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# Spatially distributed flood forecasting in flash flood prone areas: Application to road network supervision in Southern France.

J.-P. Naulin<sup>a</sup>, O. Payrastré<sup>a</sup>, E. Gaume<sup>a,\*</sup>

<sup>a</sup>*LUNAM Université, IFSTTAR, GERS, F - 44344 Bouguenais cedex, France*

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## Abstract

Accurate flood forecasts are critical to an efficient flood event management strategy. Until now, hydro-meteorological forecasts have mainly been used to establish early-warnings in France (meteorological and flood vigilance maps) or over the world (flash-flood guidances). These forecasts are typically limited either to the main streams covered by the flood forecasting services or to specific watersheds with specific assets like check dams, which in most cases are well gauged river sections, thus leaving aside large parts of the territory. This paper presents a distributed hydro-meteorological forecasting approach, which makes use of the high spatial and temporal resolution rainfall estimates that are now available, to provide information at ungauged sites. The proposed system intended to detect road inundation risks had initially been developed and tested in areas of limited size. This paper presents the extension of such a system to an entire region (i.e. the Gard region in Southern France), including over 2,000 crossing points between rivers and roads and its validation with respect to a large data set of actual reported road

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\*Corresponding author. Tel.: +33(0)2 40 84 58 84, Fax: +33(0)2 40 84 59 98  
*Email address: eric.gaume@ifsttar.fr* ()

inundations observed during recent flash flood events. These initial validation results appear to be most promising. The eventual proposed tool would provide the necessary information for flood event management services to identify the areas at risk and adopt appropriate safety and rescue measures: i.e. pre-positioning of rescue equipment, interruption of the traffic on the exposed roads and determination of safe access or evacuation routes. Moreover, beyond the specific application to the supervision of a road network, the research undertaken herein also provides also results for the performance of hydro-meteorological forecasts on ungauged headwaters.

*Keywords:* Flash flood, forecast, distributed model, event management, ungauged watershed

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## 1. Introduction

2 Europe's Mediterranean region is frequently affected by severe flash floods,  
3 which can be characterized by their very fast dynamics. According to Gaume  
4 et al. (2009), these so called "flash floods" probably represent the most de-  
5 structive natural hazard in the Mediterranean zone. The catastrophic flood-  
6 ing that occurred in the Var region in southern France in June 2010 once again  
7 illustrates the destructive effects of such floods. Furthermore, the lack of an-  
8 ticipation of these events combined with their very rapid evolution limit the  
9 efficiency of event management and rescue operations to a considerable ex-  
10 tent. If good preparation is able to help authorities cope with such events, the  
11 availability of short-term forecasts could offer a major improvement, which  
12 is essential to providing the necessary information for a correct diagnosis of  
13 the situation as well as the organization of rescue operations.

14 Several systems are currently used to produce operational flood warnings  
15 in Europe. One recently developed approach consists of introducing Ensem-  
16 ble meteorological predictions as input to hydrological and/or hydraulic mod-  
17 els in order to generate river discharge forecasts (Cloke and Pappenberger,  
18 2009). This approach lies at the core not only of the European Flood Alert  
19 System (EFAS) developed by the European Joint Research Center (Thielen  
20 et al., 2009), but also of the advanced Hydrological Prediction Service pro-  
21 posed by the U.S. NOAA (McEnery et al., 2005) or of the Vigicrue system  
22 run by the SCHAPI in France (Tanguy et al., 2005). These methods however  
23 mostly apply to gauged sections of relatively large rivers with forecasting lead  
24 times of at least 12 to 24 hours and are not suited to flash flood conditions  
25 (Borga et al., 2009). Flash flood forecasting must cope with the complex  
26 spatio-temporal patterns of the generating rainfall events which significantly  
27 limits the accuracy and relevance of meteorological forecasts. Recent im-  
28 provements in the EFAS approach (Alfiery et al., 2012) have shown that  
29 relevant flash flood warnings may be expected for medium-sized watersheds  
30 (i.e. greater than 500 km<sup>2</sup>). Since damage often occurs in headwater catch-  
31 ments a few km<sup>2</sup> in size (Ruin et al., 2008), it is also necessary to provide  
32 information in these areas that are often ungauged. This implies implemen-  
33 tating rainfall-runoff models based on distributed rainfall observations, with  
34 shorter lead times and limited calibration possibilities.

35 A variety of methods have been developed to produce short-term flash  
36 flood forecasts or alerts on small streams (1 to 500 km<sup>2</sup>). The most com-  
37 mon of these are based on rainfall thresholds associated with risk levels,  
38 such as Flash Flood Guidance (Carpenter et al., 1999; Georgakakos, 2006) or

39 Bayesian decision approach (Martina et al., 2006). Other methods, based on  
40 distributed rainfall-runoff simulations and discharge thresholds (Reed et al.,  
41 2007; Younis et al., 2008; Javelle et al., 2010) have been developed yet based  
42 on limited tests and validation at ungauged sites. Moreover, the selected  
43 alert thresholds are typically uniform over a given territory, or else deter-  
44 mined based on knowledge of the local consequences of flooding. In an ideal  
45 case, flood forecasting methods should be combined with an exposure rating  
46 method so as to provide valuable outputs at a large spatial scale and not just  
47 at a small number of strategic points.

48 More recently, Versini et al. (2010a,b) proposed a prototype of a road  
49 inundation warning system (RIWS) adapted to flash floods. This system  
50 also relies on distributed rainfall-runoff simulations, though several reasons  
51 have led to focusing on road inundations as a specific consequence of flash  
52 floods. First, roads are particularly vulnerable: they generally are the as-  
53 sets affected first and nearly half of all flash flood victims are car passengers  
54 trapped in their vehicles by the rapid rise of water (Drobot et al., 2007; Ruin  
55 et al., 2007). Second, the road network is sufficiently dense throughout the  
56 territory and moreover inundations are often reported. These reports provide  
57 indirect information on flood location and intensity. Third and last, warn-  
58 ings of possible road inundations may be of strategic value for emergency  
59 services in identifying the areas at risk and selecting safe accesses or evacu-  
60 ation routes. The RIWS is intended to provide a real time estimation of the  
61 road submersion risk at each intersection between roads and the stream net-  
62 work. These intersections mainly correspond to bridges, dams, culverts (for  
63 channelized streams) or fords. The computed risk level results from the com-

64 parison of forecasted discharges using a rainfall-runoff model and discharge  
65 thresholds established according to the estimated susceptibility to flooding  
66 of each single intersection.

67 The initial version of the RIWS has been developed and tested on a ter-  
68 ritory with limited areal (240 km<sup>2</sup>, see Figure 1) under relatively favorable  
69 conditions: homogeneous hydrological behavior, and the availability of ex-  
70 tensive information on road susceptibility to flooding.

71 The work presented herein is aimed at both, extending the RIWS to  
72 the entire Gard region (5000 km<sup>2</sup>), which corresponds to an actual pre-  
73 operational test and further developing and testing this tool using a larger  
74 data set.

75 A spatial extension of the initial RIWS presents two main difficulties.  
76 The first one is the implementation of a rainfall-runoff model at high spatial  
77 resolution, mainly on ungauged catchments of a limited area (less than 2 km<sup>2</sup>  
78 on average), and on a territory that features a wide array of hydrological and  
79 hydraulic conditions: variability of soil and land use characteristics (in some  
80 cases with karstic conditions), a stream network including small upstream wa-  
81 tercourses and downstream rivers with broad floodplains. The model should  
82 also take into account the spatial heterogeneity of rainfall inputs, with com-  
83 putation times being compatible with a real-time application. The second  
84 difficulty lies in the definition of the susceptibility of roads to flooding in  
85 areas where little or no data on past reported inundations are available, in  
86 comparison with the areas initially selected (Versini et al., 2010a).

87 The paper's next section will present the case study and the develop-  
88 ments introduced in the initial RIWS methodology in an effort to answer the

89 aforementioned questions. Several tests of the expanded system will then be  
90 provided, based on a dataset that includes 10 recent flooding events, which  
91 lead to observations of significant disruptions to the road network. These  
92 initial results will then be discussed as a preliminary to proposing further  
93 system improvements.

## 94 **2. Presentation of the Gard region and available datasets**

### 95 *2.1. The Gard region*

96 The Gard region is an administrative jurisdiction located in southeast-  
97 ern France. Its boundaries are presented in Figure 1: the northwest part of  
98 this area includes the Cévennes Mountains, a medium elevation chain cul-  
99 minating at Mont Lozère (1,699 m); on the other hand, the southeast part  
100 corresponds to plateaus and plains extending to the Mediterranean coast,  
101 with elevations varying between 0 and 200 meters. This region displays typ-  
102 ical Mediterranean climate, as revealed by heavy rainfall events during the  
103 autumn season. The 10-year daily rainfall accumulation ranges from 100 mm  
104 near the Mediterranean coast to more than 270 mm in the Cévennes foothills  
105 (CNRS-INPG, 1997).

