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# On the Solubility of Group IV Elements (Ti, Zr, Hf) in Liquid Aluminum Below 800°C

O. Dezellus, B. Gardiola, and J. Andrieux

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The solubility of group IV transition metals Ti, Zr, and Hf in liquid Al was measured by the settling technique coupled with ICP-AES analysis after dissolution in hydrochloric acid. The kinetic aspect of the settling technique was studied in order to show that, after a cooling step, thermodynamic equilibrium between the liquid and solid phases could be achieved after only 1 h. Finally, it was verified that solubility values obtained after a cooling or a heating step were fully consistent. The present results demonstrate that the immersion-and-settling technique allows reliable solubility values to be determined. The results confirm the values previously reported in the literature and the good description for the three binaries by the existing CALPHAD optimizations concerning the liquidus below 800°C.

**Keywords** aluminum alloys, binary system, experimental techniques, liquidus

## 1. Introduction

The alloying of Al with group IV transition metals (Ti, Zr, and Hf) constitutes a promising solution for the development of creep-resistant and thermally stable Al-based alloys.<sup>[1]</sup> A strengthening effect is obtained by precipitation of an ordered Al<sub>3</sub>M aluminide (M = Ti, Zr, or Hf) from the supersaturated solid solution matrix. The temporal sequence of precipitation consists initially of the formation of metastable cubic L1<sub>2</sub> Al<sub>3</sub>M precipitates which transform to their equilibrium tetragonal forms (D0<sub>22</sub> or D0<sub>23</sub>) after prolonged aging at temperatures above 450°C.<sup>[2]</sup> This precipitation sequence has been demonstrated for alloys prepared by non-equilibrium processing routes, such as rapid solidification techniques<sup>[3–6]</sup> or mechanical alloying,<sup>[7–10]</sup> that allow the formation of a supersaturated  $\alpha$ -Al solid solution followed by the precipitation of the L1<sub>2</sub> metastable form of the aluminide. However, some difficulties arise when conventional solidification is used.

According to the accepted phase diagrams, among Al-Ti, Al-Zr, and Al-Hf systems are characterized by the presence of a peritectic transition between the  $\alpha$ -Al solid solution and the Al<sub>3</sub>M aluminide.<sup>[11–13]</sup> For liquid Al enriched in transition metals, the first crystallization phase to form is a pro-peritectic Al<sub>3</sub>M ordered phase. During conventional casting, this primary phase nucleates and grows into coarse grains (typically 100  $\mu$ m), leading to a significant decrease

in the liquid of the transition metal. As a consequence, the final  $\alpha$ -Al solid solution is also depleted in solute, and this—associated with the peritectic nature of the phase diagram—limits the driving force for solid-state nucleation, i.e., the potential for age hardening.<sup>[14,15]</sup> According to the classical nucleation theory,<sup>[14]</sup> the ability of a peritectic alloy to be strengthened by precipitation during conventional casting is strongly related to the relative position of the liquidus and solvus lines. This results from the difficulty in obtaining a sufficient chemical driving-force (in other words supersaturation) in the solid solution at the aging temperature. As a consequence, accurate determination of liquid solubility is a key point for understanding the whole precipitation hardening process by a liquid route. The solubility of Ti in liquid aluminum has been extensively studied by different authors and techniques<sup>[16–21]</sup> and the results have been recently reviewed by Schuster et al.<sup>[13]</sup> Solubility of Zr in liquid Al was determined both by Fink et al. in 1939<sup>[22]</sup> and Chiotti et al. in 1964.<sup>[23]</sup> Finally, the solubility of Hf in liquid Al has been successively determined by Rath et al.<sup>[24]</sup> and Rokhlin et al.<sup>[25]</sup> and reviewed by Murray et al.<sup>[11]</sup> It should be noted that a good agreement was observed between the different authors for the solubility of Ti, Zr, and Hf in liquid Al.

