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Localized strain field measurement on laminography data with mechanical regularization

Thibault Taillandier-Thomas^{a,b}, Stéphane Roux^a, Thilo F. Morgeneyer^b,
François Hild^a

^a*LMT-Cachan, ENS Cachan/CNRS/UPMC/PRES UniverSud Paris
61 avenue du Président Wilson, 94235 Cachan Cedex, France*

^b*Mines ParisTech, Centre des Matériaux, CNRS UMR 7633, BP 87
91003 Evry Cedex, France*

Abstract

For an in-depth understanding of the failure of structural materials the study of deformation mechanisms in the material bulk is fundamental. *In situ* synchrotron computed laminography provides 3D images of sheet samples and digital volume correlation yields the displacement and strain fields between each step of experimental loading by using the natural contrast of the material. Difficulties arise from the lack of data, which is intrinsic to laminography and leads to several artifacts, and the little absorption contrast in the 3D image texture of the studied aluminum alloy. To lower the uncertainty level and to have a better mechanical admissibility of the measured displacement field, a regularized digital volume correlation procedure is introduced and applied to measure localized displacement and strain fields.

Keywords: Artifacts, Digital Volume Correlation, Laminography, Regularization, Strain localization

1. INTRODUCTION

Thin sheet structures are widely used in the transportation industry but their failure behavior is not always well understood. The three stages of ductile fracture, namely, void nucleation, growth and coalescence, are established but bulk data are still needed to assess the interaction between damage and strain localization at low levels of triaxiality, as shown in Figure 1. Thanks to the development of 3D imaging and full-field measurement techniques, quantitative data can be obtained to address these issues. Synchrotron X-ray computed laminography (akin to tomography) allows 3D imaging to be performed at the

Email addresses: thibault.taillandier-thomas@lmt.ens-cachan.fr (Thibault Taillandier-Thomas), stephane.roux@lmt.ens-cachan.fr (Stéphane Roux), thilo.morgeneyer@mines-paristech.fr (Thilo F. Morgeneyer), francois.hild@lmt.ens-cachan.fr (François Hild)

micrometer scale for sheet like samples at the cost of additional noise due to the lack of information [1, 2, 3, 4].

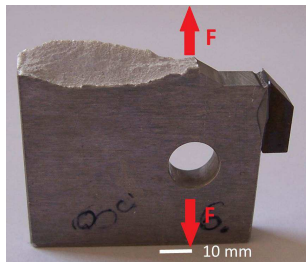


FIGURE 1: Illustration of typical ductile fracture path of aluminum alloy sheet loaded in opening mode

The volumes that are naturally contrasted can be used in digital volume correlation (DVC) analyses to measure 3D displacement and strain fields in the bulk. DVC is an extension of 2D digital image correlation [5] to 3D situations [5, 6]. The first implementations of DVC have consisted of registering small interrogation volumes (or subvolumes) to determine their mean rigid body translations [7]. Local rotations have been added later on [8]. The warping of the interrogation volume has also been introduced in DVC codes [9]. All these approaches are referred to as local, since each analysis is local (*i.e.*, at the scale of the interrogation volume) and no kinematic constraint is prescribed between neighboring subvolumes.

Global approaches to DVC have been introduced thereafter [10]. Contrary to local approaches, the displacement field is defined over the whole region of interest. In particular, in many instances, its continuity is enforced *a priori*. For example, the kinematics associated with finite element discretizations have been considered [10]. If cracks are to be analyzed, enriched kinematics have also been implemented to account for displacement discontinuities [11, 12]. One further step is to regularize the correlation problem by requiring the measured displacement field to satisfy mechanical constraints such as the equilibrium [13, 14]. In particular, in areas where the image texture is not sufficiently contrasted, mechanics is utilized to extrapolate the displacement field. If this type of information is not available, then the displacement measurement in these areas would not be possible. This issue is particularly important in 3D imaging as no artificial texture (*e.g.*, secondary particles) can be added without altering the behavior of the studied material.

The aim of the present study is to evaluate the potential of these regularized approaches in the case of little absorption contrast in the 3D images in addition to the fact that complex kinematic fields are sought (*i.e.*, strain localization). The main challenge is related to the fact that if the regularization is too strong, it may smear out the localized region. Conversely, if the regularization is too weak, the DVC calculations may not converge. One additional question is related to the

impact of noise induced by laminography. It was shown that the measurement uncertainty achieved by C8-DVC (*i.e.*, global approach to DVC using 8-noded cubes) reaches levels [4] that are significantly higher than those achieved by analyzing tomographic data [15, 16]. The latter are themselves higher than what is usually observed when dealing with standard 2D images [5, 6].

The paper is organized as follows. The experiment analyzed herein is introduced in Section 2. It deals with the analysis via laminography of a notched sample made of aluminum alloy. Section 3 summarizes the regularized DVC approach to be used to measure displacement fields of the reconstructed volumes. The proposed regularization combines different functionals, which requires scaling to be performed. Associated with a given choice of normalizing displacement fields, new length scales are obtained. Strain resolutions are first determined in Section 4.1. A scaling strategy is proposed to get a almost unique tendency for different trial displacement fields. For the measured displacement field it is possible to determine strain data (Section 4.2). The cumulative total strain fields are shown and the effect of regularization length is assessed in terms of capturing localized strain fields.

2. EXPERIMENT

2.1. Laminography

Synchrotron radiation computed tomography (CT) is a 3D non-destructive technique for objects extended in one direction and thin in the other two directions. By inclining the specimen with an angle $\theta < 90$ degrees with respect to the beam direction, a region of interest that expands along two directions can be scanned [1], see Figure 2. This technique is referred to as synchrotron radiation computed laminography (CL). A filtered-backprojection algorithm is then used to reconstruct the 3D volume [1, 2].