106 This territory is the French region most frequently affected by flash floods  
107 (Gaume et al., 2009). Over the last 25 years three exceptional rainfall events  
108 have caused considerable damage and losses. In 1988 the city of Nîmes was  
109 completely devastated by a flood associated with rainfall accumulations in  
110 excess of 400 mm within 6 hours (Desbordes et al., 1989), causing 9 deaths.  
111 The extraordinary flood event of the 8<sup>th</sup> and 9<sup>th</sup> of September 2002 affected  
112 the entire Gard region, with rainfall accumulations that locally exceeded 600

113 mm in 12 hours, causing 24 deaths in addition to economic losses estimated  
114 at €1.2 billion (Delrieu et al., 2004). Lastly, a major event was also observed  
115 on September 2005 6<sup>th</sup>-8<sup>th</sup> in the southern part of the region, with local  
116 rainfall accumulations of about 300 mm on the 6<sup>th</sup> and 250 mm on the 8<sup>th</sup>,  
117 responsible for significant inundations in Nîmes, but more predominantly in  
118 the downstream plains (Maréchal et al., 2007).

119 This region is divided into six main watersheds covering 4/5<sup>th</sup> of the  
120 Gard territory: the Gardon (1858 km<sup>2</sup>), the Cèze (1355 km<sup>2</sup>), the Vidourle  
121 (798 km<sup>2</sup>), the Vistre (600 km<sup>2</sup>), the Hérault (817 km<sup>2</sup>), and the Dourbie  
122 (468 km<sup>2</sup>) (see Figure 1). Except for the Vistre, these rivers all originate in  
123 the Cévennes Mountains, which correspond to primary geological formations.  
124 Over their downstream part, the Gardon, the Vidourle and the Cèze rivers all  
125 cross a plateau area, characterized by sedimentary bedrock mostly composed  
126 mainly of marls and locally of karstified limestone. The extreme southern  
127 part of the Gard region corresponding to the Vistre watershed and extreme  
128 downstream part of the Vidourle River, is a flat and low elevated plain,  
129 covered by thin and diversified Quaternary alluvial formations.

## 130 *2.2. Road network and road inundation inventories*

131 The road network considered herein includes all road sections except for  
132 local connections at the district scale. Since 2007 this road network has been  
133 managed in large part by the Gard Departmental Council whose oversight  
134 includes maintenance operations, traffic management and the construction of  
135 new road sections. This involvement extends to field surveillance during floods  
136 and, if necessary, closing the inundated roads to the traffic, and information  
137 dissemination on road traffic conditions to other authorities and to the media.



138 The total number of intersections between roads and rivers depends on the  
139 river network definition. This number lies close to 2,200 when the Carthage  
140 <sup>1</sup> hydrographic database is used with an average upstream watershed area of  
141 less than 2 km<sup>2</sup> (Fig. 2). The RIWS will be required to provide an estimated  
142 discharge value every 15-min at each of these intersections.

143 One important specificity of the region considered in this analysis is the  
144 availability of a relatively thorough information (when compared to other  
145 regions) regarding road network susceptibility to flooding. This information  
146 relies on two distinct sources.

147 First, a systematic inventory of critical road sections, known from field  
148 experience and human memory, was conducted after the major 2002 flood.  
149 This initial compilation, called the PICH, basically covers a 40-year period  
150 and identifies 160 road sections displaying a potential risk of submersion.  
151 This PICH inventory also includes an estimation of the flood return period  
152 of each identified vulnerable road section. This compilation however only  
153 covers the northwest part of the Gard region, and does not provide event-  
154 specific information. The PICH has been used to adjust the susceptibility  
155 rating method in the RIWS. Note that only 71% of the points reported in  
156 the PICH actually correspond to intersections identified in Figure 2: the  
157 remaining 29% may correspond to local road sections not considered herein,  
158 or else to inundations that cannot be associated with a river intersection:  
159 low points and or lateral overflow of a stream. Consequently, the RIWS will

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<sup>1</sup>The BD CARTHAGE® database, produced by the French National Geographic Institut, the MEDD (French Ministry of Ecology and Sustainable Development) and the various Water agencies, constitutes the hydrographic reference in France.

160 not be able to detect all types of localized inundations or disruptions but will  
161 capture the majority of them.

162 Second, since 2002, inventories of the road disruptions associated with  
163 single flood events have gradually been developed. These inventoried road  
164 closures are mainly caused by road submersions but might also sometimes be  
165 induced by snow, landslides or rock falls, or even road accidents. The most  
166 exposed roads may also be closed preventively. This information collection  
167 system at the event scale has been progressively implemented and has just  
168 recently reached maturity: these inventories have only become systematic  
169 since 2007. Ten event reports are ultimately available over the period 2002-  
170 2008; they have been presented in Table 1. Nonetheless, this information is  
171 heterogeneous and probably far from being exhaustive. The first reports did  
172 not indicate the timing or exact locations and causes of the road closures;  
173 reports on more recent events tend to be more accurate in space and time.  
174 These event reports of road disruptions have still been used to evaluate the  
175 RIWS performance.

176 According to both the PICH and the event-specific reports, 528 of the  
177 2,172 intersections represented in Figure 2 have been inundated at least once  
178 over the last 40 years.

### 179 *2.3. Rainfall and stream flow data*

180 The Gard region is covered by a relatively dense network of rain gauges  
181 (about 1 gauge every 150 km<sup>2</sup>) and two weather radars providing high spa-  
182 tial and temporal resolution quantitative precipitation estimates (QPE). The  
183 available operational datasets have been subjected to a thorough quality con-  
184 trol and can be considered of above-average accuracy (Boudevillain et al.,

2011). The results presented in this paper are based on an interpolation  
of rain gauge measurements through simple kriging with a climatological  
isotropic variogram (Lebel et al., 1987). Radar quantitative precipitation  
estimates would probably be more appropriate in this context of flash floods.  
Due however to the evolution in radar data post-processing and to the radar  
disruptions for certain specific events, radar data of homogeneous quality  
were only available for 5 out of the 10 reported flooding events selected for  
this study (see Table 1). A comparison of the RIWS results with various types  
of rainfall inputs, based on these 5 events (Naulin et al., 2011), showed that  
the detailed location and levels of risk alarms triggered are significantly mod-  
ified by the type of inputs (radar-based QPEs or kriged rain gauge data), but  
that the overall detection performance based on skill scores were not highly  
altered. The results obtained with the kriged rainfall data were selected for  
this paper in order to maintain an extensive evaluation dataset with rela-  
tively homogeneous rainfall inputs. The generated rainfall fields display a  
1-kilometer spatial resolution and a 1-hour temporal resolution: they have  
been divided into four equivalent 15-minute time steps to match the needs  
of the rainfall runoff-model.

The Gard region counts 23 stream gauges located for the most part on  
the major streams. The stream gauge measurements have been used herein  
to verify the performances of the rainfall-runoff model prior to its applica-  
tion in the RIWS. Nevertheless, these measurements yield little information  
regarding the accuracy of the rainfall-runoff simulations on the upstream  
tributaries.

209 *2.4. Selection of the flood event dataset*

210 The 13 events with a maximum measured point rainfall accumulation  
211 exceeding 50 mm/day over the period 2007-2008 were selected in order to test  
212 the RIWS. Four additional events from the period 2002-2006 with available  
213 event-specific reports of road disruptions were added to the dataset. The final  
214 event dataset is presented in Table 1: it includes a wide variety of hydro-  
215 meteorological configurations: from exceptional and generalized events, to  
216 more localized and/or lower magnitude events. Seven of the selected events  
217 did not induce any reported disruptions, while the other events illustrate the  
218 features and frequency of floods inducing road inundations across this region.

219 **3. Description of the RIWS**

220 *3.1. General principle*

221 Versini et al. (2010a,b) proposed to consider the risk of submersion as  
222 the combined consequences of the magnitude of the forecasted discharge in  
223 a given river section and the susceptibility to flooding of the corresponding  
224 road-river intersection. This susceptibility is determined using the estimated  
225 flood return period for the road; it can be compared to the theoretical return  
226 period of the forecasted discharge. The RIWS therefore includes three sepa-  
227 rate components, namely: i) a rainfall-runoff model producing the forecasted  
228 discharges at each intersection, ii) a road-river intersection susceptibility rat-  
229 ing method, and iii) a method for estimating the discharge return periods at  
230 each intersection (i.e. the SHYREG regional flood frequency method Lavabre  
231 et al. (2003)).

232 Since the flood return period depends to a great extent on the local config-  
233 uration of each road-river intersection, it might not be determined accurately  
234 without specific observations which are generally unavailable. Versini et al.  
235 (2010a) therefore proposed to simplify the description of susceptibility and  
236 sort intersections into just four susceptibility classes (from high to very low  
237 susceptibility), with each class assigned its own distribution of flood return  
238 periods. For a given discharge return period, the probability of inundation  
239 (i.e. the flood risk level) thus differs for each susceptibility class.

240 Lastly, three inundation risk levels, corresponding to an increased proba-  
241 bility of flooding, may be generated by the RIWS at each computation time  
242 step and intersection, on the basis of the contingency table 2.

243 The first application presented by Versini et al. (2010a,b) is based on the  
244 Cinecar rainfall-runoff model (Gaume et al., 2004), which has been applied  
245 using homogeneous production parameters given the limited extent of the  
246 considered areas (240 km<sup>2</sup>). The susceptibility rating method, i.e. the process  
247 of sorting intersections into the four susceptibility classes, was based on three  
248 morphological parameters: local slope of the river bed, upstream watershed  
249 area, and elevation. Versini et al. (2010a) observed that the more vulnerable  
250 road sections identified in the PICH inventory were in fact concentrated  
251 on smaller slopes and lower elevation areas with large upstream watersheds  
252 (Fig. 3). The four susceptibility classes were defined using combinations of  
253 thresholds for these three parameters, with the high susceptibility class only  
254 containing PICH points and the very low susceptibility class containing no  
255 PICH points (see Table 4).

