

## Ice volume and subglacial topography for western Canadian glaciers from mass balance fields, thinning rates, and a bed stress model

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## Ice volume and subglacial topography for

- western Canadian glaciers from mass balance
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#### ABSTRACT

A method is described to estimate the thickness of glacier ice using information derived from 12 the measured ice extent, surface topography, surface mass balance, and rate of thinning or 13 thickening of the ice column. Shear stress beneath an ice column is assumed to be simply 14 related to ice thickness and surface slope, as for an inclined slab, but this calculation is 15 cast as a linear optimization problem so that a smoothness regularization can be applied. 16 Assignment of bed stress is based on the flow law for ice and a mass balance calculation but 17 must be preceded by delineation of the ice flow drainage basin. Validation of the method 18 is accomplished by comparing thickness estimates to the known thickness generated by a 19 numerical ice dynamics model. Once validated, the method is used to estimate the subglacial 20 topography for all glaciers in western Canada that lie south of 60°N. Adding the present ice volume of each glacier gives the estimated total volume as 2320 km<sup>3</sup>, equivalent to 5.8 mm of sea-level rise. Taking the glaciated area as 26 590 km<sup>2</sup> gives the average glacier thickness 23 as 87.2 m. A detailed error analysis indicates that systematic errors are likely to increase the estimated sea-level rise and when random errors are included the combined result is 25  $6.3 \pm 0.6 \,\mathrm{mm}$  or, expressed as ice volume,  $2530 \pm 220 \,\mathrm{km}^3$ . 26

## 1. Introduction

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The projected shrinkage of Earth's glaciers and ice caps will raise sea level (e.g., Radić and Hock 2011) and affect the water cycle over large areas of Asia, Europe, and the Americas (e.g., Kaser et al. 2010). Improved knowledge of the rate and magnitude of these changes, on a region-by-region basis, is essential and ice flow modeling provides one method to quantify these changes and make projections. Before such models can be used it is necessary to obtain a digital elevation model (DEM) of the underlying subglacial topography. For Earth's ~200 000 glaciers this is problematic because few have been geophysically mapped and at present no satellite remote sensing instrument can image subglacial topography.

Recent work on ice thickness estimation includes methods that are predominantly geometrical, such as that of Clarke et al. (2009) which is based on artificial neural networks, and those that incorporate assumptions from glacier physics (e.g., Farinotti 2010; Farinotti et al. 2009a; Huss and Farinotti 2012; Linsbauer et al. 2009, 2012; Li et al. 2011; Marshall et al. 2011; Morlighem et al. 2011; Paul and Linsbauer 2011). The attraction of the former approach is its parsimony, but it is cumbersome to implement and can lead to subglacial topography that diverges from the true topography — a concern when the estimated bed topography is to be used as a boundary condition for ice dynamics modeling. For this reason physics-rooted approaches are favored.

The aims of the present contribution are to develop a physically-based method for ice 45 thickness estimation, to validate the method by applying it to artificial datasets generated by 46 a numerical ice dynamics model, and to use the method to estimate the subglacial topography 47 of glaciers in the mountainous regions of British Columbia (BC) and Alberta (AB) in western 48 Canada. The 2005 AD ice volume and its sea-level equivalent are then calculated by summing 49 calculated ice volume for individual glaciers. A recent inventory of glaciers in the study area 50 indicated that in 2005 the number of glaciers was  $\sim 17\,600$  and the area of glacierized terrain 51 was  $\sim 26700 \,\mathrm{km^2}$  (Bolch et al. 2010). For reference, in the 1970s some 5050 "perennial surface 52 ice bodies" with a combined area of 2909 km<sup>2</sup> were identified in the European Alps (Haeberli 53 and Hoelzle 1995) and for the Swiss Alps alone there are 1483 glaciers with a total area of  $\sim 1063 \,\mathrm{km}^2$  (Farinotti et al. 2009b). Our point in making these comparisons is that the BC-AB dataset is too large to be dissected on a glacier-by-glacier basis, so any procedure for generating ice thickness estimates must heavily rely on unguided automatic computation 57 rather than expert intervention. 58

Comparisons between scientific knowledge of glaciers in western North America and those in Europe also justify the departure from methods that have been successfully applied to glaciers in the Swiss Alps. The western North America study region is data poor and of the  $\sim 17,600$  glaciers, few have received scientific attention, yielding only a handful of

published ice thickness measurements (e.g., Doell 1963; Kanasewich 1963; Paterson 1970;
Raymond 1971a,b; Holdsworth et al. 2006). Most of these measurements were taken decades
before our study and, in most cases, the map locations and surface elevations of the sites
were not tied to a conventional geodetic reference frame. Furthermore the glaciers have
thinned substantially so that the surface elevation is now much lower than at the time of
measurement.

Historically, methods of ice thickness estimation have used the idea that glacier ice can be approximated as an ideal plastic material so that bed stress  $\tau^*$  corresponds to the constant 70 plastic yield stress  $\tau_0$  (Orowan 1949). While the implication of a well-defined yield stress is 71 conceptually attractive it suggests that  $\tau_0$  is a physical property of ice and invites misleading 72 assertions such as the "yield stress of glacier ice is 1 bar". If this were truly the case then 73 a single yield stress value could be applied to all glaciers that were sufficiently healthy to 74 maintain the basal stress at this value. Nonetheless several authors have made good use 75 of the plasticity idea. From a 1938 map of the ice surface topography and the assumption 76 that  $\tau^* = 88 \,\mathrm{kPa}$ , Nye (1952a) produced a first map of the subglacial topography of the 77 Greenland Ice Sheet. Later, Reeh (1982) presented an elegant account of three-dimensional 78 plasticity modeling of ice sheet form and in subsequent publications Reeh (1984) and Fisher 79 et al. (1985) applied this to the contemporary Greenland Ice Sheet, ice caps of the Canadian 80 Arctic islands, and the Laurentide Ice Sheet. Crucially, Reeh noted that the assignment of 81 basal shear stress depended on "accumulation rate, basal temperature, etc." (Reeh 1984, p. 116). 83

Rather than assign a single bed stress for all cases, it is better to assign a single stress  $\tau^*$  for each glacier or, more ambitiously, a spatially-varying bed stress  $\tau^*_{i,j}$  based on factors such as the mass balance forcing and observed rate of surface elevation change. A recent approach to this problem, described in Linsbauer et al. (2009) and Paul and Linsbauer (2011), assumes

a constant glacier-wide bed stress given by

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$$\tau^* = \begin{cases} 0.005 + 1.598\Delta Z - 0.435(\Delta Z)^2 & \Delta Z \le 1.6 \text{ km} \\ 1.5 & \Delta Z > 1.6 \text{ km}, \end{cases}$$
(1)

where  $\Delta Z = Z_{\rm H} - Z_{\rm L}$  with  $Z_{\rm H}$  being the highest elevation of the flowshed,  $Z_{\rm L}$  is the lowest, and  $\tau^*$  has units of bars (hPa). Equation 1 is empirical (Haeberli and Hoelzle 1995, Fig. 1) but clever and is based on data from the European Alps. The elevation span  $\Delta Z$  is an indirect though readily observed indicator of the mass balance turnover for a particular glacier. However, there is a concern that (1) must be tuned to specific geographical settings. For this reason, we focus on estimating glacier-specific but space-varying bed stress (Section 3).

## 6 2. Thickness estimation as an optimization problem

We assume that surface topography is represented by a matrix of elevation values  $S_{i,j}$ 97 expressing the elevation map positions  $(x_i, y_j)$  in a Cartesian coordinate system. The cells 98 are assumed to be square with dimensions  $\Delta x \times \Delta y$  which, for our study, are 200 m  $\times$  200 m 99 which matches the resolution of a prognostic ice flow model that we are also developing. 100 Co-registered with this DEM is a second matrix, referred to as the ice mask, which has the 101 properties  $I_{i,j} = 1$  when the ice cover is greater or equal to 50% and  $I_{i,j} = 0$  otherwise. 102 Given  $S_{i,j}$  and  $I_{i,j}$  together with information on the mass balance forcing and the rate of 103 surface elevation change, we estimate the ice thickness  $H_{i,j}$  for the  $I_{i,j} = 1$  cells and, from 104 this, produce a map of the bed topography  $B_{i,j}$ , where  $B_{i,j} = S_{i,j} - H_{i,j}$  when  $I_{i,j} = 1$  and 105  $B_{i,j} = S_{i,j} \text{ when } I_{i,j} = 0.$ 106

For an ice slab of uniform thickness inclined at an angle  $\theta$ , the relationship between

bottom stress  $\tau^*$  and slab thickness is

$$h = \frac{\tau^*}{\rho g \sin \theta},\tag{2}$$

where  $\rho$  is the density and g is the gravity acceleration. In the shallow ice approximation (e.g., Fowler and Larson 1978), Equation 2 is valid everywhere, and thus can be written  $h_{i,j} = \tau_{i,j}^*/\rho g \sin \theta_{i,j}$ . The vertical distance between the upper and lower boundary of the slab is given by  $H_{i,j} = h_{i,j}/\cos \theta_{i,j}$  so (2) gives

$$H_{i,j} = \frac{\tau_{i,j}^*}{\rho g \sin \theta_{i,j} \cos \theta_{i,j}}.$$
 (3)

The obvious implication of (3) is that ice thickness  $H_{i,j}$  can be estimated if the surface slope  $\theta_{i,j}$  and bed stress  $\tau_{i,j}^*$  are known. When the base is not parallel to the surface, Nye (1952b) showed that surface slope has the dominant influence on bed stress — at least for small values of slope — so we take  $\theta_{i,j}$  to correspond to the glacier surface slope  $|\nabla_{xy}S_{i,j}| = \tan \theta_{i,j}$ , where  $\nabla_{xy}S_{i,j}$  denotes the two-dimensional gradient of the surface topography at the grid point (i,j). Equation 3 can therefore be written

$$H_{i,j} = \frac{1 + \left| \nabla_{xy} S_{i,j} \right|^2}{\left| \nabla_{xy} S_{i,j} \right|} \frac{\tau_{i,j}^*}{\rho g}.$$
 (4)

Solving (4) is equivalent to minimizing a cost function of the form

$$\mathcal{J}_{0} = \sum_{I_{i,j}=1} \left[ H_{i,j} - \frac{1 + \left| \nabla_{xy} S_{i,j} \right|^{2}}{\left| \nabla_{xy} S_{i,j} \right|} \frac{\tau_{i,j}^{*}}{\rho g} \right]^{2}, \tag{5}$$

where the summation is performed over all ice-covered cells.

A second approach to estimating  $H_{i,j}$  is to use Laplacian interpolation (e.g., Press et al. 2007, p. 151), which is equivalent to solving  $\nabla^2_{xy}H_{i,j}=0$  subject to the boundary condition  $H_{i,j}=0$  beyond the glacier margins. Combining the two approaches and introducing a

spatially-varying tradeoff parameter  $\chi_{i,j}$ , the ice thickness estimates are obtained by minimizing the modified cost function

The factor  $\lambda^4 := \sigma_H^2/\sigma_{\text{Lap}\,H}^2$  has been inserted to yield dimensional consistency and to ensure

$$\mathcal{J} = \sum_{I_{i,j}=1} \left\{ \chi_{i,j} \left[ H_{i,j} - \frac{1 + \left| \nabla_{xy} S_{i,j} \right|^2}{\left| \nabla_{xy} S_{i,j} \right|} \frac{\tau_{i,j}^*}{\rho g} \right]^2 + (1 - \chi_{i,j}) \lambda^4 \left[ \nabla_{xy}^2 H_{i,j} \right]^2 \right\}.$$
 (6)

that the two cost terms have comparable magnitude before they are subjected to the  $\chi_{i,j}$ 127 weightings;  $\sigma_H$  is an estimate of the standard deviation of the first square-bracketed term 128 and  $\sigma_{\text{Lap }H}$  is that for the second. Hereafter we assume  $\sigma_H = 25 \,\text{m}$  and  $\sigma_{\text{Lap }H} = 0.0025 \,\text{m}^{-1}$ , 129 so that  $\lambda$  is fixed at  $\lambda = 100 \,\mathrm{m}$ , and then use  $\chi_{i,j}$  to manage the tradeoff between the cost 130 terms. For  $\chi_{i,j} = 1$  the thickness estimate is entirely based on the stress relation (4) and for 131  $\chi_{i,j} = 0$  the estimate is generated by Laplacian interpolation among neighboring cells. 132 The tradeoff parameter  $\chi_{i,j}$  can be set to vary with spatial position in order to give the 133 greatest weight to the estimator that has the most authority at a given point. For example, 134 in the central regions of ice caps, where the surface slope is small and the stress-based 135 estimator (3) becomes sensitive to small fluctuations in  $\theta_{i,j}$ , the tradeoff parameter  $\chi_{i,j}$  can be set to a small value so that the thickness estimate is largely or entirely based on Laplacian

Substituting a finite-difference approximation for  $\nabla^2_{xy}H_{i,j}$  in (6) gives

interpolation.