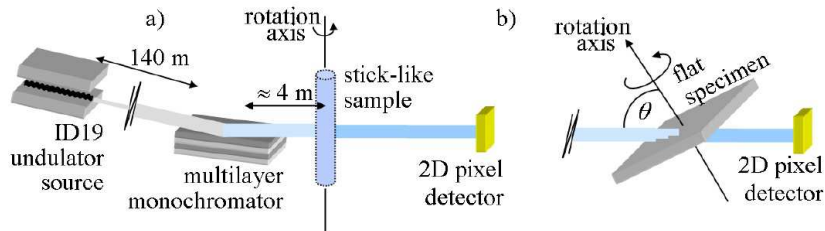


FIGURE 2: Schematic view of the CT (a) and CL (b) setup with the ESRF parallel beamline (after [4])

The 3D images utilized herein were obtained at beamline ID19 of the European Synchrotron Radiation Facility (Grenoble, France) with a monochromatic beam of 25 keV, with a 65-degree rotation axis inclination angle and 1,500 projections. The reconstructed volumes have a size of $2,040 \times 2,040 \times 2,040$ voxels, with a voxel size of $0.7 \mu\text{m}$. More details on the experimental configuration and on analyses of the reconstructed volumes themselves can be found in Reference [17].

2.2. Material and experimental setup

The material used for this study is a commercial Al-Cu aluminum alloy (AA 2198) in T8 condition. The geometry of the flat and notched specimen is schematically shown in Figure 3(a). The 1-mm thick sample (60-mm in width and 70-mm in height) has a notch that has been machined by EDM leading to a radius of 0.17 mm. The loading consists of opening the notch mouth with a displacement controlled by 2-screw device. Stepwise loading has been applied between each laminography scan. An anti-buckling device, which is not shown, has been mounted around the specimen, leaving a window close to the notch to scan the volume close to the notch. From the scanned region, the region of interest for DVC analyses is chosen to be away from the notch root (Figure 3(b)).

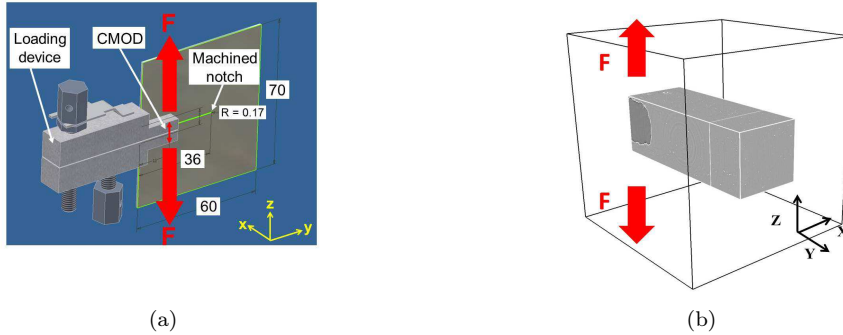


FIGURE 3: (a) Schematic view of the analyzed test [4]. The x -axis lies along the thickness of the plate, the y -axis corresponds to the main propagation direction, and the z -axis is aligned with the load direction. (b) The scanned volume is sketched as a cube delineated in black. The region of interest is a parallelepipedic volume away from the notch, which can be seen as a dark region for small y . It is a gray volume limited by white lines for large y .

For the analyzed region of interest, the amount of information is quite low, as shown in the histogram of gray level in Figure 4(a) and in the volume with enhanced contrast from Figure 4(b). Further, the inclusion volume fraction is of 0.3-0.4 %. The presence of ring and reconstruction artifacts can be noticed in Figure 4(b) and makes DVC difficult because it has to be based on true microstructure and not on artifactual features. It is interesting to assess the

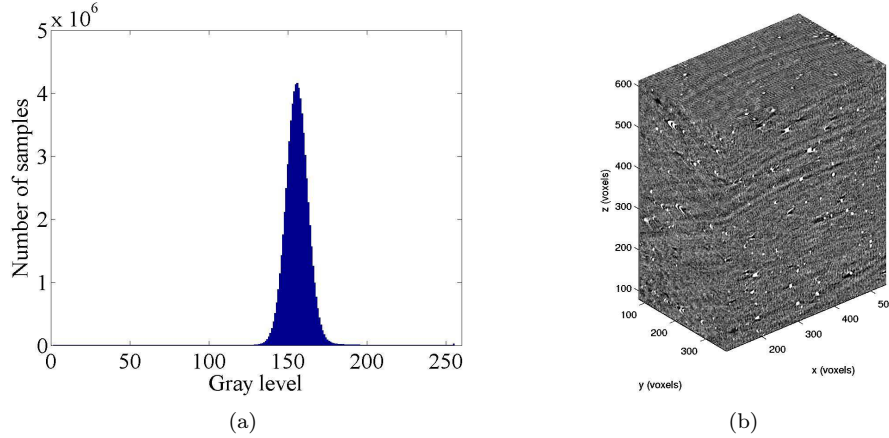


FIGURE 4: (a) Gray level histogram of (b) the view of the region of interest with an enhanced contrast to reveal reconstruction artifacts

development of strains and in particular the strain pattern in such type of experiment and its impact on the final damage change. To address this issue, there is a need for reliable kinematic measurements (*i.e.*, displacement and strain fields) in the presence of very poor textures (Figure 4). Once such data are available, the next question to answer is linked with the detection of damage. These two points are solved by resorting to global and regularized digital volume correlation thanks to the measured displacement fields and the corresponding correlation residuals.