Recently, Janghorban et al.<sup>[26]</sup> revised the Al-rich part of the Al-Zr binary system. The authors performed a specific bi-differential thermal analysis of an Al-1wt.%Zr alloy versus pure Al in a DSC apparatus and concluded that the transition of the binary alloy is observed at  $656 \pm 2^\circ\text{C}$ , i.e., 4 degrees lower than the melting temperature of pure Al. This result indicates a eutectic nature rather than the previously accepted peritectic.<sup>[11]</sup> As a consequence, if the last invariant is eutectic, then the solubility of Zr in solid  $\alpha$ -Al has to be lower than that in the liquid phase. This would be in disagreement with the solubility values reported in the literature for the liquid<sup>[22,23]</sup> and the solid phase.<sup>[22,27–29]</sup> Janghorban et al.<sup>[26]</sup> argued that solubility values obtained for the liquid phase by the immersion technique were not reliable, and usually underestimated, because of the

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formation of intermetallic compounds at the liquid-solid interface. Solid-state diffusion of the solute metal M through these compounds toward the liquid phase can then limit the kinetics of saturation of the liquid.

The aim of this work is to bring new insights in the discussion of the eutectic/peritectic nature of the transition in the Al-rich part of Al-M phase diagrams, where M = Ti, Hf, Zr. More specifically, the first objective of this study is to report reliable and unquestionable values for the solubility of Zr in liquid Al at temperatures below 800°C. The immersion technique has been used and experimental conditions have been carefully controlled to ensure thermodynamic equilibrium between the liquid and the solid. Moreover, the kinetic aspects of the immersion technique have also been studied in the case of Al-Zr. The second objective is to propose a consistent experimental determination of the solubility of Ti, Zr, and Hf in liquid Al. The crystallographic structures of the Al<sub>3</sub>M phases in the melts have been determined by single crystal XRD in order to remove ambiguities about the stability of the aluminides.

## 2. Experimental Procedure

Binary Al-M (M = Ti, Zr, or Hf) alloys were first prepared from pure aluminum (Alfa-Aesar 99.999% Al) and from lumps of pure M. Typical analyzes are shown in Table 1. For each set of experiments, a mass of about 80 g of these constituents was melted by radio frequency (rf) heating in an alumina crucible lined with Al<sub>2</sub>O<sub>3</sub> powder. The crucible has a conical shape with the following typical inner dimensions: height is about 70 mm, average diameter is about 30 mm. Aluminum was melted first at about 900°C and Group IV elements were then added either as pure metal (Ti and Hf) or, in case of Zr, in the form of the Al<sub>3</sub>Zr intermetallic compound previously synthesized by arc melting. The overall compositions of the melt prepared were 1.96 wt.%, (1.11 at.%), 3.44 wt.% (1.04 at.%), and 4.14 wt.% (0.65 at.%) for Ti, Zr, and Hf, respectively. These amounts were optimized to be in the liquid-Al<sub>3</sub>M region in the temperature range of the study and to minimize the amount of crystals in order to avoid accidental aspiration of settled crystals. The temperature was measured, with a precision better than ±0.2°C, by plunging a K-type (Ni/Cr) thermoelectric couple into the melt.

Dissolution of group IV elements and saturation of the melt was ensured by a holding time of about 2 h at 900°C and with regular stirring. The alloy was then removed from the induction coil device, placed in a radiant furnace at

