases constitute a complete basis of loadings in the three dimensions loading linear space.

By convenience, a matrix representation of the local fields for the three basic loading cases is adopted for further identification processes. Local strain total matrix is given Eq. (12).

$$\epsilon_{[tot]} = [\epsilon^I \quad \epsilon^{II} \quad \epsilon^{III}] = \begin{bmatrix} \epsilon_1^I & \epsilon_1^{II} & \epsilon_1^{III} \\ \epsilon_2^I & \epsilon_2^{II} & \epsilon_2^{III} \\ \epsilon_6^I & \epsilon_6^{II} & \epsilon_6^{III} \end{bmatrix} \quad (12)$$

Perturbation fields are concatenated this way and the localization tensor is identified as explained in Eq. (13).

$$M_i^\Omega = \tilde{\epsilon}_{i[tot]} \bar{\epsilon}_{[tot]}^{-1} \quad (13)$$

In order to validate the numerical performance of this procedure, it is applied to a square periodic microstructure of fibres in matrix submitted to periodic loading conditions. This configuration is commonly used in multiscale modelling of composite materials. In our case, the simulation cell contains four fibres as seen Fig. 3 to sample various locations of the homogenization subcell. The micro/meso energy balance is systematically verified with periodic fields, the average of perturbations product being equal to zero [9]. This is one reason why most of homogenization approach use periodic boundary conditions on RVEs.

The influence of mesh refinement parametrized by the number of nodes on edges was investigated: three simulation cells were build with 20, 50 and 100 nodes on edges as seen Fig. 3. The homogenization subcells are squares, a quarter of the total cell

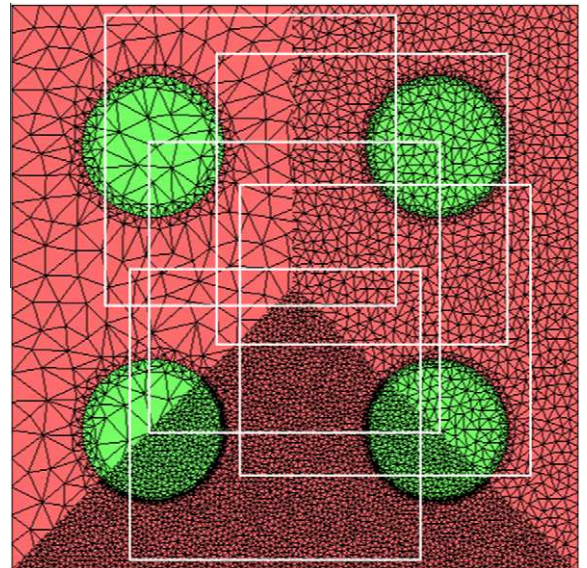


Fig. 3. Mesh refinement of the periodic cell with four fibres, 20, 50 and 100 nodes on boundaries and various homogenization subcells location (white squares).

Table 1
Influence of meshing refinement on the estimation of effective properties.

N_{elts}	C_{11}	C_{22}	C_{12}	C_{21}	C_{66} [MPa]
20	12777	12778	7893	7893	2153
50	12839	12834	7871	7869	2174
100	12789	12789	7788	7788	2158

square, each containing one entire or splitted fibre and random locations were chosen.

As expected, for a given refinement, the effective stiffness is independent of subcell location. Behaviour tensors are symmetric, as shown in Table 1. There is still a small variability depending on mesh refinement, inferior to 0.3% for C_{ii} and 0.7% for C_{ij} . The method was performed with localization and concentration tensors and gave equal elastic properties.

The energy balance indicator is inferior to 1^{-3} for 20 nodes on edges, 1^{-4} for 50 nodes and 5^{-5} for 100 nodes. It remains satisfactory regardless to mesh refinement characteristics. The use of linear interpolation elements is not a limiting point. The numerical procedure is validated and can be confidently applied to sample homogenization of random heterogeneous media.

3. Application to a LFRC with carbon fibres and epoxy matrix

3.1. Microscopic scale modelling of the heterogeneous ply

The FE modelling is based on a transverse micrography of a ply, seen on Fig. 4(a). The contrast of the heterogeneities is balanced all over the image to perform a threshold on grey levels. Fibre sections, whose shape are actually quite irregular probably due to fabrication process, are fitted by ellipses and their geometric characteristics – centre, minor and major axes and orientation.