3. REGULARIZED DIGITAL VOLUME CORRELATION

3.1. Global DVC

DVC consists of registering two reconstructed volumes, namely, a volume f in the reference configuration, and volume g in the deformed configuration assuming gray level conservation

$$f(\mathbf{x}) = g(\mathbf{x} + \mathbf{u}(\mathbf{x})) \quad (1)$$

where \mathbf{x} is the position of any voxel and \mathbf{u} the unknown displacement. Because the strict conservation is not satisfied, especially in CL where noise appears due to reconstruction artifacts due to missing information/angles [3], the correlation residual $\phi_c(\mathbf{x})$ expressed as

$$\phi_c(\mathbf{x}) = |f(\mathbf{x}) - g(\mathbf{x} + \mathbf{u}(\mathbf{x}))| \quad (2)$$

is used in the sum of squared differences

$$\Phi_c^2 = \int_{ROI} \phi_c^2(\mathbf{x}) d\mathbf{x} \quad (3)$$

that is minimized with respect to kinematic unknowns. This problem is ill-posed and nonlinear. Thus a weak formulation based on C8 finite element is chosen in which the displacement is decomposed as

$$\mathbf{u}(\mathbf{x}) = \sum_n u_n \psi_n(\mathbf{x}) \quad (4)$$

where u_n are the degrees of freedom (to be measured) associated with the trilinear shape functions ψ_n of C8 elements. By using a modified Newton iterative procedure [10], linear systems are to be solved

$$[\mathbf{M}]\{\delta\mathbf{u}\} = \{\mathbf{b}\} \quad (5)$$

where $[\mathbf{M}]$ is the correlation matrix, $\{\delta\mathbf{u}\}$ the correction to vector $\{\mathbf{u}\}$ gathering all unknown degrees of freedom, and $\{\mathbf{b}\}$ the RHS vector that needs to decrease so that convergence is achieved (*i.e.*, the corrections $\{\delta\mathbf{u}\}$ become vanishingly small).

3.2. Regularized DVC

Regularization consists of adding some mechanical requirements with additional functionals, some based on the equilibrium gap method [18], which constrains the displacement field to be the solution to an elastic problem with known body forces

$$[\mathbf{K}]\{\mathbf{u}\} = \{\mathbf{f}\} \quad (6)$$

where $[\mathbf{K}]$ is the stiffness matrix, and vector $\{\mathbf{f}\}$ gathers all the nodal forces. Equilibrium residuals arise for (usually unloaded) inner nodes if \mathbf{u} does not satisfy equilibrium. The equilibrium gap functional reads

$$\Phi_m^2 = \{\mathbf{u}\}^t [\mathbf{K}]^t [\mathbf{K}]\{\mathbf{u}\} \quad (7)$$

When the latter vanishes, equilibrium is strictly satisfied for inner nodes so that mechanical admissibility is satisfied.

The previous strategy cannot be used as such for boundary nodes, except those that belong to a free edge. In that case the previous setting is extended to these particular nodes. For the other boundary nodes, an edge regularization is considered in the same spirit as what was recently proposed for 2D situations [19]

$$\Phi_b^2 = \{\mathbf{u}\}^t [\mathbf{L}]^t [\mathbf{L}]\{\mathbf{u}\} \quad (8)$$

where matrix $[\mathbf{L}]$ behaves on the ROI boundaries.

These three functionals cannot be added since they do not have the same physical units [14]. Consequently, a reference displacement field \mathbf{v} is needed to normalize each functional. The three normalized functionals are dimensionless and thus can be combined. A weight w_m and w_b is given to functionals Φ_m^2 and Φ_b^2 , thereby defining regularization lengths that act as cut-off wavelength of low pass filters [14, 19]. The regularized correlation procedure consists of iteratively solving linear systems

$$([\mathbf{M}] + [\mathbf{N}])\{\delta\mathbf{u}\} = \{\mathbf{b}\} - [\mathbf{N}]\{\mathbf{u}\} \quad (9)$$

with

$$[\mathbf{N}] = w_m \frac{\{\mathbf{v}\}^t [\mathbf{M}] \{\mathbf{v}\}}{\{\mathbf{v}\}^t [\mathbf{K}]^t [\mathbf{K}] \{\mathbf{v}\}} [\mathbf{K}]^t [\mathbf{K}] + w_b \frac{\{\mathbf{v}\}^t [\mathbf{M}] \{\mathbf{v}\}}{\{\mathbf{v}\}^t [\mathbf{L}]^t [\mathbf{L}] \{\mathbf{v}\}} [\mathbf{L}]^t [\mathbf{L}] \quad (10)$$

In the present case, displacement \mathbf{v} is associated with a wave of vector \mathbf{k} so that the two weights are defined as

$$w_m = w_b = (2\pi|\mathbf{k}|\ell_r)^4 \quad (11)$$

where ℓ_r is the regularization length.

Regularization makes use of a constitutive law, which in the present case is that of a linear and isotropic elastic medium. Based on a decomposition of the strain tensor $\boldsymbol{\epsilon}$ into a spherical part, $\boldsymbol{\epsilon}_{sph} = (1/3)\text{tr}(\boldsymbol{\epsilon})\mathbf{I}$, and a deviatoric part, $\boldsymbol{\epsilon}_{dev} = \boldsymbol{\epsilon} - \boldsymbol{\epsilon}_{sph}$, the stress tensor $\boldsymbol{\sigma}$ reads

$$\boldsymbol{\sigma} = 3K\text{tr}(\boldsymbol{\epsilon})\mathbf{I} + 2G\boldsymbol{\epsilon}_{dev} \quad (12)$$

where K (resp. G) is the bulk (resp. shear) modulus, and \mathbf{I} the second order identity tensor. The moduli ratio is given by

$$\frac{K}{G} = \frac{2(1+\nu)}{3(1-2\nu)} \quad (13)$$

As Poisson's ratio ν approaches the incompressibility limit, *i.e.*, $\nu = 1/2$, or $\nu = 1/2 - \eta$ with $\eta \rightarrow 0$, $K/G \sim 1/(2\eta)$.