256 In the application presented herein, the general principles of the RIWS

257 have been preserved. The extension of this system to the entire Gard ter-  
258 ritory, which involves a wider variety of local configurations, has however  
259 required introducing some changes into both the rainfall-runoff model and  
260 susceptibility rating method. The next two sections will present in detail  
261 the corresponding methodological evolution. The return periods in Table 2  
262 have remained unchanged. The selected discharge return period estimation  
263 method is based on a stochastic simulation of long rainfall-runoff series, yet is  
264 not directly correlated with the rainfall-runoff model used in the RIWS. This  
265 situation may cause biases; therefore, the RIWS was tested on the 2007-2008  
266 continuous period (including 13 significant rainfall events but only 6 inundat-  
267 ing events) to evaluate the possible system under or over-reaction (Section  
268 4.2).

### 269 *3.2. Modifications of the rainfall-runoff model*

270 The CINECAR model has once again been selected here to compute the  
271 discharges every 15-min at the 2,172 intersections identified in the Gard re-  
272 gion. This model is distributed and based on a representation of the water-  
273 shed as a ramified series of stream reaches with a rectangular cross-section, to  
274 which both left and right hand hillslopes with schematic rectangular shapes  
275 are connected (Fig. 4).

276 This model only depicts the rapid runoff and is suited for simulating the  
277 rising limb and peak phases of significant flood events. The Soil Conserva-  
278 tion Service - Curve Number (SCS-CN) model has been used to compute  
279 runoff rates and the corresponding effective rainfall on the hillslopes at each  
280 computation time step. The effective rainfall is then propagated on both the  
281 hillslopes and downstream river network using the kinematic wave model,

282 which has been resolved by the method of characteristics according to an  
283 approach proposed by Borah et al. (1980). The model is flexible and its  
284 space and time scales can easily be adapted to meet user needs. Moreover,  
285 the model is capable of accounting for the spatial variability of rainfall. For  
286 this particular application, the hyetographs corresponding to each individual  
287 hillslope have been extracted from interpolated rainfall fields.

288 This model, initially developed to support the hydrological analysis of  
289 data collected after extreme flash flood events, has provided satisfactory re-  
290 sults for reconstructing the floods that occurred in September 2002 in the  
291 Gard (Delrieu et al., 2005; Gaume et al., 2004). Due to model simplicity,  
292 its computation time is limited: less than 60 sec. CPU for a 12-hours event  
293 over the entire Gard region. Moreover, CINECAR has a limited number  
294 of calibration parameters. The widths of river reaches constitute the main  
295 parameters controlling the transfer function. The roughness coefficients are  
296 considered to be constant and their values are set at 0.05 for channels and  
297 0.1 for hillslopes. Channel widths can be determined through field surveys  
298 or an analysis of aerial photographs. For the sake of simplicity, fixed average  
299 channel width values  $W_{I,T}$ , related to the the Strahler order  $I$  of the reach,  
300 and the return period  $T$  of the simulated discharge, have been introduced  
301 according to a simple relation:

$$W_{I,T} = W_{1,T} \cdot I^2 \quad (1)$$

302 with  $W_{1,T}$  being the channel width for reaches of Strahler order 1 (see Table 3  
303 for the calibrated values in the Gard).

304 Some modifications of the transfer function have been introduced in order

305 to extend the model to the region, namely: a model simulating the effects  
306 of the five major check dams, the diffusive wave model and Hayami method  
307 (Hayami, 1951; Moussa, 1996) for river reaches with slopes of less than 1%  
308 (to simulate the attenuation of the flood waves in the downstream part of  
309 the river network).

310 The Curve Number (CN) value is the second important calibration pa-  
311 rameter and controls the temporal evolution of runoff rates and, as a conse-  
312 quence, the flood magnitude. In the initial version, the CN value was assumed  
313 to be homogeneous over the limited application areas; its variation in space  
314 has been taken into consideration for the RIWS extension to the entire Gard  
315 region. This step is based on the USDA proposed method (USDA, 1986) to  
316 determine the CN values as a function of land use, soil types (Corine Land  
317 Cover data base and European Soil Database) and during the 5 days pre-  
318 ceding rainfall accumulation. As opposed to the conclusions of other recent  
319 works (Huang et al., 2007; Soulis et al., 2009), this method has led to satis-  
320 factory results, without requiring further adjustments, for the major recent  
321 flood events (Table 1) at the 23 gauged sites of the Gard region.

322 Most of the target sites (intersections) are located on small ungauged up-  
323 stream watersheds. The hydrological model which has only undergone slight  
324 adjustments, has in fact been mostly validated with respect to measured  
325 data. No real systematic calibration has been performed. The objective  
326 here was to obtain a model that could produce homogenous results at the  
327 regional level while avoiding site specific models requiring an intensive cal-  
328 ibration phase. As such, the ultimatemodel performance is satisfactory for  
329 the major events selected to test the RIWS (Fig. 5): with an average Nash



330 criterion computed for each single event equal to 0.49.

331 These results can be compared with the validation outcome of a concep-  
332 tual rainfall runoff model calibrated on each specific stream gauge observed  
333 series. The GR4 model, chosen for such a comparison, is a lumped model de-  
334 veloped by Edijatno and Michel (1989) and advanced by Perrin et al. (2003).  
335 This hourly rainfall-runoff model requires four parameters to be automati-  
336 cally calibrated with respect to measured data.

337 A comparative test between Cinecar and GR4 has been conducted for the  
338 Anduze stream gauge on the Gardon River: i.e. the largest and highest  
339 quality discharge series in the region. A 2-year series was used to calibrate  
340 the GR4 model. The obtained Nash score derived over a 6-year validation  
341 period reached 0.59, which lies in the average range of values reported in  
342 the literature for applications of continuous rainfall-runoff models (Perrin,  
343 2002). The corresponding "event-specific" Nash criteria are then compared  
344 with the Cinecar criteria for the largest validation floods in Figure 6.

345 Results indicate that while the Cinecar model is less efficient for minor  
346 events, the two models present a similar performance for the larger events  
347 (i.e. unit peak discharge exceeding  $2 \text{ m}^3/\text{s}/\text{km}^2$ ) which do constitute the  
348 focus of the present study and more generally of flood forecasting models  
349 for this region.

350 Since the RIWS is based on thresholds and not directly on simulated  
351 discharge values, its performance will mainly be controlled by the correct  
352 forecast of the magnitude or, more precisely, the correct position of the sim-  
353 ulated discharge when compared to the discharge quantiles. Figure 7 shows  
354 that the Cinecar model predicts peak discharges with typically the same

355 range of estimated return periods as the observed peak discharges. Except  
356 for some few obvious overestimations, the differences between simulated and  
357 observed discharges do not exceed one return period class. In considering  
358 the additional filtering introduced when computing risk levels (Table 2),  
359 it is anticipated that these differences will have little impact on the RIWS  
360 performance.

### 361 *3.3. Modifications to the susceptibility rating method*

362 Extending the RIWS to the entire Gard region also required adapting  
363 the susceptibility rating method to account for the large spatial variability of  
364 observed inundations and geomorphic characteristics throughout the region.

365 The distribution of PICH points into the four susceptibility classes, as  
366 presented in Table 4, reveals that the efficiency of a sorting method based  
367 on morphological parameters decreases when moving from the initial area  
368 considered by Versini to the entire region covered by the PICH inventory  
369 (approx. half of the entire Gard region), with the proportion of PICH points  
370 in susceptible classes markedly decreasing.

371 A detailed analysis shows that the geographical distribution of PICH  
372 points, as presented in Figure 2, is very heterogeneous at the PICH territorial  
373 scale. The initial sorting method is not able to capture this variability since  
374 it generates susceptibility classes with a relatively homogeneous geographical  
375 density. In order to improve the results of the susceptibility rating results,  
376 the sorting method has therefore been applied separately to three sub-areas  
377 displaying significantly different PICH point densities:

- 378 • the mountainous area, where the density of PICH points is very low  
379 (i.e. less than 5 % of the intersections). The intersections located in

380 this area are only assigned to the low and very low susceptibility classes  
381 depending on local slope, altitude and upstream catchment area;

- 382 • the plateau and plain area with an intermediate PICH point density  
383 and where the intersection points may be assigned to any of the three  
384 lowest susceptibility classes (very low, low and average);
- 385 • the identified flood plains in the plateau and plain area, with a very high  
386 PICH point density (exceeding 30 %). In these areas, all intersections  
387 are assigned to the high and very high susceptibility classes.

388 The results presented in Table 4 indicate that this application to three  
389 homogeneous sub-areas improves the sorting results to a fair extent, which in  
390 turn leads to decreasing the proportion of intersections considered as vulner-  
391 able (as reflected by an increase in the very low susceptibility class). A higher  
392 proportion of intersections is also assigned to the high and average suscepti-  
393 bility classes with an equivalent proportion of PICH points in these classes.  
394 To validate this evolution in the susceptibility rating method, a comparison  
395 of RIWS performances will be presented in Section 5.1 below.