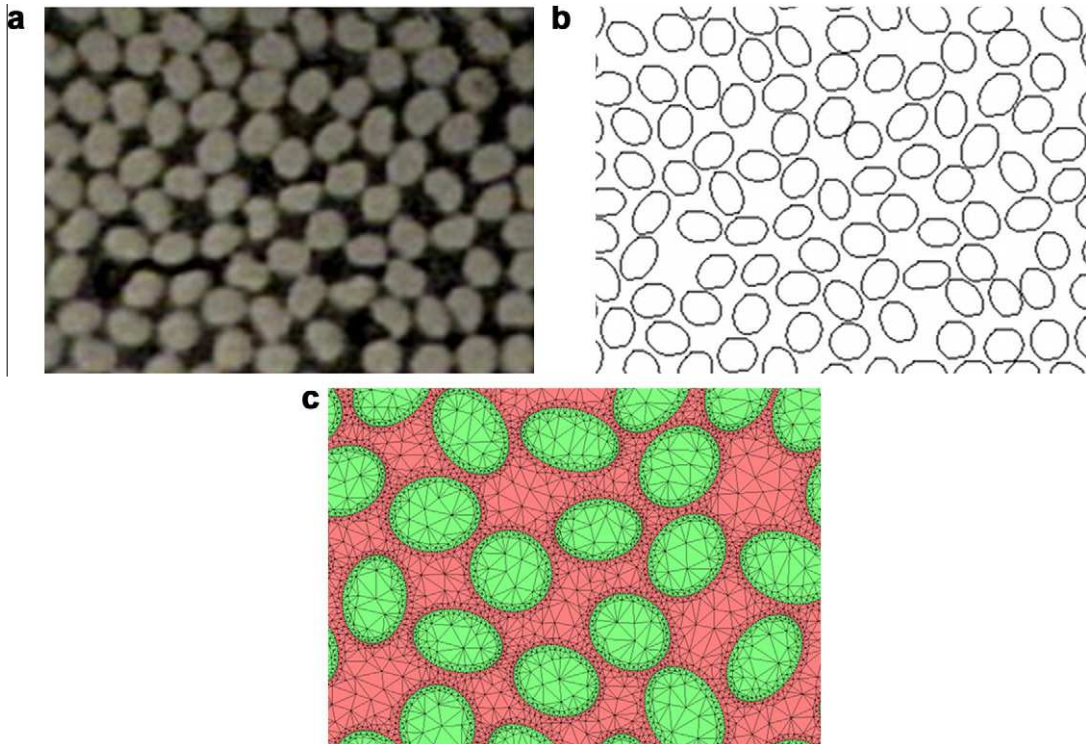


Fig. 4. Numerical model from a micrography: (a) micrography of a ply transverse section in a carbon fibre/ epoxy composite, (b) object analysis: elliptical sections of fibres, (c) mesh of the ply microstructure: fibres and matrix.

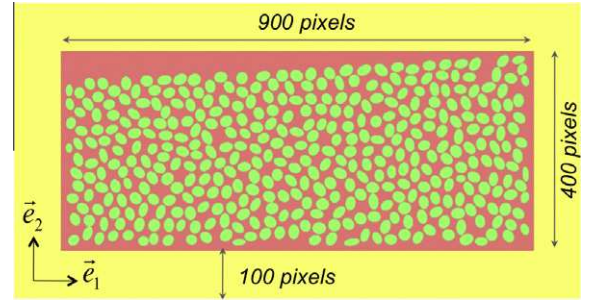


Fig. 5. Simulation cell: microstructure of fibres and matrix surrounded by a band of equivalent homogeneous medium and length scale in pixels.

These data are computed in a specifically developed meshing procedure to produce the FE mesh, as shown on Fig. 4(c).

A large part of a ply's heterogeneous microstructure, $0.073 \times 0.171 \text{ mm}^2$ equals $400 \times 900 \text{ pp}$, is modelled. It is surrounded with a band of Homogeneous Equivalent Medium (HEM) to reduce edge effects on nearby fibres, as shown on Fig. 5 as in the Embedded Cell Approach developed in [2] and applied in [19]. The average behaviour of the heterogeneous microstructure is estimated through an iterative procedure based on the balance of average stresses in the heterogeneous and homogeneous media.

