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Electrostatic method to estimate the mechanical properties of suspended membranes applied to nickel-coated graphene oxide

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We propose a method to estimate the bending rigidity and Young's modulus of thin conducting suspended membranes based on measuring the deflection of the membranes submitted to an electrostatic force. Our electrostatic method appears easier to implement and more reliable than AFM-based localized force-displacement measurements to estimate the bending rigidity and Young's modulus of slightly inhomogeneous materials. We apply the method on suspended graphene oxide (GO) sheets coated with a 5 nm thick Ni layer, providing a demonstration of electrostatic actuation for GO sheets. For a 7.7 nm thick membrane, a Young modulus of 360 GPa is found. © 2013 AIP Publishing LLC. [<http://dx.doi.org/10.1063/1.4817301>]

Graphene, like other two dimensional materials,¹ offers a wide range of sp²-specific physical and chemical properties² which has motivated its integration into a variety of devices, such as electromechanical resonators³ and actuators,⁴ field effect transistors,⁵ or electrochemical sensors.⁶ In the field of NanoElectromechanical Systems (NEMS), graphene is invaluable because of its high stiffness, its high surface over volume ratio, and its high sensitivity to environmental changes.^{7,8} A variety of graphenes resulting from the chemical exfoliation of graphite or graphite oxide,⁹ graphene oxide (GO), often under reduced form (RGO),¹⁰ has attracted attention for device fabrication, as it is easier than pristine graphene to fabricate, process, and functionalize,¹¹ while it has similar mechanical properties.¹² However, no examples of GO or RGO based NEMS devices are reported in the literature, because GO and RGO conductivities remain too low for electrostatic actuation. Here, we fabricate an electrostatically actuated suspended GO sheets. Sufficient conductivity is obtained by coating the GO sheet with a thin nickel layer.

While the nickel coating is used to ensure the overall conductivity of the material, its Young's modulus is quite low.¹³ The stiffness required for electromechanical applications is expected from the GO sheets. However, once processed and integrated, the mechanical properties of graphene and GO/RGO sheets are known to widely differ from theoretical expectations and from bulk material properties,^{12,14} so that the overall mechanical properties of the suspended membranes cannot be anticipated.

It is a hurdle for further use of the material into NEMS devices, as any difference in the mechanical properties, especially in the Young's modulus E , may affect device operation¹⁵ (resonance frequency, quality factor, bandwidth, amplitude of vibrations, operating voltage, etc.) through a change in the bending rigidity D , defined for a plate-like

material as $D = Et^3/12(1 - \nu^2)$ with ν the Poisson's ratio and t the thickness.¹⁶

The bending rigidity is often estimated from AFM based localized force-displacement measurements,^{17,18} resonance frequency measurements,¹⁹ or bulge test method.²⁰ More recently, the snap-through voltage of convex-buckled membranes has been used to estimate D .²¹ Alternately, the bending rigidity may be calculated from the Young's modulus derived by nanoindentation,²² Raman spectroscopy,²³ or *ab initio* calculations.²⁴

Here, we propose a method to estimate the bending rigidity and Young's modulus of suspended metal-coated GO sheets, and more generally of slightly inhomogeneous, thin, conducting membranes, following their integration into an electromechanical system. Our method relies on measuring by AFM the membrane deflection under electrostatic actuation. This approach is compared to results from AFM localized force-displacement experiments.

Devices are fabricated on Si(n++)/SiO₂(200 nm) substrates with Cr/Au (5/100 nm) top-side electrodes. The electrodes are shaped into pairs of 1 mm-long, 150 μm-wide rectangles spaced by a gap ranging from 1.4 μm to 5 μm. To serve as a conducting under-layer for the graphene oxide sheets, we first deposit a 5 nm thin nickel film by electron gun evaporation (Plassys MEB 550S). Nickel is used for its compatibility with the rest of the fabrication process (especially availability of deposition method and selectivity of wet etching) as well as for its good compatibility with graphene-based material as a graphene catalyst.²⁵ High purity (>90%) graphite oxide is exfoliated in ultra-pure water for 90 min to obtain GO suspension at a concentration of 4 mg/ml. A film of overlapping GO flakes is formed on the Ni layer by three successive depositions using the bubble deposition method. The deposition process is detailed elsewhere.²⁶ The average flake diameter is 3 μm. The average thickness of a single GO flake is 1.5 nm ± 0.3 nm.²⁶ The thickness of the GO film depends on the folding of the flakes

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and the number of superposed flakes. The GO sheets lying over the Ni layer are patterned into $20\ \mu\text{m}$ by $250\ \mu\text{m}$ stripes using optical lithography on AZ 1512 HS photo-resist followed by oxygen plasma etching.³ Aqueous hydrochloric acid at 12 mol/l is then used at room temperature to etch away the nickel not covered by GO and photoresist. Finally, the underlying SiO_2 layer is etched away to suspend the thin stripes. To prevent stiction during rinsing and drying,²⁷ HF is used in vapor phase at room temperature for 2 min (Ref. 28) (see Fig. 1).