800°C and left undisturbed for a minimum of 4 h at constant temperature. During this time, the undissolved crystals of the Al<sub>3</sub>M phase settled to the bottom of the crucible because of the difference in density between Al<sub>3</sub>M (3.4 g.cm<sup>-3</sup> for Al<sub>3</sub>Ti,<sup>[30]</sup> 4.13 g/cm<sup>3</sup> for Al<sub>3</sub>Zr, 6.32 g/cm<sup>3</sup> for Al<sub>3</sub>Hf<sup>[31]</sup>) and liquid Al (about 2.36 g/cm<sup>3</sup> below 800°C<sup>[32]</sup>). After careful removal of the dross at the center of the liquid surface, samples of liquid were taken from alloy melts by aspiration through a silica tube (inner and outer diameters: 4 and 6 mm, respectively) about 10 mm below the surface of the liquid-bath. To avoid metal/oxide reaction, the silica tube was previously lined with carbon black. Solidification of the melt in the carbon-lined silica tube upon aspiration was almost instantaneous, and fine-grained homogeneous rods, 10-30 mm in length, were obtained. The temperature was continuously monitored during liquid sampling and a decrease of a few Kelvin (3-7 K) was observed during immersion of the silica tube. As a consequence, the effective temperature of the sample was considered as the mean value during aspiration of the liquid with an uncertainty of ±3 K. The temperature of the liquid was then decreased (or increased) by a few tens of Kelvins, and the liquid left undisturbed for a minimum of 8 h before the next liquid sampling.

Small slices of 20-40 mg were then cut from the ingots obtained after liquid sampling by a diamond saw and their group IV element content was determined by chemical analysis (plasma emission spectroscopy, ICP-AES) after chemical dissolution in commercially pure hydrochloric acid. The relative uncertainty on measured values is about 5%. It should be noted that, while the kinetic phenomena may lead to an underestimation of solubility, another source of measurement error, associated with the liquid sampling technique, could lead to an overestimation: instead of pure liquid sampling, accidental aspiration of isothermal crystals in equilibrium with the liquid could occur. In this case, the overall chemical analysis will systematically lead to overestimated solubility values because of dissolution of both Al supersaturated solid solution and isothermal Al<sub>3</sub>M crystals in HCl. This problem can be avoided by sampling at a controlled depth in the liquid-bath, thus avoiding the lower part of the crucible, where the liquid is enriched with equilibrium crystals. The extent of the zone containing Al<sub>3</sub>M crystals is evaluated after solidification by optical micrographs performed on a cross-section of the solidified ingots. The results indicate an extent lower than 8 mm. As a consequence, from the comparison of this result with the height of the solidified ingots (about 60 mm) and the depth of liquid sampling (about 10 mm), it can be conclude that liquid sampling is performed at a distance higher than

**Table 1 Chemical composition (in ppm) of the metallic elements used in the present study as reported in the supplier certificates of analysis**

| Metal | Supplier   | Al     | Ca   | C   | Cr    | Cu   | Fe  | Ni   | Hf     | Si  | Zr     |
|-------|------------|--------|------|-----|-------|------|-----|------|--------|-----|--------|
| Al    | Alfa-Aesar | Matrix |      |     |       | 8    | 0.4 |      |        |     |        |
| Ti    | Goodfellow | 0.65   | <0.2 | 11  | <0.35 | 0.25 | 2   | 0.11 |        | 0.5 | 0.75   |
| Zr    | Goodfellow |        |      | 250 | 200   |      | 200 |      | 2500   |     | Matrix |
| Hf    | Neyco      | <15    |      |     | <15   | <5   |     | <5   | Matrix | <2  | <35    |

30 mm from the zone where settling of  $\text{Al}_3\text{M}$  crystals occurs.

In the present study, in order to validate the experimental procedure (liquid sampling, HCl dissolution, and ICP-AES analysis) and to obtain unquestionable results, a second analysis technique was used in the case of the Ti solute. Electron probe microanalysis (EPMA) was used to perform local analyzes of the sample after a visual inspection of the microstructure to avoid the possible presence of equilibrium crystals (present in the liquid during isothermal treatment). Some slices were embedded in resin to prepare polished sections that were examined by optical microscopy (OM) and scanning electron microscopy (SEM) and were characterized by EPMA in wavelength dispersive x-ray spectroscopy (WDS) mode. The latter analyzes were carried out using a Camebax apparatus (Cameca) under an accelerating voltage of 15 kV and with a beam current of 11 nA on areas of  $100 \times 100 \mu\text{m}^2$  by repeating six counts of 10 s on about 10–12 different areas. Analyzes were performed near the periphery of the ingots, where the quenching effect was the most effective and the microstructure was the finest on the same representative areas. The different counting rates obtained were corrected for background noise and compared with counting rates recorded under the same conditions on complex standards of  $\text{Al}_3\text{Ti}$  single crystals that were present in the bottom of the solidified ingot. With this procedure, the Ti content of the samples was obtained with a typical relative uncertainty of less than 5%.<sup>[33]</sup>