Kinematic loading conditions are applied on the boundaries to simulate the three basic loading cases described in Section 3.1, under 2D plane strain hypothesis. Material properties correspond to a carbon fibres and epoxy matrix composite transversely to the fibres:

- fibres: $E_f = 390 \text{ GPa}$, $\nu_f = 0.35$,
- matrix: $E_m = 4.5 \text{ GPa}$, $\nu_m = 0.4$,
- HEM: $E_{HEM} = 15 \text{ GPa}$, $\nu_{HEM} = 0.35$,

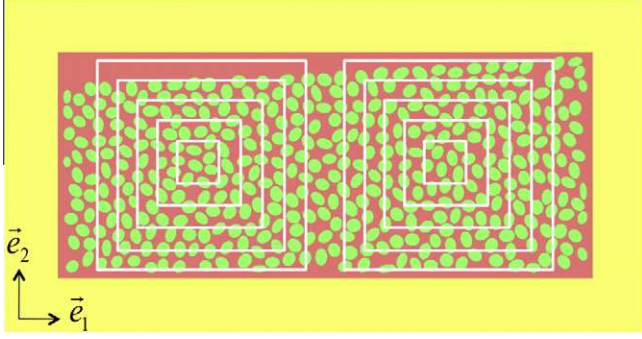


Fig. 6. Simulation cell: locations of two sets of variable size homogenization sampling cells.

3.2. Influence of subsampling size on energy accuracy

The first sampled set of subcells allows to investigate the influence of homogenization subcells size on the energy balance. As explained in [6], there is an intrinsic homogenization size under which the general theory presented does not verify Hill's energy balance. This minimal length concept was investigated on periodic homogenization and is assumed to be transposable to our work on non periodic homogenization. Two locations are chosen to generate two sets of variable size concentric square subcells, as depicted on Fig. 6.

The strong variations of subcells effective properties versus the homogenization size are shown on Fig. 7. Stiffness increases from small to medium subcells: smaller ones might be centred on a matrix zone. It decreases from medium to high sizes: the biggest cells contain a higher ratio of matrix as they approach the heterogeneous medium boundaries. As expected, the energy balance is better on bigger cells, as shown on Fig. 8.

The negative values of the average of perturbations product are pointed out. Indeed it is not a regular elastic strain energy which would be positive. It can be seen as a energy offset between scales, which can be either positive or negative – or zero. It is caused by the existence of elements in which perturbation strain and stress are of opposite signs.

For the following analyses the energy unbalance is supposed to be acceptable for a subcell size larger than 100 p. With a given size we can investigate the variability of effective properties and the influence of sampling parameters on the statistical moments.

3.3. Statistical distributions of effective properties

Various spatial subsampling schemes are performed to investigate their effect on statistical characteristics of mechanical properties variability. It is indeed necessary to control the statistical inference as the characterized distribution functions will be used in mesoscopic simulations.

3.3.1. Regular pattern subsampling

Two realizations of subcells sampling with two different sizes are presented: 200 p equals 0.036 mm – half the height of the ply – and 300 p equals 0.056 mm. A regular spatial scheme is chosen for both sampling sizes: the cells are repartitioned every ten pixels in both \vec{e}_1 and \vec{e}_2 directions.

These sizes are larger than the limit size validated in the previous section to verify the inter scale energy equivalence. It is confirmed by the relative energy error indicator inferior to 1.5%. The dispersion are presented in function of the fibre volume fraction on Fig. 9(a) and (b). It shows an important variability of stiffness for a given volume fraction, around 10% which is far higher than