Membranes are deflected downward electrostatically by applying a DC bias voltage V between the suspended membrane and the highly doped Si substrate.¹⁷ The AFM tip scans lines in tapping mode to acquire the vertical profile of the membranes along the suspended span. The suspended profiles are recorded for both null and non-null voltage V , and the vertical deflection is derived point by point as the difference between the two profiles. The voltage changes are applied very slowly so that the system remains in quasi-static regime.

Measurements are performed on several NiGO stripes under different bias voltages. Figure 2 presents the deflection with respect with position and the maximum deflection (at the middle of the suspended span) with respect to voltage.

An analytical model relying on Kirchoff-Love plate theory²⁹ is used to fit the experimental data and deduce the bending rigidity. The rectangular plate is assumed to be elastic, homogeneous, isotropic, and thin. The thin plate hypothesis is valid as the ratio of span ($1.4\text{--}1.8\ \mu\text{m}$) to thickness (lower than 15 nm) is larger than 20. We study the pure bending regime¹⁶ (deflections smaller than thickness) in static regime.

Let us denote l the span of the plate, y (resp. z) the spatial coordinate in the direction parallel (resp. perpendicular) to the trench axis, and $w(y, z)$ the vertical deflection (see Fig. 1). The system can be assumed translation-invariant along the y axis, so that $w(y, z) = w(z)$.

The equation governing the deflection w under an electrostatic force per unit area $Q(w(z))$ is

$$D \frac{d^4 w(z)}{dz^4} = Q(w(z)) = \frac{\epsilon V^2}{2(d_0 - w(z))^2}, \quad (1)$$

with D the bending rigidity, ϵ the permittivity of the gap material (here air), and d_0 the initial distance between membrane and substrate.

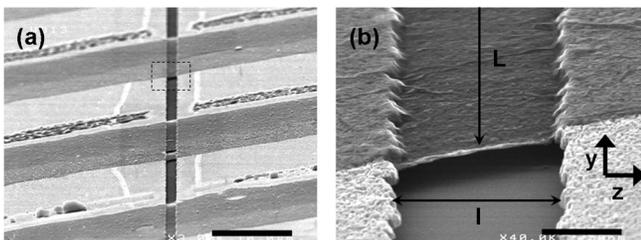


FIG. 1. SEM images of nickel-coated graphene oxide stripes suspended over a 200 nm deep, $1.4\ \mu\text{m}$ wide trench. (a) Stripes are $20\ \mu\text{m}$ wide and $250\ \mu\text{m}$ long and are spaced by $30\ \mu\text{m}$. Scale bar: $10\ \mu\text{m}$. (b) Zoomed image of the edge of a suspended stripe. Scale bar: 750 nm.

With $w(z) \ll d_0$ (small displacement regime), $Q(w(z))$ can be linearized as

$$Q_{lin}(w(z)) \simeq \frac{\epsilon V^2}{2d_0^2} \left(1 + \frac{2w(z)}{d_0} \right). \quad (2)$$

Solving the fourth-order linear differential Eq. (1) under the linearized force 2, we find

$$w(z) = -\frac{d_0}{2} + C_1 \cos\left(\alpha\left(z - \frac{l}{2}\right)\right) + C_2 \cosh\left(\alpha\left(z - \frac{l}{2}\right)\right), \quad (3)$$

with $\alpha = (\epsilon V^2 / D d_0^3)^{1/4}$. The coefficients $C_{1,2}$ are calculated using the boundary conditions of a rectangular plate with two opposite clamped edges and two opposite free edges.

The experimental deflection-versus-position profiles are fitted by the least square method using Eq. (3) with the bending rigidity D as fitting parameter (see Figure 2). Results are summarized in Table I.

In order to validate the electrostatic approach, the bending rigidity of the membranes is calculated from AFM force-displacement measurements. The suspended membranes are loaded by lowering the AFM tip. The vertical force applied by the tip and the membrane displacement at the tip contact point are simultaneously acquired, yielding one force-displacement $F(\delta)$ curve for each contact point. The portion of this curve corresponding to small displacements (with respect to thickness) is linear (the whole curve is generally well fitted by a third order polynomial), and its slope yields the spring constant of the membrane at the contact point. We acquire the force-displacement curves $F(\delta)$ on a regular 32×32 grid taken over a $3\ \mu\text{m} \times 3\ \mu\text{m}$ area containing the suspended zone and both its edges. After calibration, linear portions of $F(\delta)$ curves are fitted with a $k_l \delta$ model, k_l being the local spring constant.

