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Niobium-based superconducting nano-devices fabrication using all-metal suspended masks

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Abstract. We report a novel method for the fabrication of superconducting nano-devices based on niobium. The well-known difficulties of lithographic patterning of high-quality niobium are overcome by replacing the usual organic resist mask by a metallic one. The quality of the fabrication procedure is demonstrated by the realization and characterization of long and narrow superconducting lines and niobium-gold-niobium proximity SQUIDs.

1. Introduction

Superconductivity is an essential ingredient in quantum nano-electronics. Its macroscopic phase coherence allows to produce easily large objects obeying quantum mechanics [1, 2]. Aluminum is presently the emblematic material in this field. Its popularity is mainly due to the ease of its lithographic patterning and the high quality of its native oxide. The critical temperature $T_c = 1.17$ K of bulk aluminum is however rather low, calling for the use of dilution refrigerators and elaborate electronic filtering as temperatures $T \ll T_c$ are usually needed. Moreover, the relevant energy scale of superconductivity, namely the superconducting gap Δ , is usually proportional to T_c . A low critical temperature T_c is therefore synonymous of a low critical current in short Josephson junctions or superconducting quantum interference devices (SQUIDs) [3].

Higher T_c elemental superconducting metals such as vanadium and lead are occasionally used [4], but they suffer from rapid aging under ambient air conditions. Niobium is the highest- T_c simple element (9.2 K) and is also rather immune to aging. Its main drawback is the strong sensitivity of its thin film superconducting properties to contamination. As niobium is a refractory metal, its evaporative deposition implies extremely high target temperatures. In the case of lift-off processes, this leads to significant heating and outgassing of the organic resist mask, provoking a strong reduction and scatter of the effective critical temperature T_c [5, 6]. Nb nanostructures with a high T_c can be fabricated within a lift-off process using a deposition set-up in which the Nb target is far away from the sample [7]; this method is however difficult to transpose to most setups.

Several techniques have been used to circumvent this severe limitation to niobium applications. Sputtering can provide niobium films of high quality without the use of a high temperature target. Such films can be subsequently patterned by dry reactive ion etching. This however sets constraints on possible materials combinations in hybrid structures [8] and is incompatible with connecting niobium to fragile material such as graphene, carbon nanotubes or thin sheets of topological insulators. Sputtering through a mask (resist or mechanical) is also possible [9, 10, 11, 12] but, due to the lack of directionality of the deposition, leads to poorly defined edges. This can cause a gradual loss of the superconducting properties over a broad transition region.

Suspended masks made of Si, Ge or SiN, supported by thermostable resists like poly-ethersulfones have further been developed [13, 14]. Such processes provided Nb sub-micron structures with a critical temperature up to 8 K, including hybrid Josephson junctions with a high Nb-Cu interface transparency [15]. The use of these particular resists is nevertheless cumbersome; for instance, the ambient hygrometry has to be controlled during resist spinning. Non-organic evaporation stencil masks based on a suspended bilayer of Si_3N_4 and SiO_2 have been developed in the past [16]; lift-off and integration of arbitrary non-superconductors (graphene etc.) are yet again impossible. Finally, the possibility of using metallic bilayer masks has been demonstrated in the past [17]. This method was in particular used to pattern large niobium devices with