The expression of the equilibrium gap density in the continuum limit reads

$$\|\text{div}(\boldsymbol{\sigma})\|^2 = \sum_i ((3K + 2G/3)u_{j,ji} + Gu_{i,jj})^2 \quad (14)$$

Among the two elastic constants that come into play in this expression, one disappears through the normalization (or can be included in the prefactor of Φ_m). However, the relative weight of the deviatoric and volumetric strain terms in the sum, which is controlled by K/G , allows for some flexibility in the introduction of the kinematic regularization as discussed below.

Let us stress that this regularization does not necessarily imply that the solid is linearly elastic and described accurately by the above constitutive law. Seen as a mere *ad hoc* regularization to smooth out high spatial frequencies, it can be shown that the most general form of linear operator acting on the displacement field that is invariant under a rigid body motion (translation and rotation) has precisely the form of Lamé's operator $\text{div}(\boldsymbol{\sigma})$. For a solid medium that is loaded away from its elastic limit, a tangent stiffness $\partial\boldsymbol{\sigma}/\partial\boldsymbol{\epsilon}$ can be defined, which looks alike the above elastic constant. As will be argued below, as plastic flow occurs at constant volume, a Poisson's-like ratio close to $1/2$ may be chosen to prescribe incompressibility rather than the actual elastic Poisson's ratio. The actual limitation comes from the assumption of a uniform stiffness, which is generally untrue for nonlinear mechanical behaviors. However, as the mechanical filter affects only the small scales, this inhomogeneity may not have severe consequences unless too much weight is given to the regularization kernel.

4. DVC RESULTS

In the sequel, four volumes will be considered. Two volumes in the undeformed configuration are reconstructed to assess the resolution level of the DVC technique. The third volume has been acquired at an early stage of the test, and the fourth at a later stage. In both latter cases, yielding has already occurred. Consequently, the cumulative total strain will be reported. Since the elastic strains are very small, the cumulative total strain cannot be distinguished from the cumulative plastic strain p_{eq} . The size of the volume of interest (see Figure 4(a)) is $650 \times 450 \times 700$ voxels, and the region of interest (ROI) for DVC has a size of $448 \times 288 \times 544$ voxels. The discretization is based on C8 elements with an edge size ℓ of 16 pixels. The regularization lengths ℓ_r considered hereafter are equal to 500 voxels (*i.e.*, most of the weight is put on regularization since $\ell_r \gg \ell$), 50, 40, 30, 10 and 5 voxels (regularization effects become negligible when $\ell_r < \ell$). In the early loading stages considered herein, no damage nucleation on intermetallic particles was observed in the region of interest. This finding stands in contrast to a related study [20] where damage at very brittle particles occurs very early on. However, these particles were of different nature (*i.e.*, Mg_2Si) than those found herein (*i.e.*, Fe-based) and of substantially bigger individual size favoring early fracture/debonding.

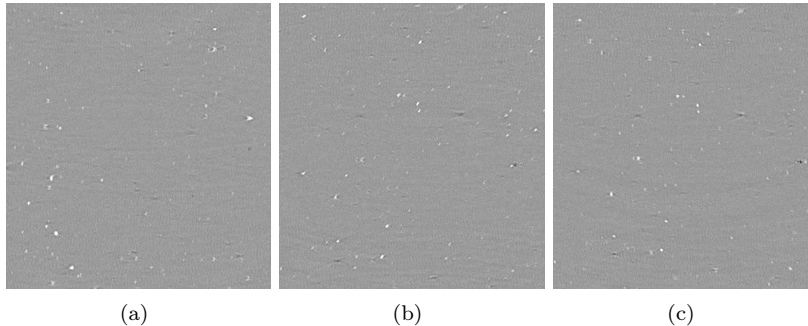


FIGURE 5: Slices parallel to the $x-z$ plane taken from the undeformed volume (a), the volume at early (b) and late (c) stages of the test

4.1. Resolution analysis

The resolution analysis consists of correlating the first two volumes. Very small displacements have occurred between the two acquisitions. However, because of various artifacts, these two volumes are not identical but essentially corrupted by noise. Regularized DVC is run and the results yield nodal displacements associated with the finite element discretization. The mean displacement gradient in each element is then evaluated. From the latter, the Green Lagrange strain tensor is computed and its second invariant (*i.e.*, the cumulative Von Mises' strain) is obtained. More details can be found in Reference [21].

The standard deviation of the measured values is reported. It is referred to as standard strain resolution since it corresponds to the largest level below which the measurement can be confused with noise. Three different displacement fields \mathbf{v} are considered for the normalization procedure of regularized DVC. The first displacement field involves a change of volume

$$v_{0x} = v_{0y} = v_{0z} = \sin(2\pi kx) \sin(2\pi ky) \sin(2\pi kz) \quad (15)$$

while the two others are incompressible

$$\begin{cases} v_{1x} = \sin(2\pi ky) \\ v_{1y} = \sin(2\pi kz) \\ v_{1z} = \sin(2\pi kx) \end{cases} \quad (16)$$

and

$$\begin{cases} v_{2x} = \sin(2\pi ky) \sin(2\pi kz) \\ v_{2y} = \sin(2\pi kx) \sin(2\pi kz) \\ v_{2z} = \sin(2\pi kx) \sin(2\pi ky) \end{cases} \quad (17)$$

where k is a wavenumber equal to 0.1 voxel^{-1} . The aim of the following analysis is to study the influence of the normalization displacement field on the measurement results.