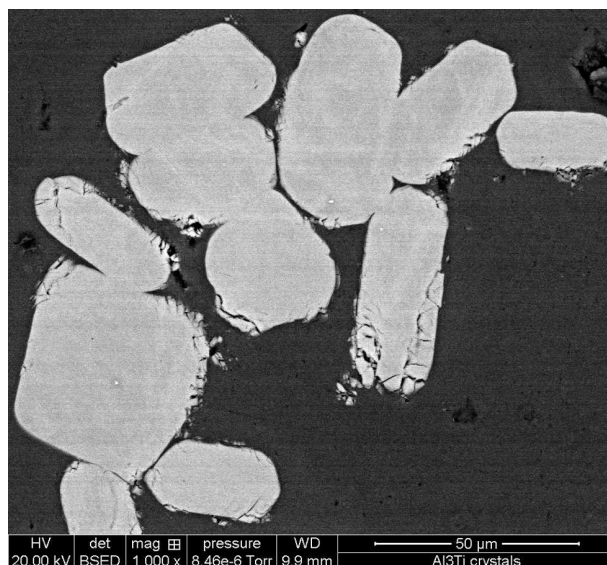
After cooling of the crucible containing the Al–M alloy, the solidified ingot was cut, embedded in resin, and polished. Micrographic analysis on cross-sections was then used to verify the presence and settling of  $\text{Al}_3\text{M}$  crystals and the complete consumption of the initial pieces of Ti or Hf. A small part of the bottom of the ingots, where the crystals of solid phase had settled, was then heat treated for 48 h at 700°C, quenched in water and finally dissolved in a 10 wt.% NaOH solution in order to remove the aluminum matrix and to extract some  $\text{Al}_3\text{M}$  crystals, which were subsequently characterized by single crystal x-ray diffraction (XRD).

### 3. Results

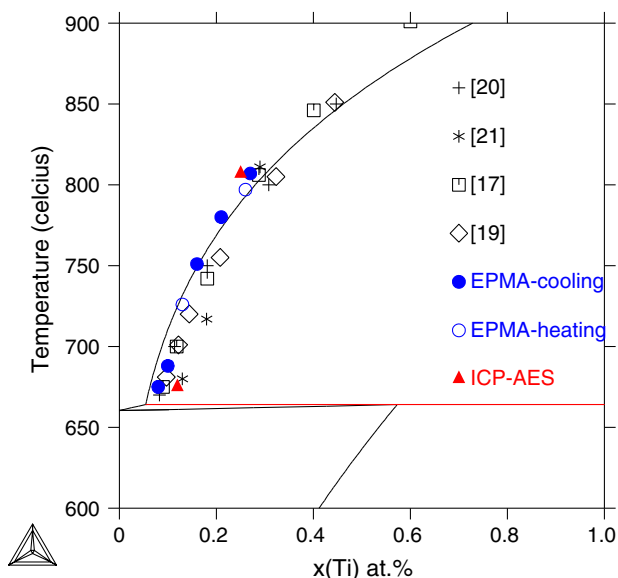
#### 3.1 Ti solubility in Liquid Al

Figure 1 shows the crystals present in the bottom part of the ingot in the backscattered electron mode. The most important feature is the absence of chemical contrast through the crystals, illustrating the consumption of the initial pure Ti pieces that were fully transformed into coarse  $\text{Al}_3\text{Ti}$  grains (confirmed by EDS measurements) with a spheroid shape and a typical size of about 30  $\mu\text{m}$ . This result indicates that saturation of the liquid Al in the Ti solute is not limited by a kinetic effect such as diffusion of Ti across a diffusion barrier of aluminides.

