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A condition-based imperfect replacement policy for a periodically inspected system with two dependent wear indicators

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Abstract

A two-component system is considered, which is subject to accumulative deterioration. Due to common stress, the components are dependent. Their joint deterioration is modelled with a bivariate non decreasing Lévy process. The deterioration level of both components is known only through perfect and periodic inspections. By an inspection, components with deterioration level beyond a specific threshold are instantaneously replaced by new ones (corrective or preventive replacements). Otherwise, they are left as they are. Between inspections, failures remain unrevealed. This replacement policy is classical in a univariate setting, with deterioration modelled by a Gamma process. In the bivariate case, it leads to imperfect repairs at the system level, which highly complicates the study. The replacement policy is assessed through cost functions on both finite and infinite horizons, which take into account some economical dependence between components. Markov renewal theory is used to study the behaviour of the system, in a continuous and bivariate setting. Numerical experiments illustrate the study, considering a specific Lévy process with univariate Gamma processes as margins. Though technical details are not provided here for the numerical computations, the paper shows that there is a technical gap between the traditional one-dimensional studies and the present two-dimensional one, especially for the computation of the asymptotic distribution of the underlying Markov chain. Hence there is a need for further development in the bivariate (or multivariate) setting. *Keywords:* Reliability; multivariate Lévy processes; dependent wear indicators; Gamma processes; Markov renewal theory.

1 Introduction

In reliability, stochastic models for deterioration based on actual measurements of the system deterioration level have been the subject of many studies during

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the last decades. In case of non decreasing deterioration, classical models include compound Poisson processes and Gamma processes, according to whether the deterioration is due to isolated shocks or continuous wear accumulation, see [1], [2] or [3] e.g.. These classical models are both univariate non decreasing Lévy processes, also called subordinators. We here consider a two-component system, where the deterioration of each component is measured by a univariate subordinator. Because of a common stressing environment, the deterioration levels of the two components are correlated. Hence the need for a bivariate stochastic model to describe the system evolution.

Up to our knowledge, multivariate non decreasing wear indicators have not been much studied in the previous literature. Several notable exceptions may however be found such as [4] and [5], which both use specific constructions leading to some specific bivariate increasing Lévy processes (though not recognized as such in the quoted papers). Following [6], we here propose to model the evolution of our two-component system by a general bivariate subordinator (or non decreasing bivariate Lévy process). This englobes lots of possible dependence between the two marginal processes. As an example, let us consider two components in a common stressing environment, where the stress arrive by shocks according to a Poisson process. Without considering the common environment, the deterioration of the two components is measured by two univariate and independent subordinators (Gamma processes e.g.). Assume that the common shocks make both components older, with identically and independently distributed bivariate increments of age at each shock. The bivariate "virtual" age of the two components submitted to the shocks then appears as a bivariate compound Poisson process. The process describing the two components submitted to the shocks hence appears as a bivariate Lévy process (composed of the two initial independent Gamma processes) subordinated by a bivariate compound Poisson process, and it consequently is a bivariate subordinator.

Both series and parallel structures are envisioned for the two-component system. Each component is considered as failed as soon at its deterioration level has reached a pre-determined failure threshold. In [6], the system was assumed to be continuously monitored and repairs to be perfect. In the present paper, the deterioration level of the two components is known only through periodic inspections. By an inspection, failed components are instantaneously replaced by new ones (corrective replacements). In case where one single component is down by an inspection, this leads to an imperfect repair at the system level. For the two envisioned structures (series and parallel), the system may remain failed for a while before an inspection. To lower the system down-time, a condition-based maintenance policy is considered, where preventive replacements are performed at inspection times, when the deterioration level of each component is observed to be beyond a preventive threshold (lower than the corrective threshold). The preventive maintenance policy is assessed through a cost function, both on a finite and infinite horizon. This cost function takes into account down-time unitary costs, inspection costs as well as replacement costs, with economical dependence between replacement costs. (Simultaneous replacements are less costly than separate replacements). Our model hence takes into account two kinds of dependence: 1. stochastic dependence between the random deterioration levels of each component (induced by common stress); 2. economical dependence, which may lead to grouped replacements to lower replacement costs, and consequently implies some kind of functional dependence. This twofold dependence

highly complicates the study (and especially the stochastic one), as well as the imperfect repairs.

Similar preventive and corrective threshold-based replacement policies have already been considered in the literature on a large scale in the univariate setting, see [3] for numerous references in case the system deterioration is modelled by a Gamma process. Papers are much fewer in the multivariate setting. One may however quote [7], where the authors envision a two-unit series system with stochastically independent but economically dependent components, in a discrete time setting. Though their study is highly simplified by the assumption of stochastic independence between components, their condition-based inspection scheme is however more complicated than our periodic one. Also, like lots of other papers on similar subjects, they only envision long-time runs whereas we also consider the case of a finite horizon time, additionally.

The article is organized as follows: the model is presented in Section 2, both for the unmaintained and preventively maintained system. Section 3 is devoted to theoretical developments, based on Markov renewal theory. Numerical experiments illustrate the study in Section 4, considering a specific Lévy process with univariate Gamma processes as margins. Concluding remarks end the paper in Section 5.

2 The model

2.1 The unmaintained system

The deterioration of the two-component system is measured by a bivariate non-decreasing Lévy process $X = \left(X_t^{(1)}, X_t^{(2)} \right)_{t \geq 0}$, also called bivariate subordinator. This means that the process starts from $(0, 0)$ and has homogeneous and independent increments, see [8] for more details. As in [6], the process X is assumed to have null drift, so that X is a pure jump process.

For each $i = 1, 2$, the marginal process $\left(X_t^{(i)} \right)_{t \geq 0}$ stands for the deterioration of the i -th component and is a univariate subordinator. The i -th component is considered as failed as soon as its deterioration level is beyond threshold L_i and we set

$$\sigma^{(i)} = \inf \left(t > 0 : X_t^{(i)} > L_i \right)$$

to be the time-to-failure of the i -th component. In the series case, the system time-to-failure is

$$\sigma_S = \min \left(\sigma^{(1)}, \sigma^{(2)} \right).$$

In the parallel case, it is

$$\sigma_P = \max \left(\sigma^{(1)}, \sigma^{(2)} \right).$$

The respective distributions of X_t and $X_t^{(i)}$ are denoted by μ_t and $\mu_t^{(i)}$, their cumulative distribution functions (c.d.f.) by F_t and $F_t^{(i)}$, and their survival functions by \bar{F}_t and $\bar{F}_t^{(i)}$. Note that we do not assume μ_t and $\mu_t^{(i)}$ to admit a density with respect to Lebesgue measure.

The state of the system is perfectly controlled via periodic inspections at time $0, T, 2T, \dots$. To avoid the trivial case where the system never fails, we assume

in all the paper that $\mathbb{P}\left(X_T^{(1)} > L_1, X_T^{(2)} > L_2\right) = \mathbb{P}\left(\sigma^{(1)} \leq T, \sigma^{(2)} \leq T\right) > 0$. Between inspections, failures remain unrevealed. At time nT , $n \geq 0$, only failed components are replaced (corrective replacements). This means that, by an inspection, deterioration levels of failed components are reset to zero whereas they are left unchanged otherwise. Replacements are assumed to be instantaneous and perfect.

2.2 The preventive maintenance policy

In order to avoid failures and to shorten down periods, preventive maintenance thresholds M_i are next introduced (with $0 \leq M_i \leq L_i$, $i = 1, 2$), with a similar replacement policy as for corrective replacements otherwise. More specifically, at time nT , $n \geq 0$, if the deterioration level of the i^{th} component is between M_i and L_i , a preventive replacement is performed. If its deterioration is beyond L_i , the component is failed and a corrective replacement takes place. Preventive replacements (PR) are assumed to be instantaneous and perfect, just as for corrective replacements (CR).