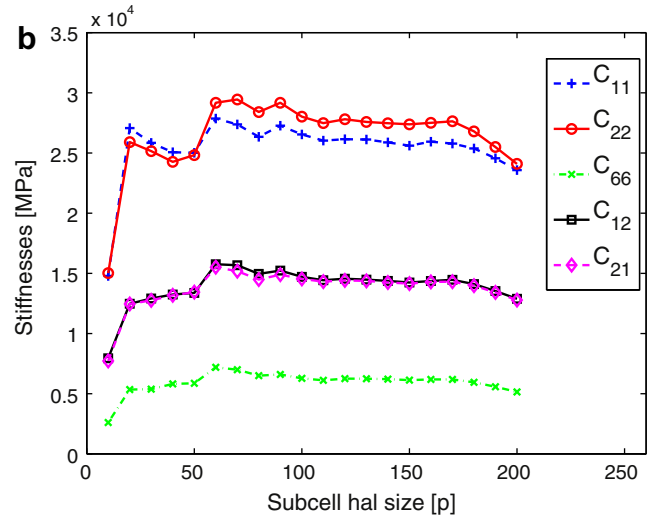
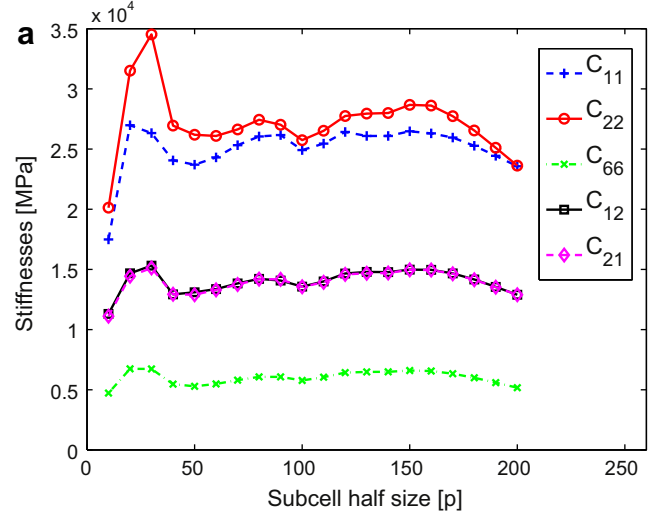


Fig. 7. Variations of effective properties on the two sets versus cell size.

th 1% value obtained in [4] with non-cutte fibres on edges. This result confirms those obtained in [1].

A linear regression using least square method gives approximations of C_{11} and C_{22} in function of fibre volumic fraction V_f for 200 pp and 300 pp subcells Eqs. (14), (15).

$$200 \text{ pp} : C_{11} = 39577V_f + 4513, \quad C_{22} = 62354V_f - 5880 \quad (14)$$

$$300 \text{ pp} : C_{11} = 36510V_f + 6141, \quad C_{22} = 61144V_f - 5183 \quad (15)$$

Global effective properties can be evaluated applying the non-periodic geometry homogenization procedure to the largest subcells as possible taken in the ply, around 400 p wide. They are listed Table 2. They fit correctly with Eqs. (14), (15) which can be considered as appropriate estimations of average stiffnesses in regard to the volume fraction.

In order to model the variability in FE meshes at meso scale, we need to statistically characterise the dispersions. The identification of normal distribution parameters (average μ and standard deviation σ) for C_{11} stiffness resulted in:

- for 200 pp subsample: $\mu = 24986$ and $\sigma = 1261$,
- for 300 pp subsample: $\mu = 25099$ and $\sigma = 742$.

It clearly shows, as expected, that dispersions on volume fractions and equivalent properties are smaller with the larger subcells. For