396 Furthermore, the distributions of flooding frequencies for intersections  
397 placed in each susceptibility class may be estimated on the basis of the PICH  
398 inventory. The dispersion in these distributions, combined with the uniform  
399 risk thresholds presented in Table 4, will logically lead the RIWS to generate  
400 a significant number of false alarms. Ideal detection rates and False Alarm  
401 Ratios of the system (FAR, see definition in Section 4.2) linked to the dis-  
402 persion of flooding frequencies in each susceptibility class can be estimated  
403 in an *a priori* manner for each risk level, i.e.:

- 404 • Risk level 3: Inundation highly probable (over 40% of the alarms corre-  
405 spond to actual inundations, hence FAR<60%, i.e. a discharge return  
406 period threshold exceeding the reported inundation return period for  
407 about 40% of all intersections listed in the class);
- 408 • Risk level 2: Inundation possible with a significant probability (over  
409 20% of alarms corresponding to actual inundations, FAR<80%);
- 410 • Risk level 1: Inundation possible with low probability (over 10% of  
411 alarms corresponding to actual inundations, FAR<90%);

412 These values will serve as a benchmark for the RIWS performance evalua-  
413 tion. The relatively high theoretical false alarm ratios are due to the difficulty  
414 involved in evaluating the susceptibility of intersections to flooding on the  
415 basis of available data; these figures provide an idea of the possible perfor-  
416 mances of the RIWS performance if the rainfall-runoff forecasts were nearly  
417 perfect.

#### 418 **4. Evaluation of the Road Inundation Warning System (RIWS)**

419 For starters, it is worth noting that over the period 2007-2008, during  
420 which the reports on flood events are certainly comprehensive, the RIWS  
421 only produces warnings (risk levels 1 to 3) for the 6 events with actually  
422 reported road inundations. This finding confirms that the RIWS is neither  
423 under-reacting nor over-reacting and is moreover capable of distinguishing  
424 the most significant flood events. Given these initial results, it seems that the  
425 rainfall-runoff model estimates discharges with the correct order of magnitude  
426 and that the risk thresholds were appropriately selected and estimated.

427 Given this initial positive outcome, the results presented below are mainly  
 428 focused on a detailed performance analysis of RIWS during each inundating  
 429 event. These results comprise 10 events if the 2002-2006 period is included  
 430 (Table 1). The events examined have very distinct characteristics, i.e. vari-  
 431 able intensities and total rainfall amounts, more or less concentrated in space,  
 432 thus allowing for an in-depth analysis of the RIWS performance.

#### 433 *4.1. Evaluation criteria*

434 The comparison between computed risk levels and reported floodings will  
 435 be based on standard criteria used to evaluate meteorological forecasts, com-  
 436 puted based on the contingency Table 5 and then calculated separately for  
 437 each risk level.

438 From this table, four scores will be calculated as follows (Schaefer, 1990;  
 439 Wilks, 2006):

- Probability of detection (POD) :

$$POD = \frac{H}{H + M} \quad (2)$$

- False Alarm Ratio (FAR):

$$FAR = \frac{Fa}{H + Fa} \quad (3)$$

- Probability of False Detection (POFD) which relates the number of false alarms to the total number of non-flooded points and offers an idea of the legibility of warnings:

$$POFD = \frac{Fa}{Cn + Fa} \quad (4)$$

- The Peirce Skill Score (PSS) has been used as a global score.

$$PSS = POD - POFD \quad (5)$$

440 A perfect forecasting system should feature both a POD and a PSS equal  
 441 to 1 and a FAR and a POFD of 0. Yet, the limitations of the road inun-  
 442 dation observations must be considered when applying these skill scores to  
 443 evaluate the RIWS. First, a comparison between simulated stream discharges  
 444 and reported road disruptions reveals possible inconsistencies along with the  
 445 lack of exhaustiveness in the reports. Road sections are often reported as  
 446 closed for relatively moderate floods and not for more intense ones over the  
 447 considered period, according to the rainfall-runoff simulations. If we were  
 448 to consider that the rainfall-runoff model, despite its lack of accuracy, is at  
 449 least able to correctly rank the discharges between events most of the time,  
 450 this confirms the limitations of available inundation inventories. Such incon-  
 451 sistencies are present in 41% of the reported road disruptions; they have two  
 452 main potential origins:

- 453 • The road closure reports are not likely to be comprehensive.
- 454 • The reasons behind road closures are sometimes unknown, hence some  
 455 road sections present in the inventory may not have been submerged but  
 456 instead affected by other phenomena (e.g. landslide, snow, accidents).

457 Furthermore, the inundation location may have imprecisely logged. Re-  
 458 ported closures can sometimes be attributed to several intersections; in this  
 459 situation, if at least one possible corresponding intersection has been tar-  
 460 getted by a warning, then all forecasts would be considered as correct (either

461  $H$  or  $Cn$ ). Otherwise, if no warning had been issued, only one missed alarm  
462 would be counted. Such a case is nevertheless rare: this simplification has  
463 limited impact on the evaluation criteria.

464 It is also important to note that in the case of events presenting just a few  
465 inundated roads, the POD scores are very sensitive to the number of actual  
466 detections. For instance, if only 10 roads are reported to be flooded, each  
467 detected point increases the POD score by 10%.

#### 468 *4.2. RIWS performance*

469 Examples of POD and FAR obtained by the system are shown in Figure 8.  
470 The false alarm ratios are very high which is clearly correlated with the  
471 difficulties involved in defining the susceptibility to flooding of intersections.  
472 Section 3.3 pointed out that given the limitations of this susceptibility rating,  
473 FAR ratios of about 90% for risk level 1 are to be expected. The FAR ratios  
474 observed here lie in this same range (around 90%). Improvements to the  
475 rainfall-runoff model can therefore only exert a small impact on the FAR  
476 scores.

477 The POD scores depend on the flood event under consideration. A de-  
478 tailed analysis shows that the POD is correlated with the total number of  
479 reported inundations, which serves as an indicator of the flood magnitude.

480 The POD are very high for the extreme floods of 2002 and 2005, in  
481 exceeding or nearing 90%. In such cases, the susceptibility rating plays a less  
482 important role since the return period of the computed as well as observed  
483 discharges at the affected intersections generally exceeds 10 or even 50 years  
484 (Fig. 8). For the less intense events, the discharge values are lower and both  
485 the risk level and corresponding warnings are much more dependent on the

486 susceptibility rating of the intersections, which is the weakest part of the  
487 RIWS, thus explaining lower and more variable POD values.

488 For risk level 2, Figure 8 also confirms the correlation between the number  
489 of reported road closures (and hence the local magnitudes of floods and the  
490 POD) and the September 2007 exception, which affected a particularly sus-  
491 ceptible area according to the susceptibility rating method: i.e. the southern  
492 part of the region at low elevation over an area with expansive floodplains.  
493 Once again, FAR values basically match the forecasts of section 3.3 (on the  
494 order of 80 %).

495 Some POD scores nevertheless appear to be on the low side. On De-  
496 cember 13<sup>th</sup> 2008, the relatively high number of road closures appears to be  
497 inconsistent with the magnitude of floods according to the simulated as well  
498 as to the observed discharges. These closures may have been due to other  
499 factors than inundation, in particular snow accumulation. This phenomenon  
500 has been mentioned in the logs of the road management services with no  
501 further details. On December 29<sup>th</sup> 2008, the limited POD value is related to  
502 the underestimation of the discharges as a result of an incorrect evaluation  
503 of the initial wetness state of the watershed. A discharge assimilation pro-  
504 cedure is under study in order to resolve the initialization problems of this  
505 rainfall-runoff model.

506 On the basis of these results, it is now possible to conclude that the  
507 RIWS, in its present form, is able to correctly assess not only the magnitude  
508 of the floods (with the exception of some particular events) but also the con-  
509 sequences of floods in terms of the number of inundated roads and risk levels.  
510 On the other hand, RIWS fails to accurately identify the actually affected



511 road/river intersections. Figures 9 and 10 illustrate this last point and the  
512 information content in RIWS output. On the whole, the affected areas of  
513 the Gard region have been correctly depicted for these two events. The risk  
514 levels are clearly contrasted between these two floods, thus indicating local-  
515 ized and significant consequences for the September 2007 flood and a larger  
516 area affected during October-November 2008, yet with a lower density of high  
517 risk warnings (basically limited to the most susceptible areas: i.e. the valleys  
518 of the main streams). These forecasts match field observations: localized yet  
519 significant inundations in 2007 and sparsely scattered local problems in 2008.

520 It has also been verified that despite the short forecasting lead time (no  
521 longer than 15 min. on the headwater catchments given that the system  
522 is based on rainfall measurements), the first warnings have for the most  
523 part been delivered well ahead of the first field report. Such a system, if  
524 operationally implemented, could, for all the aforementioned reasons, be of  
525 great utility for the real-time evaluation of situations as well as for organizing  
526 the rescue response and managing the road network. It is currently tested  
527 by the Gard Departmental Road Management Office and the initial feedback  
528 has been positive overall.