This preventive maintenance (PM) policy is illustrated in Figure 1, where there are: two simultaneous corrective replacements at time T , one single preventive replacement at times $2T$ and $3T$, two simultaneous preventive replacements at times $4T$ and $5T$. In this sequence, the maintenance actions at times $2T$ and $3T$ are imperfect, at the system level.

Note that though the system state (up or down) depends on its structure (series or parallel), the replacement policy is the same for both structures.

Taking $M_i = L_i$ for $i = 1, 2$, the unmaintained system appears as a special case of the preventively maintained system. Taking $M_i = 0$ for $i = 1, 2$, the system is replaced every T time units and the classical periodic replacement policy with no repair at failure and period T also is a special case of the PM policy.

To assess the PM policy, cost functions are considered, which takes into account a down-time unitary cost per unit time (c_u), inspection costs (c_p) and replacement costs. The cost of simultaneous replacements of both components is $c_1 + c_2 + c_r$. If only the i -th component is replaced ($i = 1, 2$), the cost is $c_i + c_r$. This induces an economical dependence between cost replacements. Note that we do not consider different costs for preventive or corrective replacements. Indeed, whatever their nature is, all replacements are instantaneously performed at inspection times and there is no special delay for the corrective ones, nor special action either (just replace too degraded components). However, if necessary, the results might easily be adapted in case of different replacement costs.

3 Theoretical results

3.1 Structure of the underlying stochastic process

Let $Y = \left(Y_t^{(1)}, Y_t^{(2)}\right)_{t \geq 0}$ be the stochastic process describing the maintained system. Considering the system state after each inspection, the sequence $(Y_{nT})_{n \geq 0}$ is a Markov chain with continuous state space $[0, M_1] \times [0, M_2]$. Indeed, regardless of whether the components are replaced or not at inspection time nT , their

future evolution after time nT only depends on their state at time nT . This means that $(Y_t)_{t \geq 0}$ is a semi-regenerative process, with $(Y_{nT})_{n \geq 0}$ as embedded Markov chain. Both processes $(Y_{nT}^{(i)})$, $i = 1, 2$ have similar properties and also are semi-regenerative processes, with $(Y_{nT}^{(i)})_{n \geq 0}$, $i = 1, 2$ as embedded Markov chains and state spaces $[0, M_i]$, $i = 1, 2$.

We next provide the transition kernels of the different Markov chains, denoted by $\mathcal{Q}(x, dy)$ and $Q^{(i)}(x_i, dy_i)$, $i = 1, 2$. Setting \mathbb{P}_x (resp. \mathbb{P}_{x_i}) to refer to the conditioning by $Y_0 = x$ (resp. $Y_0^{(i)} = x_i$) and $dy = (dy_1, dy_2)$, we recall that

$$\mathcal{Q}(x, dy) = \mathbb{P}(Y_T \in dy | Y_0 = x) = \mathbb{P}_x(Y_T \in dy)$$

for all $x = (x_1, x_2) \in [0, M_1] \times [0, M_2]$ and

$$Q^{(i)}(x_i, dy_i) = \mathbb{P}(Y_T^{(i)} \in dy_i | Y_0^{(i)} = x_i) = \mathbb{P}_{x_i}(Y_T^{(i)} \in dy_i)$$

for all $x_i \in [0, M_i]$, $i = 1, 2$.

In case $x = (0, 0)$ or $x_i = 0$, we just write $\mathbb{P} = \mathbb{P}_{(0,0)}$ or $\mathbb{P} = \mathbb{P}_0$ in the following.

Proposition 1 *For $i = 1, 2$, the transition kernel of the Markov chain $(Y_{nT}^{(i)})_{n \in \mathbb{N}}$ is given by*

$$Q^{(i)}(x_i, dy_i) = \overline{F}_T^{(i)}(M_i - x_i) \delta_0(dy_i) + \mathbf{1}_{[x_i, M_i]}(y_i) \mu_T^{(i)}(dy_i - x_i) \quad (1)$$

for all $x_i \in [0, M_i]$, where $\delta_0(dy_i)$ stands for the Dirac mass at 0.

The transition kernel of the Markov chain $(Y_{nT})_{n \in \mathbb{N}}$ is given by

$$\mathcal{Q}(x, dy) = \sum_{i=1}^4 \mathcal{Q}_i(x, dy)$$

with

$$\mathcal{Q}_1(x, dy) = \mathbf{1}_{[x_1, M_1]}(y_1) \mathbf{1}_{[x_2, M_2]}(y_2) \times \mu_T(dy_1 - x_1, dy_2 - x_2), \quad (2)$$

$$\mathcal{Q}_2(x, dy) = \mathbf{1}_{[x_2, M_2]}(y_2) \times \left(\int_{(M_1, +\infty[} \mu_T(du_1 - x_1, dy_2 - x_2) \right) \delta_0(dy_1), \quad (3)$$

$$\mathcal{Q}_3(x, dy) = \mathbf{1}_{[x_1, M_1]}(y_1) \times \left(\int_{(M_2, +\infty[} \mu_T(dy_1 - x_1, du_2 - x_2) \right) \delta_0(dy_2), \quad (4)$$

$$\mathcal{Q}_4(x, dy) = \overline{F}_T(M_1 - x_1, M_2 - x_2) \times \delta_0(dy_1) \delta_0(dy_2) \quad (5)$$

for all $x = (x_1, x_2) \in [0, M_1] \times [0, M_2]$.

Proof. For $i = 1, 2$, there are two possible scenarios for the i^{th} component at time T : either the component is replaced by a new one and its level deterioration is reset to 0, or it is left as it is. Starting from x_i , the first scenario happens with the probability

$$\mathbb{P}_{x_i}(X_T^{(i)} > M_i) = \overline{F}_T^{(i)}(M_i - x_i).$$

As for the second scenario, it means that the level of the i^{th} component at time T is $x_i + X_T^{(i)}$, with $x_i + X_T^{(i)} \leq M_i$. This provides expression Eq.(1) for $Q^{(i)}(x_i, dy_i)$.

As for the whole system, at time T , there are three possibilities: either no replacement, or one single replacement, or two simultaneous replacements. According to which component is replaced in case of one single replacement (component 1 or 2), this leads to four different possible scenarios. As for the second scenario (replacement of component 1 only), we have:

$$\mathbb{E}_x \left[\varphi(Y_T) \mathbf{1}_{\{Y_T^{(1)}=0; Y_T^{(2)}=X_T^{(2)}\}} \right] = \iint_{\mathbb{R}^2} \varphi(y_1, y_2) \mathcal{Q}_2(x, dy)$$

for all measurable and non negative function φ (and all x), with

$$\begin{aligned} & \mathbb{E}_x \left[\varphi(Y_T) \mathbf{1}_{\{Y_T^{(1)}=0; Y_T^{(2)}=X_T^{(2)}\}} \right] \\ &= \mathbb{E}_x \left[\varphi(0, X_T^{(2)}) \mathbf{1}_{\{X_T^{(1)} > M_1; X_T^{(2)} \leq M_2\}} \right] \\ &= \iint_{\mathbb{R}_+^2} \varphi(0, x_2 + z_2) \mathbf{1}_{\{x_1 + z_1 > M_1; x_2 + z_2 \leq M_2\}} \mu_T(dz_1, dz_2) \\ &= \iint_{\mathbb{R}^2} \varphi(0, y_2) \mathbf{1}_{(M_1, +\infty[}(u_1) \mathbf{1}_{[x_2, M_2]}(y_2) \mu_T(du_1 - x_1, dy_2 - x_2) \\ &= \iint_{\mathbb{R}^2} \varphi(y_1, y_2) \mathbf{1}_{[x_2, M_2]}(y_2) \times \left(\int_{(M_1, +\infty[} \mu_T(du_1 - x_1, dy_2 - x_2) \right) \delta_0(dy_1) \end{aligned}$$

setting $(u_1, y_2) = (x_1 + z_1, x_2 + z_2)$ for the third line, and using $\varphi(0, y_2) = \int_{\mathbb{R}} \varphi(y_1, y_2) \delta_0(dy_1)$ and Fubini's theorem for the last line. (Note that the integration on $(M_1, +\infty[$ is made with respect to u_1). This provides Eq.(3). Similar computations provide Eq.(2), Eq.(4) and Eq.(5). ■

Remark 1 In case X_t admits a probability density function (p.d.f.) f_t with respect to Lebesgue measure, we get:

$$\mathcal{Q}_2(x, dy) = \mathbf{1}_{[x_2, M_2]}(y_2) \times \left(\int_{M_1}^{+\infty} f_T(u_1 - x_1, y_2 - x_2) du_1 \right) \delta_0(dy_1) dy_2,$$

with similar formulas for the other terms.