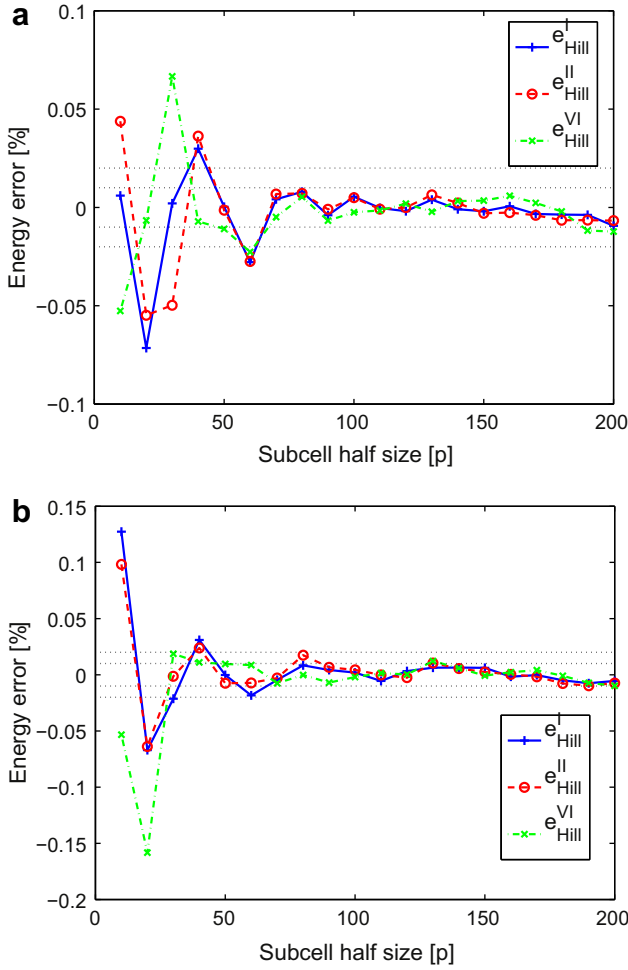


Fig. 8. Energy balance indicator on the two sets versus cell size, dotted lines at $\pm 1\%$ and $\pm 2\%$.

example, for a given volume fraction, dispersion of effective properties is wider for smaller subcells. It is also clear that microstructure is unbalanced and the material is stiffer in direction \vec{e}_2 .

3.3.2. Random subsampling

Several independent random subsamplings have been computed varying the size of the sample $N_{sb,amp}$: 25 (three times), 50 (two times), 300 and 500; they constitute a whole global sample of 975 subcells. A uniform distribution was used to generate the positions (x, y) of subcells center. Normal dispersion functions for C_{11} stiffness have been identified, the average and standard deviations are listed in Table 3. The estimation of average μ is accurate with low size subsampling but not for standard deviation σ .

To refine these results, the intern combinations in the 500 subsamples population has been explored in details. For a N elements population, subpopulations of p elements ($p \in [1, N]$) can be extracted with a counting of A_p^N possibilities. It is possible to identify p subpopulation with highest or lowest stiffness, which defines bounds for average value μ . For each p value, 15 combinations have been randomized, their statistical parameters are given in Fig. 10.

Low size subpopulation gives rapidly an accurate estimation of average value μ but standard deviation needs high size subsampling. One can notice that standard deviation for highest or lowest stiffness subpopulation are not bounds for random subsampling.

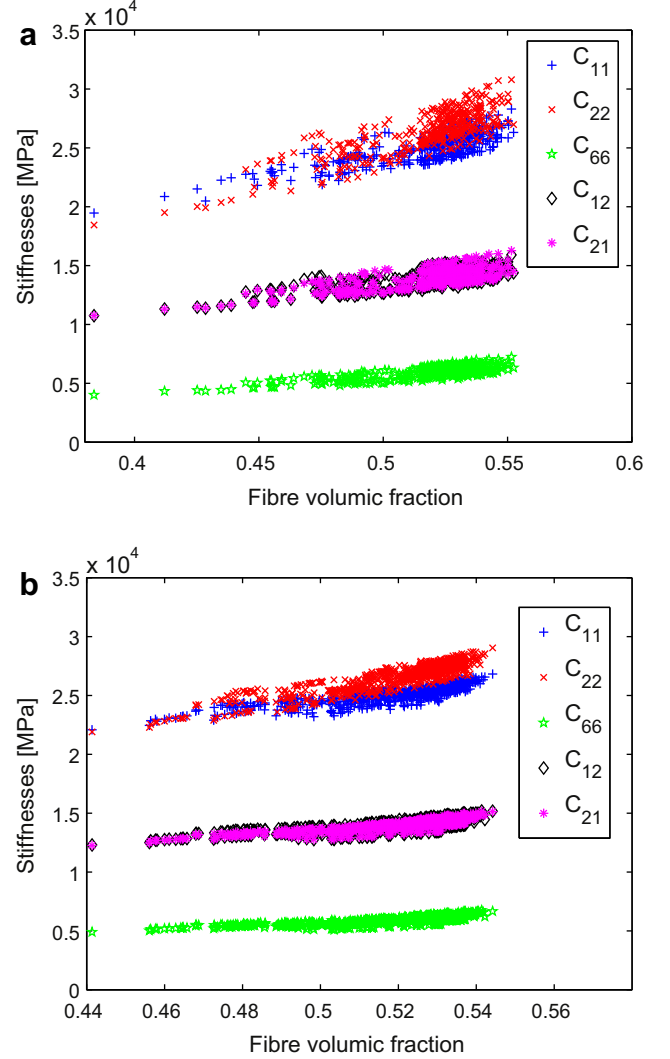


Fig. 9. Variability of C_{ii} versus fibre volume fraction with linear interpolation of average stiffnesses for C_{11} and C_{22} : (a) 200×200 pp subcells and (b) 300×300 pp subcells.