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$$\mathcal{J} = \sum_{I_{i,j}=1} \left\{ \chi_{i,j} \left[ H_{i,j} - \frac{1 + \left| \nabla_{xy} S_{i,j} \right|^2}{\left| \nabla_{xy} S_{i,j} \right|} \frac{\tau_{i,j}^*}{\rho g} \right]^2 + (1 - \chi_{i,j}) \left( \frac{\lambda}{\Delta x} \right)^4 \left[ H_{i-1,j} + H_{i+1,j} + H_{i,j-1} + H_{i,j+1} - 4H_{i,j} \right]^2 \right\}.$$
(7)

Differentiating  $\mathcal J$  with respect to  $H_{i,j}$  and setting the result to zero gives a system of equations

that minimizes  $\mathcal{J}$ ,

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$$\chi_{i,j} \left[ H_{i,j} - \frac{1 + \left| \nabla_{xy} S_{i,j} \right|^2}{\left| \nabla_{xy} S_{i,j} \right|} \frac{\tau_{i,j}^*}{\rho g} \right] -4\alpha (1 - \chi_{i,j}) \left[ H_{i-1,j} + H_{i+1,j} + H_{i,j-1} + H_{i,j+1} - 4H_{i,j} \right] = 0,$$
(8)

where  $\alpha := \lambda^4/(\Delta x)^4$ . Reorganizing (8) gives

$$-4\alpha(1-\chi_{i,j})H_{i-1,j} - 4\alpha(1-\chi_{i,j})H_{i+1,j} - 4\alpha(1-\chi_{i,j})H_{i,j-1} - 4\alpha(1-\chi_{i,j})H_{i,j+1}$$

$$+ \left[\chi_{i,j} + 16\alpha(1-\chi_{i,j})\right]H_{i,j} = \chi_{i,j} \left[\frac{1+\left|\nabla_{xy}S_{i,j}\right|^{2}}{\left|\nabla_{xy}S_{i,j}\right|}\frac{\tau_{i,j}^{*}}{\rho g}\right],$$
(9)

which represents a set of linear equations having the form  $\mathbf{AH} = \mathbf{C}$ , where  $\mathbf{H}$  is a column vector formed from the unknown ice thickness values  $H_{i,j}$ ,  $\mathbf{A}$  is the matrix of coefficients, and  $\mathbf{C}$  is a column vector formed from the known righthand-side terms of (9). For a large domain the coefficient matrix  $\mathbf{A}$  can be huge but the matrix is sparse and the solution can be found remarkably rapidly (e.g., 420 000 unknown  $H_{i,j}$  values in roughly 4 hours of machine time on a desktop workstation). From test runs it was established that computing time increases linearly with problem size.

The tradeoff parameter  $\chi_{i,j}$  controls the weighting that is assigned to the stress-based estimator relative to that assigned for the Laplacian interpolation estimator. First a default value  $\chi_0$  must be assigned and this is decided by balancing the conflicting requirements of resolving changes in ice thickness while maintaining a smooth spatial pattern. By applying the inversion method to the output of a numerical ice dynamics model (for which the simulated ice thickness is perfectly known), we found that  $\chi_0 = 0.40$  yields a satisfactory compromise. Where surface slopes were small we reduced  $\chi_{i,j}$  in a smooth fashion, as described in Section 4.

## 3. Estimation of basal stress

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Our approach to estimating basal stress is similar to that of Farinotti et al. (2009a) and is based on automated delineation of glacier flowsheds and application of the continuity equation. The term "flowshed" has been adopted to describe a glacier flow unit that is defined by its ice catchment. In many situations there is no distinction between a glacier and a glacier flowshed, but for glaciers that share a common catchment region the boundary between individual glaciers emanating from that catchment is defined by ice drainage divides.

The principle of ice volume conservation can be expressed as

$$\operatorname{div}_{xy} \mathbf{q} = \dot{b} - \dot{H} \tag{10}$$

where  $\operatorname{div}_{xy}$  denotes the two-dimensional divergence,  $\mathbf{q}$  is the vertically-integrated volume 166 flux of ice per unit width  $(m^2 yr^{-1})$ ,  $\dot{b}$  is the ice-equivalent mass balance rate  $(m yr^{-1})$ , and 167  $\dot{H}$  is the rate of change of ice thickness (m yr<sup>-1</sup>). In the glacier accumulation zone the mass 168 balance rate is positive; in the ablation zone it is negative. For notational efficiency and consistency with antecedent work (Farinotti et al. 2009a), we define an apparent balance 170 rate  $\hat{b} = \dot{b} - \dot{H}$  which varies from a minimum value  $\min(\hat{b})$  to a maximum value  $\max(\hat{b})$ . By sampling  $\hat{b}$  at regular intervals  $\Delta \hat{b}$  we generate a series of balance zones, where for zone  $\alpha$ 172 the limits are  $\hat{b}_{\alpha} - \frac{1}{2}\Delta \hat{b} \leq \hat{b} < \hat{b}_{\alpha} + \frac{1}{2}\Delta \hat{b}$ . In this manner flowsheds in the region of interest 173 can be partitioned into a series of banded zones. Letting  $\Gamma_{\alpha}$  denote the curve that separates 174 the lower boundary of zone  $\alpha$  from the upper boundary of the zone immediately below it, 175  $\Gamma_{\alpha}$  traces the lower boundary of a catchment area  $A_{\alpha}$  for which  $\hat{b} > \hat{b}_{\alpha}$ . The ice discharge 176  $(m^3 yr^{-1}) across \Gamma_{\alpha} is$ 177

$$Q_{\alpha} = \int_{A_{\alpha}} \widehat{b} \, \mathrm{d}A. \tag{11}$$

Defining  $l_{\alpha}$  as the length of  $\Gamma_{\alpha}$ , the length-averaged ice flux (m<sup>2</sup> yr<sup>-1</sup>) traversing  $\Gamma_{\alpha}$  is  $\overline{q}_{\alpha} = Q_{\alpha}/l_{\alpha}$ .

Our aim is to use  $\overline{q}_{\alpha}$  as the basis for estimating  $\overline{\tau}_{\alpha}$ , the characteristic bed stress along the  $\Gamma_{\alpha}$  line. The volume flux of ice per unit width of channel is given by

$$q = v_{\rm s}h + \frac{2\mathcal{A}}{n+2}\tau^{*n}h^2,\tag{12}$$

(e.g., Cuffey and Paterson 2010, p. 310) where  $q_s = v_s h$  is the sliding contribution and the second term represents ice flux due to creep

$$q_{\rm c} = \frac{2\mathcal{A}}{n+2} \tau^{*n} h^2. \tag{13}$$

The parameters  $\mathcal{A}$  and n are the creep rate factor and exponent of Glen's flow law for ice.

Taking  $\tau^* = \rho g h \sin \theta$ , (13) can be rewritten as

$$q_{\rm c} = \frac{2\mathcal{A}}{n+2} \tau^{*n} \left(\frac{\tau^*}{\rho g \sin \theta}\right)^2,\tag{14}$$

leading to the expression

$$\tau^* = \left[ \frac{(n+2)(\rho g \sin \theta)^2 q_c}{2\mathcal{A}} \right]^{\frac{1}{n+2}}.$$
 (15)

The key step in our approach is to take  $\overline{q}_{\alpha} = q_{\alpha c} + q_{\alpha s}$ , where  $q_{\alpha c}$  and  $q_{\alpha s}$  are the creep and sliding contributions to  $\overline{q}_{\alpha}$  respectively, and then calculate the corresponding  $\overline{\tau}_{\alpha}$ . Rather than separately calculate  $q_{\alpha s}$ , we postulate that it is some fixed fraction of the total ice flux, and therefore take  $q_{\alpha c} = \xi q_{\alpha}$  and  $q_{\alpha s} = (1 - \xi)q_{\alpha}$ , to obtain

$$\overline{\tau}_{\alpha} = \left[ \frac{(n+2)(\rho g \overline{\sin \theta_{\alpha}})^2 \xi q_{\alpha}}{2\mathcal{A}} \right]^{\frac{1}{n+2}}, \tag{16}$$

where  $\overline{\sin \theta_{\alpha}}$  is obtained from the ice surface slope averaged along the line  $\Gamma_{\alpha}$ . Next we assume that the calculated value for  $\overline{\tau}_{\alpha}$  provides an estimate of  $\tau_{\alpha}^*$  for the balance band  $\alpha$  within a given flowshed. The resulting  $\tau_{\alpha}^*$  value is then applied to the (i,j) grid points that lie within balance band  $\alpha$  to obtain  $\tau_{i,j}^*$  for that balance band and flowshed. Finally these

values are substituted into the cost minimization equation (9) which is solved to obtain the desired  $H_{i,j}$  estimates.

Farinotti et al. (2009a) follow a similar line of thought. Assuming a simple elevation dependence for the net mass balance field, they evaluate the ice flux  $q_f$  and averaged surface slope  $\bar{\theta}$  along the flow line and then apply the integrated form of Glen's flow law to express this in terms of ice thickness h to obtain

$$h = \left[\frac{(n+2)q_{\rm f}}{2\mathcal{A}(C\rho g\sin\overline{\theta})^n}\right]^{\frac{n+2}{2}}.$$
(17)

This is similar to our approach of estimating  $\tau^*$  (Equation 16) and then using (3) to calculate 201 the corresponding ice thickness. Their parameter C is a dimensionless correction factor to 202 account for the partitioning between creep and sliding contributions to ice flow. The main 203 points of difference between our method and that of Farinotti et al. (2009a) are that we do not 204 restrict our analysis to flowlines (and hence do not need to delineate them, automatically 205 or otherwise) and that spatial smoothing is applied implicitly as an integral part of the 206 inversion procedure (by means of the Laplacian interpolator), rather than as a distinct and 207 explicit step (e.g., initial smoothing of the surface slope  $\theta$ ). 208

## 209 4. Technical matters

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This section contains much of the technical detail and justifications that underlie our approach to ice thickness estimation. The casual reader can skip this section and move directly to the section on performance analysis.

a. Physical constants and glaciological parameters

For the flow law parameters we take n=3 and  $\mathcal{A}=2.4\times10^{-24}\,\mathrm{Pa^{-3}\,s^{-1}}$ , which match the values recommended in (Cuffey and Paterson 2010, Table 3.4), together with  $\rho=910\,\mathrm{kg\,m^{-3}}$ 

for ice density and  $g=9.81\,\mathrm{m\,s^{-2}}$  for the gravity acceleration. We make the approximation that sliding does not contribute to ice flow ( $\xi=1$  in (16)). In reality  $\xi=\xi_{i,j}$  could vary from cell-to-cell in the model but lacking this information we apply a single value to all cells. Although for large active glaciers sliding can be significant, for most cells  $\xi\approx 1$  is probably acceptable. In any case, we will show that  $\xi$  is not a sensitive parameter of the inversion scheme.

### $^{222}$ b. Calculation of surface slope

There are several ways of calculating the magnitude of the surface slope by numerical differentiation of  $S_{i,j}$ . Our preferred method is to calculate the slope in each of four quadrants (NE, SE, SW, NW) and take the average. For example, for the NE quadrant,

$$\left|\nabla S_{\text{NE}}\right|_{i,j} = \left\{ \left[ (S_{i+1,j} - S_{i,j})/\Delta x \right]^2 + \left[ (S_{i,j+1} - S_{i,j})/\Delta y \right]^2 \right\}^{\frac{1}{2}}$$
 (18)

 $_{226}$  and the quadrant-averaged slope is

$$\left|\nabla S\right|_{i,j} = \frac{1}{4} \left[ \left|\nabla S_{NE}\right|_{i,j} + \left|\nabla S_{SE}\right|_{i,j} + \left|\nabla S_{SW}\right|_{i,j} + \left|\nabla S_{NW}\right|_{i,j} \right]. \tag{19}$$

A second consideration is how best to deal with the problem of small slopes. As already noted, expressions such as (2), (3), and (4) tend to infinity when  $\theta \to 0$ . We deal with this problem by applying a limiter to the slope expression (19) to avoid the  $|\nabla S_{i,j}|=0$  limit. In the present work we use the slope limiter

$$|\nabla S|_{\lim} = \begin{cases} \delta_0 + (\delta_1 - \delta_0)|\nabla S|^2/\delta_1^2 & 0 \le |\nabla S| \le \delta_1\\ |\nabla S| & |\nabla S| > \delta_1 \end{cases}$$
(20)

with  $\delta_0 = 0.01$  and  $\delta_1 = 0.03$ . This sets the minimum slope to  $\delta_0 = 0.01$  which corresponds

to an angle of 0.57°. When  $|\nabla S| < \delta_1$  and the slope limiter is active we also reduce the tradeoff parameter  $\chi_{i,j}$  in a systematic manner, tapering it to zero, as follows:

$$\chi = \max \left[ \frac{|\nabla S| - \delta_0}{\delta_1 - \delta_0}, 0 \right] \chi_0. \tag{21}$$

Thus the minimum slope  $\delta_0$  is never actually applied because the tradeoff parameter assigns no weight to the stress-based estimator when  $|\nabla S| \leq \delta_0$ .