In case X_t takes range in \mathbb{N}^2 and $M = (M_1, M_2) \in \mathbb{N}^2$, we have:

$$\begin{aligned} & \mathcal{Q}_2(x, dy) \\ &= \sum_{k_2=x_2}^{M_2} \left(\sum_{k_1=M_1+1}^{+\infty} \mathbb{P}(X_T^{(1)} = k_1 - x_1, X_T^{(2)} = k_2 - x_2) \right) \delta_0(dy_1) \delta_{k_2}(dy_2) \end{aligned}$$

for all $x = (x_1, x_2) \in \mathbb{N}^2$ such that $0 \leq x_1 \leq M_1$ and $0 \leq x_2 \leq M_2$.

Remark 2 For the two-component system with dependent components, a natural question is: what is the influence of the dependence between the two components on the performance of the maintained system? More specifically, consider two different systems with identical characteristics, except from the fact that the two components are more dependent in one system than in the other (perhaps because of different levels of stress, which induces more or less dependence between components). Then, is it possible to get comparison results between performance indicators of the two maintained systems, such as reliability or cost e.g.? In mathematical terms, assume that $X = \left(X_t^{(1)}, X_t^{(2)} \right)_{t \geq 0}$ and $\tilde{X} = \left(\tilde{X}_t^{(1)}, \tilde{X}_t^{(2)} \right)_{t \geq 0}$ are two bivariate subordinators with identically distributed marginal processes $\left(X_t^{(i)} \right)$ and $\left(\tilde{X}_t^{(i)} \right)$, $i = 1, 2$, and such that the components of $X = \left(X_t^{(1)}, X_t^{(2)} \right)_{t \geq 0}$ are "less dependent" than the components of $\tilde{X} = \left(\tilde{X}_t^{(1)}, \tilde{X}_t^{(2)} \right)_{t \geq 0}$. Following [9], this may be specified through assuming that X_t is smaller than \tilde{X}_t in the sense of the concordance order, namely that $F_t \leq \tilde{F}_t$ (or $\bar{F}_t \leq \bar{\tilde{F}}_t$, equivalently), where we add \sim to refer to \tilde{X} . To get comparison results on reliability/cost indicators of the two maintained systems, a reasonable way might be to get comparison results between processes Y and \tilde{Y} (with clear notations). However, taking $y_1 = 0$ and $0 < y_2 \leq M_2$, we have:

$$\begin{aligned} F_{Y_T}(0, y_2) &= \mathbb{P} \left(M_1 < X_T^{(1)}; M_2 < X_T^{(2)} \right) + \mathbb{P} \left(M_1 < X_T^{(1)}; X_T^{(2)} \leq y_2 \right) \\ &= \bar{F}_T(M_1, M_2) + \bar{F}_T^{(1)}(M_1) - \bar{F}_T(M_1, y_2) \end{aligned}$$

and, in general, there is no reason why $F_{Y_T}(0, y_2)$ should be comparable with $F_{\tilde{Y}_T}(0, y_2)$. As a consequence, assuming that, without maintenance, the components of one system are less dependent than the components of the other one (with the same characteristics otherwise), the respective levels of the two maintained systems are not comparable (at least in a general setting). Hence, we do not expect the respective reliability/cost indicators of the two maintained systems to be comparable either. This is confirmed by numerical experiments from Section 4, where an example is provided, for which the probability of simultaneous replacement (which is involved in cost) is not monotone with respect to the dependence between components (see Example 3).

3.2 The cost function on a finite horizon time

The total cost on a given time interval depends on the number of replacements (simultaneous or not), on the down-time duration and on the number of inspections. The cost is typically computed on some specified time interval of the form $[0, t)$, and in case $t = nT$, $n \geq 1$, no replacement cost is considered at time t . (Indeed, we do not want to replace components once the horizon time t is reached). Of course, this does not infer on the mean down time, which is the same on $[0, t]$ or $[0, t)$.

For $x = (x_1, x_2) \in [0, M_1] \times [0, M_2]$ and given that the system starts from $Y_0 = x$, we set:

- $C(x, [0, t)) =$ mean cumulated cost on $[0, t)$;

- $U(x, [0, t])$ = mean cumulated down time on $[0, t)$ (= cumulated unavailability on $[0, t)$);
- $R_{12}(x, nT)$ = mean number of simultaneous replacement of both components at time nT (= probability of simultaneous replacement at time nT because one single simultaneous replacement may occur at time nT);
- $R_i(x, nT)$ = mean number of replacement of the i -th component at time nT (= probability of replacement of the i -th component at time nT).

With these notations, we get the following expression for the cost function.

Proposition 2 *Let $x = (x_1, x_2) \in [0, M_1] \times [0, M_2]$. Given that the system starts from $Y_0 = x$, the mean cost on $[0, t)$ is:*

$$C(x, [0, t]) = c_u U(x, [0, t]) + (c_1 + c_r) \sum_{n:nT < t} R_1(x_1, nT) \quad (6)$$

$$+ (c_2 + c_r) \sum_{n:nT < t} R_2(x_2, nT) - c_r \sum_{n:nT < t} R_{12}(x, nT) + c_p \lfloor \frac{t}{T} \rfloor,$$

where $\lfloor \frac{t}{T} \rfloor$ stands for the integer part of $\frac{t}{T}$ (with $\lfloor \frac{t}{T} \rfloor \leq \frac{t}{T} < \lfloor \frac{t}{T} \rfloor + 1$).

Proof. With our notations, the probability that only the first component is replaced at time nT (given that $Y_0 = x$) is:

$$R_1(x, nT) - R_{12}(x, nT).$$

We get:

$$C(x, [0, t]) = c_u U(x, [0, t]) + (c_1 + c_r) \sum_{n:nT < t} [R_1(x_1, nT) - R_{12}(x, nT)]$$

$$+ (c_2 + c_r) \sum_{n:nT < t} [R_2(x_2, nT) - R_{12}(x, nT)]$$

$$+ (c_1 + c_2 + c_r) \sum_{n:nT < t} R_{12}(x, nT) + c_p \lfloor \frac{t}{T} \rfloor$$

which may be synthetized into Eq.(6). ■

We now have to compute the different quantities involved in $C(x, [0, t])$, which is done in the following proposition.

