

Nonlinear ultrasound monitoring of single crack propagation in cortical bone

Sylvain Haupert, Sandra Guerard, David Mitton, Françoise Peyrin, Pascal Laugier

▶ To cite this version:

Sylvain Haupert, Sandra Guerard, David Mitton, Françoise Peyrin, Pascal Laugier. Nonlinear ultrasound monitoring of single crack propagation in cortical bone. Proceedings of meetings on acoustics, 2012, 16, 9p. 10.1121/1.4757253]. hal-01006658

HAL Id: hal-01006658

https://hal.science/hal-01006658

Submitted on 16 Jun 2014

HAL is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers.

L'archive ouverte pluridisciplinaire **HAL**, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d'enseignement et de recherche français ou étrangers, des laboratoires publics ou privés.

Science Arts & Métiers (SAM)

is an open access repository that collects the work of Arts et Métiers ParisTech researchers and makes it freely available over the web where possible.

This is an author-deposited version published in: http://sam.ensam.eu
Handle ID: http://hdl.handle.net/10985/8259

To cite this version:

Sylvain HAUPERT, Sandra GUERARD, David MITTON, Françoise PEYRIN, Pascal LAUGIER - Nonlinear ultrasound monitoring of single crack propagation in cortical bone - Proceedings of Meetings on Acoustics, - Vol. 16, p.9p. - 2012

XVII International Conference on Nonlinear Elasticity in Materials

Cefalu, Sicily, Italy 1 - 7 July 2012

Nonlinear ultrasound monitoring of single crack propagation in cortical bone

Sylvain Haupert*, Sandra Guerard, David Mitton, Françoise Peyrin and Pascal Laugier

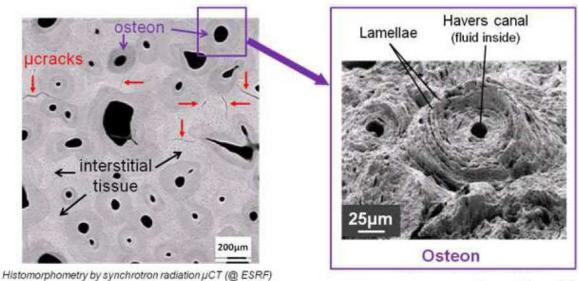
*Corresponding author's address: Univ Paris 6 UPMC, CNRS 7623, Laboratoire d'Imagerie Paramétrique, PARIS, 75006, idf, France, sylvain.haupert@upmc.fr

Accumulation of bone microdamage is suspected to lead to severe impairment of mechanical properties with an increase in skeletal fragility and fracture risk. The objective of the study was to evaluate the sensitivity of nonlinear resonant ultrasound spectroscopy (NRUS) measurements to the propagation in cortical bone of a single microcrack induced by 4-point bending mechanical loading. Twelve human cortical bone specimens were machined as parallelepiped beams (50*2*2mm) to unambiguously identify resonant modes for NRUS measurements. A central notch of 600 {lower case mu}m was made to control crack initiation and propagation during four-point bending loading. The nonlinear hysteretic elastic coefficient ({lower case alpha} $_f$) was derived from NRUS measurements achieved in dry and wet conditions. Each bone specimen was probed by a swept-sine around its first compression mode, applying progressively increasing drive levels. Moreover, the buried crack length was assessed by synchrotron radiation micro-computed tomography with a spatial resolution of 1.4 {lower case mu}m. Despite between-sample variability, {lower case alpha} $_f$ increased significantly in the damaged state (44.9±85.4) compared to the initial value (5.5±1.5) in the control undamaged state. Crack length was significantly correlated to the nonlinear elastic parameter {lower case alpha} $_f$ ($_f$ =0.78, p<0.001). These results suggest that NRUS is sensitive to damage accumulation and can be used as a marker of bone damage.

I. Introduction

a) Microdamage in cortical bone

 Two types of bone microdamage coexist: the microcrack (50-500μm) and the so-called diffuse damage. In this study, we will focus on microcracks in human cortical bone.



Excerpt from [1]

b) Why assessing bone microdamage?

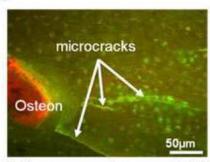
Context:

Bone microdamage accumulation is suspected to have important consequences

- 1. on bone *mechanical* properties => Increasing of skeletal fragility and risk of fracture.
- 2. on bone *biological* properties => initiating bone remodeling process

c) How to evaluate bone microdamage?