The results for Ti solubility in liquid Al are presented in Fig. 2 and compared both with other experimental values.<sup>[17,19–21]</sup> Several optimization of the Al–Ti system have been performed<sup>[34–36]</sup> that are in fairly good agreement for the description of the  $\text{Al}_3\text{Ti}$  liquidus below 900°C, as a



**Fig. 1** SEM backscattered electron image of  $\text{Al}_3\text{Ti}$  crystals observed in the bottom of the Al–Ti ingot after the complete liquid sampling process



**Fig. 2** Solubility limit of Ti in liquid Al determined by isothermal experiments at different temperatures and by using different analytical techniques: filled triangles are ICP-AES analysis, circles are EPMA analysis in WDS mode (the liquid sample is taken respectively during cooling—filled circles—and during heating—open circles). Experimental data are compared to previous experimental determinations<sup>[17,19–21]</sup> and to the calculated liquidus<sup>[34]</sup>

consequence, for sake of clarity the experimental results are only compared with the liquidus calculated from the set of parameters reported in Ref 34. It is worth noting first of all that chemical analysis and WDS analysis led to a coherent



set of solubility limit values for Ti in pure Al liquid. This quantitative agreement between a general and a local analysis technique highlights the fact that no aspiration of equilibrium crystals occurred during liquid sampling. Therefore, the solubility values reported in Fig. 2 are not overestimated. Moreover, it should be emphasized that EPMA results obtained on liquid samples both during cooling, i.e., desaturation of the liquid by precipitation of  $\text{Al}_3\text{Ti}$  crystals, or during heating, i.e., saturation of the liquid by dissolution of  $\text{Al}_3\text{Ti}$  crystals, are both aligned on the same liquidus curve. This convergence attests that the experimental values were obtained after thermodynamic equilibrium is reached.

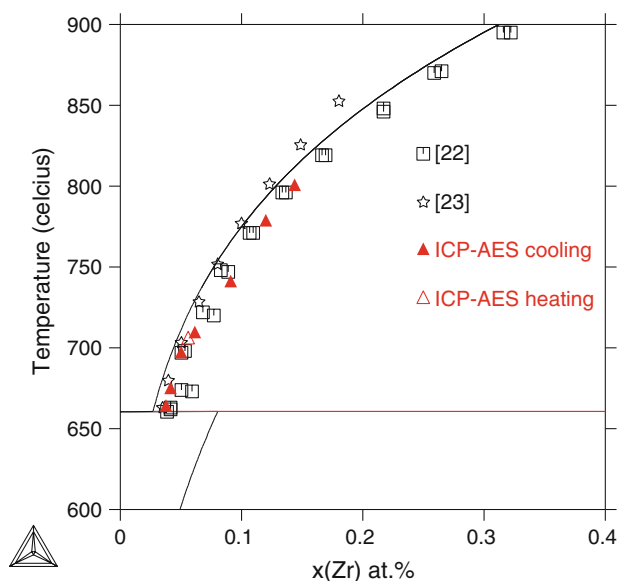
In the case of Ti solute, the dissolution of the Al matrix in a NaOH solution was not sufficiently selective to allow the extraction of  $\text{Al}_3\text{Ti}$  single crystals. As a consequence, it was not possible to determine by single crystal XRD the crystallographic structure of the solid phase present in the solidified ingot.