236 c. Balance zone delineation and calculation of width and slope at zone boundaries

For gridded data the zone boundary  $\Gamma_{\alpha}$  can be found algorithmically by searching for 237 cells having  $I_{i,j} = 1$  (ice-covered) with  $\hat{b}_{i,j} > \hat{b}_{\alpha}$  and one or more neighboring cells for which 238 cells  $\hat{b}_{i,j} \leq \hat{b}_{\alpha}$ . For each flowshed and every balance zone, we calculate the length of the zone 239 boundary  $l_{\alpha}$ , by summing over the length contribution from individual cells using a flux-240 weighted estimate of the length. Some form of weighting is necessary because the direction 241 of ice flow is not usually aligned with the cell orientation; thus, for an individual cell having 242 dimensions  $\Delta x \times \Delta y$ , its length contribution  $\Delta l_{i,j}$  is unlikely to be  $\Delta l_{i,j} = \Delta x$  or  $\Delta y$ . For the faces of the cell (i, j), the surface slope components in the cardinal directions can be 244 written 245

$$\nabla_{N} S_{i,j} = (S_{i,j+1} - S_{i,j})/\Delta y, \qquad \nabla_{S} S_{i,j} = (S_{i,j} - S_{i,j-1})/\Delta y,$$

$$\nabla_{E} S_{i,j} = (S_{i+1,j} - S_{i,j})/\Delta x, \qquad \nabla_{W} S_{i,j} = (S_{i,j} - S_{i-1,j})/\Delta x,$$
(22)

and the corresponding *outward* creep flux magnitudes  $[Q_N]_{i,j}$ ,  $[Q_E]_{i,j}$ , etc. are proportional to the following:

$$\begin{bmatrix} w_{\mathrm{N}} \end{bmatrix}_{i,j} = \max \left( -\nabla_{\mathrm{N}} S_{i,j}, 0 \right)^{n}, \qquad \begin{bmatrix} w_{\mathrm{S}} \end{bmatrix}_{i,j} = \max \left( \nabla_{\mathrm{S}} S_{i,j}, 0 \right)^{n},$$
$$\begin{bmatrix} w_{\mathrm{E}} \end{bmatrix}_{i,j} = \max \left( -\nabla_{\mathrm{E}} S_{i,j}, 0 \right)^{n}, \qquad \begin{bmatrix} w_{\mathrm{W}} \end{bmatrix}_{i,j} = \max \left( \nabla_{\mathrm{W}} S_{i,j}, 0 \right)^{n}. \tag{23}$$

where the negative signs in the North and East terms have been applied so that outward cell fluxes are positive. As the length contribution for a single cell, we take the flux-weighted average for all cell walls through which there is an outward flux of ice, i.e.,

$$\left[\Delta l_{\alpha}\right]_{i,j} = \frac{\left[w_{\rm N}\right]_{i,j} \Delta y + \left[w_{\rm E}\right]_{i,j} \Delta x + \left[w_{\rm S}\right]_{i,j} \Delta y + \left[w_{\rm W}\right]_{i,j} \Delta x}{\left(\left[w_{\rm N}\right]_{i,j}^{2} + \left[w_{\rm E}\right]_{i,j}^{2} + \left[w_{\rm S}\right]_{i,j}^{2} + \left[w_{\rm W}\right]_{i,j}^{2}\right)^{\frac{1}{2}}}$$
(24)

$$\left[l_{\alpha}\right]_{g} = \sum_{G=g} \left[\Delta l_{\alpha}\right]_{i,j},\tag{25}$$

where  $[l_{\alpha}]_q$  is the length of the  $\Gamma_{\alpha}$  balance zone boundary for the g-th flowshed.

#### 252 d. Ice masks and flowsheds

It is important to distinguish between connected regions of ice that lie within a single ice mask and the individual ice flow units that can subdivide a mask. A high-elevation icefield, for example, might function as the common collection area for many individual glaciers but different flow units can be distinguished, sometimes very subtly, by topographic divides. The analogy with watersheds is obvious.

There is a substantial literature on algorithms for automated delineation of watersheds (e.g., Marks et al. 1984; Fairfield and Leymarie 1991; Meyer 1994; Tarboton 1997) but automated delineation of glacier flowsheds presents special challenges. Although the flows of water and ice are both gravity driven, glaciers have morphological differences that cause problems for conventional watershed algorithms. For example, a single glacier can have a multi-lobed terminus which, in a watershed algorithm, can be misinterpreted as multiple distinct glaciers, causing the algorithm to assign labels to many more flowsheds than actually exist. Rather than start from scratch we tailored the watershed algorithm included in the TopoToolbox (Schwanghart and Kuhn 2010) software package to deal with this problem (see next subsection for details). Figure 1 shows the results of applying this new flowshed delineation algorithm to a DEM of surface topography S (Fig. 1a) and ice mask I (Fig. 1b)

to generate a flowshed map G (Fig. 1c) in a test example.

### e. Orphaned, fissioned, and problematic flowsheds

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Accurate delineation of glacier flowsheds is required for accurate estimation of  $Q_{\alpha}$  (Equa-271 tion 11) and  $\bar{\tau}_{\alpha}$  (Equation 16). This subsection summarizes the corrective actions that are 272 taken after applying a conventional watershed algorithm (Schwanghart and Kuhn 2010) to 273 the DEM of an ice-covered surface. Three different kinds of problems are encountered: (i) 274 Not all glacierized cells are assigned a watershed label and in effect they are "orphaned" 275 by the watershed algorithm. (ii) The algorithm wrongly classifies glacier flow lines as flow 276 divides and thus fissions a single glacier into one or more child glaciers. (iii) The lobate ter-277 minus of a single glacier can be wrongly dissected into fragments. Typically these fragments 278 are small and lie mainly or entirely below the equilibrium line altitude (ELA) so they tend 279 to be unviable in the sense that they have insufficient accumulation to maintain themselves. Orphaned glacierized cells are readily identified because for these  $I_{i,j} = 1$  and  $G_{i,j}$  is 281 unassigned. If such cells are adjacent to cells that have been assigned a flowshed label 282

unassigned. If such cells are adjacent to cells that have been assigned a flowshed label they are merged with that flowshed; if they lack an adjacent neighboring flowshed they are assigned a new label and treated as an additional flowshed. This situation is very rare and arises from shortcomings of conventional watershed algorithms.

Fissioned flowsheds are a consequence of applying a watershed algorithm to glaciers that
have a multilobed terminus. If the algorithm erroneously designates each lobe as a separate
flowshed then this distinction will be preserved farther upstream even though the flowsheds
are separated by a flowline rather than a flow divide. Fortunately the situation is easily
detected. Cells p and q that are separated by a flowline boundary will tend to have the
same slope direction whereas those that are separated by a flow divide boundary will tend
to have opposite slope directions. A simple dot product test  $\nabla_{xy}S_p \cdot \nabla_{xy}S_q$  is sufficient to
discriminate between the two situations.

We classify a flowshed as "problematic" if  $Q_{\alpha} \leq 0$  everywhere within it. For such

flowsheds  $[Q_{\text{ela}}]_g$  and  $[l_{\text{ela}}]_g$  either vanish or are unacceptably small and the estimate of the ELA ice flux  $\bar{q}_{\text{ela}} = Q_{\text{ela}}/l_{\text{ela}}$  fails. In many cases the unviable flowshed is contiguous to a viable one (for example when the unviable flowshed corresponds to some fragment of a glacier tongue which is adjacent to a viable flowshed). In this situation the unviable flowshed is merged with its viable neighbor (i.e., the label of the unviable flowshed is replaced by that of the viable flowshed and its area added to that of the viable flowshed). In situations when there is more than one viable contiguous flowshed the unviable flowshed is merged with its largest viable neighbor.

### f. Last resort estimates of bed stress

In unusual situations it is impossible to calculate  $\bar{\tau}_{\alpha}$  and a fall-back strategy is required.

As an example, a flowshed that comprises a single ice cell cannot be decomposed into distinct accumulation and ablation areas and thus the mass balance analysis (11) that leads to estimates of  $\bar{\tau}_{\alpha}$  cannot be carried out. For such cases we apply a stress-area scaling expression to estimate a single bed stress for the flowshed. The scaling relationship  $V \propto A^{\gamma}$  which relates glacier volume to glacier area is derived in important papers by Bahr (1997) and Bahr et al. (1997). A lesser known but potentially useful result from the same work is  $\tau^* \propto A^{\beta}$  which we write as

$$\tau^* = k \left( A/A_0 \right)^{\beta},\tag{26}$$

where k is a proportionality constant having units of stress,  $A_0$  is a characteristic glacier area (we arbitrarily take  $A_0 = 1 \,\mathrm{km^2}$ ), and  $\beta = 2(\gamma - 1) - \frac{1}{2}$ . The scaling theory yields  $\gamma = 11/8 = 1.375$  whereas a prior linear regression of data from 63 mountain glaciers (Chen and Ohmura 1990) yielded  $\gamma = 1.36$ . Accepting  $\gamma = 11/8$  gives  $\beta = 1/4$ , indicating a weak dependence of bed stress on glacier area. The proportionality constant k is estimated by evaluating the statistic

$$k_g = \frac{[\tau_{\text{ela}}]_g}{(A_q/A_0)^{\frac{1}{4}}} \tag{27}$$

for all viable flowsheds and then calculating the mean using a weighted average. In (27)  $k_g$  is the calculated proportionality constant,  $[\tau_{\text{ela}}]_g$  is the estimated bed stress at the ELA, and  $A_g$  is the area of the g-th flowshed. We find that root area-weighting

$$\langle k \rangle = \frac{\sum_{g} \sqrt{A_g} k_g}{\sum_{g} \sqrt{A_g}} \tag{28}$$

gives satisfactory results.

322 g. Adjustment of the mass balance field

For a glacier flowshed that is delineated by the curve  $\mathcal{C}$  which encloses a surface area A, the integral form of the expression for ice volume balance is given by

$$\frac{\mathrm{d}}{\mathrm{d}t} \int_{A} H \, \mathrm{d}A = \int_{A} \dot{b} \, \mathrm{d}A,\tag{29}$$

 $^{325}$  which expands to

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$$\int_{A} \dot{H} \, \mathrm{d}A + \int_{C} \mathbf{n} \cdot \mathbf{q} \, \mathrm{d}C = \int_{A} \dot{b} \, \mathrm{d}A,\tag{30}$$

where  $\mathbf{q} = \mathbf{v}H$ ,  $\mathbf{v}$  is the column-averaged ice velocity vector, and  $\mathbf{n}$  is the outward normal vector (in two dimensions) to the curve  $\mathcal{C}$ . The second lefthand-side term of (30) is associated with an increase or decrease in the flowshed area and merits special discussion. For advancing glaciers, such as those undergoing a surge, the term can be non-negligible and positive. For retreating glaciers, upflow velocities are non-physical and  $\mathbf{v}$  vanishes along  $\mathcal{C}$ . For most situations, especially in a warming climate where glacier retreat prevails, the term can be neglected and (30) gives

$$\int_{A} (\dot{b} - \dot{H}) \, \mathrm{d}A = \int_{A} \widehat{b} \, \mathrm{d}A = 0. \tag{31}$$