- Current growing interest in bone microdamage assessment:
 - Reference technique:
 Histomorphometry by optical microscopy
 (conventional or by epifluorescence)
 - ⇒ Destructive, 2D, time consuming and operatordependent



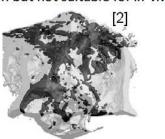
Epifluorescence microscopy (@ LIP)

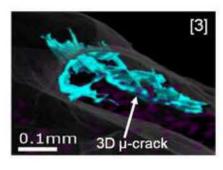
New techniques are emerging:

 μ CT with contrast agent [2], Synchrotron radiation μ CT [3]

⇒ Volumetric information but not suitable for in-vivo measurement

 121





⇒ Nonlinear acoustic techniques is a promising solution [4-6]

d) Nonlinear acoustics

- · Advantages of nonlinear acoustics methods :
 - ⇒ Very sensitive to microcracks and microdamage (in composites, concrete, metals...)
 - ⇒ Non-destructive techniques (possible transfer to the *in-vivo*)
- Two types of elastic nonlinearity [7]:

$$K(ε) = K_0 [(1 + (β ε + δ ε^2 + ...) + α (Δε, ε')]$$
Linear elastic Classical nonlinearity Hysteretic nonlinearity πonlinearity

- Classical nonlinearity (atomic origin) << hysteretic nonlinearity (cracked materials)
 - \Rightarrow In this study we investigate the nonlinear hysteretic α parameter as its nonlinearity is known to be very sensitive to damage in materials.

e) Preliminary results

- Previous in vitro nonlinear ultrasonic measurements in cortical bone:
 - First results: Nonlinear Resonant Ultrasound Spectroscopy (NRUS) method [4] was used to
 evaluate bone damage accumulation on human cortical bone diaphysis having undergone
 fatigue compression cycling.
 - \Rightarrow Nonlinear elastic parameter (α) \nearrow after fatigue \nearrow
 - $\Rightarrow \alpha \nearrow$ with age (and its was observed that microcracks density also \nearrow with age)
- ⇒ **But critical issue:** No bone microdamage evaluation and quantification

- Recent results: A group of cortical bone specimens having a calibrated parallelepiped shape were taken through a progressive fatigue protocol consisting of four steps of cyclic four-point bending. Microdamage quantification by NRUS and SR-μCT was performed on the same set of samples.
 - ⇒ NRUS is sensitive to **non-localized** bone **micro-damage** accumulation.
 - ⇒ Fatigue test induced early damage by increasing the density of small microcracks
 - \Rightarrow For the 1st time: significant **correlation** between the variation of α and the variation of **small microcracks** density.
 - ⇒ Linear Young's modulus not sensitive to early bone microdamage

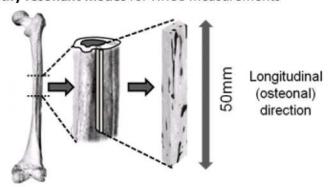
Aim of this study

- 1. To assess NRUS sensitivity to bone single and localized crack propagation
- 2. Clarify the relationship between NL hysteretic parameters and crack characteristics

II. Material & methods

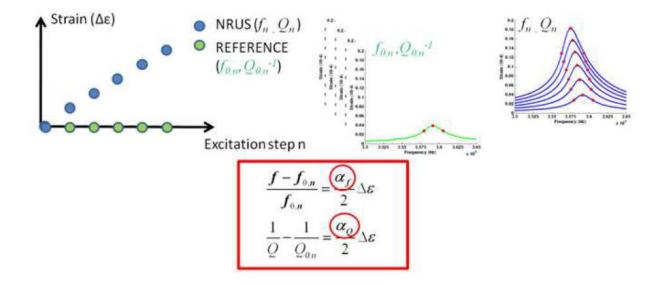
a) Human cortical bone samples

- 14 parallelepiped beams (50x2x2mm³) from 4 femoral mid-diaphysis in order to:
 - ⇒ Control damage during 4-point bending test (toughness)
 - ⇒ Identify resonant modes for NRUS measurements



b) Sensitive NRUS protocol:

• Tracking reference frequency $f_{0,n}$ and damping $Q^{-l}_{0,n}$ variations during the NRUS experiment by measuring $f_{0,n}$ and $Q^{-l}_{0,n}$ before each increasing amplitude step. This protocol allows to correct small variations of the references due to environmental fluctuation (i.e. temperature changes) and/or material conditioning [8].