### 3.2 Zr Solubility in Liquid Al

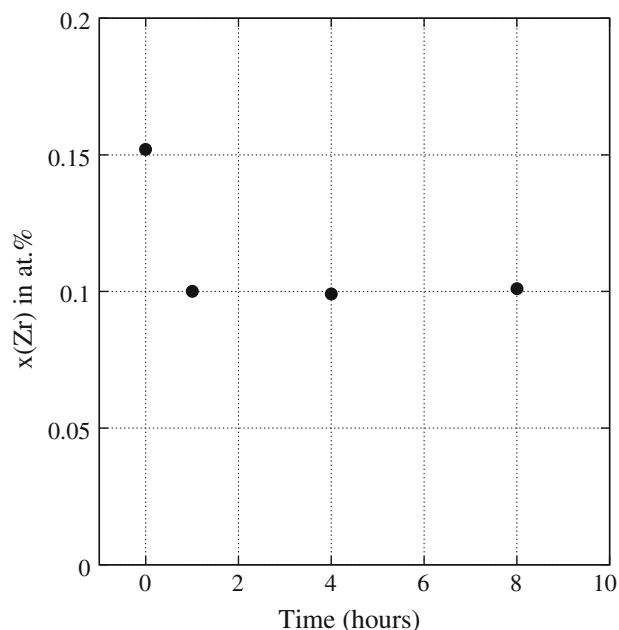
In the case of the Zr solute, liquid Al was saturated from  $\text{Al}_3\text{Zr}$  pellets synthesized using an arc furnace, a non-consumable tungsten electrode, and a copper water-cooled hearth. In order to ensure a homogeneous composition of the pellets, the alloys were re-melted at least five times and heat treated for several hundreds of hours at 600°C.

The results for Zr solubility in liquid Al are presented in Fig. 3 and compared both with other experimental values<sup>[22,23]</sup> and with the most recent optimisation of Wang et al.<sup>[37]</sup> Like Ti, the results of the present study are in good agreement with previous results given in the literature. After dissolution of the Al matrix in a 10 wt.%NaOH solution, the structure of the  $\text{Al}_3\text{Zr}$  aluminide was determined by single crystal XRD to be the tetragonal  $\text{D}_{023}$  form with lattice parameters  $a = 0.399$  nm and  $c = 1.73$  nm that are also in good agreement with existing literature.<sup>[38–41]</sup>

Kinetic effects at two different time scales can hinder the establishment of thermodynamic equilibrium, and thus limit the reliability of solubility results obtained by settling techniques. Firstly, when the liquid is saturated by dissolution of the pure metal, the saturation kinetics may be rate controlled by the formation of intermetallic compounds at the liquid/metal interface and solid-state diffusion through these phases. In the present case, this problem was avoided by the immersion of  $\text{Al}_3\text{Zr}$  pieces in pure Al. Secondly, when the temperature was increased or decreased between two liquid sampling operations, the variation in solute content in the liquid was limited by the dissolution kinetics or precipitation of  $\text{Al}_3\text{Zr}$ , respectively. Therefore, in order to confirm that no kinetic effects alter the solubility values measured in the present study, a specific experiment was performed. A supersaturated ingot of Al-Zr alloy was heated by rf coupling at 800°C and rapidly cooled down to 750°C. Liquid samples were then taken at different times from 0 to 8 h after the temperature of 750°C had been reached. The chemical analyzes of the samples are presented in Fig. 4. By comparing the values with the isothermal values from Fig. 3, it is clear that, in cooling conditions, thermodynamic equilibrium was obtained after a holding time of just 1 h. As