## 529 **5. Discussion of RIWS components**

### 530 *5.1. Utility of the susceptibility model*

531 Given the limitations of available road inundation inventories, the sus-  
532 ceptibility assessment is probably the weakest RIWS component. In order to  
533 evaluate its real utility to the system and feasible improvements, two tests  
534 have been conducted:

- 535 • The system was run with discharge thresholds of identical return peri-  
536 ods for all intersections: without introducing any susceptibility ratings.  
537 Risk level 3 has been associated with a 2-year return period, the level 2  
538 with a 10-year return period and level 1 with a 50-year return period.
- 539 • Susceptibility has been defined on the basis of the inundations actually  
540 observed during the 10 test events: This is the pseudo perfect case.  
541 The intersections inundated once have been assigned to the low sus-  
542 ceptibility class, those inundated twice to the moderate class and those  
543 inundated more than twice to the high class. The intersections not re-  
544 ported as inundated have been assigned to the very low susceptibility  
545 class.

546 This last procedure does not claim to establish a valid susceptibility layer,  
547 but rather has been implemented in order to evaluate the system with a  
548 susceptibility assessment close to perfect and moreover to illustrate potential  
549 improvements that could be achieved if reported inundations were to be  
550 assimilated.

551 System performance was compared using the two susceptibility rating  
552 method configurations presented in Section 3.3. The results are shown in  
553 Figure 11. Though far from perfect, the susceptibility rating method clearly  
554 improves system performance, as the improved susceptibility rating method  
555 leads to higher scores. A detailed analysis also indicates that the scores of  
556 the system without susceptibility rating appear to be extremely variable with  
557 a high POD, but also POFD and FAR scores for high intensity flood events  
558 and scores close to zero for less intense events. The susceptibility rating  
559 method introduces stability and nuance into the RIWS response, thereby

560 producing warnings for every significant event. The magnitude and location  
561 of the floods determine both the warning density and the level of risks (see  
562 Fig. 9 and 10) yet have less influence on the detection scores.

563 This "pseudo perfect" configuration furthermore indicates that an im-  
564 provement in susceptibility rating, through data assimilation for instance,  
565 would clearly improve the overall performance, mainly by reducing the pro-  
566 portion of false detections. The room for improvement is indeed significant,  
567 given that the PICH inventory used to calibrate of the susceptibility rat-  
568 ing method is likely to be far from perfect. As an example, Table 6 lists  
569 the number of road sections included in recent event-specific reports of road  
570 disruptions that had not been identified in the PICH inventory: 228 road  
571 sections are applicable, with 13 of them having been closed more than twice.  
572 This finding exposes the probable lack of comprehensiveness in the PICH  
573 inventory.

#### 574 *5.2. Comparison of the rainfall-runoff model configurations*

575 The rainfall-runoff model developed for the Gard region has evolved from  
576 its first configuration with homogeneous CN parameters to a distributed CN  
577 assessment, according to the USDA methodology. The transfer function has  
578 also been improved by implementating the diffusive wave model on the down-  
579 stream reaches of the river network. These changes have led to improving  
580 the Nash criteria computed on the gauged sections (Fig. 5). However the  
581 effect of these improvements on the RIWS performance, while not totally  
582 undetectable, still appears to be very limited as illustrated in Figure 12.

583 This confirms that only orders of magnitudes of the discharges are nec-  
584 essary to deliver relevant alarms in the context of the RIWS. Overall system

585 performance is therefore relatively insensitive, even with significant improve-  
586 ments, to the rainfall-runoff model. One positive conclusion drawn is that  
587 useful forecasts can be derived from output of hydro-meteorological models  
588 affected by significant uncertainties. A more disappointing conclusion how-  
589 ever is that the observed local consequences of flood events in ungauged wa-  
590 tersheds, like road inundations, do not provide useful indirect measurements  
591 of discharges when evaluating rainfall-runoff models.

## 592 **6. Conclusion**

593 A prototype of a road inundation warning system (RIWS), initially tested  
594 on a limited spatial scale, has been extended to an entire French region and  
595 has yielded promising results. The resulting system is able to provide warn-  
596 ings at 2,172 intersections between roads and rivers every 15 minutes. Tests  
597 conducted in batch mode on 10 recent flood events with observed road in-  
598 undations have revealed the system's capacity to forecast the location and  
599 magnitude of floods and their consequences with relatively good accuracy,  
600 yet it remains unable to locate the affected road sections with precision.  
601 The main limitation of this system pertains to poor knowledge on the actu-  
602 all susceptibility of individual road sections to flooding. A data assimilation  
603 method, based on the comparison of field reports and forecasted risk levels, is  
604 currently being tested. Early results are encouraging and in time this method  
605 could lead to system improvements. For the interested readers, a demonstra-  
606 tor ([prediflood.lthe.fr/cartto.php](http://prediflood.lthe.fr/cartto.php)) has been developed to provide the  
607 simulated warnings and field observations for 5 of the tested events.

608 Beyond the specific application to the supervision of a road network, this

609 research has also produced results relative to hydro-meteorological forecasts  
610 and monitoring at ungauged sites. It appears that rainfall-runoff models may  
611 offer valuable information for flood event management over small space and  
612 time scales even on ungauged watersheds. With a limited calibration and  
613 validation effort, rainfall-runoff models could at least provide relatively ac-  
614 curate flood magnitude forecasts that would certainly be sufficient for many  
615 event management decisions as has been illustrated herein. To some extent,  
616 the philosophy behind the approach presented in this paper has similarities  
617 with the philosophy of the EFAS system (Younis et al., 2008; Thielen et al.,  
618 2009; Alfieri et al., 2012) though at different time and space scales and with  
619 a focus on flash floods. Such approaches contrast with the traditional fore-  
620 casting methods, which are focused on gauged locations and are definitely  
621 forging new avenues in the field of hydrological forecasting.

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## 627 **References**

628 Alfieri, L., Thielen, J., Pappenberger, F., 2012. Ensemble hydro-  
629 meteorological simulation for flash flood early detection in southern  
630 switzerland. *Journal of hydrology* 424-425, 143153.

- 631 Borah, D., Prasad, S., Alonso, C., 1980. Kinematic wave routing incorporat-  
632 ing shok fitting. *Water resources research* 3, 529–541.
- 633 Borga, M., Creutin, J.D., Gaume, E., Martina, M., Todini, E., Thielen, J.,  
634 2009. *Flood Risk Management : Research and Practice*. Taylor and Francis  
635 Group. chapter Flash flood risk management : Advances in hydrological  
636 forecasting and warning. pp. 1305–1314.
- 637 Boudevillain, B., Delrieu, G., Galabertier, B., Bonnifait, L., Bouilloud, L.,  
638 Kirstetter, P.E., Mosini, M.L., 2011. The Cévennes-Vivarais Mediter-  
639 ranean Hydrometeorological Observatory database. *Water Resources Re-*  
640 *search* 47, 6.
- 641 Carpenter, T., Sperflage, J., Georgakakos, K., Sweeney, T., Fread, D., 1999.  
642 National threshold runoff estimation utilizing gis in support of operational  
643 flash flood warning systems. *Journal of Hydrology* 224, 21–44.
- 644 Cloke, H., Pappenberger, F., 2009. Ensemble flood forecasting : a review.  
645 *Journal of hydrology* 375, 613–626.
- 646 CNRS-INPG, 1997. *Atlas expérimental des risques de pluies intenses,*  
647 *cévennes-vivarais*. Laboratoire d'étude des Transferts en Hydrologie et En-  
648 *vironnement*, Grenoble, France. 21p.
- 649 Delrieu, G., Kirstetter, P.E., Nicol, J., Neppel, L., 2004. L'événement plu-  
650 vieux des 8-9 septembre 2002 dans le Gard : Estimation des précipitations  
651 par radars et pluviomètres. *La Houille Blanche* 6, 93–98.
- 652 Delrieu, G., Nicol, J., Yates, E., Kirstetter, P.E., Creutin, J.D., Anquetin,  
653 S., Obled, C., Saulnier, G.M., Ducrocq, V., Gaume, E., Payrastre, O.,

- 654 Andrieu, H., Ayrat, P.A., Bouvier, C., Neppel, L., Livet, M., Lang, M.,  
655 du Chtelet, J.P., Walpersdorf, A., Wobrock, W., 2005. The catastrophic  
656 flash-flood event of 8-9 september 2002 in the gard region, france: A first  
657 case study for the cévennes-vivarais mediterranean hydrometeorological  
658 observatory. *Journal of Hydrometeorology* 6, 34–52.
- 659 Desbordes, M., Durepaire, P., Gilly, J., Masson, J., Maurin, Y., 1989. 3  
660 octobre 1988, inondations sur nmes et sa région, manifestation, causes et  
661 conséquences. ed. C. Lacour.
- 662 Drobot, S., Benight, C., Grunfest, E., 2007. Risk factors for driving into  
663 flooded roads. *Environmental Hazards* 7, 227–234.
- 664 Edijatno, Michel, C., 1989. Un modèle pluie-débit trois paramètres. *La*  
665 *Houille Blanche* 2, 113–121.
- 666 Gaume, E., Bain, V., Bernardara, P., Newinger, O., Barbuc, M., Bateman,  
667 A., Blaškovičova, L., Blöschl, G., Borga, M., Dumitrescu, A., Daliakopou-  
668 los, I., Garcia, J., Irimescu, A., Kohnova, S., Koutroulis, A., Marchi, L.,  
669 Matreata, S., Medina, V., Preciso, E., Sempere-Torres, D., Stancalie, G.,  
670 Szolgay, J., Tsanis, I., Velascom, D., Viglione, A., 2009. A compilation of  
671 data on european flash floods. *Journal of Hydrology* 367, 70–78.
- 672 Gaume, E., Livet, M., Desbordes, M., Villeneuve, J.P., 2004. Hydrological  
673 analysis of the river aude, france, flash flood on 12 and 13 november 1999.  
674 *Journal of Hydrology* 286, 135–154.
- 675 Georgakakos, K.P., 2006. Analytical results for operationnal flash flood guid-  
676 ance. *Journal of Hydrology* 317, 81–103.