Two different values for Poisson's-like ratio will be considered (*i.e.*, $\nu = 0.27$ and $\nu = 0.49$). The former corresponds to a rough estimate of the actual Poisson's ratio of the studied material. However, since plasticity is likely to occur, a value of Poisson's-like ratio close to 0.5 allows the displacements to be quasi incompressible. Figure 6(a) shows the change of the mean correlation residuals, in percent of the dynamic range of the ROI, for the different regularization lengths ℓ_r and for the four normalizing displacement fields. There is virtually no variation (note the very small dynamic range in the figure) of the residuals. From a pure correlation stand point, all the results are equivalent and have properly converged.

However, the standard strain resolution shown in Figure 6(b) does not follow the same trend. The larger the regularization length ℓ_r , the smaller the resolution. As expected [14], the regularization length defines the spatial resolution of regularized DVC once it becomes greater than the element size ℓ . The overall trend is identical for any chosen displacement field \mathbf{v} . However, the relative levels are different. For field \mathbf{v}_0 two results are reported by using the two Poisson's-like ratio values. When $\nu = 0.49$, the deviatoric strain field is very weakly regularized. Therefore it is expected that the strain and displacement fluctuations are larger than those obtained for $\nu = 0.27$. This is observed in Figure 6(b). As the regularization length increases, this effect is more pronounced since the mechanical regularization has a larger weight. Let us note that whatever the regularization length and the normalization field, the standard strain resolution is still lower than without regularization for the same element size as can be seen by comparing Figure 6(b) and Figure 6(c).

As the limit of an incompressible material is considered, it is to be emphasized that the reference displacement field \mathbf{v} chosen to normalize the regularization

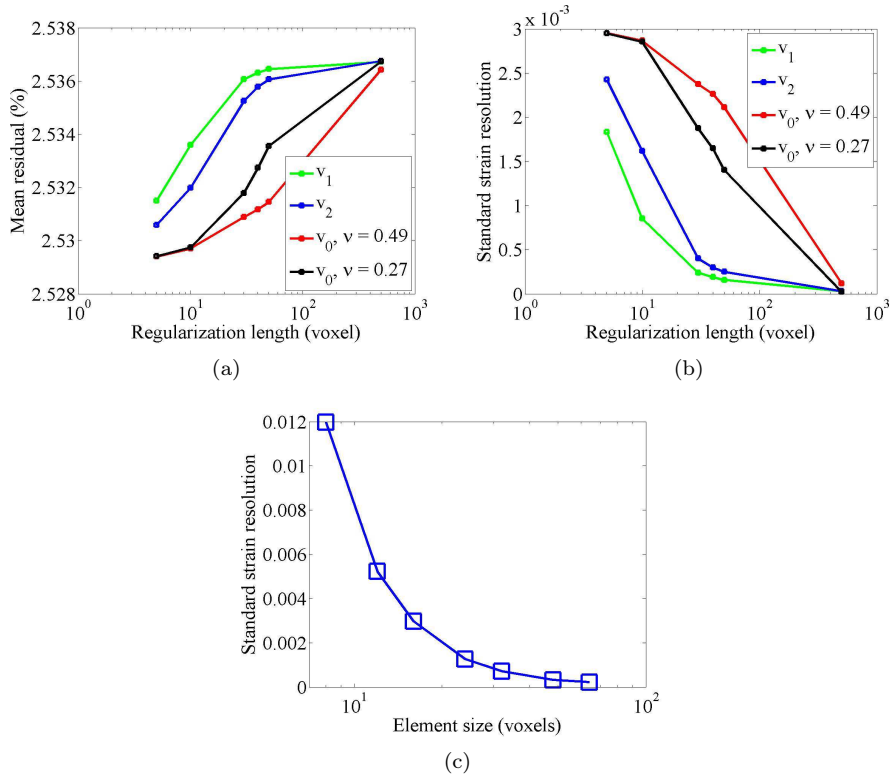


FIGURE 6: Mean correlation residuals (in percentage of the dynamic range of the volume in the reference configuration) (a) and corresponding standard strain resolution (b) for different regularization length ℓ_r , and normalizing fields \mathbf{v} . (c) Standard strain resolution for different C8 element sizes without regularization

part may have a very strong weight on the result. Let us consider a dimensional analysis, where terms such as $u_{a,jk}$ are assumed to be of order U/λ^2 where U is a characteristic displacement magnitude and λ the characteristic scale over which the displacement varies. If the displacement field is not isochoric, then the order of magnitude of the equilibrium gap is (to dominant order) $K^2 U^2 / \lambda^4$, while if it is divergence-free, the equilibrium gap amounts to $G^2 U^2 / \lambda^4$. The ratio of these two terms is therefore of order $1/\eta^2$.

In fact, there are not one but two regularization lengths. They can be considered as of the same magnitude when ν differs significantly from 0.5. However in the incompressible limit, they have to be distinguished as their ratio diverges. One length is relative to the volume change, ℓ_{sph} , while the second is linked to the deviatoric part, ℓ_{dev} . Their ratio is given by the square root of the ratio of

elastic properties, K/G , and hence

$$\frac{\ell_{sph}}{\ell_{dev}} \approx \frac{1}{\sqrt{\eta}} \quad (18)$$

In the cases considered below, when $\nu = 0.49$, a factor of 10 is expected in the ratio of these two length scales. The cut-off length that was introduced earlier ℓ_r will essentially set $\ell_{sph} = \ell_r$ if the reference displacement field \mathbf{v} has the volumetric strain of the same magnitude as the equivalent deviatoric strain. However, if the reference displacement field is traceless, then $\ell_{dev} = \ell_r$. It should be emphasized that the ratio between length scales (see Equation (18)) is independent of the choice of ℓ_r , and hence changing the reference field from non-isochoric to isochoric can be exactly compensated for by a corresponding change in ℓ_r . In terms of displacement field wavelength, λ , three regimes are to be considered :

- at large wavelength, $\lambda > \ell_{sph}$, DVC is the dominant contribution,
- at intermediate wavelength, $\ell_{dev} < \lambda < \ell_{sph}$, the DVC functional is optimized in the subspace of isochoric displacement fields,
- at small wavelength, $\lambda < \ell_{dev}$, the displacement field has to be the solution to an elastic incompressible problem. Within this much more constrained choice, image registration decides for the best candidate.