Proposition 3 *Let $x = (x_1, x_2) \in [0, M_1] \times [0, M_2]$. Given that the system starts from $Y_0 = x$, for the first period, we have:*

$$R_i(x, T) = \bar{F}_T^{(i)}(M_i - x_i), \text{ for } i = 1, 2,$$

$$R_{12}(x, T) = \bar{F}_T(M_1 - x_1, M_2 - x_2),$$

$$U_P(x, [0, t]) = \int_0^t \bar{F}_u(L_1 - x_1, L_2 - x_2) du \text{ for } t \leq T,$$

$$U_S(x, [0, t]) = t - \int_0^t F_u(L_1 - x_1, L_2 - x_2) du \text{ for } t \leq T,$$

where subscripts P and S refer to the parallel and series cases, respectively.

For $n \geq 2$, we have the following Markov renewal equations:

$$R_i(x_i, nT) = \int_{\mathbb{R}_+} R_i(y_i, (n-1)T) Q^{(i)}(x_i, dy_i)$$

for $i = 1, 2$ and $x_i \in [0, M_i]$ and

$$\begin{aligned} R_{12}(x, nT) &= \iint_{\mathbb{R}_+^2} R_{12}(y, (n-1)T) \mathcal{Q}(x, dy), \\ U(x, [T, t)) &= \iint_{\mathbb{R}_+^2} U(y, [0, t-T)) \mathcal{Q}(x, dy) \end{aligned}$$

for $x = (x_1, x_2) \in [0, M_1] \times [0, M_2]$ and $t > T$, where $U = U_S$ or U_P .

Proof. The two first equations are clear, noting that

$$\begin{aligned} R_{12}(x, T) &= \mathbb{P}\left(x_1 + X_T^{(1)} > M_1, x_2 + X_T^{(2)} > M_2\right) \\ &= \bar{F}_T(M_1 - x_1, M_2 - x_2) \end{aligned}$$

(with a similar reasoning for the first one). As for the third and fourth equations, for $t \leq T$, we have for the series case (e.g.):

$$\begin{aligned} U_S(x, [0, t)) &= \mathbb{E}_x \left(\int_0^t (1 - \mathbf{1}_{[0, L_1] \times [0, L_2]}(X_u)) du \right) \\ &= t - \int_0^t \mathbb{P}_x \left(X_u^{(1)} \leq L_1, X_u^{(2)} \leq L_2 \right) du \\ &= t - \int_0^t F_u(L_1 - x_1, L_2 - x_2) du. \end{aligned}$$

From the second period, conditioning on the whole history at time T ($\mathcal{F}_T = \sigma(Y_s, s \leq T)$) and using the Markov property at time T , we get for all $n \geq 2$:

$$\begin{aligned} R_{12}(x, nT) &= \mathbb{E}_x \left[\mathbf{1}_{\{Y_{nT}^{(1)} > M_1, Y_{nT}^{(2)} > M_2\}} \right] \\ &= \mathbb{E}_x \left[\mathbb{E}_x \left(\mathbf{1}_{\{Y_{nT}^{(1)} > M_1, Y_{nT}^{(2)} > M_2\}} \mid \mathcal{F}_T \right) \right] \\ &= \mathbb{E}_x \left[\mathbb{E}_x \left(\mathbf{1}_{\{Y_{nT}^{(1)} > M_1, Y_{nT}^{(2)} > M_2\}} \mid Y_T \right) \right] \\ &= \mathbb{E}_x [R_{12}(Y_T, (n-1)T)] \\ &= \iint_{\mathbb{R}_+^2} R_{12}(y, (n-1)T) \mathcal{Q}(x, dy). \end{aligned}$$

Similar arguments may be used for the other quantities. ■

Such results allow to recursively compute the different quantities involved in the cost, using discretized versions of the underlying transition kernels and of the different quantities.

3.3 The cost on an infinite horizon time

Setting $c(I)$ to be the random cumulated cost on some time interval I , the point here is to prove existence and to compute the asymptotic unitary cost per unit time, which is defined by

$$C_\infty = \lim_{t \rightarrow \infty} \frac{c([0, t])}{t}.$$

As a first step, one can note that each time both components are simultaneously replaced, the system is as good as new, and its future evolution is stochastically identical to that of the initial system and independent of its past. The stochastic process $Y = (Y_t)_{t \geq 0}$ hence appears as a regenerative process, where simultaneous replacements of both components are regeneration times. The length of a generic cycle is τT , where

$$\tau = \inf (n \geq 1 : Y_{nT} = (0, 0)). \quad (7)$$

Lemma 4 *Under the assumption $\bar{F}_T(M_1, M_2) > 0$, the mean length of a generic cycle is finite: $\mathbb{E}(\tau) < +\infty$.*

Proof. Let

$$\alpha = \mathbb{P}(\tau > 1) = 1 - \bar{F}_T(M_1, M_2),$$

with $\alpha \in [0, 1)$ by assumption. For all $n \in \mathbb{N}^*$, we have:

$$\begin{aligned} \mathbb{P}(\tau > n + 1) &= \mathbb{P}(\tau > n; \tau > n + 1) \\ &= \mathbb{E}[\mathbf{1}_{\{\tau > n\}} \mathbb{E}(\mathbf{1}_{\{\tau > n+1\}} | \mathcal{F}_{nT})] \\ &= \mathbb{E}[\mathbf{1}_{\{\tau > n\}} h(Y_{nT})] \end{aligned}$$

with

$$\begin{aligned} h(x) &= \mathbb{E}(\mathbf{1}_{\{\tau > n+1\}} | Y_{nT} = x) \\ &= \mathbb{P}_x(\tau > 1) \\ &= 1 - \bar{F}_T(M_1 - x_1, M_2 - x_2) \\ &\leq \alpha \end{aligned}$$

due to the Markov property. We hence have

$$\mathbb{P}(\tau > n + 1) \leq \mathbb{E}[\mathbf{1}_{\{\tau > n\}} \alpha] = \alpha \mathbb{P}(\tau > n)$$

for all $n \geq 1$ and consequently $\mathbb{P}(\tau > n) \leq \alpha^n$, all $n \geq 1$. This provides:

$$\mathbb{E}(\tau) = \sum_{n=0}^{\infty} \mathbb{P}(\tau > n) \leq \sum_{n=0}^{\infty} \alpha^n < \infty.$$

■

As $(Y_t)_{t \geq 0}$ is a regenerative process with finite mean length cycle $\mathbb{E}(\tau T) = T\mathbb{E}(\tau)$, we derive from classical renewal theory [10] the almost sure existence of the asymptotic unitary cost C_∞ and its following expression:

$$C_\infty = \frac{\mathbb{E}(c([0, \tau T]))}{\mathbb{E}(\tau T)}.$$

The point now is to compute this quantity. With that aim, we follow [11] and we express it with respect to the stationary distribution of the Markov chain $(Y_{nT})_{n \geq 0}$.

Proposition 5 Under the assumption $\bar{F}_T(M_1, M_2) > 0$, the Markov chain $(Y_{nT})_{n \geq 0}$ admits a unique stationary distribution π (say). Besides:

$$C_\infty = \frac{\mathbb{E}_\pi [C(\cdot, [0, T])]}{T} \quad (8)$$

where

$$\mathbb{E}_\pi [C(\cdot, [0, T])] = \iint_{[0, M_1] \times [0, M_2]} C(x, [0, T]) \pi(dx) \quad (9)$$

and where we recall that $C(x, [0, T])$ stands for the mean cumulated cost on $[0, T)$, given that the system starts from x , see Section 3.2.

Proof. This proof follows step by step [11]. We recall the reasoning here, for sake of completeness.