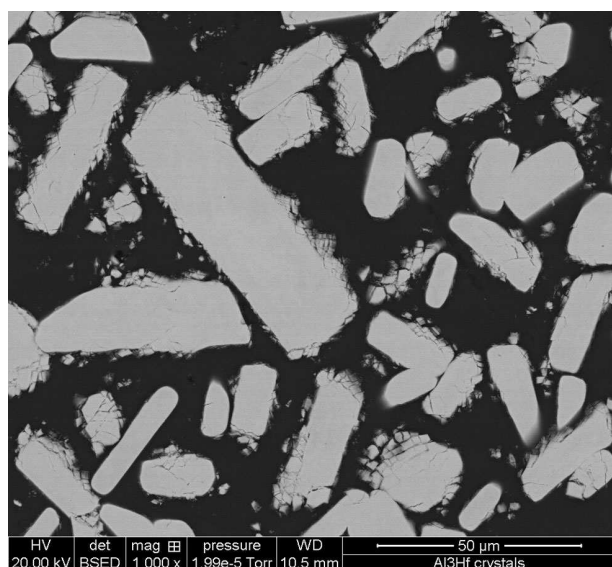


**Fig. 3** Solubility limit of Zr in liquid Al determined by isothermal experiments at different temperatures by ICP-AES analysis. Liquid samples are taken respectively during cooling—filled symbols—and during heating—open symbols. Experimental data are compared to previous experimental determinations<sup>[22,23]</sup> and to the calculated liquidus<sup>[37]</sup>



**Fig. 4** Solubility of Zr in liquid Al at 750°C, determined by ICP-AES analysis after liquid sampling as a function of time

a consequence, it can be concluded that with the holding time of 8–10 h used in the present study, no kinetic effects prevented the equilibrium conditions from being obtained. Moreover, as the three metals belong to the same group and as the Al-M binary systems are very similar,<sup>[11,12,42]</sup> it is



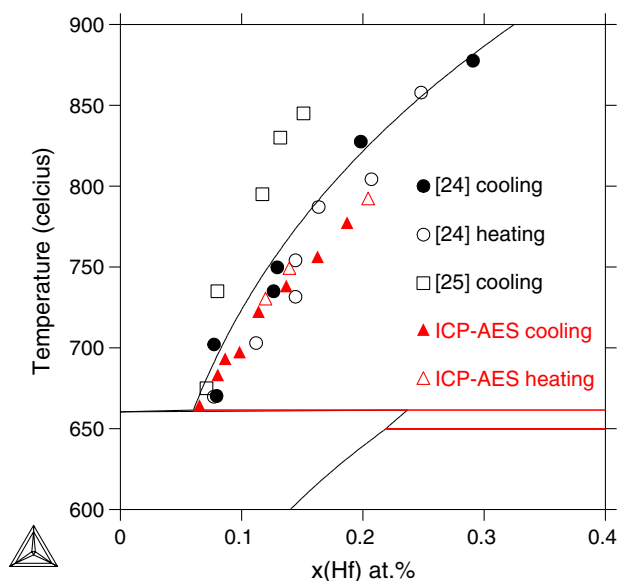
**Fig. 5** SEM backscattered electron image of  $\text{Al}_3\text{Hf}$  crystals observed in the bottom of the Al-Hf ingot after the full liquid sampling process

considered that this conclusion is also valid for the Ti and Hf solute in liquid Al.

### 3.3 Hf Solubility in Liquid Al

After solidification and cooling, the Al-Hf ingot was cut, embedded in resin and polished to confirm the formation and settling of the  $\text{Al}_3\text{Hf}$  crystals and to characterize the microstructure. Figure 5 presents the resulting microstructure of the bottom part of the ingot. The absence of chemical contrast through the crystals illustrates their homogeneity and the conversion of pure Hf into coarse  $\text{Al}_3\text{Hf}$  grains with a typical size of a few tenths of a micrometer (confirmed by EDS measurements).

Figure 6 presents the variation in Hf solubility in liquid Al below  $800^\circ\text{C}$  in comparison with experimental values reported in the existing literature<sup>[24,25]</sup> and the optimisation of Wang et al.<sup>[43]</sup> In the existing literature, two sets of values were reported. The results obtained in the present study are in better agreement with the largest solubility values of Rath et al.<sup>[24]</sup>, rather than with those of Rokhlin et al.<sup>[25]</sup> It should be noticed that while Rokhlin et al. have only reported values of solubility obtained during cooling, Rath et al. reported a consistent set of values both for cooling and heating. Moreover, from the experimental details given by Rokhlin et al.<sup>[25]</sup> it appears that the initial saturation of the liquid by Hf at  $900^\circ\text{C}$  is ensured by a plateau of 1 h. Dissolution of the Hf pieces into the liquid requires a diffusion step of Hf through the hafnium aluminides that form at the liquid-Hf interface. As a consequence, if saturation of the melt from metallic pieces of Hf is not fulfilled after 1 h of plateau at  $900^\circ\text{C}$ , then the liquid is not saturated, and during cooling, the measured solubilities will be smaller than the true values. In the present study, the isothermal plateau before sampling of the liquid has duration of about 6 h in order to limit this problem of