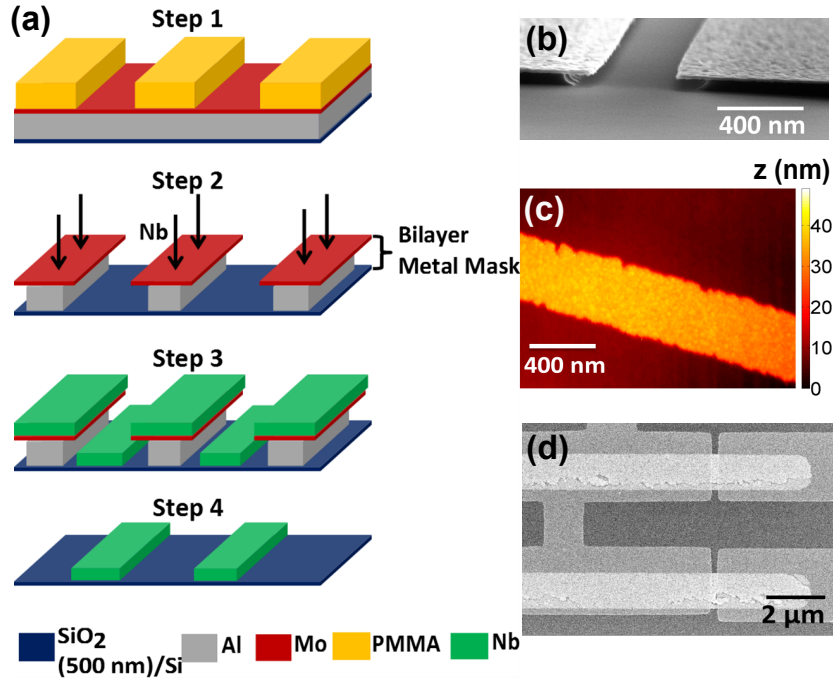


Figure 1. (a) Process for a Nb device fabrication. From the top: starting with an Al/Mo (200 nm/40 nm) multilayer, a thin layer of photoresist PMMA (350 nm) is spin coated and patterned using e-beam lithography. In step 2, the Mo layer is patterned using reactive ion etching. This is followed by the wet etching of Al with a basic solution (see text), leaving the Mo top layer free-standing over about 200 nm from the openings. The Nb layer is then evaporated in step 3. In the last step, the remaining Al is dissolved, leaving the sole Nb devices on the substrate. (b) Scanning electron micrograph of the Al/Mo bilayer mask for the wires prior to Nb evaporation. (c) Atomic force micrograph of a small portion of a 400 nm wide Nb line. (d) Scanning electron micrograph of a niobium-gold-niobium proximity SQUID (device C) with 210 nm spacing between the Nb contacts.

dimensions in the upper 100 μm range [18].

We report here a new and simple method for lithographic patterning of extremely narrow and well-defined Nb nanostructures with a high critical temperature. Our approach relies on replacing the traditional organic resist mask by a fully metallic one. We take advantage of the high wet etch rates of aluminum, with respect to most other metals, by high pH chemicals used as organic resist developers. We demonstrate the fabrication and good operation of SQUIDs based on hybrid Josephson junctions.

2. Fabrication process and submicron lines characterization

We start by depositing an Al/Mo (200 nm/40 nm) bilayer on a Si/SiO₂ substrate. Electron-beam lithography is performed on an organic resist (PMMA) spun on top of the metal bilayer, see Fig. 1a. In the developed regions, the Mo layer is removed by a reactive ion etch with a 20 W SF₆ plasma for 2 minutes. The resist is afterwards

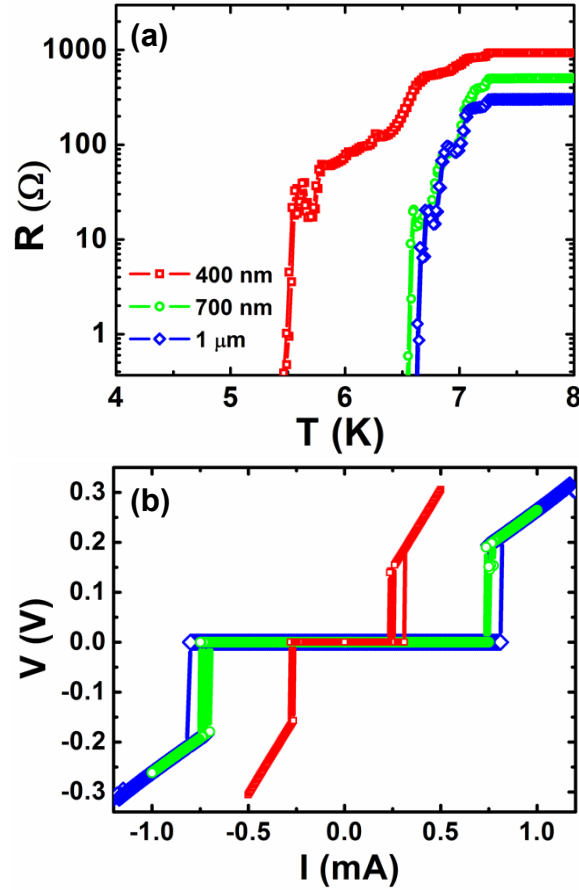


Figure 2. (a) Resistance versus temperature of three niobium lines of different widths ($I_{bias} = 5 \mu\text{A}$). (b) Voltage versus current characteristics of the same samples measured at 4.2 K. These display hysteresis (as high as 32% for the 400 nm line) as well as random fluctuations of the measured resistance at $I \approx I_c$.