The bending rigidity is deduced from the spring constant at the center of the membrane using linear analytical models. For suspended 1D materials such as nanotubes^{30,31} and nanowires,¹⁷ the linear clamped beam model (Euler-Bernoulli beam theory) is used to derive the relationship between the spring constant at the middle of the beam k_m and the Young's modulus E : $k_m = 192 \frac{E t^3 w}{12 l^3}$, where t , w , and l are, respectively, the thickness, the width, and the length of the beam. For plate geometries, the relationship is significantly different and depends strongly on the boundary conditions. For circular plates of radius r with clamped edges, the analytical model $k_m = 16\pi D \frac{1}{r^2}$ derived in Ref. 16 is used.^{32,33} For rectangular plates with two opposite edges clamped and two opposite edges free, one of the most common experimental configuration for graphene-like material, the analytical derivation of the deflection is highly involved: no author has ever provided an analytical, exact, or approximate, relationship between the spring constant at the center of the plate and the bending rigidity. The beam relationship is commonly used,^{18,23,34} but is expected to yield significantly underestimated values for the bending rigidity and the Young's modulus.

Here we use finite elements to derive an approximate analytic expression for the spring constant at the center of the plate. The suspended membrane is modeled as a

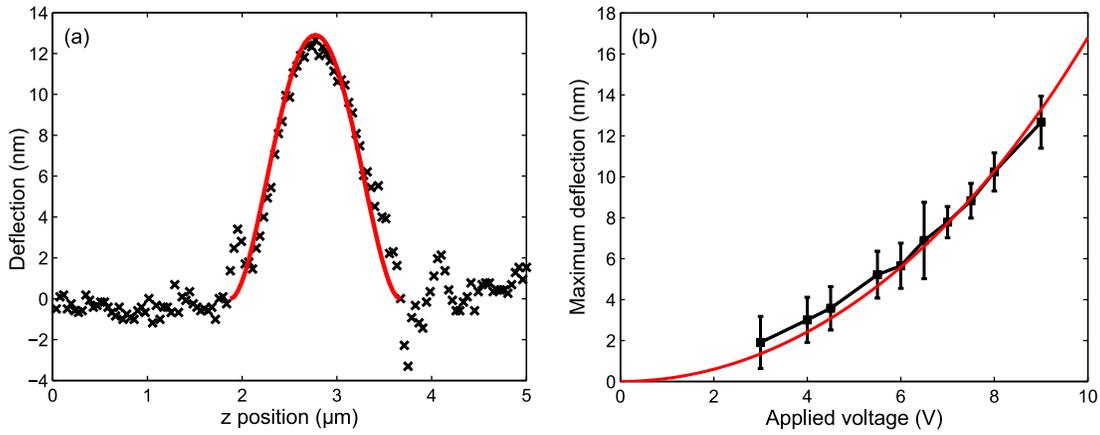


FIG. 2. (a) Deflection of a $1.8 \mu\text{m}$ wide and 8.1 nm thick membrane at DC bias of 9 V . Experimental measures (in black crosses) are fitted (red lines) by the linear model (3). (b) Maximum deflection (at the center of the membrane) with respect to DC bias voltage (in black squares). Measurements are fitted (red line) using (3).

rectangular, elastic, homogeneous, isotropic, thin (thickness t) plate clamped along its long edges (size L) and free along its short edges (size l). The force is applied at the center and is modeled as a point load because the radius of the AFM tip (around 10 nm) is much smaller than the short edge l and the characteristic size of finite element meshes suitable to such geometries. Pre-stress is neglected.

The relationship between force F and deflection at the center δ is derived as follows: according to the linear plate model, F/δ is proportional to $E/(1-\nu^2)$. We verify numerically that δ is independent from L as soon as $L > 1$. Then, with $L = 20 \mu\text{m}$, we calculate the plate deflection δ for 16 different (t, l) pairs, with t ranging from 10 nm to 30 nm and l ranging from $0.5 \mu\text{m}$ to $1.8 \mu\text{m}$. Using these 16 values for the deflections, we establish with better than 2% accuracy (fit by least square method) the relationship

$$k_m = 137 \frac{E}{12(1-\nu^2)} \frac{t^3}{l^2} = 137 \frac{D}{l^2}. \quad (4)$$

Using this analytical relationship (4) between spring constant and bending rigidity, we derive the bending rigidity of the NiGO stripes as summarized in Table II.