In reality the flowshed boundary  $\mathcal{C}$  and enclosed area A as well as the surface balance

rate  $\dot{b}$  and thinning rate  $\dot{H}$  are imperfectly known so that when the integration of (31) is performed using imperfect quantities  $A^{(\pm)}$ ,  $\dot{b}^{(\pm)}$ , and  $\dot{H}^{(\pm)}$  the result is unlikely to vanish. For this case

$$\int_{A^{(\pm)}} (\dot{b}^{(\pm)} - \dot{H}^{(\pm)}) \, dA^{(\pm)} = \int_{A^{(\pm)}} \widehat{b}^{(\pm)} \, dA^{(\pm)} = b_0 A^{(\pm)}, \tag{32}$$

where  $b_0$  is a constant and  $A^{(\pm)}$  is the estimated flowshed area. A non-vanishing result in 337 (32) can lead to systematic over- or underestimates of the ice discharge  $Q_{\alpha}$  in (11) and thus 338 to errors in estimates of basal stress and ice thickness. If, for example,  $b_0$  is negative then  $Q_{\alpha}$ will vanish along a line  $\Gamma_{\alpha}$  which is upglacier from the glacier terminus. Thus in the region between the terminus and  $\Gamma_{\alpha}$  the computed ice discharge will be negative, corresponding 341 to up-slope transport of ice. To deal with this situation we adjust the estimated apparent 342 mass balance field  $\hat{b}^{(\pm)}$  by simply subtracting the balance error  $b_0$ , in effect assuming  $\hat{b}^{(\pm)} =$ 343  $\dot{b}^{(\pm)} - \dot{H}^{(\pm)} - b_0$  so that the computed integral (31) vanishes as it should. We refer to this 344 procedure as "balance adjustment". 345

h. Influence of uncertainty in values of flow law coefficient and flow partitioning parameter

The expected sensitivity of ice thickness inversions to uncertainty in model parameters

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such as the flow law coefficient  $\mathcal{A}$  and flow partitioning  $\xi$  can be inferred from the relationship

$$H = \frac{1}{\rho g \sin \theta \cos \theta} \left[ \frac{(n+2)(\rho g \sin \theta)^2 \xi q}{2\mathcal{A}} \right]^{\frac{1}{n+2}}$$
(33)

obtained from (3) and (15). Concentrating attention on the parameters  $\mathcal{A}$  and  $\xi$  we assume that  $H = H(\mathcal{A}, \xi)$  and take logarithmic derivatives to obtain

$$\frac{\mathrm{d}H}{H} = \frac{1}{n+2} \left( \frac{\mathrm{d}\xi}{\xi} - \frac{\mathrm{d}\mathcal{A}}{\mathcal{A}} \right). \tag{34}$$

With n=3 the fractional change in ice thickness is 1/5th the fractional change in  $\xi$  and  $\mathcal{A}$ , with increased  $\xi$  leading to increased ice thickness and increased  $\mathcal{A}$  leading to decreased

thickness. Clearly the thickness estimates are not sensitively dependent on uncertainty in these parameters, a result that we also have confirmed by testing the effect of varying  $\mathcal{A}$  and  $\xi$  in the inversion models.

#### 356 i. Shape factors and debris cover

Paul and Linsbauer (2011) apply a shape factor correction to their bed stress estimates 357 but assume this to be constant at f=0.80 so its only effect is to systematically increase the 358 estimated ice thickness. In contrast, Farinotti et al. (2009a) do not include a shape factor 359 although their correction factor C in (17) could be adjusted to include a channel shape 360 correction. We do not include an explicit shape factor because we are wary of applying 361 an all-embracing correction factor to our thickness estimates, preferring to view the role of 362 shape factors as a potential source of systematic error that is subject to scrutiny. 363 In their analysis of Swiss Glaciers, Farinotti et al. (2009a) include the affect of debris 364

cover on mass balance. At present Tiedemann Glacier, BC is one of the few glaciers in our study region for which a debris mask has been generated. For our study region this effort would need to be expanded before we could follow their example.

#### 368 j. Regularization

We use  $\nabla_{xy}^2 H_{i,j}$  (e.g., Equation 6) to smooth the estimated ice thickness. An alternative approach, which seems reasonable but leads to problems, is to smooth the bed topography  $B_{i,j} = S_{i,j} - H_{i,j}$  rather than the ice thickness  $H_{i,j}$ . This can lead to negative ice thickness estimates which must then be dealt with. To avoid this difficulty we use the  $\nabla_{xy}^2 H$  regularization and have also tested the  $|\nabla_{xy} H_{i,j}|$  regularization, finding that it gives comparable results.

## 5. Performance analysis and error estimates

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To assess the performance of the ice thickness estimation scheme, we used a numerical ice dynamics model to generate synthetic ice cover over known deglacierized topography and then tested the skill of the inversion scheme for a range of situations. A potentially serious shortcoming of this stratagem is that the ice dynamics model could have unknown physical or numerical defects that cause it to produce non-physical representations of glaciers.

The ice dynamics model was originally developed by C. G. Schoof and is based on the shallow ice approximation; it uses a semi-implicit finite-difference method together with flux limiters to solve mass conservation and vertically-integrated momentum equations on a rectangular grid (Jarosch et al. 2012b). The basic equations of the model are

$$\dot{H} = \dot{b} - \operatorname{div}_{xy} \mathbf{q} \tag{35}$$

$$\mathbf{q} = -\frac{2\mathcal{A}(\rho g)^n |\nabla S|^{n-1}}{n+2} H^{n+2} \nabla S + \mathbf{v}_s H_s, \tag{36}$$

with the parameter assignments  $\mathcal{A}=2.4\times10^{-24}\,\mathrm{Pa^{-3}\,s^{-1}},\;n=3,\;\rho=910\,\mathrm{kg\,m^{-3}},\;g=3$  $9.81\,\mathrm{m\,s^{-2}}$ , and  $\mathbf{v}_{\mathrm{s}}=0$ . We assume the glaciers are isothermal at the melting temperature 386 of ice so there is no need to include an energy equation. For the vast majority of glaciers in 387 the study area this is likely to be a valid assumption but it would become dubious if applied 388 universally to glaciers of the Yukon interior, farther to the north. Huss and Farinotti (2012) 389 face this problem in estimating the glacier contribution to global ice volume and use the 390 mean annual temperature at the ELA as a basis for modifying the creep rate factor  $\mathcal{A}$  in 391 expressions such as our Equation 16. It follows from (17) that the effect of reducing the rate 392 factor is to increase the estimated ice thickness. 393 We used DEMs for unglacierized mountainous topography in British Columbia (BC) 394 and the Yukon Territory (YT) to represent the deglaciated surface B(x,y). The labels and coordinates of the map centers for these regions are BC1 (55.4635°N, 124.8151°W), BC2 396

(58.9000°N, 125.8714°W), BC3 (59.4545°N, 130.3566°W), and YT1 (61.6014°N, 133.3684°W).

Ice cover was then grown on this landscape by applying simplified mass balance forcings of the form

$$\dot{b}(x,y,t) = \frac{\mathrm{d}\dot{b}^{-}}{\mathrm{d}z} \min\left(S - z_{\mathrm{ela}}(t),0\right) + \frac{\mathrm{d}\dot{b}^{+}}{\mathrm{d}z} \max\left(S - z_{\mathrm{ela}}(t),0\right)$$
(37)

$$z_{\rm ela}(t) = z_{\rm L} + \frac{1}{2} (z_{\rm H} - z_{\rm L}) (1 + \cos(2\pi t/T_0)),$$
 (38)

where  $d\dot{b}^-/dz$  and  $d\dot{b}^+/dz$  are constant elevation gradients of mass balance,  $z_{\rm L}$  and  $z_{\rm H}$  are the lowest and highest elevation of the ELA, and  $T_0$  is the assumed periodicity of the climate cycle. We explore a wide range of mass balance forcings for steady-state runs involving the four test regions by varying  $z_{\rm ela}$  (Fig. 2). The resulting ice masks, though not the ice thicknesses, are quite similar for the low- and high-rate models so we only plotted those for the high-rate case.

The numerical ice dynamics model generates time-evolving surface topography S(x, y, t)406 from which we can compute the ice thickness H(x,y,t), surface slope  $\nabla S(x,y,t)$ , time-407 evolving ice mask I(x, y, t), and flowshed map G(x, y, t). We then perform calculations to 408 estimate  $[Q_{\alpha}]_g$ ,  $[l_{\alpha}]_g$ ,  $[\overline{q}_{\alpha}]_g$ ,  $[\overline{\tau}_{\alpha}]_g$ , and, finally,  $H_{i,j}$  at any given snapshot time t. Because 409  $B_{i,j}$  is known a priori, the true ice thickness  $H_{i,j}$  is known and can be compared with 410 the estimated thickness  $\widetilde{H}_{i,j}$  to yield the estimation error  $\varepsilon_{i,j} = \widetilde{H}_{i,j} - H_{i,j}$ . We use this 411 approach to evaluate the performance of the thickness estimator and assess the influence of 412 assumptions and parameter assignments on performance (Table 1). For this suite of runs 413 the ELA was set to a constant value  $(z_{\rm ela}=z_{\rm L}=z_{\rm H})$  and the simulations continued until a 414 steady-state was achieved. Model names, such as BC1·1550H, combine information about 415 the geographical site (BC1), ELA (1550 m), and whether the model is strongly-forced (large 416 elevation gradients of mass balance rate  $d\dot{b}^-/dz$  and  $d\dot{b}^+/dz$  labeled H (high)) or weakly-417 forced L (low gradients). For each site and ELA there exists an H and L pair of models. 418 Interestingly, for each model pair the area fractions  $\alpha_{\rm I}$  do not differ much between the H 419 model and the L model but the ice volumes differ by roughly a factor of two. This has 420

possible implications for the effectiveness of the volume—area scaling approach (e.g., Bahr 1997; Bahr et al. 1997) which would predict that glaciers having similar area would also have similar volume assuming that the scaling constant is universal. To be fair, Bahr has never viewed the scaling constant as universal but users of his theory have occasionally treated it as such.

#### a. Results of performance test

There are substantial performance differences among the model runs analyzed and among 427 the performance measures for any given run (Table 2). Rather than dwell on individual cases 428 we shall treat the 32 model runs as an ensemble and summarize the ensemble properties by 429 taking the mean and median of the performance indicators for each member of the ensemble. 430 These indicators include r (the correlation coefficient between the true ice thickness  $H_{i,j}$ 431 and the estimated thickness  $\widehat{H}_{i,j}$ ), the mean thickness error  $\langle \widetilde{H}_{i,j} - H_{i,j} \rangle$ , standard error  $\sigma = \langle \left[ \widetilde{H}_{i,j} - \langle H_{i,j} \rangle \right]^2 \rangle$ , and fractional error in ice volume  $(\widetilde{V} - V)/V$ . The average and median properties of the thickness estimates are good but among members of the ensemble 434 there are some conspicuous exceptions. 435

We single out model YT1·1700H for additional attention. Relative to other members 436 of the ensemble, the performance indicators are neither bad nor good: of the 32 model 437 runs analyzed, it ranks 24th for standard deviation (23.29 m) and rms ice thickness error 438  $(23.29 \,\mathrm{m})$ , 12th for mean thickness error  $(2.27 \,\mathrm{m})$ , and 9th for fractional volume error (4.40%). 439 Nonetheless the overall quality of the ice thickness estimate is encouraging. Plots of the 440 estimated ice thickness vs. the ice thickness in the simulation runs (Fig. 3a) show good 441 correspondence except for large values of ice thickness, where the estimated thickness greatly 442 exceeds the true thickness. However, the number of these outliers is small relative to the total number of points. A histogram of the distribution of the ice thickness estimation error (Fig. 3b) shows that the distribution is slightly asymmetrical, consistent with the fact that 445 thickness cannot be negative. The distribution functions for the actual and estimated ice 446

thickness (Fig. 3c) match reasonably well.

A suite of maps illustrates the performance of the estimation model for this particular case (Fig. 4). The assigned bed stress, based on (16) with  $\xi=1$  and mass balance adjustment of each flowshed to enforce (31), is shown in Fig. 4a. Also shown are the estimated ice thickness (Fig. 4b), the thickness error (Fig. 4c), and the resulting estimate of bed surface topography (Fig. 4d). It is reassuring that the estimated bed surface topography actually resembles a deglaciated landscape because our larger aim is to use such estimates as the starting geometry for projection modeling of the climate-forced deglaciation of western Canada.