removed by 10 minutes of 50 W O_2 plasma etch. In the next step, a wet etch in a basic solution ($\text{pH} \approx 13$) of MF-26A [19] etches Al isotropically through the openings in the Mo layer, creating undercuts of about 200 nm after a 90 s time. This leaves a locally suspended Mo mask on top of the over-etched aluminum supporting layer, see Fig. 1b,c. This sequence of steps ensures vanishing organic contamination of deposited materials.

A niobium thin film is then e-gun evaporated in an ultra-high vacuum chamber. The metallic Al/Mo mask is finally removed by a wet etch in MF-319 [20] for about 45 minutes. Including regularly spaced extra holes in the initial lithographic pattern allows the etchant to start lifting the metal mask from a larger number of starting points. The related minimization of this wet-etch time is important because beyond 2 hours we observe MF-319 starting to etch the Si/SiO₂ substrate as well as the metallic layers (Nb, Au,...) present in the device.

As a first test, we have prepared Nb narrow lines using the technique described above. In these samples, a 10 nm Ti layer was deposited in situ prior to Nb, as to

improve adhesion and mimic the frequently used approach to contact a superconductor to novel low-dimensional materials [21, 22, 23]. The presence of Ti however contributes to reducing the T_c of the wires. Atomic force microscopy (AFM) inspection of the Nb-wires obtained (Fig. 1c) shows that the edges are extremely sharp and well-defined. The 3σ (standard deviations) line edge roughness of the wires is 10 nm, on the order of the grain size of in both the Nb film and the Mo mask. Line edge smearing is inferior to the lateral resolution of a standard AFM tip. The roughness of the Nb surface is 1.1 nm.

We have performed transport measurements on these samples in a variable temperature (2-300 K) cryostat, using a d.c. 4-probe configuration. Figure 2a shows the temperature dependence of the low temperature resistance R of three devices, based on lines of length 30 μm , thickness 30 nm and widths 400, 700 and 1000 nm respectively. The devices display stepwise decrease of resistance below $T = 7.3$ K. Since the entire on-chip structure is made of niobium, we attribute these steps to transitions to the superconducting state of wire elements of decreasing width in series. The small resistance steps in the low resistance region can also be related to pinning and depinning of residual vortices. The rapid drop to $R < 1\Omega$ corresponds to the critical temperature T_c of the narrowest part of each circuit. While the critical temperature T_c of the 400 nm wide line is considerably reduced, it is hardly affected for widths above 700 nm. The $I(V)$ characteristics at 4.2 K show a marked resistive transition and some hysteresis. The latter is due to Joule heating in the Nb wire once in the normal state, which elevates the local electronic temperature compared to the bath temperature. As a result the critical current is reduced, which creates an hysteresis in the current-voltage characteristics. Thermal hysteresis is enhanced in narrower structures.

3. Fabrication and study of SQUIDS

We have further fabricated Nb-Au-Nb proximity SQUIDS (Figure 1d) using a two-step process. We first patterned two long parallel lines of gold, 1 μm wide and 30 nm thick, by conventional e-beam lithographic techniques. The metallic mask method described above is then used to pattern Nb proximity junctions on top of these. We deposited a 50 nm thick Nb layer without sticking layer. Over the proximity junction, the metal mask is free-hanging, as to form junctions as short as 200 nm. The device parameters of the three tested devices, labelled A, B and C, are summarized in Table 1.

In a hybrid Josephson junction made of a normal metal bridging two superconducting electrodes, as a Au wire between two Nb electrodes here, the length scale for inducing superconductivity in the normal metal is set by the normal metal thermal length $L_T = \sqrt{\hbar D / 2\pi k_B T}$. Here, D is the electronic diffusion coefficient in the normal metal. L_T is estimated to be about 180 nm at 135 mK while the junction lengths L are in the range 200 – 400 nm.