The values obtained for the bending rigidity of the $1.4 \mu\text{m}$ wide membrane can be divided into three groups (as identified in Table II). We postulate that these groups correspond to three different thicknesses $(t_1, t_1 + 1.5, t_1 + 3) \text{ nm}$ corresponding to an increasing number of overlapping GO flakes.²⁶ The best fit for the thickness is $t_1 = 7.7 \pm 1.6 \text{ nm}$, corresponding to $E = 360 \text{ GPa}$ for the Young's modulus. Table II and the Figure 3 summarize the different thicknesses derived using this value for E . Using the classical relationship between Young's modulus and thickness for composite

materials undergoing bending ($E t_1 = t_{\text{Ni}} E_{\text{Ni}} + t_{\text{GO}} E_{\text{GO}}$)³⁵ and using literature value for thin Ni films ($E_{\text{Ni}} = 240 \text{ GPa}$ for 20 nm thick Ni (Ref. 36)), we deduce $E_{\text{GO}} = 580 \pm 120 \text{ GPa}$. This value is about twice larger than typical experimental values for GO. Three factors can explain this elevated value: an underestimation of the Ni Young's modulus is likely, as the Young's modulus varies with the film thickness.³⁷ Additionally, the GO here has been transferred by the bubble deposition method, which is expected to induce very little structural damage in the material.³⁸ Finally, pre-stress has been neglected in our calculation. If NiGO membranes are pre-stressed, an overestimation of the bending rigidity and the Young's modulus is induced.

The values of bending rigidity obtained with the electrostatic approach for devices a, b, and c would correspond to 14.5 nm , 15.8 nm , and 8.8 nm thick membranes, respectively. This is in agreement with the measured thickness using AFM in contact mode (8.1 nm for device c in Table I).

Contrary to the classical AFM-based method which relies on localized measurements highly sensitive to heterogeneity and defects, our electrostatic approach accounts for the global mechanical behavior of the membrane. Hence, the influence of technological artifacts and measurement noise is lowered. Furthermore, the electrostatic method is easier to implement since it does not require prior (Sader model-based) derivation of the AFM cantilever spring constant.³⁹ Derivation of the intrinsic mechanical parameters from the measurements is easier too, as the models for homogeneous forces are much more easily derived analytically for any geometric configuration. Admittedly the electrostatic method

TABLE I. Bending rigidity of the NiGO stripes deduced from the AFM-measured displacements under electrostatic actuation.

Label	Gap (μm)	D (10^{-14} N.m)	Fit error (%)
a	1.4	9.3	26
b		12	24
c	1.8	2.1	15

TABLE II. Bending rigidity and thickness of the NiGO stripes.

No	l (μm)	D (10^{-14} N.m)	Std (%)	Group	t (nm)
1		1.2	24	♣	7.7
2		1.4	23	♣	
3		1.6	14	♣	
4	1.4	2.3	16	■	9.2
5		2.5	13	■	
6		3.6	10	♠	10.7
7		3.9	16	♠	

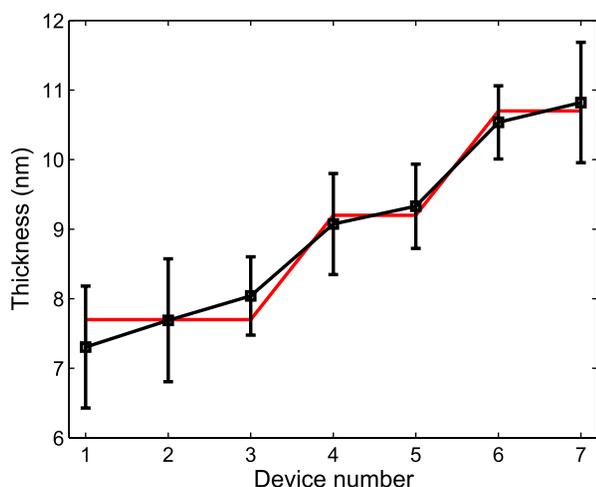


FIG. 3. In black squares, the estimated thickness of each measured device with error bars. In red line, theoretical thickness corresponding to $(t_1, t_1 + 1.5, t_1 + 3)$ nm.

requires the prior electrical connection of the electrodes and implies that the membrane is entirely suspended in order to avoid short circuits, but these requirements are similar to what any transducer device should satisfy and are thus not reducing the impact of our method for electromechanical systems.

In this paper, we propose a method to determine the bending rigidity of suspended membranes which relies on measuring by tapping-mode AFM the deflection of the membrane under electrostatic loading and on interpreting the data using an analytical plate model.

We apply this method to the electrostatically actuated suspended GO membranes. Sufficient conductivity of the membrane material is obtained using a thin nickel coating. Results are found to agree with bending rigidity values determined using the reference method relying on localized AFM force-displacement curves.

Compared to this reference method, our electrostatic method appears more suitable to assess the properties of slightly inhomogeneous or defect-free materials. It is significantly easier to implement, and the results are more straightforward to analyze in terms of bending rigidity. This technique is not limited to NiGO films but can be applied to any other kind of suspended conducting materials.

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