Similar performance tests have been carried out for models having a cyclic variation in 455 ELA. We accomplish this by setting  $z_L = z_0 - \Delta z_{\rm ela}$ ,  $z_H = z_0 + \Delta z_{\rm ela}$ , and  $t_0 = 1000\,{\rm yr}$  in 456 (38) and running the model for 80 000 simulation years until a periodically repeating state is 457 achieved. Then for each model we select output states from the final cycle of the simulation 458 that correspond to intervals of fastest deglaciation and fastest reglaciation. Owing to system 459 lags and geometrical effects these usually differ from the times at which the ELA is changing 460 most rapidly so the snapshot times can vary among models. Transient model outputs are 461 assigned labels such as BC1·1550 $\pm$ 100H $\uparrow$  or BC1·1550 $\pm$ 100L $\downarrow$  where BC1 denotes the region, 462 1550, the mean ELA in metres,  $\pm 100$  the amplitude of the sinusoidal elevation excursions, H 463 or L, a high or low mass balance forcing rate, and ↑ a maximally increasing or ↓ maximally 464 decreasing rate of ice area change. 465

We summarize the results of performance tests carried out when the glacier cover is 466 rapidly decreasing (Table 3) or rapidly increasing (Table 4). Comparing these results with 467 those in Table 2 indicates that the ensemble mean and median of mean thickness error and 468 fractional volume error are larger for the transient inversions than for the steady-state ones. 469 Interestingly, for both the deglaciation and reglaciation datasets there is a strong positive 470 bias to the mean thickness error and fractional volume error, so for both situations there 471 is a tendency to overestimate the ice volume. We have no explanation for this. Of the 64 472 cases listed in Tables 3 and 4, only BC3·1650±100H↓ yields an underestimate of average ice 473

thickness and volume. Ensemble mean and median thickness error and fractional volume error are greater, by a substantial margin, for the situation of rapid reglaciation than for rapid deglaciation. Worldwide, rapid deglaciation predominates (Lemke et al. 2007) so for this situation the smaller errors should apply.

## 6. Application to glaciers of western Canada

a. Comparison with thickness measurements on three glaciers

We have previously commented that actual measurements of ice thickness in the study 480 region are few and their usefulness for testing the ice thickness estimation method is open 481 to question. The main sources of difficulty are that the geographical locations and true 482 elevations of the measurements are not well controlled and that substantial surface lowering has occurred between the time that the measurements were taken and the date of the dig-484 ital elevation model and ice mask used in the inversion. We have attempted to recover the 485 measurement positions as best we can and, where possible, have applied the 1985–1999 mea-486 surements of surface elevation change (Schiefer et al. 2007) to correct for thickness changes 487 that have occurred between the measurement dates and the estimation date. 488

Figure 5 compares measured and estimated ice thicknesses for the three glaciers in the 489 study area that have been geophysically surveyed and for which a published record exists. 490 For Athabasca Glacier (52.19°N, 117.26°W) seismic sounding and drilling data were collected 491 from 1959–1961 and are tabulated in Paterson's doctoral thesis (Paterson 1962). Although 492 measurement locations were precisely determined using optical surveying, the survey coordinate system was not georeferenced and lacks an elevation datum. It was therefore necessary to adjust its orientation and offset to align with the DEM of estimated bed topography. Since 495 1961 the surface elevation and spatial extent of the glacier have changed substantially. The Southern Rockies region, which contains both Athabasca and Peyto Glaciers, includes parts 497 of British Columbia and Alberta. For BC glaciers, the Schiefer et al. (2007) time-averaged 498

thinning rates were calculated by subtracting two DEMs to obtain cell-by-cell estimates.

Both Athabasca and Peyto Glaciers are located in Alberta and one of the two DEMs is not
defined beyond the BC boundary. Thus we have applied less accurate and more coarselyresolved elevation-dependent estimates (Schiefer et al. 2007, Fig. 3) to obtain a thinning
correction. The average amount of thinning between 1960 and 2005 was 52.4 m.

Radio echo soundings of Peyto Glacier (51.66°N, 116.56°W), documented in Holdsworth et al. (2006), were taken from 1983–1985. The results are tabulated in Table 1 of that work and include UTM coordinates of all measurement sites. Accepting these at face value (making plausible assumptions concerning the assumed geodetic datum), the data need only be corrected for changes in ice extent and surface thinning. Using the same elevation-dependent relationship as for Athabasca Glacier, we found the average glacier-wide thinning for 1984–2005 to be 14.3 m.

For Salmon Glacier (56.15°N, 130.19 W), in British Columbia, depths were measured using seismic sounding and drilling (Mathews 1959; Doell 1963) but were presented as plotted cross sections and maps. We extracted thickness data from a contour map of surface and bed elevation (Doell 1963, Fig. 5) so the associated uncertainties are considerable. The average thinning for 1956–2005 was 107.7 m and ranged from 145.9 m to 32.4 m. Gravity survey results are also available for Athabasca Glacier (Kanasewich 1963) and Salmon Glacier (Russell et al. 1960) but these are expected to be less accurate than direct sounding methods and have not been used.

Figure 5a shows the estimated ice thickness vs. measured ice thickness for the three glaciers with no correction for ice thinning. Figure 5b shows the same data but corrected for surface lowering. Although the thinning correction improves the agreement between measurements and estimates there is still a general tendency for our model to underestimate the thickness of the three glaciers. Some of the disagreement can be attributed to uncertainties in the measurement locations and the thinning correction but one plausible explanation for underestimated ice thickness is that the stress system is more complex than that for an

inclined slab (Equation 2). The simplest approach to correcting for this situation is to in-526 troduce a dimensionless shape factor  $0 < f \le 1$  (e.g., Nye 1964; Cuffey and Paterson 2010) 527 and rewrite the bed stress as  $\tau^* = f \rho g h \sin \theta$  which, reworking (13), leads to a systematic 528 increase in estimated ice thickness by a factor  $F = (1/f)^{n/n+2}$ . Taking n = 3 and assuming 529 f = 0.70, a reasonable value, gives F = 1.24. Multiplying the estimated ice thickness values 530 by this "correction factor" yields an improved fit to the 1:1 line in Figure 5b but we have substantial misgivings about the trustworthiness of this three-glacier performance test and 532 many concerns about applying this as a global correction to a region that contains more than 533 17 000 glaciers. Thus for our thickness estimates we take f = 1 and flag this assumption as 534 a potential source of error. The shape factor is only relevant to the portions of glaciers that 535 flow through confined channels so, for icefields, f=1 is more likely to apply. Furthermore 536 the shape-corrected bed stress is only meant to apply along the central flow axis of confined 537 channels and not near the channel walls. 538

#### b. Ice volume estimates

Finally we apply the ice thickness estimation method that has been described and validated in previous sections to the problem of estimating the ice volume and subglacial topography of all glaciers in the study region. Our ice mask (Fig. 6) represents glacier extent in Alberta and British Columbia from 2005 AD with subregions chosen to match those of Bolch et al. (2010). The DEM for BC and AB is from the Shuttle Radar Topography Mission (SRTM) version 4.1 with 90 m spatial resolution (Farr et al. 2007) and downloaded from http://srtm.csi.cgiar.org/.

For the BC-AB study region we relied mainly on ice masks that were derived from Landsat ETM data and based on scenes captured in 2005 (Bolch et al. 2010). The original masks are in the form of vector graphic polygons but, for present purposes, have been converted to rasterized objects that align with the  $200 \,\mathrm{m} \times 200 \,\mathrm{m}$  cells of our computational grid. The St. Elias (SE) and Northern Coast (NC) subregions required special treatment because the

Bolch et al. (2010) masks are truncated at the British Columbia-Alaska boundary. For ice 552 thickness estimation we require intact ice masses in order to integrate the ice discharge as 553 in Equation 11 so for these subregions we used the same ice masks as Berthier et al. (2010). 554 These masks were extracted from the GLIMS glacier database (Beedle 2006) and are mainly 555 derived from USGS sources but are heterogeneous in terms of the data sources and dates of 556 acquisition. The most serious consequence of this methodological inconsistency is that our 557 calculated ice areas (hence estimated volumes) for the SE and NC subregions differ slightly 558 from those tabulated in Bolch et al. (2010). 559

We model the mass balance fields (Anslow et al. in preparation) using climate fields that 560 have been downscaled from the North American Regional Reanalysis (Mesinger et al. 2006) 561 following a methodology that has been described and validated by Jarosch et al. (2012a). 562 As input DEMs for our downscaling methods, we resample the 90-m SRTM dataset at 1 km 563 for precipitation and 200 m for surface topography and temperature. We do not consider 564 knowledge of the glacier mass balance fields to be an onerous requirement because our main 565 motivation for estimating subglacial topography is to perform computer simulations of the 566 climate-forced deglaciation of our study regions. Mass balance fields are essential for any 567 serious modeling effort, so we would require these in any case. 568

Because few contemporary glaciers are in balance with their climate forcings, we also 569 require estimates of the ice thinning (or thickening) rates. We are obliged to use two different 570 sources for these data. Within British Columbia (BC) the spatial variation of thinning rates 571 is based on the datasets published by Schiefer et al. (2007) and applies to the time interval 1985–1999. These were generated by differencing the SRTM DEM for February 2000 and a 573 ca. 1985 DEM based on aerial photography (Anonymous 1992). We reprojected these data 574 from the native BC Albers projection to the Lambert conical conformal projection used in 575 the NARR and then resampled at 200 m to match our computational grid. For Alberta and 576 those parts of Alaska and Yukon that are contiguous to BC, no suitable DEMs existed for 577 the 1980s so spatial representation of the thinning rate was not possible. For these cells, 578

beyond the limits of the BC data, we applied elevation-dependent thinning rates using data from Fig. 3 of Schiefer et al. (2007).

Downscaled NARR climate fields are used to construct annually-averaged glacier mass 581 balance rates for the study region. The degree of time-averaging that should be applied to 582 these data is not clearcut and is likely to depend on glacier size as well as other factors. 583 A one-year time-average is too short because it is considerably smaller than representative values of the glacier response time. However, in a warming climate, a century-long time average might assign too much weight to the past state of glaciers. This sensitivity of ice 586 volume estimates depends on how the mass balance field is time-averaged (Table 5). We take decadal averages over the time spans 1980–1989, 1990–1999, and 1999–2008 as well as 588 the 29-year average 1980–2008 and denote these time-averaged balance rates by  $\dot{b}_{1980}^{-1989}$ , etc. 589 By repeating the ice thickness inversions for each of the time-averaged forcings, we calculate 590 the sea-level-equivalent (SLE) volume contribution from each of the sub-regions. For this 591 dataset, at least, the differences that result from different time-averaging treatments are 592 small and we conclude that the duration of time-averaging has a minor influence on the 593 estimates. Our preferred result is that for  $\dot{\bar{b}}_{1980}^{2008}$  (the rightmost column in Table 5). 594

We foresee that good estimates of the time-averaged thinning rate fields will not necessar-595 ily be available for all regions where ice thickness estimates are needed. Various treatments 596 of the thinning rate affect the inversion results (Table 6). The different possibilities that 597 were considered are indicated by  $\dot{H}=0$  (thinning rate assumed to vanish),  $\dot{H}=\dot{H}(z)$ (elevation-dependent rate), and  $\dot{H} = \dot{H}(x,y)$  (space-varying rate). The preferred results 599 are those for space-varying rate (two rightmost columns) and match to the preferred result 600 in Table 5. The space-varying thinning rate yields the lowest estimate of SLE volume and 601 the differences between the  $\dot{H}=0$  column the  $\dot{H}=H(x,y)$  column are too large to justify 602 ignoring the thinning rate if this information is available. If a space dependent rate is not 603 known then adopting an empirically-based elevation-dependent rate is preferable to simply 604 ignoring the effect. 605

We also calculate the total number of ice masses (i.e., unique ice masks with no regard to 606 whether they constitute one or more flowsheds) and the total number of delineated flowsheds 607 (Table 6). For gridded data each cell has neighbors to the North, East, South, and West 608 as well as diagonally-situated neighbours to the NE, SE, SW, and NW. Whether one allows 609 diagonal connectivity (C8) or disallows it (C4) influences the results of these calculations. 610 We assume C8 connectivity for ice masses and flowsheds (Table 6). The total ice area for 611 each region is given in column 4 and for most regions closely matches that presented in Bolch 612 et al. (2010); this is not surprising because we used the same ice masks. However our ice 613 areas for the SE and NC regions differ from those of Bolch et al. (2010) because for these 614 regions we use the USGS ice masks that spanned the political boundary between BC and 615 Alaska. 616

We now compare the estimated sea level equivalent from our inversion method to those 617 derived from volume-area scaling (Bahr 1997; Bahr et al. 1997; Radić and Hock 2010). From 618  $V = K(A/A_0)^{\gamma}$  with  $\gamma = 1.375$  and K = 0.036544 km<sup>3</sup> (which with dimensional adjustments 619 corresponds to the  $c=0.2055\,\mathrm{m}^{3-2\gamma}$  adopted by Chen and Ohmura (1990) and Radić and 620 Hock (2010)) the estimated volume using the scaling formula is 6.214 mm SLE (ice volume 621 2470 km<sup>3</sup>). It is interesting that the volume–area scaling method yields ice volumes that are 622 not vastly different from those obtained by our estimation technique. Before error analysis, 623 our best estimate of the present day (ca. 2005) ice volume for glaciers of British Columbia 624 and Alberta is 5.83 mm SLE (ice volume 2320 km<sup>3</sup>). 625

#### 626 c. Error analysis

Table 7 represents an attempt to summarize and quantify the known sources of error.