**Fig. 6** Solubility limit of Hf in liquid Al determined by isothermal experiments at different temperatures by ICP-AES analysis. Liquid samples are taken respectively during cooling—filled symbols—and during heating—open symbols. Experimental data are compared to previous experimental determinations<sup>[24,25]</sup> and to the calculated liquidus<sup>[43]</sup> (the lowest temperature reaction correspond to the polymorphous transformation of  $\text{Al}_3\text{Hf}$  from the low-temperature to the high-temperature crystal structure)

kinetics. From this discussion, it appears that the most reliable solubility values in the literature have been reported by Rath et al.<sup>[24]</sup>, and the results of the present study confirm these solubility values of Hf in liquid Al against the more recent values of Rokhlin et al.<sup>[25]</sup>

One of the arguments that can be used against the settling technique is related to the existence of a composition gradient in the liquid phase leading to non-equilibrium conditions far away from the settled crystals, where sampling is performed. Indeed saturation during heating occurs by dissolution of the settled crystals at the bottom of the crucible, while during cooling it occurs by precipitation of crystals in the liquid phase. The first process is localized and establishment of equilibrium requires a diffusion step in the liquid phase. The second one can occur everywhere in the liquid, without any diffusion step. Convergence of solubility values obtained both during cooling and heating is therefore a strong evidence of thermodynamic equilibrium.

After dissolution of the Al matrix in a 10 wt.%NaOH solution, the structure of the  $\text{Al}_3\text{Hf}$  aluminide was determined by single crystal XRD to be the tetragonal  $\text{D0}_{23}$  form with lattice parameters  $a = 0.3983$  nm and  $c = 1.7104$  nm that are in good agreement with the existing literature.<sup>[12,40,44]</sup>

## 4. Conclusion

In the present study, the solubility of group IV transition metals Ti, Zr, and Hf in liquid Al was measured by the

settling technique coupled with ICP-AES analysis after dissolution in hydrochloric acid. The results confirmed the values previously reported in the literature and the good description for the three binaries by the existing CALPHAD optimizations concerning the liquidus below 800°C.

After the existing experimental liquidus of Al-Zr was questioned by Janghorban et al.<sup>[26]</sup>, it was important to report new values with special attention being paid to their arguments, i.e., to insure and verify the establishment of thermodynamic equilibrium between the liquid and solid phases. This was achieved firstly by saturation of the liquid in Zr from Al<sub>3</sub>Zr crystals and not from pure Zr. Then, no intermediate layers were formed around the solid phase; and the saturation kinetics of the melt were not limited by a solid-state diffusion process. Secondly, the kinetic aspect of the settling technique was studied in order to show that, after a cooling step, thermodynamic equilibrium between the liquid and solid phases could be achieved after only 1 h. Finally, it was verified that solubility values obtained after a cooling or a heating step were fully consistent. The present results demonstrate that the immersion-and-settling technique allows reliable solubility values to be determined.

In addition, the crystallographic structure of the Al<sub>3</sub>M aluminide in equilibrium with the liquid was determined in the case of Zr and Hf. X-ray diffraction was performed on single crystals and confirmed the presence of the phase recognized as being the most stable for the Al-Zr and Al-Hf systems.

It should be noted that the liquid solubility results of the present study cannot be used to draw any conclusions concerning the nature of the last invariant in the Al-Zr system until new and careful solid solubility limit measurements have been obtained.

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