First, with the help of Lemma 4, we know that the Markov chain almost surely comes back to state $(0, 0)$ in a finite time. So that $(Y_{nT})_{n \geq 0}$ is a Harris chain. According to [10], there consequently exists a stationary measure ν for the Markov chain $(Y_{nT})_{n \geq 0}$, which is given by

$$\nu(A) = \mathbb{E} \left(\sum_{n=0}^{\tau-1} \mathbf{1}_{\{Y_{nT} \in A\}} \right) \quad (10)$$

for any Borel set A of $[0, M_1] \times [0, M_2]$, where ν is unique up to a multiplicative constant. As $\nu([0, M_1] \times [0, M_2]) = \mathbb{E}(\tau)$ is finite, the measure ν can be normalized into one single stationary distribution, which is provided by

$$\pi = \frac{\nu}{\nu([0, M_1] \times [0, M_2])} = \frac{\nu}{\mathbb{E}(\tau)}. \quad (11)$$

Also

$$\begin{aligned} \mathbb{E}(c([0, \tau T])) &= \mathbb{E} \left(\sum_{i=0}^{\tau-1} c([iT, (i+1)T]) \right) \\ &= \sum_{i=0}^{+\infty} \mathbb{E} (c([iT, (i+1)T]) \mathbf{1}_{\{\tau > i\}}) \end{aligned}$$

Now, for all $i \in \mathbb{N}$, using that the event $\{\tau > i\}$ belongs to \mathcal{F}_{iT} and due to the Markov property at time iT , we get:

$$\begin{aligned} &\mathbb{E} (c([iT, (i+1)T]) \mathbf{1}_{\{\tau > i\}}) \\ &= \mathbb{E} (\mathbb{E} (c([iT, (i+1)T]) | \mathcal{F}_{iT}) \mathbf{1}_{\{\tau > i\}}) \\ &= \mathbb{E} (C(Y_{iT}, [0, T]) \mathbf{1}_{\{\tau > i\}}). \end{aligned}$$

This provides

$$\begin{aligned} \mathbb{E}(c(\tau T)) &= \mathbb{E} \left(\sum_{i=0}^{\tau-1} C(Y_{iT}, [0, T]) \right) \\ &= \iint_{[0, M_1] \times [0, M_2]} C(x, [0, T]) \nu(dx) \end{aligned}$$

due to Eq.(10), from where we derive Eq.(9), using $\nu = \mathbb{E}(\tau) \pi$ (see Eq.(11)). ■

To compute the asymptotic unitary cost provided by Eq.(9), we now have left to compute the stationary distribution π of the Markov chain $(Y_{nT})_{n \in \mathbb{N}}$. The results are provided under the assumption that the distribution μ_T of X_T admits a density with respect to Lebesgue measure. This assumption is only meant to make the results more readable but is in no case mandatory.

Proposition 6 *Assume that the distribution μ_T admits a density f_T with respect to Lebesgue measure and let*

$$\begin{aligned} g(y_1, y_2) &= \int_{M_1}^{\infty} f_T(u_1 - y_1, y_2) du_1, \\ h(y_1, y_2) &= \int_{M_2}^{\infty} f_T(y_1, u_2 - y_2) du_2, \\ k(y_1, y_2) &= \bar{F}_T(M_1 - y_1, M_2 - y_2), \end{aligned}$$

for all $0 \leq y_1 \leq M_1$ and all $0 \leq y_2 \leq M_2$.

The invariant distribution π of the Markov chain $(Y_{nT})_{n \geq 0}$ is of the shape

$$\begin{aligned} \pi(dx) &= a_{12}(x_1, x_2) dx_1 dx_2 + a_1(x_1) dx_1 \delta_0(dx_2) \\ &\quad + a_2(x_2) \delta_0(dx_1) dx_2 + a_4 \delta_0(dx_1) \delta_0(dx_2), \end{aligned} \quad (12)$$

where (a_{12}, a_1, a_2, a_4) is solution of the following set of integral equations:

$$\begin{aligned} a_{12}(x_1, x_2) &= \int_0^{x_1} \int_0^{x_2} a_{12}(y_1, y_2) f_T(x_1 - y_1, x_2 - y_2) dy_1 dy_2 \\ &\quad + \int_0^{x_2} a_2(y_2) f_T(x_1, x_2 - y_2) dy_2 + \int_0^{x_1} a_1(y_1) f_T(x_1 - y_1, x_2) dy_1 + a_4 f_T(x_1, x_2), \end{aligned} \quad (13)$$

$$\begin{aligned} a_1(x_1) &= \int_0^{x_1} \int_0^{M_2} a_{12}(y_1, y_2) h(x_1 - y_1, y_2) dy_1 dy_2 \\ &\quad + \int_0^{M_2} a_2(y_2) h(x_1, y_2) dy_2 + \int_0^{x_1} a_1(y_1) h(x_1 - y_1, 0) dy_1 + a_4 h(x_1, 0), \end{aligned} \quad (14)$$

$$\begin{aligned} a_2(x_2) &= \int_0^{M_1} \int_0^{x_2} a_{12}(y_1, y_2) g(y_1, x_2 - y_2) dy_1 dy_2 \\ &\quad + \int_0^{x_2} a_2(y_2) g(0, x_2 - y_2) dy_2 + \int_0^{M_1} a_1(y_1) g(y_1, x_2) dy_1 + a_4 g(0, x_2), \end{aligned} \quad (15)$$

and

$$\begin{aligned} a_4 &= \int_0^{M_1} \int_0^{M_2} a_{12}(y_1, y_2) k(y_1, y_2) dy_1 dy_2 \\ &\quad + \int_0^{M_2} a_2(y_2) k(0, y_2) dy_2 + \int_0^{M_1} a_1(y_1) k(y_1, 0) dy_1 + a_4 k(0, 0) \end{aligned} \quad (16)$$

for all $0 \leq x_1 \leq M_1$ and all $0 \leq x_2 \leq M_2$,

with the additional normalizing constraint:

$$\int_0^{M_1} \int_0^{M_2} a_{12}(y_1, y_2) dy_1 dy_2 + \int_0^{M_1} a_1(y_1) dy_1 + \int_0^{M_2} a_2(y_2) dy_2 + a_4 = 1. \quad (17)$$

Proof. Writing $\pi(dx) = (\pi\mathcal{Q})(dx)$, where \mathcal{Q} is provided in Proposition 1, we have

$$\pi(dx) = \sum_{i=1}^4 \iint_{[0, M_1] \times [0, M_2]} \pi(dy) \mathcal{Q}_i(y, dx)$$

which may be written as:

$$\begin{aligned} \pi(dx) = & \left(\int_0^{x_1} \int_0^{x_2} f_T(x_1 - y_1, x_2 - y_2) \pi(dy) \right) dx_1 dx_2 \\ & + \left(\int_0^{M_1} \int_0^{x_2} g(y_1, x_2 - y_2) \pi(dy) \right) \delta_0(dx_1) dx_2 \\ & + \left(\int_0^{x_1} \int_0^{M_2} h(x_1 - y_1, y_2) \pi(dy) \right) dx_1 \delta_0(dx_2) \\ & + \left(\int_0^{M_1} \int_0^{M_2} k(y_1, y_2) \pi(dy) \right) \delta_0(dx_1) \delta_0(dx_2). \end{aligned} \quad (18)$$

This proves that the invariant distribution is of the form Eq.(12).

Next, introducing Eq.(12) into Eq.(18) and identifying the terms with respect to $dx_1 dx_2$, $dx_1 \delta_0(dx_2)$, $\delta_0(dx_1) dx_2$ and $\delta_0(dx_1)\delta_0(dx_2)$, we obtain the expressions of a_{12} , a_1 , a_2 and a_4 provided by Eq.(13)-Eq.(16), respectively. Eq.(17) simply is $\int_0^{M_1} \int_0^{M_2} \pi(dy) = 1$. ■

The stationary distribution π (or rather (a_{12}, a_1, a_2, a_4)) now appears as solution of a set of Volterra integral equations of the second kind. Taking f_T smooth enough as in the next section, a discretized version of π may be computed using an iterative scheme based on the method of successive approximations [12, 13], as in [7].