For temperate ice, the flow law coefficient is uncertain and recent studies cited in Cuffey
and Paterson (2010) (Hubbard et al. 1998; Gudmundsson 1999; Adalgeirsdóttir et al. 2000;
Albrecht et al. 2000; Truffer et al. 2001), in which glacier flow modeling is used to calibrate
the flow law, have led to a substantial revision of  $\mathcal{A}$ . Among these studies there is excellent

agreement and  $\mathcal{A}=2.4\pm0.5\times10^{-24}\,\mathrm{Pa^{-3}\,s^{-1}}$  encloses their spread. We assume that all ice in the study region is temperate so there is no need to consider temperature effects on  $\mathcal{A}$ .

From (34) it is apparent that errors in the flow law coefficient do not strongly affect the thickness estimates. A non-sliding glacier will be thicker than a sliding glacier in the same setting subjected to the same mass balance forcing. Thus our assumption that  $\xi=1$  (no sliding) contributes to an overestimation of ice thickness. In reality  $\xi$  varies from glacier-to-glacier and from point-to-point in any given glacier. Although for parts of some fast-flowing surging glaciers  $\xi < 0.1$ , we suspect that  $\xi \approx 0.8$  is typical of the majority of healthy mountain glaciers; for glaciers in retreat, the sliding contribution is likely to be even smaller. Lastly, (34) indicates that ice thickness estimates are comparatively insensitive to uncertainly in  $\xi$ . We set the default value of the tradeoff parameter to  $\chi_0 = 0.4$  in order to smooth out the estimated bed topography but this also leads to a reduction in estimated thickness. With  $\chi \to 1$  the average estimated thickness is maximized but the exaggeration of bed topography is unacceptable and could pose problems when used as the substrate geometry for ice dynamics modeling. By rerunning the inversion model for a range of  $\chi_0$  values we conclude that for  $\chi_0 = 0.4$  an overestimate of ice volume is unlikely and that underestimation should not exceed 5% (0.3 mm SLE).

Other potential sources of systematic error are associated with suspected errors in the ice masks for the St. Elias and Northern Coast subregions and with the physical assumptions of the inversion model. As previously discussed, the ice mask areas for the SE and NC subregions differ slightly from than those calculated by Bolch et al. (2010) and for which his estimated error is small. If one accepts the Bolch et al. values as correct then the ice volume for these subregions, taken together, could be underestimated by as much as 0.1 mm SLE.

The modeling assumptions that warrant scrutiny are (i) that  $\tau^* = \rho g h \sin \theta$  provides an acceptable approximation to the bottom stress irrespective of proximity to valley walls, and (ii) that  $\overline{\tau}_{\alpha}$  calculated using (16) yields a useful estimate of  $\tau^*$ . We view this as the weakest link of the inversion procedure and one that could lead to underestimates of ice thickness

and thus of total ice volume. The magnitude of this underestimate might be as large as

1.5 mm SLE.

For sources of systematic error that would lead to an overestimate of ice volume (Table 661 7) errors total to 0.6 mm SLE; for sources that would lead to an underestimate the total 662 is 2.2 mm SLE. However, it is highly unlikely that the combined systematic errors would 663 conspire to produce either of these extrema but deciding how best to combine systematic and random error contributions is a subjective task. For each source of systematic error 665 we shall postulate a form for the error distribution function and use the lower and upper 666 range estimates to guide our assignment of the mean value and standard deviation for each distribution. Thus, for the flow law coefficient  $\mathcal{A}$  the error is assumed to be Gaussian 668 distributed with zero mean and standard deviation of  $\sigma = 0.3 \,\mathrm{mm}$ . The remaining sources 669 of systematic error are either all-negative (e.g.,  $\xi$  errors) or all-positive (e.g., model physics 670 and shape factor f) and we approximate these by exponential distributions. A convenient 671 property of exponential distributions is that the magnitudes of the mean and standard 672 deviation are identical. The range limits in Table 7 are intended to indicate extreme limits 673 of the individual distribution functions so we shall associate the magnitudes of the range 674 limits with the  $3\sigma$  values of the exponential distribution. The sign of the limit determines 675 whether the exponential function is left- or right-sided. The remaining errors are random 676 and assumed to be Gaussian distributed with zero mean and standard deviations given by 677 the range values. Thus, for example, the standard deviation of the DEM elevation error is  $\sigma = 0.001 \,\mathrm{mm}\,\mathrm{SLE}$ . A Monte-Carlo procedure (with  $N = 100\,000$ ) was then followed 679 to generate a statistical dataset formed by summing the random contributions from each 680 error term and the mean and standard deviation were then calculated for the combined 681 dataset. The mean value of the combined error is 0.54 mm and its standard deviation is 682 0.55 mm. Thus we conclude that when random and systematic errors are taken into account 683 the estimated ice volume is  $6.3 \pm 0.6 \,\mathrm{mm} \,\mathrm{SLE}$  or  $2530 \pm 220 \,\mathrm{km}^3$ . (It is a simple matter to 684 convert between glacier ice volume and the equivalent sea-level rise in Table 7. Taking the 685

ocean area as  $3.62 \times 10^8$  km<sup>3</sup> (Lemke et al. 2007) with  $\rho = 910$  kg m<sup>-3</sup> and  $\rho_w = 1000$  kg m<sup>-3</sup> the conversion relations are  $1 \text{ km}^3$  ice =  $2.51 \mu \text{m}$  SLE and 1 mm SLE =  $398 \text{ km}^3$  ice.)

## <sup>88</sup> 7. Discussion and conclusions

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Scientific interest in the thickness of glaciers (e.g., Agassiz 1847) preceded, by almost 689 a century, the advent of geophysical instruments capable of measuring this quantity. Re-690 cent interest has focussed on ice volume and the potential contribution to sea level rise. 691 Volume-area scaling (Chen and Ohmura 1990; Bahr 1997; Bahr et al. 1997; Radić and Hock 692 2010) was a first response to the problem of estimating the volume of Earth's mountain 693 glaciers and has the attraction of involving a readily observable quantity (area) as its sole 694 input. Our estimates of ice volume (Table 6) show good agreement with those based on 695 volume—area scaling. We suspect that, in part, this is fortuitous but both methods start 696 from similar physical assumptions so the result is not altogether surprising. Whatever the 697 merits of estimating ice volume using volume—area scaling, the method has limited usefulness 698 for estimating the map of bed topography lying beneath the surface of glaciers – essential 699 information for using computational ice dynamics models to project the future volume and 700 extent of Earth's mountain glaciers. However, the use of geophysical inversion methods to 701 estimate bed topography has its own pitfalls. As emphasized by Bahr et al. (1994) the 702 problem of calculating the basal stress from boundary conditions imposed at the ice surface 703 yields a boundary-value problem that is ill-posed and unstable, causing surface errors to 704 increase exponentially as depth increases. 705 706

In our study we have described an approach to estimating ice thickness that is based on simplified glacier physics and on mass balance accounting applied to automatically delineated glacier flowsheds. By framing the question as a geophysical inversion problem, smoothness can be controlled using a space-varying tradeoff parameter rather than applied separately at some later stage. The method performs best when glaciers are near equilibrium with a steady

climate. Tests on synthetically-generated ice cover indicate a tendency for ice thickness to be overestimated when climate is varying, irrespective of whether this leads to glacier growth or to shrinkage. Applying the method to the mountain glaciers of the Canadian Cordillera yields a DEM of the subglacial topography and new estimates of ice volume for this region.

Our best estimate of the ice volume is  $2530 \pm 220 \,\mathrm{km}^3$ , equivalent to  $6.3 \pm 0.6 \,\mathrm{mm}$  of sea-level rise.

We see many areas where future improvements are called for. Accurate DEMs and ice
masks are an essential starting point. Development of reliable algorithms for delineating
glacier flowsheds should be viewed as a high priority. More challenging will be to remove
the reliance on simple stress assumptions and to reframe the question as a nonlinear inverse problem. This will require substantial ingenuity combined with abundant computing
resources. Without better knowledge of the mass balance fields this level of complexity is
not yet warranted.

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## List of Tables

| 876 | 1 | Input and derived properties of steady-state glacier test models. $d\dot{b}^-/dz$ =elevation  | on |
|-----|---|---|----|
| 877 |   | gradient of mass balance rate in the ablation zone; $\mathrm{d}\dot{b}^+/\mathrm{d}z=$ elevation gradient   |    |
| 878 |   | of mass balance rate in the accumulation zone; $\alpha_{\rm I}=$ fractional area of ice cover.  | 41 |
| 879 | 2 | Summary of estimation errors in performance tests of steady-state models.   |    |
| 880 |   | Model averages are calculated for ice-covered cells and not the entire map.   | 42 |
| 881 | 3 | Summary of estimation errors in performance tests of transient models having  |    |
| 882 |   | temporally decreasing ice-cover. Model averages are calculated for ice-covered  |    |
| 883 |   | cells and not the entire map.   | 43 |
| 884 | 4 | Summary of estimation errors in performance tests of transient models having  |    |
| 885 |   | temporally increasing ice-cover. Model averages are calculated for ice-covered  |    |
| 886 |   | cells and not the entire map.   | 44 |
| 887 | 5 | Sensitivity of ice volume estimates to changes in mass balance field. From  |    |
| 888 |   | downscaled mass balance rates fields $\dot{b}(x,y,t)$ we construct the time aver-   |    |
| 889 |   | ages $\dot{b}_{1980}^{-2008}$ , $\dot{b}_{1980}^{-1989}$ , $\dot{b}_{1990}^{-1999}$ , and $\dot{b}_{1999}^{-2008}$ and compare their effect on ice volume es- |    |
| 890 |   | timates. Ocean area is taken as $3.62 \times 10^8  \mathrm{km^2}$ with $\rho = 910  \mathrm{kg  m^{-3}}$ , and  |    |
| 891 |   | $\rho_{\rm w} = 1000  {\rm kg  m^{-3}}.$  | 45 |
| 892 | 6 | Summary of ice volume estimates for glaciers of western Canada. The $\dot{b}_{1980}^{-2008}$  |    |
| 893 |   | mass balance rate fields in combination with three different thinning rate  |    |
| 894 |   | models: $\dot{H}$ =0 (no thinning), $\dot{H}$ = $\dot{H}(z)$ (elevation-dependent thinning), and  |    |
| 895 |   | $\dot{H}{=}\dot{H}(x,y)$ (spatially-varying thinning). Ocean area is taken as $3.62\times10^8\mathrm{km}^2$   |    |
| 896 |   | with $\rho = 910 \mathrm{kg} \mathrm{m}^{-3}$ , and $\rho_{\mathrm{w}} = 1000 \mathrm{kg} \mathrm{m}^{-3}$ .  | 46 |

Summary of sources of error and estimates of error magnitude. Ocean area is taken as  $3.62 \times 10^8 \,\mathrm{km^2}$  with  $\rho = 910 \,\mathrm{kg} \,\mathrm{m^{-3}}$ , and  $\rho_\mathrm{w} = 1000 \,\mathrm{kg} \,\mathrm{m^{-3}}$ . Thus  $1 \,\mathrm{km^3}$  ice volume corresponds to  $2.51 \,\mu\mathrm{m}$  of sea-level rise and  $1 \,\mathrm{mm} \,\mathrm{SLE}$  corresponds to  $398 \,\mathrm{km^3}$  ice volume. For the error estimates the total area of ice cover is taken as  $26586 \,\mathrm{km^2}$  (the  $2005 \,\mathrm{value}$  from Table 6) and the total ice volume as  $5.8 \,\mathrm{mm} \,\mathrm{SLE}$  (from Table 5).