Transport properties of the Nb-Au-Nb proximity SQUIDS were measured using a four-probe d.c. current bias scheme inside a dilution refrigerator. Each electrical lead to

the samples was thoroughly filtered by individual 2 m long lossy coaxial lines thermalized at the cryostat base temperature. Fig. 3a shows the $V(I)$ characteristics of SQUID C at zero magnetic field and 135 mK. A critical current I_c is observed in the two shorter Nb-Au-Nb SQUIDs B and C, while none is observed in A.

SQUID	$L(\text{nm})$	$W(\mu\text{m})$	$R_N(\Omega)$	$\rho_N(\mu\Omega.\text{cm})$	$D(\text{cm}^2/\text{s})$	$L_T(\text{nm})$	$I_c(\mu\text{A})$	$\epsilon_c(\mu\text{eV})$
A	430	0.98	1.99	13.6	29	160	-	10.2
B	340	1.00	1.04	9.20	42	190	2.7	24.1
C	210	0.98	0.89	12.4	31	170	11.8	46.7

Table 1. Device parameters of the Nb-Au-Nb SQUIDs. L is the geometrical length of the normal weak link (uncovered gold line). R_N is the normal state resistance of the weak link only, measured at 4.2 K, ρ_N the corresponding resistivity and D the diffusion coefficient. L_T is the calculated thermal length at $T = 135$ mK. I_c is the maximum critical current measured at 135 mK. $\epsilon_c = \hbar D/L^2$ is the Thouless energy assuming the weak link length is L .

As proximity Josephson junctions have a vanishing capacitance, they are overdamped. The $V(I)$ characteristic is thus expected to follow $V = R_n \sqrt{I^2 - I_c^2}$ for $|I| > I_c$ [3]. The characteristics fit rather well this prediction, see Fig. 3a. A finite hysteresis is nevertheless observed for the highest I_c SQUID (device C) at the lowest temperatures. While sweeping the current down from large values $|I| > I_c$, the SQUID C turns non-resistive at a retrapping current $I_r \leq I_c$. This hysteresis is known to be of thermal origin [24]: the Joule heat dissipated in the normal metal elevates the electronic temperature with respect to the phonon temperature as the electron-phonon coupling is the bottleneck for the electron thermalization to the bath. Retrapping happens when the bias current becomes of the order of the critical current at the current electronic temperature.

Our samples are in the long junction limit defined as a normal metal length larger than the superconductor coherence length: $L \gg \xi_s \approx 30$ nm. In this case, the relevant energy scale for the superconducting proximity effect is the Thouless energy $\epsilon_c = \hbar D/L^2$, which is much smaller than the energy gap Δ . The evolution of critical current with temperature in a normal metal weak link at arbitrary temperatures can be understood by solving the Usadel equations. At low temperatures and in the long junction limit ($\Delta/\epsilon_c \rightarrow \infty$), the numerical solution to the Usadel equation can be approximated by [15]

$$\frac{eR_n I_c}{\epsilon_c} = \eta a \left[1 - b \exp\left(-\frac{a}{3.2} \frac{\epsilon_c}{k_B T}\right) \right]. \quad (1)$$

where $a = 10.82$, $b = 1.30$ and $\eta = 1$ for perfectly transparent S-N interfaces. From the fit to the experimental data of SQUID C, shown in Figure 3b, values of $\epsilon_c = 36.7$ μeV and $\eta \approx 0.017$ are found. The estimate of ϵ_c agrees well with the value found from geometrical arguments, see Table 1. The minor discrepancy can be understood as an effective junction length $\tilde{L} = \sqrt{\hbar D/\epsilon_c} = 236$ nm slightly longer than the geometrical