Last, let us also note that the boundary regularization can also be affected if the corresponding length scale is linked to (and, in the present case, even equal to) ℓ_r .

It is difficult to compare the results given by different normalizations because each of them has a different influence on matrix $[\mathbf{N}]$ (see Equation (10)). A way to circumvent this issue is to consider that the main part of the regularization is associated with the equilibrium gap (of inner nodes). An equivalent regularization length ℓ_{req} appears if the weight on that term is equal for a given length for every displacement field \mathbf{v}_i considered

$$w_m^{\mathbf{v}_i, \ell_{req}} = w_m^{\mathbf{v}_i, \ell_{ri}} \frac{\{\mathbf{v}_i\}^t [\mathbf{M}] \{\mathbf{v}_i\}}{\{\mathbf{v}_i\}^t [\mathbf{K}]^t [\mathbf{K}] \{\mathbf{v}_i\}} \frac{\{\mathbf{v}_1\}^t [\mathbf{K}]^t [\mathbf{K}] \{\mathbf{v}_1\}}{\{\mathbf{v}_1\}^t [\mathbf{M}] \{\mathbf{v}_1\}} \quad (19)$$

The rescaling is performed by considering the regularization length of \mathbf{v}_1 as a reference (*i.e.*, for \mathbf{v}_1 , $\ell_r = \ell_{req}$). The effect of the previous rescaling is shown in Figure 7. The trends in terms of mean correlation residuals and standard strain resolutions are virtually identical for all four normalizing fields. The fact that the collapse is not perfect is due to the other regularization terms. Figure 7(b) shows that for small equivalent regularization lengths ℓ_{req} , the standard strain resolution tends to 0.3 %. This level is associated with the resolution of C8-DVC (with an element size ℓ). Conversely, very small resolutions are observed for large equivalent regularization lengths (*i.e.*, less than 10^{-4}) even though the texture is very difficult.

4.2. Equivalent strain measurement

Now that the uncertainty is assessed, the study will focus on measurements between one of the undeformed volumes and the ones at early and late stages of

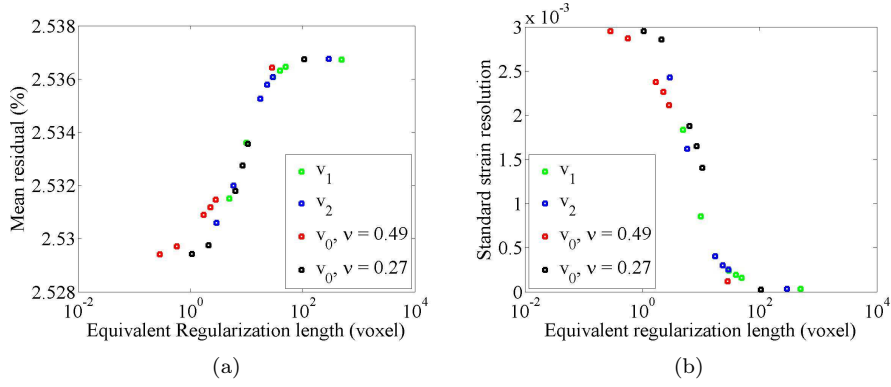


FIGURE 7: Mean correlation residuals (in percentage of the dynamic range of the volume in the reference configuration) (a) and corresponding standard strain resolution (b) for different equivalent regularization lengths ℓ_{req} and normalizing fields \mathbf{v} when the rescaling has been applied

loading. The orientation and position of all the volumes shown are those of Figure 4(a). The mean correlation residual of the different correlations (Figure 8) is almost the same as the levels obtained in the resolution analysis Figure 7. The same quality of registration is obtained for all the analyses performed herein. There is a slight degradation for the last stage of loading when larger regularization lengths are considered.

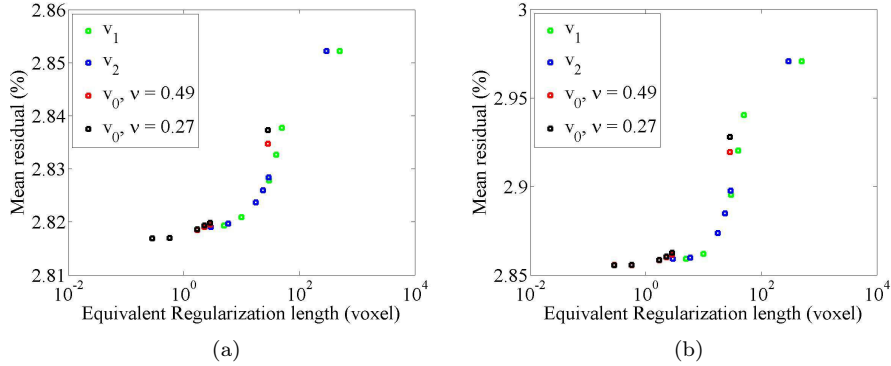


FIGURE 8: Mean residual for correlations between the undeformed volume and early (a) and later (b) stages of loading for different equivalent regularization lengths ℓ_{req} and normalizing fields \mathbf{v} when the rescaling has been applied.