Table 1. Input and derived properties of steady-state glacier test models.  $d\dot{b}^-/dz$ =elevation gradient of mass balance rate in the ablation zone;  $d\dot{b}^+/dz$ =elevation gradient of mass balance rate in the accumulation zone;  $\alpha_{\rm I}$ =fractional area of ice cover.

| Model name        | ELA  | $\mathrm{d}\dot{b}^-/\mathrm{d}z$ | $\mathrm{d}\dot{b}^+/\mathrm{d}z$ | $lpha_{ m I}$ | Ice volume        |
|-------------------|------|-----------------------------------|-----------------------------------|---------------|-------------------|
|                   | (m)  | $(yr^{-1})$                       | $(yr^{-1})$                       | (%)           | $(\mathrm{km}^3)$ |
| BC1·1550L         | 1550 | 0.0002                            | 0.0001                            | 8.77          | 20.11             |
| $BC1 \cdot 1600L$ | 1600 | 0.0002                            | 0.0001                            | 4.92          | 9.58              |
| $BC1 \cdot 1650L$ | 1650 | 0.0002                            | 0.0001                            | 2.50          | 3.82              |
| $BC1 \cdot 1700L$ | 1700 | 0.0002                            | 0.0001                            | 1.07          | 1.34              |
| $BC1 \cdot 1550H$ | 1550 | 0.0020                            | 0.0010                            | 13.37         | 71.82             |
| BC1·1600H         | 1600 | 0.0020                            | 0.0010                            | 6.24          | 23.28             |
| $BC1 \cdot 1650H$ | 1650 | 0.0020                            | 0.0010                            | 3.11          | 9.13              |
| BC1·1700H         | 1700 | 0.0020                            | 0.0010                            | 1.25          | 2.77              |
| BC1 average       | _    | _                                 | _                                 | 5.15          | 17.73             |
| BC2·1650L         | 1650 | 0.0002                            | 0.0001                            | 25.86         | 56.96             |
| $BC2 \cdot 1700L$ | 1700 | 0.0002                            | 0.0001                            | 18.07         | 28.06             |
| $BC2 \cdot 1800L$ | 1800 | 0.0002                            | 0.0001                            | 7.78          | 8.15              |
| $BC2 \cdot 1900L$ | 1900 | 0.0002                            | 0.0001                            | 2.60          | 2.26              |
| $BC2 \cdot 1650H$ | 1650 | 0.0020                            | 0.0010                            | 31.00         | 331.16            |
| BC2·1700H         | 1700 | 0.0020                            | 0.0010                            | 22.17         | 97.71             |
| BC2·1800H         | 1800 | 0.0020                            | 0.0010                            | 8.44          | 15.63             |
| BC2·1900H         | 1900 | 0.0020                            | 0.0010                            | 2.74          | 3.84              |
| BC2 average       | _    | _                                 | _                                 | 14.83         | 67.97             |
| BC3·1650L         | 1650 | 0.0002                            | 0.0001                            | 19.22         | 39.77             |
| $BC3 \cdot 1700L$ | 1700 | 0.0002                            | 0.0001                            | 13.05         | 21.14             |
| BC3·1800L         | 1800 | 0.0002                            | 0.0001                            | 5.00          | 5.51              |
| $BC3 \cdot 1850L$ | 1850 | 0.0002                            | 0.0001                            | 2.75          | 2.74              |
| BC3·1650H         | 1650 | 0.0020                            | 0.0010                            | 37.85         | 407.53            |
| BC3·1700H         | 1700 | 0.0020                            | 0.0010                            | 15.26         | 53.68             |
| BC3·1800H         | 1800 | 0.0020                            | 0.0010                            | 5.57          | 10.72             |
| BC3·1850H         | 1850 | 0.0020                            | 0.0010                            | 2.96          | 4.80              |
| BC3 average       | _    | _                                 | _                                 | 12.71         | 68.24             |
| YT1·1650L         | 1650 | 0.0002                            | 0.0001                            | 19.01         | 31.35             |
| $YT1 \cdot 1700L$ | 1700 | 0.0002                            | 0.0001                            | 12.26         | 17.68             |
| $YT1 \cdot 1800L$ | 1800 | 0.0002                            | 0.0001                            | 4.25          | 4.98              |
| $YT1 \cdot 1900L$ | 1900 | 0.0002                            | 0.0001                            | 1.06          | 0.99              |
| $YT1 \cdot 1650H$ | 1650 | 0.0020                            | 0.0010                            | 22.03         | 72.03             |
| $YT1 \cdot 1700H$ | 1700 | 0.0020                            | 0.0010                            | 13.78         | 34.80             |
| $YT1 \cdot 1800H$ | 1800 | 0.0020                            | 0.0010                            | 4.65          | 9.05              |
| $YT1 \cdot 1900H$ | 1900 | 0.0020                            | 0.0010                            | 1.12          | 1.68              |
| YT1 average       |      | <u> </u>                          | <u> </u>                          | 9.77          | 21.57             |

Table 2. Summary of estimation errors in performance tests of steady-state models. Model averages are calculated for ice-covered cells and not the entire map.

| Model name        | Ice<br>volume     | Mean<br>thickness         | Correlation coefficient | Mean error                                      | SD       | Volume error            |
|-------------------|-------------------|---------------------------|-------------------------|---|----------|-------------------------|
|                   |                   | $\langle H_{i,j} \rangle$ | r                       | $\langle \widetilde{H}_{i,j} - H_{i,j} \rangle$ | $\sigma$ | $(\widetilde{V} - V)/V$ |
|                   | $(\mathrm{km}^3)$ | (m)                       |                         | (m)   | (m)      | (%)                     |
| BC1·1550L         | 20.11             | 46.79                     | 0.8930                  | 1.54  | 16.65    | 3.30                    |
| BC1·1600L         | 9.58              | 39.68                     | 0.8830                  | -0.36   | 14.13    | -0.90                   |
| $BC1 \cdot 1650L$ | 3.82              | 31.18                     | 0.8050                  | -2.14   | 11.43    | -6.88                   |
| $BC1 \cdot 1700L$ | 1.34              | 25.72                     | 0.6176                  | -3.95   | 10.67    | -15.37                  |
| BC1·1550H         | 71.82             | 109.61                    | 0.9347                  | -0.35   | 24.90    | -0.32                   |
| BC1·1600H         | 23.28             | 76.15                     | 0.9070                  | 0.92  | 24.18    | 1.20                    |
| BC1·1650H         | 9.13              | 59.87                     | 0.8702                  | -1.02   | 19.99    | -1.70                   |
| BC1·1700H         | 2.77              | 45.26                     | 0.7781                  | -4.35   | 16.36    | -9.61                   |
| BC2·1650L         | 56.96             | 44.95                     | 0.9134                  | 8.94  | 27.62    | 19.89                   |
| $BC2 \cdot 1700L$ | 28.06             | 31.69                     | 0.8676                  | 2.19  | 16.56    | 6.92                    |
| BC2·1800L         | 8.15              | 21.36                     | 0.6569                  | -1.49   | 11.35    | -7.00                   |
| BC2·1900L         | 2.26              | 17.69                     | 0.2438                  | -3.88   | 8.99     | -21.95                  |
| $BC2 \cdot 1650H$ | 331.16            | 218.01                    | 0.8525                  | -61.72  | 104.62   | -28.31                  |
| BC2·1700H         | 97.71             | 89.94                     | 0.9194                  | 19.70   | 51.03    | 21.90                   |
| BC2·1800H         | 15.63             | 37.78                     | 0.8181                  | -0.38   | 18.68    | -1.01                   |
| BC2·1900H         | 3.84              | 28.61                     | 0.3936                  | -5.74   | 13.59    | -20.05                  |
| BC3·1650L         | 39.77             | 42.22                     | 0.9152                  | 5.34  | 20.81    | 12.66                   |
| BC3·1700L         | 21.14             | 33.06                     | 0.8698                  | 2.28  | 17.05    | 6.90                    |
| BC3·1800L         | 5.51              | 22.50                     | 0.5390                  | -3.15   | 10.62    | -13.99                  |
| BC3·1850L         | 2.74              | 20.28                     | 0.3451                  | -3.96   | 9.89     | -19.55                  |
| BC3·1650H         | 407.53            | 219.75                    | 0.8300                  | 5.60  | 92.31    | 2.55                    |
| BC3·1700H         | 53.68             | 71.76                     | 0.9346                  | 12.16   | 36.02    | 16.95                   |
| BC3·1800H         | 10.72             | 39.24                     | 0.7350                  | -3.49   | 16.75    | -8.90                   |
| BC3·1850H         | 4.80              | 33.14                     | 0.4364                  | -6.11   | 14.39    | -18.43                  |
| YT1·1650L         | 31.35             | 33.65                     | 0.8067                  | 2.41  | 16.37    | 7.16                    |
| $YT1 \cdot 1700L$ | 17.68             | 29.44                     | 0.7590                  | 0.25  | 14.25    | 0.85                    |
| YT1.1800L         | 4.98              | 23.92                     | 0.6058                  | -1.91   | 11.60    | -7.97                   |
| $YT1 \cdot 1900L$ | 0.99              | 19.09                     | 0.2842                  | -3.73   | 8.71     | -19.54                  |
| $YT1 \cdot 1650H$ | 72.03             | 66.73                     | 0.9005                  | 8.25  | 28.84    | 12.36                   |
| $YT1 \cdot 1700H$ | 34.80             | 51.55                     | 0.8256                  | 2.27  | 23.29    | 4.40                    |
| YT1.1800H         | 9.05              | 39.72                     | 0.7114                  | -2.36   | 17.49    | -5.94                   |
| YT1·1900H         | 1.68              | 30.62                     | 0.3508                  | -5.97   | 13.01    | -19.49                  |
| Ensemble mean     | 43.83             | 53.16                     | 0.7251                  | -1.38   | 23.19    | -3.43                   |
| Ensemble median   | 13.15             | 38.51                     | 0.8124                  | -0.70   | 16.60    | -1.35                   |

Table 3. Summary of estimation errors in performance tests of transient models having temporally decreasing ice-cover. Model averages are calculated for ice-covered cells and not the entire map.

| Model name                            | Ice<br>volume | Mean<br>thickness         | Correlation coefficient | Mean error                                      | SD       | Volume error            |
|---------------------------------------|---------------|---------------------------|-------------------------|---|----------|-------------------------|
|                                       |               | $\langle H_{i,j} \rangle$ | r                       | $\langle \widetilde{H}_{i,j} - H_{i,j} \rangle$ | $\sigma$ | $(\widetilde{V} - V)/V$ |
|                                       | $(km^3)$      | (m)                       |                         | (m)   | (m)      | (%)                     |
| BC1·1550±100L↓                        | 17.36         | 36.26                     | 0.8853                  | 5.54  | 17.11    | 15.29                   |
| BC1·1600±100L↓                        | 7.92          | 32.08                     | 0.8887                  | 2.33  | 13.08    | 7.25                    |
| $BC1 \cdot 1650 \pm 100L \downarrow$  | 2.93          | 22.53                     | 0.8383                  | 1.07  | 10.25    | 4.76                    |
| BC1·1700±100L↓                        | 0.99          | 15.82                     | 0.7355                  | 1.74  | 9.49     | 10.98                   |
| $BC1 \cdot 1550 \pm 100 H \downarrow$ | 42.47         | 78.14                     | 0.9307                  | 6.20  | 24.45    | 7.94                    |
| BC1·1600±100H↓                        | 13.57         | 55.82                     | 0.9060                  | 7.74  | 23.26    | 13.86                   |
| BC1·1650±100H↓                        | 3.47          | 35.03                     | 0.8560                  | 3.11  | 15.75    | 8.87                    |
| $BC1 \cdot 1700 \pm 100 H \downarrow$ | 0.86          | 22.18                     | 0.8120                  | 3.67  | 12.15    | 16.54                   |
| BC2·1650±100L↓                        | 50.71         | 39.28                     | 0.9168                  | 10.32   | 26.85    | 26.27                   |
| $BC2 \cdot 1700 \pm 100 L\downarrow$  | 24.24         | 26.38                     | 0.8755                  | 4.19  | 15.21    | 15.88                   |
| $BC2 \cdot 1800 \pm 100 L\downarrow$  | 6.61          | 15.83                     | 0.7305                  | 1.60  | 9.52     | 10.09                   |
| $BC2 \cdot 1900 \pm 100 L\downarrow$  | 1.68          | 10.87                     | 0.5713                  | 1.46  | 7.38     | 13.42                   |
| $BC2 \cdot 1650 \pm 100 H \downarrow$ | 198.64        | 133.17                    | 0.8747                  | 16.02   | 70.12    | 12.03                   |
| $BC2 \cdot 1700 \pm 100 H \downarrow$ | 69.71         | 77.88                     | 0.9195                  | 12.75   | 41.97    | 16.38                   |
| $BC2 \cdot 1800 \pm 100 H \downarrow$ | 17.95         | 30.73                     | 0.8734                  | 6.32  | 15.35    | 20.57                   |
| BC2·1900±100H↓                        | 4.44          | 19.78                     | 0.6842                  | 3.44  | 9.70     | 17.37                   |
| $BC3 \cdot 1650 \pm 100 L\downarrow$  | 35.46         | 35.09                     | 0.9177                  | 8.62  | 21.18    | 24.56                   |
| $BC3\cdot1700\pm100L\downarrow$       | 18.15         | 27.69                     | 0.8674                  | 3.98  | 15.64    | 14.39                   |
| BC3·1800±100L↓                        | 4.40          | 16.51                     | 0.6608                  | 0.39  | 9.32     | 2.39                    |
| $BC3 \cdot 1850 \pm 100L\downarrow$   | 0.98          | 11.76                     | 0.5801                  | 0.48  | 7.76     | 4.04                    |
| $BC3 \cdot 1650 \pm 100 H \downarrow$ | 329.59        | 201.23                    | 0.8366                  | -7.64   | 90.13    | -3.80                   |
| $BC3 \cdot 1700 \pm 100 H \downarrow$ | 33.98         | 57.77                     | 0.9212                  | 12.73   | 33.14    | 22.04                   |
| BC3·1800±100H↓                        | 11.68         | 29.62                     | 0.8035                  | 4.54  | 12.38    | 15.31                   |
| BC3·1850±100H↓                        | 2.73          | 20.96                     | 0.6563                  | 2.42  | 9.65     | 11.54                   |
| YT1·1650±100L↓                        | 27.27         | 28.41                     | 0.8220                  | 3.88  | 14.73    | 13.67                   |
| $YT1 \cdot 1700 \pm 100L \downarrow$  | 14.97         | 23.66                     | 0.7501                  | 3.10  | 13.87    | 13.09                   |
| YT1·1800±100L↓                        | 3.83          | 16.08                     | 0.6365                  | 3.46  | 11.48    | 21.52                   |
| $YT1 \cdot 1900 \pm 100L \downarrow$  | 0.77          | 12.77                     | 0.5342                  | 0.98  | 7.87     | 7.70                    |
| $YT1.1650\pm100H$                     | 78.51         | 59.68                     | 0.9074                  | 13.53   | 28.21    | 22.68                   |
| $YT1 \cdot 1700 \pm 100H \downarrow$  | 38.92         | 43.97                     | 0.8599                  | 8.68  | 20.67    | 19.75                   |
| YT1·1800±100H↓                        | 3.86          | 23.15                     | 0.7426                  | 6.52  | 14.10    | 28.14                   |
| YT1·1900±100H↓                        | 2.02          | 21.61                     | 0.7040                  | 3.46  | 9.00     | 16.02                   |
| Ensemble mean                         | 33.41         | 40.05                     | 0.7968                  | 4.89  | 20.02    | 14.08                   |
| Ensemble median                       | 12.55         | 28.05                     | 0.8375                  | 3.77  | 14.41    | 14.12                   |