3.3.3. Influence of sampling scheme: statistical inference

It appears from the two former paragraphs that the subsampling scheme influences the statistical characterization of elastic properties. To highlight this effect, normal variability functions are identified on various subsamples:

- two times 10 subcells with 0% overlapping,
- 24 subcells with 50% overlapping,
- 396 subcells with 95% overlapping.

The distribution functions of stiffness C_{11} for various overlapping on regular spatial schemes are presented on Fig. 11 for the 200×200 pp subcells. This effect is caused by the geostatistical representativeness of subcells in various sampled identification data sets. For example non overlapping subcells contain more matrix as they touch boundaries than cells in the center of the microstructure. This effect underlines the issue of samples representativeness and its implications on the parameters values of the dispersion functions as it was also underlined in the previous section for random subsampling. Applications of sampling have been studied for geomorphological properties of heterogeneous media.

Table 2
 C_{11} and C_{22} stiffnesses versus V_f for very large subcells.

V_f	C_{11}	C_{22} [MPa]
0.4827	23448	24417
0.4980	23931	25184
0.5067	24430	25559
0.5168	24811	26254

Table 3
 Identification of normal distribution statistical moments.

N_{SS-ech}	25	50	300	500	975			
μ	25296	25121	25394	25132	25202	25132	25234	25223
σ	975	944	1234	1206	998	1115	1045	1072

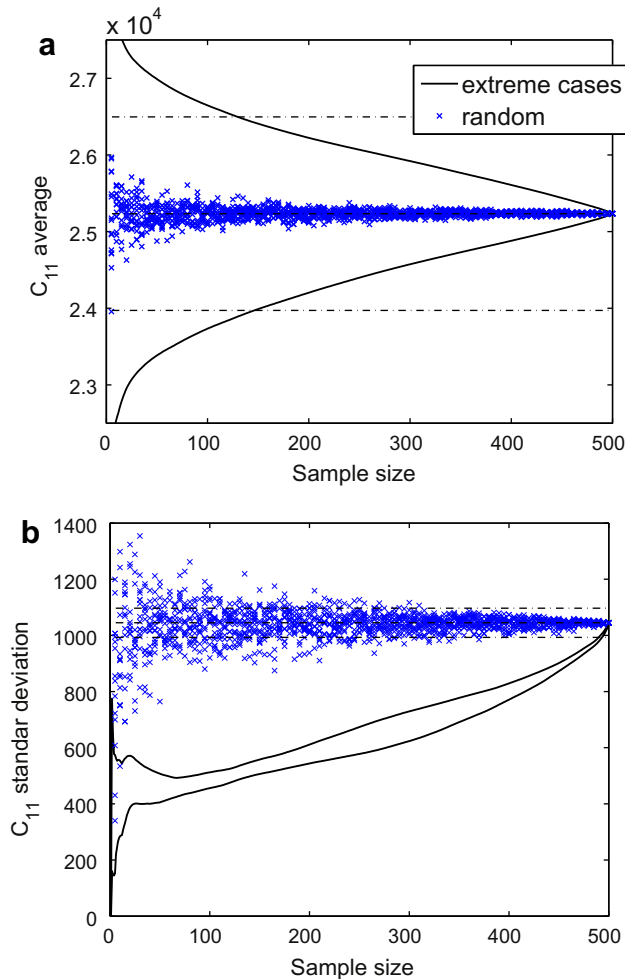


Fig. 10. Identification of statistical moments for subsamples of the 500 population; parameters for the least or most stiff subsamples traced in black lines, dotted lines stands for $\pm 5\%$ difference with average values.

The problem here for the non-overlapping sampling scheme is the small numbers of subcells that can be extracted from the entire population is not morphologically representative of the entire ply and as a consequence the effective properties aren't either. For overlapping subcells, it appears that stiffness increases with the overlapping rate. With a 90% rate, the proportion of subcells with lower fibre volume fraction located on the edges of the ply is higher in the entire population, it can explain the lower values.