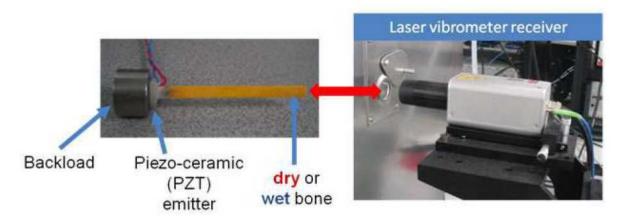


- \Rightarrow High sensitivity ($\Delta f/f_0$ limit = 10⁻⁵) and low variability (<20%)
- \Rightarrow Extraction of **2 hysteretic parameters**: elastic (α_i) and dissipative (α_0)

Experimental setup:

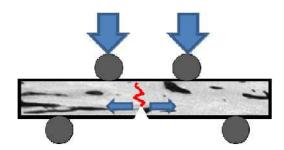
- **Emitter**: the piezo-ceramic applies progressively increasing drive levels (ε =10⁻⁶ 10⁻⁴) around the **1**st **compression mode** (≈15kHz).
- Receiver: Resonant response measured by a laser vibrometer.

Note that the specimens were measured in DRY and WET conditions after toughness test.



c) Toughness test

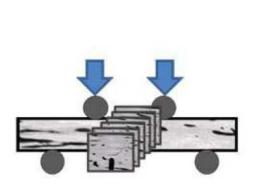
- The toughness test consists on a single crack initiation and propagation. The procedure is the following:
 - 1. Notch in the sample
 - 2. Quasi-static loading: µcrack initiation and growing
 - 3. Stop loading before the rupture

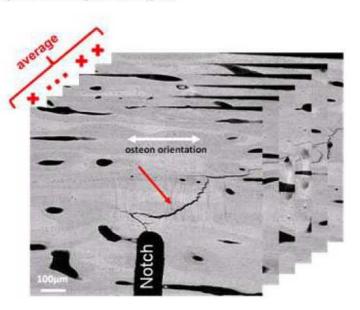


⇒ The toughness test was stopped at different loading stage for each specimen in order to get samples with different crack lengths (Cr.Le)

d) Histomorphometry

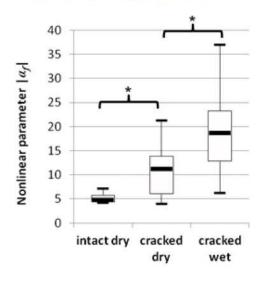
- Histomorphometry was performed for the first time using synchrotron radiation μCT (SR-μCT) [3]:
 - One region of interest (ROI) of 2.15x1.75x1.75mm³ encompassing the notch area
 - Six 2-D longitudinal SR-μCT cross-sections were extracted from the ROI volume (resolution= 1.4μm; surface = 4mm²)
 - ⇒ Evaluation of the average single crack length: Cr.Le [μm]

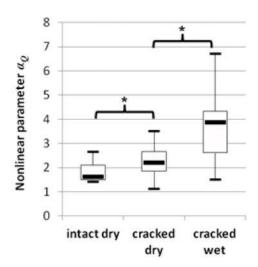




III. Results

a) Nonlinear ultrasonic parameters

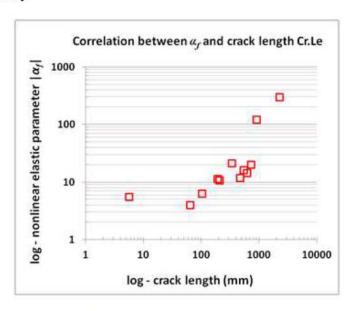




- \Rightarrow Both nonlinear parameters increase significantly (α_f : p<0.006; α_Q : p=0.02) after crack propagation.
- \Rightarrow Both nonlinear parameters are significantly higher when bone specimens are wet (α_f : p<0.002; α_O p<0.001)

Hypothesis: the variation of the nonlinear hysteretic behavior could be due to capillarity forces [9] and/or bone organic phase (collagen) properties modification.

b) Histomorphometry



- ⇒ Crack length Cr.Le ranges between 6μm to 2277μm
- \Rightarrow Significant correlation (r²=0.8; p<0.01; Spearman test) between Cr.Le and α_f (measured in dry condition)

IV. Discussion and Conclusion

- Our results evidence:
 - Nonlinear elastic α_f and dissipative α_Q parameters are sensitive to single crack propagation. This is in agreement with other studies conducted on steel [10, 11] or concrete [12].