The influence of the equivalent regularization length on the strain fields is shown in Figure 9. If too much weight is put on the regularization (*i.e.*, ℓ_{req} increases), the measured equivalent strain field is smeared out over a length

that is proportional to ℓ_{req} . Strain localization due to plasticity is not properly captured. This effect explains why the correlation residuals degrade as the equivalent regularization length increases (Figure 8). Figure 9(b) shows that with a length $\ell_{req} = 30$ voxels, which is of the same order of magnitude as the element size (*i.e.*, $\ell = 16$ voxels), many fluctuations of the strain field are filtered out. An equivalent regularization length of $\ell_{req} = 10$ voxels seems to be the best candidate, because the small fluctuation have been filtered out while essentially keeping the same level of residuals and a similar shape of the strain field (Figure 9(c)). Moreover the strain uncertainty, which is less than 0.1%, is more than three times smaller than that obtained without regularization (Figure 7). Larger values of ℓ_{req} correspond to a significant increase in the residuals, thereby indicating that the correlation results are less trustworthy.

As shown in Figure 8(a), for a small equivalent regularization length close to 5 voxels (*i.e.*, less than the element size), the mean value of the residual field and the equivalent strain field shown in Figure 10, is almost the same regardless of the displacement field used for the normalization procedure. This result can be explained by the fact that a low weight is put on the regularization part compared to the one put on the correlation itself. However, the strain resolution shown in Figure 7(b) for each normalization and regularization length is different.

For the later stage of loading and an equivalent regularization length of the same order as the element size (*i.e.*, 30 voxels as indicated in Figure 8(b)), the mean value of the residual field and the equivalent strain fields (Figure 11(a,b)) for \mathbf{v}_1 and \mathbf{v}_2 are similar. For \mathbf{v}_0 , the incompressibility is prescribed by the Poisson's-like ratio, thus the equivalent strain field obtained with a Poisson's-like ratio of 0.49 (Figure 11(c)) looks like the ones of \mathbf{v}_1 and \mathbf{v}_2 . However the mean value of the residual field, Figure 8(b), is higher.

5. CONCLUSIONS

Using computed laminography *in situ* experiments have been performed on plate-like specimen with sub-micrometer spatial resolution. The 3D images have then been successfully registered by regularized digital volume correlation to measure displacement and strain fields in spite of very little contrast due to a low content of particle used as markers. This is the case of the aluminum alloy that was analyzed herein.

To lower the measurement uncertainties, a regularization procedure was followed. Within the framework of global approaches to digital volume correlation, it consists of prescribing additional constraints on inner nodes (*i.e.*, minimization of the equilibrium gap) and boundary nodes (*i.e.*, minimizing displacement fluctuations). The weight put on various regularization terms translates into regularization lengths that can be compared to the underlying finite element discretization. The standard strain resolution could be decreased from an initial level of 0.3 % (for 16-voxel elements) to less than 0.01 % for large regularization lengths (*i.e.*, greater than 100 voxels).