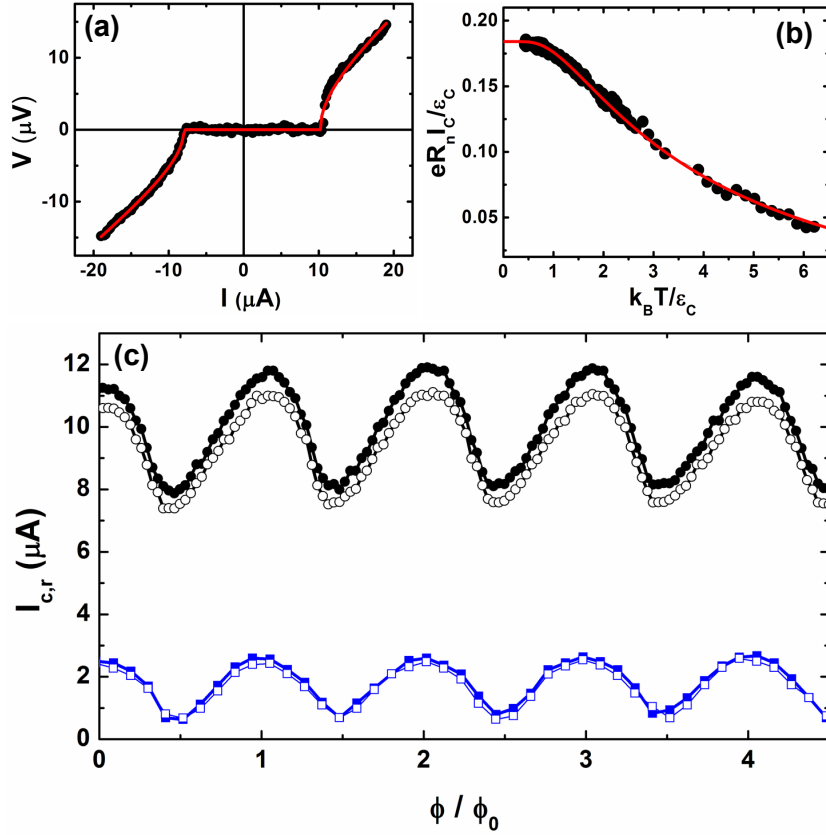


Figure 3. (a) $I(V)$ characteristic of device C (circles) at $T = 135$ mK and $B = 0$ T. The line is a fit using the over-damped junction theoretical I - V relation, see text. (b) Same device critical current versus temperature. Quantities are normalized to the adjusted Thouless energy $\epsilon_c = 36.7$ μeV . The line is a fit by Eq. (1). (c) Critical current (full symbols) and retrapping current (hollow symbols) oscillations versus applied magnetic field flux in device B (squares, $T = 125$ mK) and device C (bullets, $T = 135$ mK).

value [15]. The reduced value of η reflects a lower than ideal I_c , which is attributed to an imperfect transmission at the Nb-Au interface. Argon plasma of the Au structures prior to Nb deposition should lead to improved contact transparencies.

Finally, we have measured SQUID B and C critical current variation with the magnetic field applied perpendicular to the loop. Figure 3c shows data as a function of the magnetic flux $\phi = B.S$, where $S = 37.6$ μm^2 for SQUID B and 19.2 μm^2 for SQUID C is the geometric loop area. The critical current follows the expected ϕ_0 periodicity, where ϕ_0 is the magnetic flux quantum. At a bath temperature $T = 135$ mK, the modulation depth of I_c reaches 80 % in sample B. The retrapping current follows the same behavior. The extremal values of I_c upon flux modulation reflect the sum and the difference respectively of the critical currents of each of the two Josephson junctions in parallel. The obtained flux sensitivity is about 2 $\mu\text{V}/\phi_0$. This performance is within the expected range for hybrid SQUIDs that are characterized by a rather low normal state impedance.

4. Conclusion

We have devised a new method for the nano-fabrication of superconducting Nb structures using an all-metal mask. The method is easy to implement and uses only standard clean room chemicals and methods. It allows producing superconducting nano-devices with a high critical temperature and dimensions down to the 100 nm-scale. Its application to the realization of sensitive SQUIDS with little hysteresis is demonstrated. Applications of this technique will allow probing Josephson physics in exciting novel material systems such as single crystal nanowires [25], ferromagnetic nanowires [26], semiconducting nanowires [27] and graphene [21]. This method can also be used for the fabrication of tunnel junction-based devices like single-electron transistors.

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