- 677 Hayami, S., 1951. On the propagation of flood waves. Technical Report 1.  
678 Disaster prevention research institute. Kyoto university, Japan.
- 679 Huang, M., Gallichand, J., Dong, C., Wang, Z., Shao, M., 2007. Use of soil  
680 moisture data and curve number method for estimating runoff in the loess  
681 plateau of china. *Hydr. Process.* 21, 1471–1481.
- 682 Javelle, P., Fouchier, C., Arnaud, P., Lavabre, J., 2010. Flash flood warning  
683 at ungauged locations using radar rainfall and antecedent soil moisture  
684 estimations. *Journal of Hydrology* 394, 267–274.
- 685 Lavabre, J., Fouchier, C., Folton, N., Gregoris, Y., 2003. SHYREG: une  
686 méthode pour l'estimation régionale des débits de crues. Application aux  
687 régions méditerranéennes françaises. *Ingénierie-EAT numéro spécial Risque*  
688 *naturel et aménagement du territoire*, 97–111.
- 689 Lebel, T., Bastin, G., Obled, C., Creutin, J., 1987. On the accuracy of  
690 areal rainfall estimation : A case study. *Water Resources Research* 23,  
691 2123–2134.
- 692 Maréchal, J., Ladouche, B., Drfliger, N., 2007. Karst flash flooding in a  
693 mediterranean karst, the example of fontaine de nmes. *Engineering Geol-*  
694 *ogy* 99, 138–146.
- 695 Martina, M., Todini, E., Libralon, A., 2006. A bayesian decision approach  
696 to rainfall thresholds based flood warning. *Hydrol. Earth Syst. Sci.* 10,  
697 413–426.
- 698 McEnery, J., Ingram, J., Duan, Q., Adams, T., Anderson, L., 2005. NOAAs



- 699 advanced hydrologic prediction service; building pathways for better sci-  
700 ence in water forecasting. *American Meteorological Society BAMS*, 375–  
701 385.
- 702 Moussa, R., 1996. Analytical hayami solution for the diffusive wave flood  
703 routing problem with lateral inflow. *Hydrological processes* 10, 1209–1227.
- 704 Naulin, J., Gaume, E., Payrastre, O., 2011. Distributed flood forecasting  
705 for the management of the road network in the gard region (france), in:  
706 *Proceedings of a symposium held in Exeter, UK, April 2011* (IAHS Publ,  
707 2011).
- 708 Perrin, C., 2002. Vers une amélioration d'un modèle global pluie-débit au  
709 travers d'une approche globale comparative. *La Houille Blanche* 6, 84–91.
- 710 Perrin, C., Michel, C., Andréassian, V., 2003. Improvement of a parsimonious  
711 model for streamflow simulation. *Journal of Hydrology* 279, 275–289.
- 712 Reed, S., Schaake, J., Zhang, Z., 2007. A distributed hydrologic model and  
713 threshold frequency-based method for flash flood forecasting at ungauged  
714 locations. *Journal of Hydrology* 337, 402–420.
- 715 Ruin, I., Creutin, J.D., Anquetin, S., Lutoff, C., 2008. Human exposure to  
716 flash floods - relation between flood parameters and human vulnerability  
717 during a storm of september 2002 in southern france. *Journal of Hydrology*  
718 361, 199–213.
- 719 Ruin, I., Gaillard, J.C., Lutoff, C., 2007. How to get there? assessing mo-

- 720 tourist's flash flood risk perception on daily itineraries. *Environmental Haz-*  
721 *ards* 7, 235–244.
- 722 Schaefer, J.T., 1990. The critical success index as an indicator of warning  
723 skill. *Weather and forecasting* 5, 570–575.
- 724 Soulis, K.X., Valiantzas, J.D., Dercas, N., Londra, P.A., 2009. Investigation  
725 of the direct runoff generation mechanism for the analysis of the scs-cn  
726 method applicability to a partial area experimental watershed. *Hydrology*  
727 *and Earth System Sciences* 13, 605–615.
- 728 Tanguy, J., Carriere, J., Trionnaire, Y., Schoen, R., 2005. Reorganisation  
729 of flood forecasting in france - réorganisation de l'annonce des crues en  
730 france. *La Houille Blanche* 2, 44–48.
- 731 Thielen, J., Bartholmes, J., Ramos, M.H., de Roo, A., 2009. The European  
732 Flood Alert System - Part 1: Concept and development. *Hydrol. Earth*  
733 *Syst. Sci.* 13, 125–140.
- 734 USDA, 1986. Urban hydrology for small watersheds. Technical Report 55.  
735 United States Department of Agriculture, Natural Resources Conservation  
736 Service.
- 737 Versini, P., Gaume, E., Andrieu, H., 2010a. Application of a distributed  
738 hydrological model to the design of a road inundation warning system for  
739 flash flood prone areas. *Nat. Hazards Earth Syst. Sci.* 10, 793–803.
- 740 Versini, P., Gaume, E., Andrieu, H., 2010b. Assessment of the vulnerability  
741 of roads to flooding based on geographical information - test in a flash

- 742 flood prone area (the gard region, france). Nat. Hazards Earth Syst. Sci.  
743 10, 793–803.
- 744 Wilks, D., 2006. Statistical Methods in the Atmospheric Sciences, Second  
745 Edition. International Geophysics series.
- 746 Younis, J., Anquetin, S., Thielen, J., 2008. The benefit of high-resolution  
747 operational weather forecasts for flash flood warning. Hydrol. Earth Syst.  
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800		performance: <i>H</i> (Hits), <i>M</i> (Misses), <i>Fa</i> (False Alarms), and	
801		<i>Cn</i> (Correct negatives). . . . .	44
802	6	Proportion of PICH points among intersections identified in	
803		the recent event-specific reports of road disruptions (conducted	
804		since 2002), in areas where the PICH inventory is available. . .	48

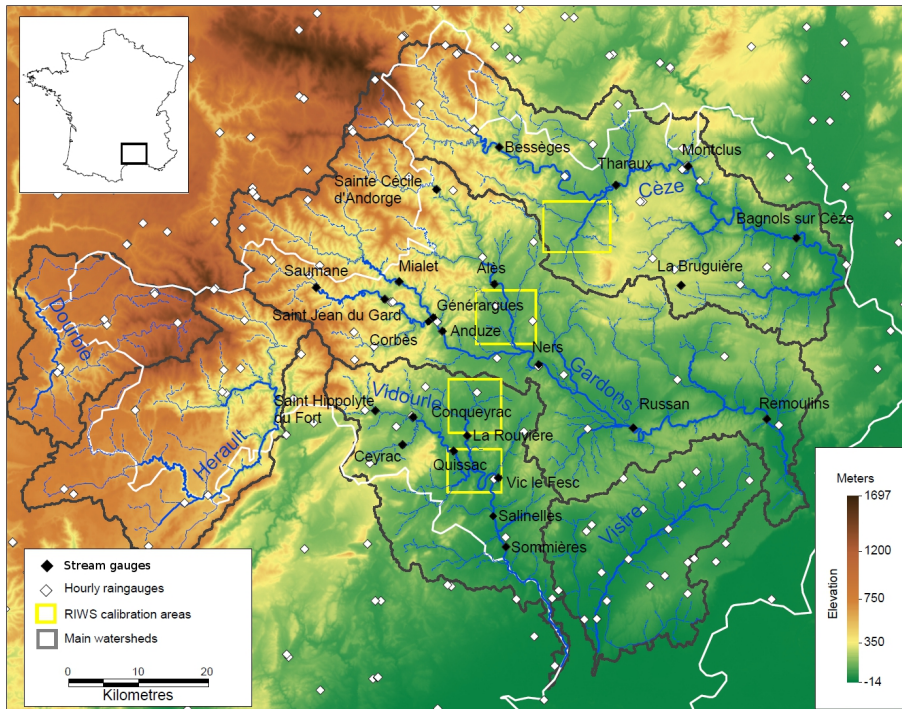


Figure 1: Gard department (shown in white), main streams and watersheds (black), initial test areas of the RIWS (white windows).