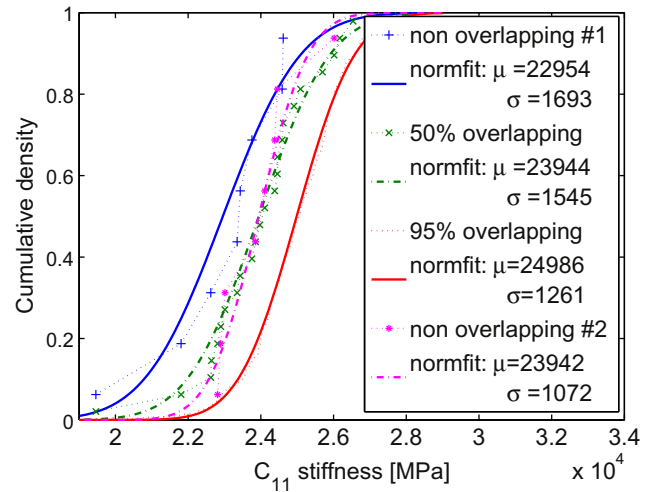


Fig. 11. Geostatistical variability of C_{11} microscopic variability depending on the overlapping scheme fitted with Normal dispersion functions: mean and variance.

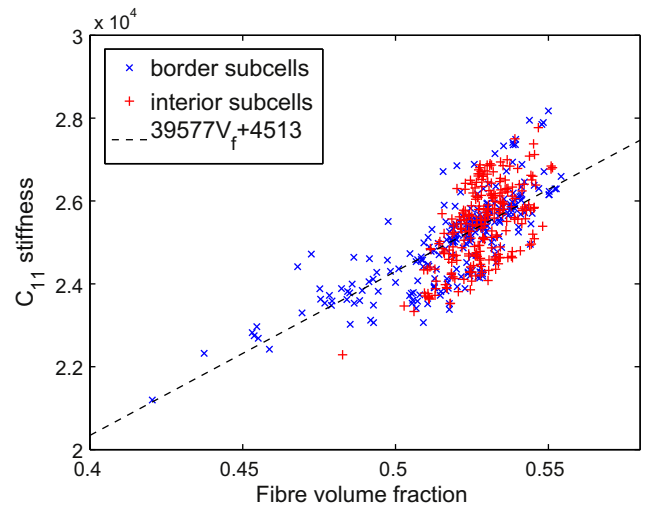


Fig. 12. C_{11} stiffness of cells located close to the borders in blue and in the central part in red. (For interpretation of the references to color in this figure legend, the reader is referred to the web version of this article.)

In comparison with Babuska's work [1], high variability was obtained as well for subcells. But it has been highlighted that spatial regular pattern is limited as it is not representative enough of the entire microstructure and introduces a high statistical bias in distribution function identification.

It is shown in previous section that a random spatial scheme avoids a bad identification. Statistical average μ is well identified with low size subsamples, around 150, and standard deviation σ needs high size subsamples, around 400. It is supposed that over-representation of subcells on border are responsible for bad identification on regular spatial schemes. The population of 500 subsamples has been split in two halves with close to border and central subcells. The dispersion for C_{11} are presented Fig. 12. Except for very low fibre volume fraction subcells, dispersion seems equal. Though, it shows that the use of the statistical distribution functions needs to be completed with a morphological analysis, for example at first order the volume fraction.

4. Conclusion and outlook

An original subsampling procedure has been developed at post-processing level for numerical homogenization on non-periodic geometry. It is applied to obtain the dispersion of LFRC effective elastic properties at mesoscopic scale. The microstructure of a transverse section ply of a LFRC is modeled and meshed to achieve FEA simulations. Various samples of subcells of the heterogeneous medium are homogenized to obtain effective properties.

A limit size to achieve the microscopic – mesoscopic energy balance with non periodic geometry an natural boundary conditions is highlighted. For a valid subcells size, the dispersion functions of stiffness at mesoscopic scale are identified. They depict a strong variability for given fibre volume fractions. It is assumed to be a consequence of the numerous random configurations of fibre cuts on subcells' boundaries.

This study also reveals the statistical inference induced by the chosen sampling spatial scheme on the effective properties variability functions confronting various results obtained with regular and random spatial scheme subsamplings. Complementary investigations could be carried out on this subject to improve reliability and representativeness of samplings mainly with morphological analysis of microstructure.

In further works, the statistical dispersions obtained here will be used to randomly assign effective properties to homogeneous subcells constituting a ply at mesoscale. This work will set for a structural analysis at mesoscale taking into account variability induced by microscale and will be presented in future publications. Another research orientation consists in modelling damage and failures and investigate its dependance on the microstructure properties.

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