4 Numerical experiments

4.1 Bivariate Gamma process

The same specific model as in [6, 14] is here used for the numerical experiments, which we call bivariate Gamma process. We recall its construction, for sake of completeness. We first remind that a univariate Gamma process with parameters (a, b) (where $a, b > 0$) is a subordinator Z such that for every $t \geq 0$, the random variable Z_t is Gamma distributed $\Gamma(at, b)$ with p.d.f.:

$$f_{at,b}(x) = \frac{1}{\Gamma(at)} b^{at} e^{-bx} x^{at-1} 1_{\{x>0\}}.$$

We only envision the case $b = 1$ in the following, which is no restriction.

Starting from three independent univariate Gamma processes $(Z_t^{(i)})_{t \geq 0}$ with parameters $(\alpha_i, 1)$ for $i = 1, 2, 3$ (where $\alpha_1, \alpha_2, \alpha_3 > 0$), we set

$$\begin{aligned} X_t^{(1)} &= Z_t^{(1)} + Z_t^{(3)}, \\ X_t^{(2)} &= Z_t^{(2)} + Z_t^{(3)}. \end{aligned}$$

The process $(X_t)_{t \geq 0} = (X_t^{(1)}, X_t^{(2)})_{t \geq 0}$ then is a bivariate subordinator with Gamma marginal processes and marginal parameters $(a_i, 1)$ where $a_i = \alpha_i + \alpha_3$ for $i = 1, 2$. Pearson's correlation coefficient between the two random variables $X_t^{(1)}$ and $X_t^{(2)}$ is independent of t and given by

$$\rho = \frac{\alpha_3}{\sqrt{a_1 a_2}}. \quad (19)$$

We consequently have $\alpha_1 = a_1 - \rho\sqrt{a_1 a_2}$, $\alpha_2 = a_2 - \rho\sqrt{a_1 a_2}$ and $\alpha_3 = \rho\sqrt{a_1 a_2}$, with $0 \leq \rho \leq \rho_{\max} = \min\left(\sqrt{\frac{a_1}{a_2}}, \sqrt{\frac{a_2}{a_1}}\right)$. Two alternate parameterizations hence are available for $(X_t)_{t \geq 0}$: either $(\alpha_1, \alpha_2, \alpha_3)$ or (a_1, a_2, ρ) . Besides, all the dependence between the marginal processes is contained in the linear correlation coefficient ρ .

4.2 Validation of the results

We here present a few numerical experiments to validate our theoretical results and their practical implementation, especially for the invariant distribution π , which is the most technical to compute.

In all the section, the parameters of the bivariate Gamma process are $(a_1, a_2, \rho) = (4, 4, 0.6)$. The preventive maintenance thresholds are $M_1 = 0.5$ and $M_2 = 0.3$ and the inspection period is $T = 0.6$. (No other parameters needed here).

As a first case, the probabilities of replacement of one or two components are computed at first and second inspection times, via the results of Proposition 3 with discretization steps $h_1 = h_2 = 0.01$. The results are displayed in Table 1, as well as those obtained by Monte-Carlo (MC) simulation, with 10^5 histories and 95% confidence intervals (CI). All results are coherent. Note that, though both components share a common deterioration parameter ($a_1 = a_2$), their preventive thresholds are different ($M_1 > M_2$), which leads to higher replacement probabilities for the second component. As expected, the probability of simultaneous replacements (R_{12}) is lower than the probability of replacing at least one component (R_i , $i = 1, 2$).

In Table 2, results are displayed for the asymptotic probabilities of replacement of one or two components by an inspection, namely for $\mathbb{E}_\pi(R_i(\cdot, T))$, $i = 1, 2$ and $\mathbb{E}_\pi(R_{12}(\cdot, T))$, with

$$\mathbb{E}_\pi(R_{12}(\cdot, T)) = \int_0^{M_1} \int_0^{M_2} R_{12}(x, T) \pi(dx)$$

and similar expressions for the other terms. The distribution π has been numerically computed as explained at the end of Section 3.3 and $R_{12}(x, T)$ is computed via Proposition 3, just as for Table 1. Results are also provided by MC simulations, with 10^7 histories. For these MC results, we have used the fact

that π is the asymptotic distribution of the Markov chain $(Y_{nT})_{n \in \mathbb{N}}$ and waited until the chain is stabilized:

$$\mathbb{E}_\pi(R_{12}(\cdot, T)) = \lim_{n \rightarrow +\infty} \mathbb{E}(R_{12}(Y_{nT}, T)) \simeq \mathbb{E}(R_{12}(Y_{NT}, T))$$

for large N . Here again, all results are coherent.

Finally, the convergence of the distribution of $(Y_{nT})_{n \geq 0}$ towards π is illustrated in Figure 2 through the numerical convergence of the mean rate of simultaneous replacements on $[0, nT]$ per unit time towards the asymptotic rate:

$$\lim_{n \rightarrow +\infty} \frac{1}{nT} \sum_{i=1}^n R_{12}(0, iT) = \frac{1}{T} \mathbb{E}_\pi(R_{12}(\cdot, T)).$$

To obtain this figure, all computations have been performed using the theoretical results of the previous sections (no Monte-Carlo simulation).

Based on the numerical results of this section (and on others not displayed here), one may think that the practical implementation of our theoretical results is correct.

4.3 Examples

Parameters for all examples are displayed in Table 3, as well as the system structure when necessary (for computations of mean down times and costs).

Example 1 *Two parts of the invariant distribution π of $(Y_{nT})_{n \geq 0}$ are displayed in Figure 3: functions $a_1(x_1)$ and $a_{12}(x)$, which are the p.d.f.'s of π with respect to dx_1 $\delta_0(dx_2)$ (replacement of component 2 only) and of $dx_1 dx_2$ (no replacement), respectively. With the chosen parameters, we observe that $a_1(x_1)$ is increasing with x_1 and that $a_{12}(x)$ is concave. Also, we get $a_4 \simeq 0.89$, so that the probability of simultaneous replacements of both components is here quite high for large times.*

This example illustrates the variations of the mean rate of simultaneous replacements per unit time with respect to the period T , both in the asymptotic and finite time cases (see Figure 4). For the finite horizon case $[0, t_0]$ (with $t_0 = 4$ fixed), this mean rate of replacements is not continuous with respect to T (Figure 4a). The discontinuity points are the points T such that there exists some number n satisfying $t_0 = nT$, because at these points, we do not consider possible replacements at t_0 . As for the asymptotic case, the rate of simultaneous replacements seems continuous with respect to T (Figure 4b).

Figure 5a next shows that, as expected, the unitary cumulated mean down time on $[0, t_0]$, namely $U(0, [0, t_0])/t_0$, is increasing with T . Though we have not studied it from a theoretical point of view, one might indeed think that $U(0, [0, t_0])$ (with t_0 fixed) increases with T . Figure 5b shows that the asymptotic unavailability $\mathbb{E}_\pi(U(\cdot, [0, T]))/T$ is also increasing with T .

The asymptotic unitary cost is plotted in Figure 6b as a function of T . The function is convex and admits a single minimum at $T_{opt}^\infty \simeq 0.52$. On the finite horizon $[0, t_0]$, the mean unitary cost as a function of T is not continuous (Figure 6a) and the minimum is at $T_{opt} \simeq 0.03$. The optimal inspection periods hence are very different for the infinite and finite horizons.