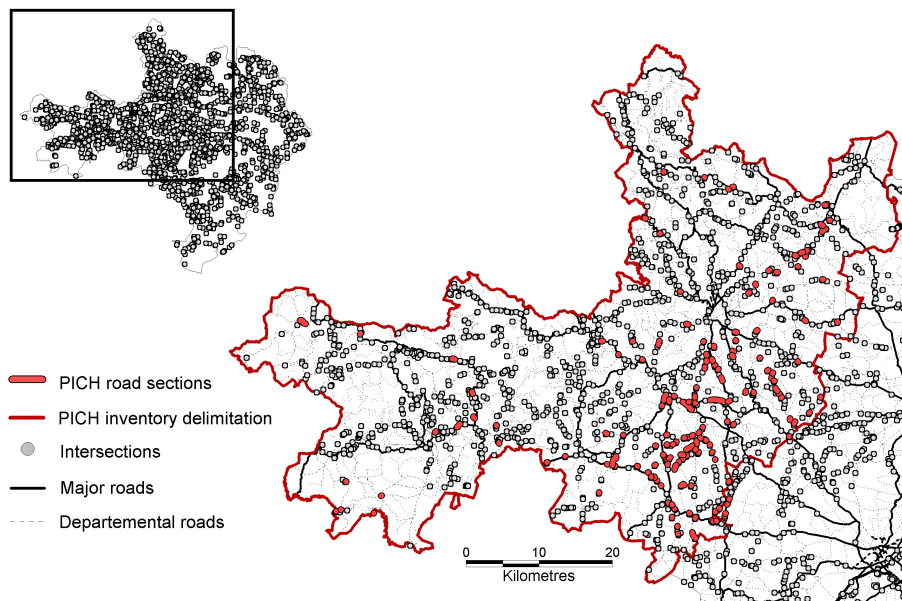


Figure 2: Presentation of the PICH inventory and identification of intersections between road and river networks in the Gard region.



Table 1: The set of test events for the RIWS.

Dates of events	Event dura- tion (days)	max rain- fall (mm)	% area > 200 mm	Nb. flooded roads
08-10/09/2002	3	679	74	367
01-04/12/2003	4	380	61	112
02-05/11/2004	4	139	0	11
04-12/09/2005	6	403	76	198
29-30/09/2007	2	204	0	26
19-23/11/2007	5	293	13	14
16-19/09/2007	4	62	0	0
03-11/10/2007	8	100	0	0
06-12/12/2007	7	70	0	0
01-07/09/2008	7	100	0	0
10-15/09/2008	6	60	0	0
07-10/10/2008	4	110	0	0
19-22/10/2008	4	497	15	18
01-02/11/2008	2	514	17	19
10-13/11/2008	4	50	0	0
13-15/12/2008	3	114	0	32
29-31/12/2008	3	218	0.5	54

Table 2: Contingency table for the determination of inundation risk levels: 0 (no risk), 1, 2 and 3.

Susceptibility	Discharge return period (years)				
	0.5	1	10	50	
High	0	2	3	3	3
Medium	0	1	2	3	3
Low	0	0	1	2	3
Very low	0	0	0	0	1

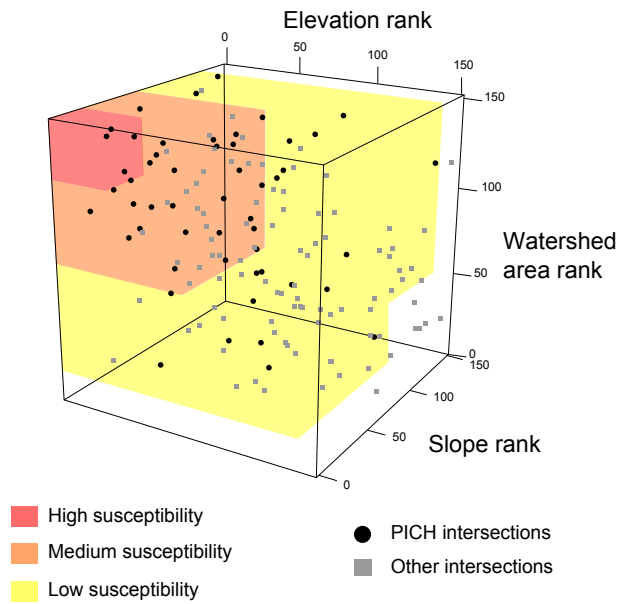


Figure 3: Illustration of the susceptibility sorting method applied by Versini on the 150 intersections of the initial testing areas.

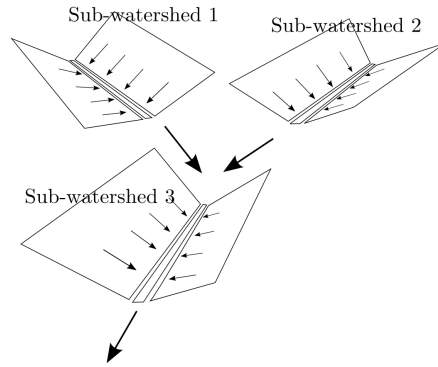


Figure 4: Schematic representation of a watershed in the CINECAR model.

Table 3: Average widths of river reaches according of their Strahler order I and return period T of the simulated stream discharge.

Return period of the discharge Q	Width of the stream (m)				
	I=1	I=2	I=3	I=4	I=5
$Q < Q_2$	4	16	36	64	100
$Q_2 < Q < Q_{10}$	8	32	72	128	200
$Q > Q_{10}$	12	48	108	192	300

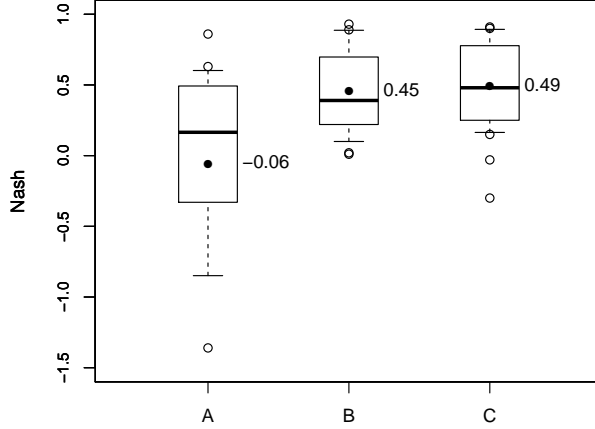


Figure 5: Distribution of the "event-specific" Nash criteria obtained at the 23 stream gauges for the validation events: A) initial version of the CINECAR model with homogeneous CN, B) CN estimated according to the USDA method, and C) introduction of the diffusive wave.

Table 4: Efficiency of the various sorting methods as applied over the entire PICH inventory territory: A) reference results obtained with the initial method on the area considered by Versini, B) initial method applied to the entire PICH territory, and C) application of the method with a sub-area distinction in the PICH territory.

	Susceptibility method	Susceptibility class			
		High	Average	Low	Very low
Distribution of intersections between the susceptibility classes	A	0%	17%	58%	25%
	B	4.5%	9.9%	67.4%	18.3%
	C	6.2%	15.6%	53.3%	24.2%
Proportion of PICH points in each susceptibility class	A	100%	60%	37%	0%
	B	37.7%	25.4%	6.2%	0%
	C	40.1%	23.5%	4%	0%

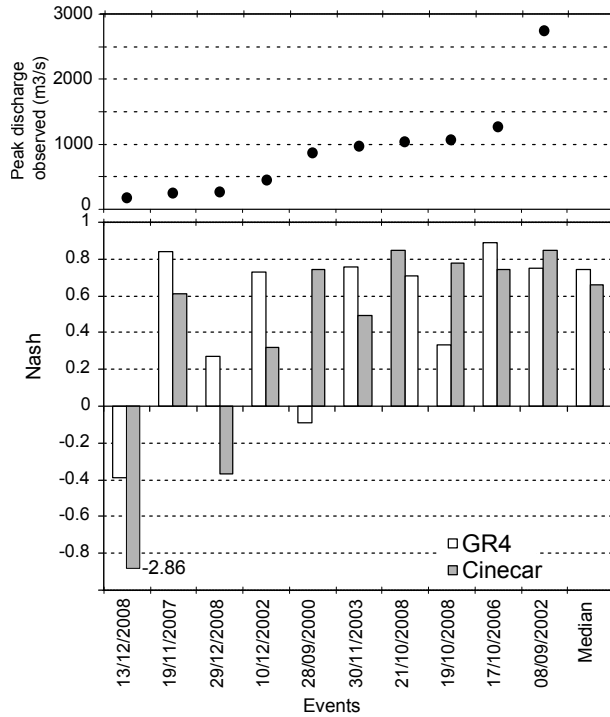


Figure 6: Comparison of Cinecar and GR4 model performance at the gauged Anduze station. The magnitude of the peak discharge is indicated in the top figure.

Table 5: Contingency table for the evaluation of the warning system performance:  $H$  (Hits),  $M$  (Misses),  $Fa$  (False Alarms), and  $Cn$  (Correct negatives).

		Reported flooding	
		Yes	No
Risk level reached	Yes	$H$	$Fa$
	No	$M$	$Cn$

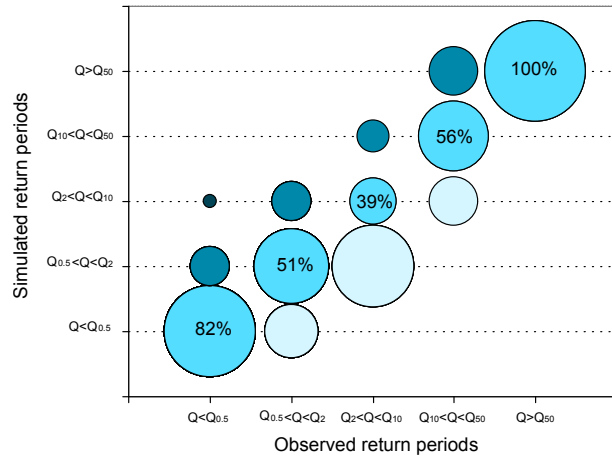


Figure 7: Comparison between the return period ranges of the observed and simulated peak discharges.  $Q_X$  stands for the discharge quantile of return period  $X$ .