 - Similar trends for the first 3 compression modes (data not shown). This confirms the robustness of the results which are independent on the compression modes.
- For the 1st time:
 - Successful **concurrent assessment** of an ultrasonic nonlinear parameter (α_f) and bone crack length (Cr.Le).
- Next step:
 - Take into account other single crack parameters (volume, thickness...)
 - ⇒ Better correlation with nonlinear parameters?

V. Acknowledgement

The authors want to thank G. Renaud and J. Rivière for their helpful comments and suggestions during the preparation of the experiments, as well as P.A. Johnson, Los Alamos National Laboratory, NM, USA for fruitful discussions and E. Boller, M. Zuluaga and M. Langer for help during the ESRF experiment performed in the framework of LTP MD431.

This research was supported by the Agence Nationale pour la Recherche (ANR), France (Grant BONUS_07BLAN0197).

VI. References

- [1] Hiller, L., Stover, S., Gibson, V., Gibeling, J., Prater, C., Hazelwood, S., Yeh, O., and Martin, R., 2003, "Osteon pullout in the equine third metacarpal bone: effects of ex vivo fatigue," Journal of orthopaedic research, 21(3), pp. 481-488.
- [2] Tang, S. Y., and Vashishth, D., 2007, "A non-invasive in vitro technique for the three-dimensional quantification of microdamage in trabecular bone," Bone, 40(5), pp. 1259-1264.
- [3] Larrue, A., Rattner, A., Peter, Z. A., Olivier, C., Laroche, N., Vico, L., and Peyrin, F., 2011, "Synchrotron Radiation Micro-CT at the Micrometer Scale for the Analysis of the Three-Dimensional Morphology of Microcracks in Human Trabecular Bone," PLoS ONE, 6(7), p. e21297.
- [4] Muller, M., Mitton, D., Talmant, M., Johnson, P., and Laugier, P., 2008, "Nonlinear ultrasound can detect accumulated damage in human bone," Journal of Biomechanics, 41(5), pp. 1062-1068.
- [5] Renaud, G., Calle, S., Remenieras, J. P., and Defontaine, M., 2008, "Non-linear acoustic measurements to assess crack density in trabecular bone," International Journal of Non-Linear Mechanics, 43(3), pp. 194-200.
- [6] Moreschi, H., Callé, S., Guerard, S., Mitton, D., Renaud, G., and Defontaine, M., 2011, "Monitoring trabecular bone microdamage using a dynamic acousto-elastic testing method,"

- Proceedings of the Institution of Mechanical Engineers, Part H: Journal of Engineering in Medicine, 225(1), pp. 1-12.
- [7] Van den Abeele, K., Carmeliet, J., Ten Cate, J. A., and Johnson, P. A., 2000, "Nonlinear elastic wave spectroscopy (NEWS) techniques to discern material damage, Part II: Single-mode nonlinear resonance acoustic spectroscopy," Research in Nondestructive Evaluation, 12(1), pp. 31-42.
- [8] Haupert, S., Renaud, G., Riviere, J., Talmant, M., Johnson, P. A., and Laugier, P., 2011, "High-accuracy acoustic detection of nonclassical component of material nonlinearity," Journal of the Acoustical Society of America, 130(5), p. 2654.
- [9] Van den Abeele, K., Carmeliet, J., Johnson, P., and Zinszner, B., 2002, "Influence of water saturation on the nonlinear elastic mesoscopic response in Earth materials and the implications to the mechanism of nonlinearity," J. Geophys. Res, 107(6), p. 2121.
- [10] Duffour, P., Morbidini, M., and Cawley, P., 2006, "A study of the vibro-acoustic modulation technique for the detection of cracks in metals," The Journal of the Acoustical Society of America, 119, p. 1463.
- [11] Donskoy, D., Sutin, A., and Ekimov, A., 2001, "Nonlinear acoustic interaction on contact interfaces and its use for nondestructive testing," Ndt & E International, 34(4), pp. 231-238.
- [12] Zardan, J. P., Payan, C., Garnier, V., and Salin, J., 2010, "Effect of the presence and size of a localized nonlinear source in concrete."
- [13] Johnson, P. A., Zinszner, B., Rasolofosaon, P., Cohen-Tenoudji, F., and Van Den Abeele, K., 2004, "Dynamic measurements of the nonlinear elastic parameter alpha in rock under varying conditions," Journal of Geophysical Research-Solid Earth, 109(B2).