Example 2 *The influence of the preventive maintenance thresholds (M_1, M_2) on the cost function is here studied, in the case of a series system. We take $c_p = c_1 = 0$ and consider several cases for (c_2, c_u, c_r) . Figures have similar shapes for the finite and infinite horizons. To save some space, they are only provided for the infinite case. As we can see, the cost function may be convex (Figure 7), concave (Figure 8) or more complicated (Figure 9). So, it seems hard to say anything about the shape of the cost function with respect to the preventive maintenance thresholds (M_1, M_2) in a general setting. This may be due to the fact that the mean number of replacements and the down-time durations may have reverse concavity with respect to (M_1, M_2) .*

Example 3 *We finally look at the influence of the dependence between the two components on the probability of simultaneous replacements of both components. Let us recall that, for the bivariate Gamma model, this dependence is measured by Pearson's correlation ρ , see Eq.(19). The probability of simultaneous replacements of both components is plotted with respect to ρ in Figure 10. We can see that it is not monotone with respect to ρ , which is in concordance with Remark 2.*

5 Conclusion

We here considered a two-component system, with deterioration modelled by a bivariate subordinator. A condition-based preventive replacement policy has been proposed, which is rather classical in the univariate setting, with deterioration modelled by a Gamma process. In the bivariate case, it leads to imperfect repairs at the system level, which highly complicates the study. As an example, the four parts of the stationary distribution of the underlying Markov chain have been characterized as the single solution of a set of four Volterra integral equations of the second kind, and the numerical computation of the stationary distribution is much more demanding than in the univariate setting. In the same way, the variations of the cost functions with respect to each parameter have been observed to be complicated and sometimes not easily predictable (see Figures 9 or 10 e.g.). The qualitative results obtained in a univariate setting cannot hence be easily adapted to the bivariate case and there consequently is a clear need for further development.

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TABLES & FIGURES

	Formula $h_1 = 0.01, h_2 = 0.01$	MC simulation $N = 10^5$	MC 95% CI
$R_1(0, T)$	0.9551	0.9555	[0.9542 0.9568]
$R_1(0, 2T)$	0.9569	0.9572	[0.9562 0.9587]
$R_2(0, T)$	0.9849	0.9850	[0.9842 0.9857]
$R_2(0, 2T)$	0.9851	0.9848	[0.9840 0.9856]
$R_{12}(0, T)$	0.9456	0.9456	[0.9441 0.9470]
$R_{12}(0, 2T)$	0.9465	0.9469	[0.9455 0.9483]

Table 1: Probabilities of replacement at first and second inspection times

	Formula $h_1 = 0.01, h_2 = 0.01$	MC Simulation $N = 10^7$	MC 95% CI
$\mathbb{E}_\pi(R_1(., T))$	0.9568	0.9568	[0.9555 0.9569]
$\mathbb{E}_\pi(R_2(., T))$	0.9851	0.9851	[0.9850 0.9851]
$\mathbb{E}_\pi(R_{12}(., T))$	0.9467	0.9466	[0.9464 0.9467]

Table 2: Asymptotic probabilities of replacement at inspection times

	Structure	a_1	a_2	ρ	L_1	L_2	M_1	M_2	T	c_1	c_2	c_r	c_p	c_u	t_0
Ex .1	-	4	9	0.5	-	-	0.6	0.9	0.5	-	-	-	-	-	-
Ex. 1	Parallel	4	4	0.5	0.7	0.6	0.5	0.5	-	1	1	1	0.01	10	4
Ex. 2	Series	4	9	0.5	1.2	1.4	-	-	0.5	0	-	-	0	-	4T
Ex. 3	-	4	9	-	-	-	4	5	1	-	-	-	-	-	4T

Table 3: Parameter values used in the examples

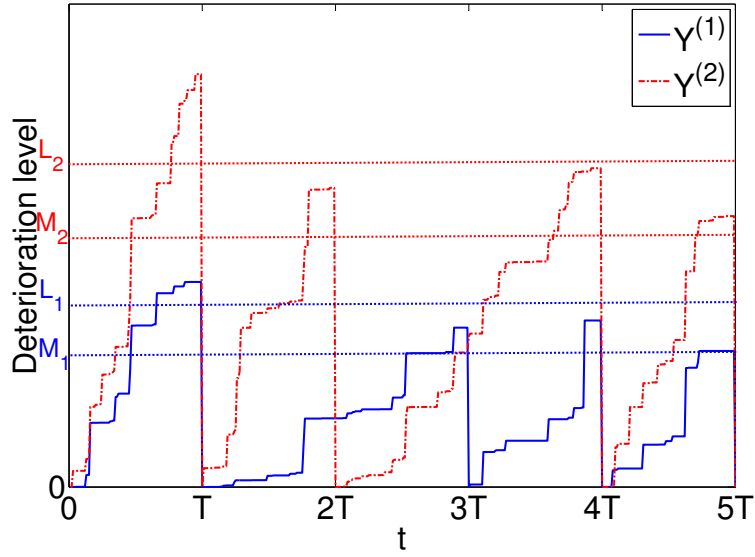


Figure 1: The preventive maintenance policy

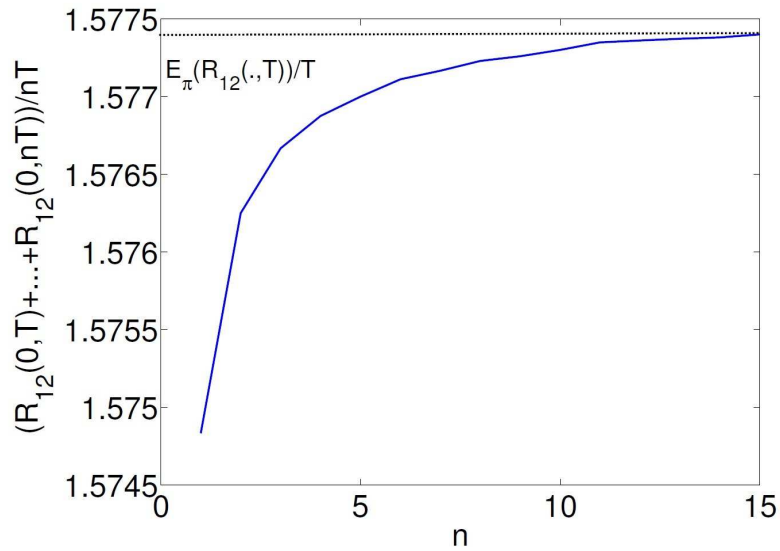


Figure 2: Illustration of the convergence of the Markov chain $(Y_{nT})_{n \geq 1}$

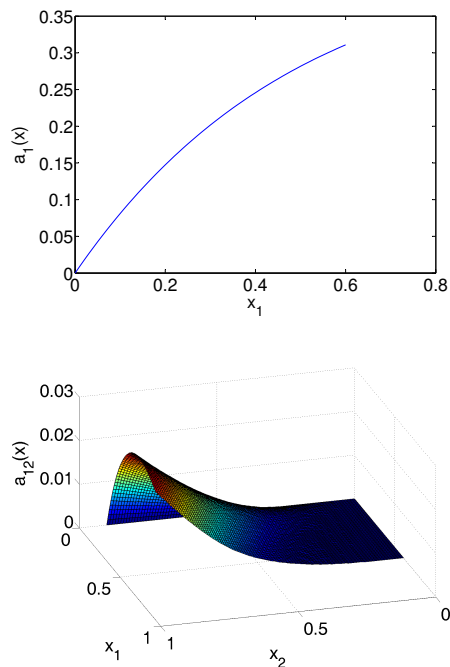
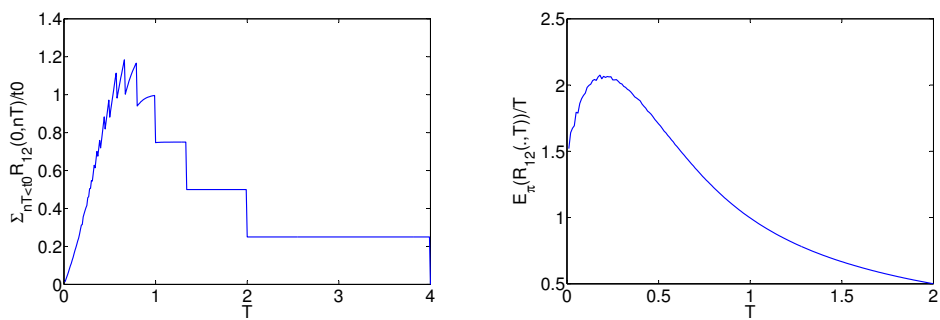