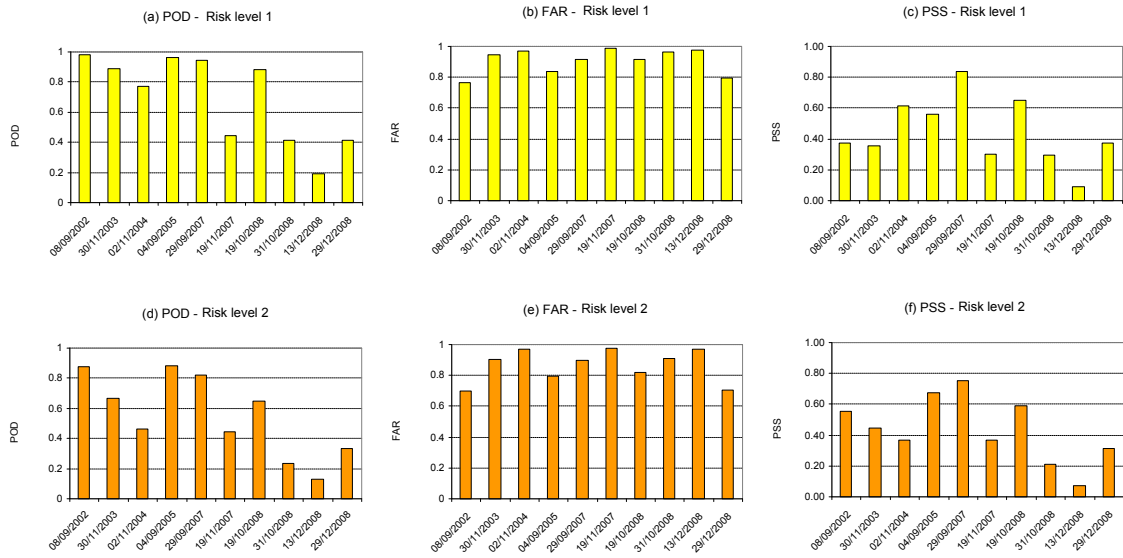


Figure 8: POD, FAR and PSS values obtained for risk levels 1 and 2

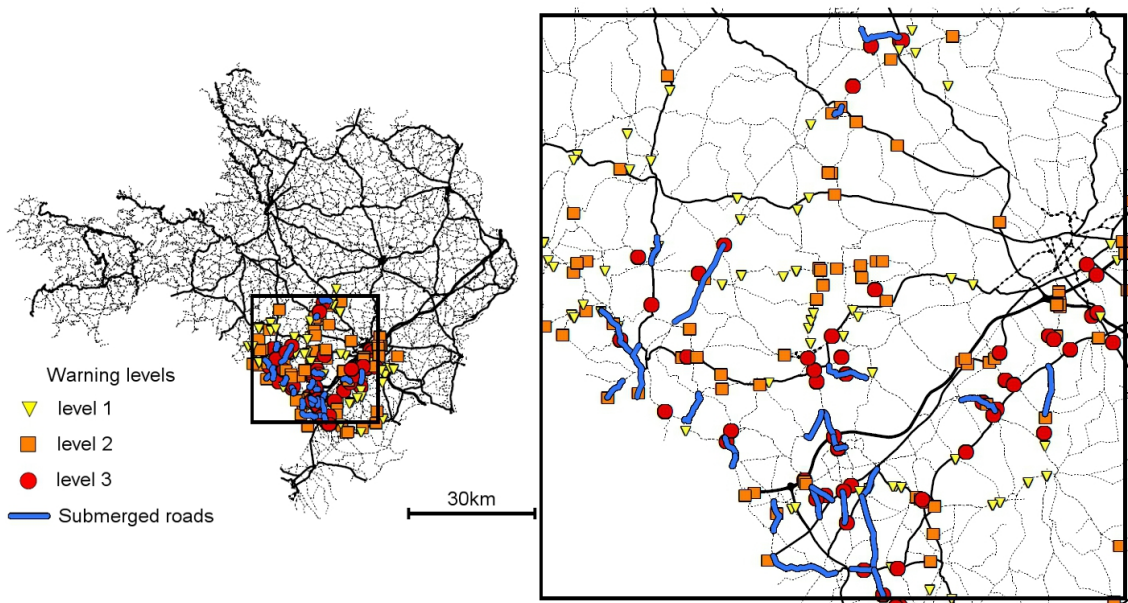


Figure 9: September 2007 flood. Map of the maximum forecasted risk levels and reported inundated roads.

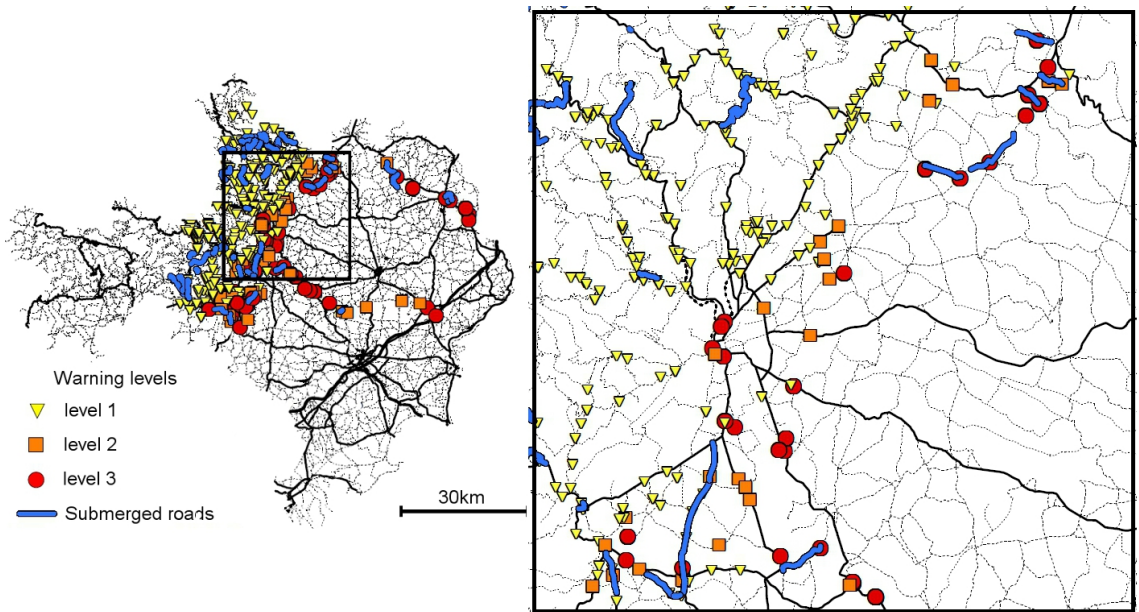


Figure 10: October 2008 flood. Map of the maximum forecasted risk levels and reported inundated roads.

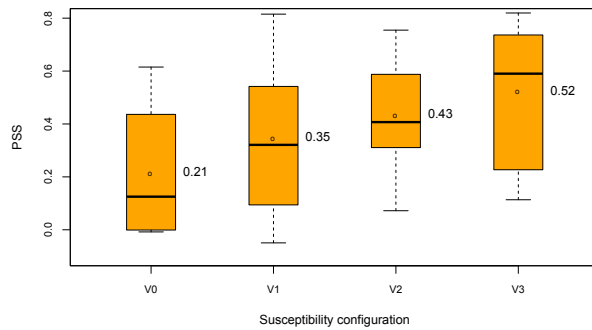


Figure 11: Box plot of PSS obtained for the risk level 2 with various susceptibility model configurations: V0) without susceptibility rating, homogeneous thresholds, V1) initial susceptibility rating method, V2) modified susceptibility rating method, V3) pseudo-perfect case, susceptibility determined based on the 10 tested events. The box plots synthesize scores obtained for the 10 tested events. The average value is indicated by the point.



Table 6: Proportion of PICH points among intersections identified in the recent event-specific reports of road disruptions (conducted since 2002), in areas where the PICH inventory is available.

Number of inundations	Non PICH	PICH
1	189	32
2	26	25
3	6	13
4	6	5
5	1	4
6	0	1
7	0	1
Total	228	81

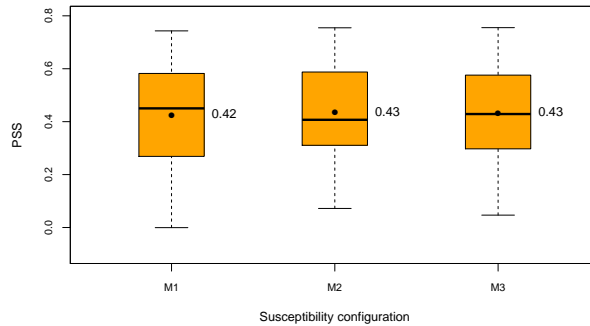


Figure 12: Comparison of the PSS distribution obtained with various rainfall-runoff model configurations for risk level 2: A) initial version of the CINECAR model with homogeneous CN, B) CN estimated according to the USDA method, and C) introduction of the diffusive wave.