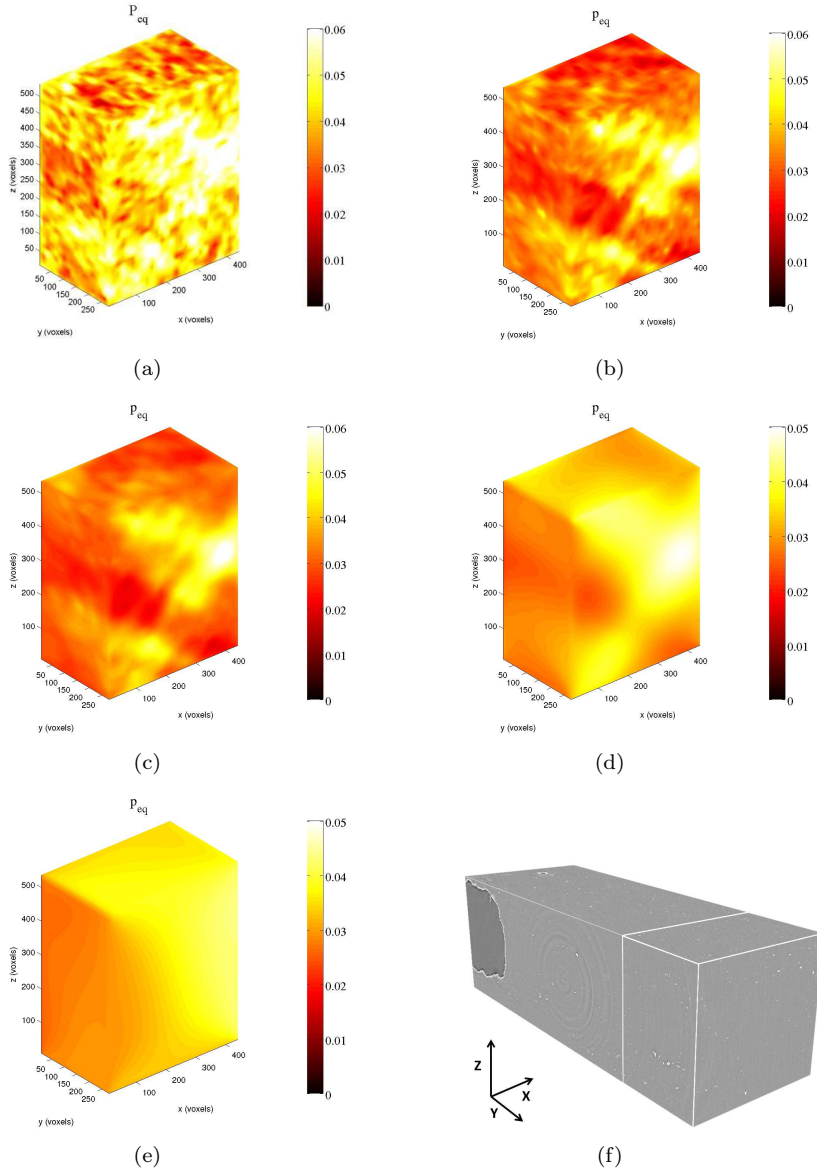


FIGURE 9: Equivalent strain for the early stage of loading without regularization (a) and with the normalizing displacement field \mathbf{v}_1 and different equivalent regularization lengths $l_{req} = 5$ voxels (b), $l_{req} = 10$ voxels (c), $l_{req} = 30$ voxels (d), and $l_{req} = 500$ voxels (e). (f) Frame and location of the region of interest

It is worth noting that the regularization length corresponds to the cut-off length of a low pass mechanical filter. Special care should be exercised when

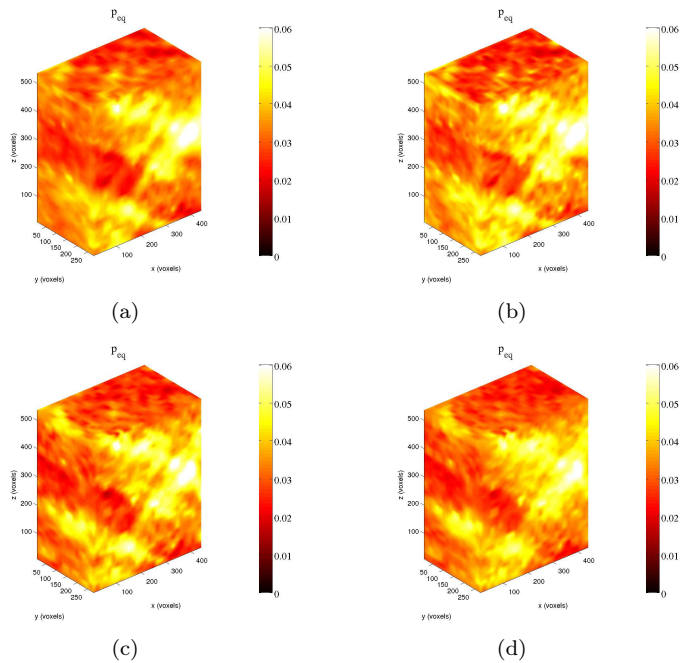


FIGURE 10: Equivalent strain for the early stage of loading with an equivalent regularization length of 5 voxels (see Figure 8(b)) that corresponds for field \mathbf{v}_1 to a length of 5 voxels (a), about 5 voxels for field \mathbf{v}_2 (b), 30 voxels for field \mathbf{v}_0 with Poisson's ratio of 0.49 (c), and 50 voxels for the Poisson's ratio of 0.27 (d). The frame is identical to that of Figure 9(f)

localization phenomena are studied. If a too large regularization length is selected, the kinematic fields are no longer faithfully evaluated. Conversely, when too small regularization lengths are chosen, measurement uncertainties become more pronounced. Consequently a trade-off is needed to account for these two opposite effects. Last, the mechanical regularization used herein is based on elastic assumption for the underlying behavior of the analyzed material. This limitation was partially circumvented by assuming quasi isochoric displacement and strain fields. However, to better capture localized bands other routes may be followed.

The method developed herein reveals to be viable for the study of complex strain patterns arising during ductile tearing. Larger regions are to be studied and the entire load history up to fracture to be analyzed to gain new insight into the ductile failure mechanisms at play.

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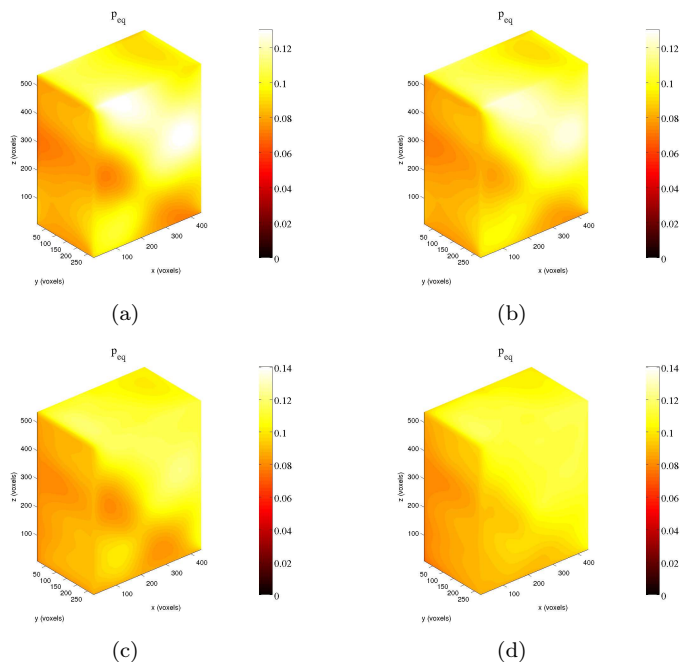


FIGURE 11: Equivalent strain for the late stage of loading with an equivalent regularization length of 30 voxels (see Figure 8(b)), which corresponds for field \mathbf{v}_1 to a regularization length of 30 voxels (a), 50 voxels for field \mathbf{v}_2 (b) and 500 voxels for field \mathbf{v}_0 with Poisson's ratio of 0.49 (c) or 0.27 (d). The frame is identical to that of Figure 9(f)

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