Figure 3: Parts of the invariant distribution of $(Y_{nT})_{n \geq 0}$, Example 1



(a) Finite time case
 (b) Asymptotic case
 Figure 4: Mean rate of simultaneous replacements as a function of T , Example 1

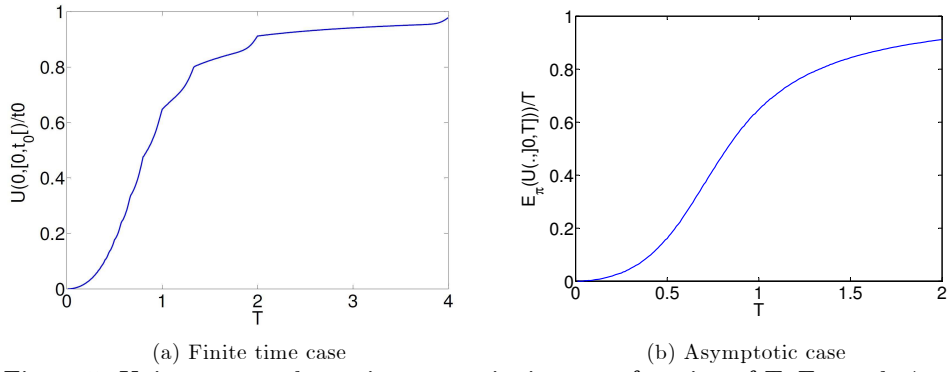


Figure 5: Unitary mean down time per unit time as a function of T , Example 1

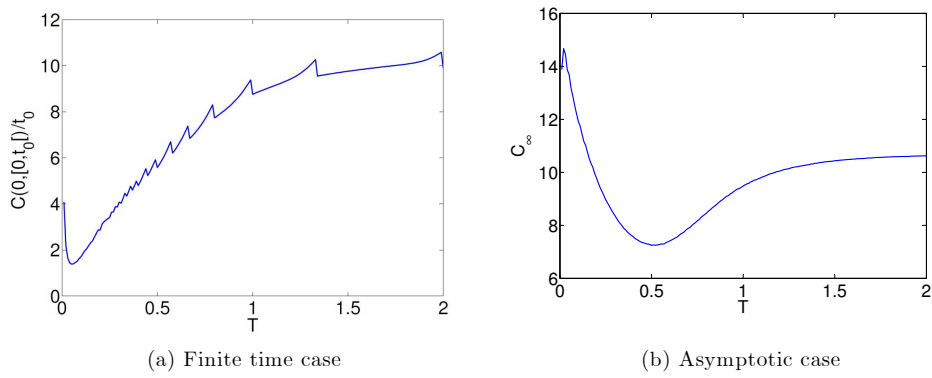


Figure 6: The cost rates with respect to T , Example 1.

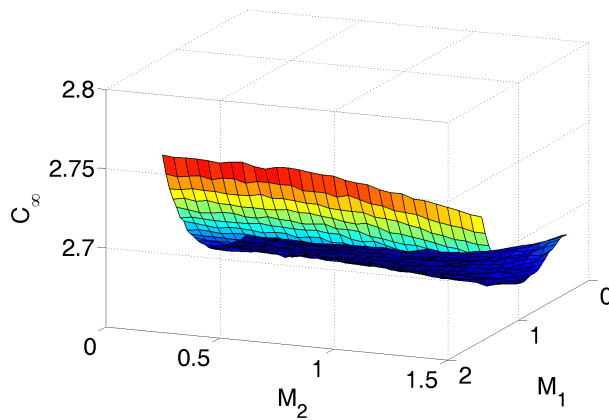


Figure 7: The asymptotic cost rate with respect to (M_1, M_2) , Example 2, $c_2 = 0$, $c_r = 1$, $c_u = 2$

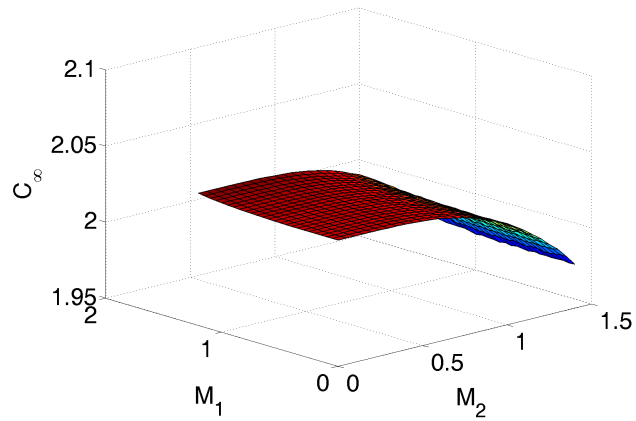


Figure 8: The asymptotic cost rate with respect to (M_1, M_2) , Example 2, $c_2 = 1$, $c_r = 0$, $c_u = 0.1$

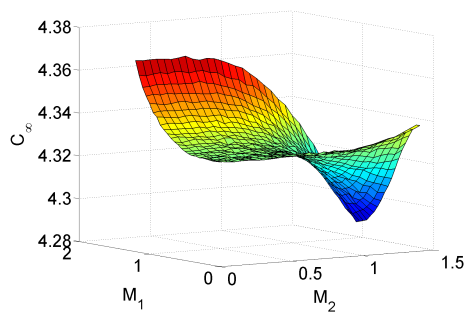


Figure 9: The asymptotic cost rate with respect to (M_1, M_2) , Example 2, $c_2 = 0$, $c_r = 2$, $c_u = 1$

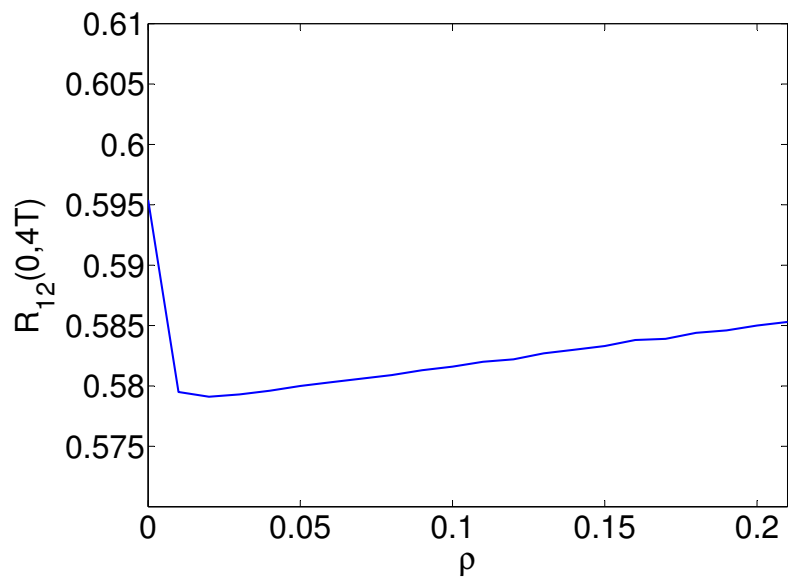


Figure 10: Probability of simultaneous replacement of both components with respect to ρ , Example 3