Table 4. Summary of estimation errors in performance tests of transient models having temporally increasing ice-cover. Model averages are calculated for ice-covered cells and not the entire map.

| Model name                         | Ice<br>volume | Mean<br>thickness         | Correlation coefficient | Mean error                                      | SD       | Volume error            |
|------------------------------------|---------------|---------------------------|-------------------------|---|----------|-------------------------|
|                                    |               | $\langle H_{i,j} \rangle$ | r                       | $\langle \widetilde{H}_{i,j} - H_{i,j} \rangle$ | $\sigma$ | $(\widetilde{V} - V)/V$ |
|                                    | $(km^3)$      | (m)                       |                         | (m)   | (m)      | (%)                     |
| BC1·1550±100L↑                     | 19.05         | 35.47                     | 0.8998                  | 6.31  | 15.27    | 17.79                   |
| BC1·1600±100L↑                     | 8.98          | 27.63                     | 0.8790                  | 7.07  | 13.69    | 25.58                   |
| BC1·1650±100L↑                     | 3.49          | 18.77                     | 0.8500                  | 6.25  | 10.57    | 33.30                   |
| BC1·1700±100L↑                     | 1.23          | 14.88                     | 0.7787                  | 5.22  | 9.41     | 35.09                   |
| BC1·1550±100H↑                     | 57.55         | 80.98                     | 0.9348                  | 7.75  | 24.98    | 9.58                    |
| BC1·1600±100H↑                     | 22.52         | 55.85                     | 0.9112                  | 8.70  | 23.21    | 15.58                   |
| BC1·1650±100H↑                     | 8.24          | 35.46                     | 0.8874                  | 7.41  | 16.17    | 20.90                   |
| BC1·1700±100H↑                     | 3.57          | 27.39                     | 0.8524                  | 6.07  | 12.76    | 22.15                   |
| BC2·1650±100L↑                     | 55.78         | 37.79                     | 0.9076                  | 9.39  | 24.15    | 24.84                   |
| BC2·1700±100L↑                     | 27.93         | 25.37                     | 0.8703                  | 5.83  | 14.35    | 22.99                   |
| BC2·1800±100L↑                     | 8.32          | 14.70                     | 0.7398                  | 4.83  | 10.08    | 32.84                   |
| BC2·1900±100L↑                     | 2.36          | 10.08                     | 0.6581                  | 4.94  | 7.62     | 48.95                   |
| $BC2 \cdot 1650 \pm 100 H\uparrow$ | 247.99        | 130.30                    | 0.9225                  | 2.91  | 53.79    | 2.23                    |
| $BC2 \cdot 1700 \pm 100 H\uparrow$ | 104.98        | 76.58                     | 0.9313                  | 15.46   | 39.55    | 20.18                   |
| $BC2 \cdot 1800 \pm 100 H\uparrow$ | 18.67         | 28.08                     | 0.8210                  | 6.10  | 15.04    | 21.72                   |
| BC2·1900±100H↑                     | 6.60          | 21.33                     | 0.7012                  | 4.73  | 11.92    | 22.17                   |
| BC3·1650±100L↑                     | 39.21         | 35.66                     | 0.9164                  | 8.29  | 18.51    | 23.25                   |
| BC3·1700±100L↑                     | 20.99         | 26.53                     | 0.8623                  | 6.57  | 15.23    | 24.78                   |
| BC3·1800±100L↑                     | 5.50          | 14.48                     | 0.6264                  | 5.04  | 10.99    | 34.83                   |
| $BC3.1850\pm100L\uparrow$          | 1.35          | 10.61                     | 0.6722                  | 4.45  | 7.86     | 41.96                   |
| $BC3 \cdot 1650 \pm 100 H\uparrow$ | 391.95        | 199.43                    | 0.8863                  | 8.61  | 78.38    | 4.32                    |
| $BC3 \cdot 1700 \pm 100 H\uparrow$ | 58.13         | 59.27                     | 0.9349                  | 10.99   | 27.09    | 18.55                   |
| BC3·1800±100H↑                     | 11.68         | 26.46                     | 0.7487                  | 5.98  | 14.43    | 22.59                   |
| BC3·1850±100H↑                     | 3.72          | 20.13                     | 0.7012                  | 4.63  | 11.71    | 23.00                   |
| $YT1 \cdot 1650 \pm 100 L\uparrow$ | 31.35         | 27.35                     | 0.8052                  | 7.51  | 15.65    | 27.47                   |
| $YT1 \cdot 1700 \pm 100L\uparrow$  | 17.72         | 22.79                     | 0.7444                  | 7.15  | 14.77    | 31.37                   |
| YT1·1800±100L↑                     | 4.85          | 14.31                     | 0.6825                  | 7.77  | 11.48    | 54.35                   |
| YT1·1900±100L↑                     | 1.05          | 9.87                      | 0.5239                  | 6.80  | 9.68     | 68.88                   |
| $YT1.1650\pm100H\uparrow$          | 77.52         | 55.85                     | 0.8988                  | 11.49   | 25.66    | 20.57                   |
| $YT1 \cdot 1700 \pm 100H\uparrow$  | 40.86         | 41.23                     | 0.8336                  | 9.13  | 20.86    | 22.14                   |
| YT1·1800±100H↑                     | 11.89         | 27.76                     | 0.7814                  | 7.36  | 16.17    | 26.52                   |
| YT1·1900±100H↑                     | 2.84          | 18.25                     | 0.5329                  | 8.28  | 16.40    | 45.38                   |
| Ensemble mean                      | 41.13         | 39.08                     | 0.7904                  | 7.16  | 19.29    | 27.06                   |
| Ensemble median                    | 14.75         | 27.37                     | 0.8337                  | 6.94  | 15.13    | 23.12                   |

Table 5. Sensitivity of ice volume estimates to changes in mass balance field. From down-scaled mass balance rates fields  $\dot{b}(x,y,t)$  we construct the time averages  $\dot{b}_{1980}^{-2008}$ ,  $\dot{b}_{1980}^{-1989}$ ,  $\dot{b}_{1990}^{-1999}$ , and  $\dot{b}_{1999}^{-2008}$  and compare their effect on ice volume estimates. Ocean area is taken as  $3.62\times10^8$  km<sup>2</sup> with  $\rho=910$  kg m<sup>-3</sup>, and  $\rho_{\rm w}=1000$  kg m<sup>-3</sup>.

| Region name       | Code                | SLE Volume                         |                                    |                               |                               |  |
|-------------------|---------------------|------------------------------------|------------------------------------|-------------------------------|-------------------------------|--|
|                   | ID                  | $\dot{\bar{b}}_{1980}^{1989}$ (mm) | $\dot{\bar{b}}_{1990}^{1999}$ (mm) | $\dot{b}_{1999}^{-2008}$ (mm) | $\dot{b}_{1980}^{-2008}$ (mm) |  |
| St. Elias         | SE                  | 0.811                              | 0.814                              | 0.805                         | 0.807                         |  |
| Northern Coast    | NC                  | 2.868                              | 2.895                              | 2.842                         | 2.866                         |  |
| Central Coast     | CC                  | 0.184                              | 0.184                              | 0.183                         | 0.184                         |  |
| Southern Coast    | SC                  | 1.334                              | 1.338                              | 1.320                         | 1.332                         |  |
| Vancouver Island  | VI                  | 0.001                              | 0.001                              | 0.001                         | 0.001                         |  |
| Northern Interior | NI                  | 0.063                              | 0.063                              | 0.063                         | 0.063                         |  |
| Southern Interior | SI                  | 0.250                              | 0.250                              | 0.248                         | 0.250                         |  |
| Northern Rockies  | NR                  | 0.053                              | 0.053                              | 0.052                         | 0.053                         |  |
| Central Rockies   | $\operatorname{CR}$ | 0.064                              | 0.064                              | 0.064                         | 0.064                         |  |
| Southern Rockies  | SR                  | 0.209                              | 0.207                              | 0.205                         | 0.207                         |  |
| Totals            |                     | 5.837                              | 5.868                              | 5.783                         | 5.826                         |  |

Table 6. Summary of ice volume estimates for glaciers of western Canada. The  $\dot{b}_{1980}^{-2008}$  mass balance rate fields in combination with three different thinning rate models:  $\dot{H}$ =0 (no thinning),  $\dot{H}$ = $\dot{H}(z)$  (elevation-dependent thinning), and  $\dot{H}$ = $\dot{H}(x,y)$  (spatially-varying thinning). Ocean area is taken as  $3.62 \times 10^8 \, \mathrm{km}^2$  with  $\rho = 910 \, \mathrm{kg \, m}^{-3}$ , and  $\rho_{\mathrm{w}} = 1000 \, \mathrm{kg \, m}^{-3}$ .

| Region name       | Code                | Number of  | Number of | Ice area          | Ice volume (SLE) |             |                        |                           | Ice volume                |
|-------------------|---------------------|------------|-----------|-------------------|------------------|-------------|------------------------|---------------------------|---------------------------|
|                   | ID                  | ice masses | flowsheds |                   | Scaling          | $\dot{H}=0$ | $\dot{H} = \dot{H}(z)$ | $\dot{H} = \dot{H}(x, y)$ | $\dot{H} = \dot{H}(x, y)$ |
|                   |                     | (C8)       | (C8)      | $(\mathrm{km}^2)$ | (mm)             | (mm)        | (mm)                   | (mm)                      | $(km^3)$                  |
| St. Elias         | SE                  | 76         | 890       | 2816.6            | 0.779            | 0.889       | 0.758                  | 0.807                     | 320.8                     |
| Northern Coast    | NC                  | 1124       | 4544      | 10290.2           | 3.018            | 3.961       | 3.425                  | 2.866                     | 1140.1                    |
| Central Coast     | CC                  | 1611       | 3200      | 1648.7            | 0.169            | 0.181       | 0.178                  | 0.184                     | 73.0                      |
| Southern Coast    | SC                  | 1820       | 5539      | 7159.1            | 1.585            | 1.658       | 1.492                  | 1.332                     | 529.9                     |
| Vancouver Island  | VI                  | 50         | 56        | 12.8              | 0.001            | 0.001       | 0.001                  | 0.001                     | 0.4                       |
| Northern Interior | NI                  | 709        | 1109      | 557.7             | 0.063            | 0.065       | 0.063                  | 0.063                     | 25.1                      |
| Southern Interior | SI                  | 1131       | 2484      | 1933.9            | 0.257            | 0.272       | 0.260                  | 0.250                     | 99.5                      |
| Northern Rockies  | NR                  | 325        | 575       | 422.0             | 0.050            | 0.051       | 0.045                  | 0.053                     | 20.9                      |
| Central Rockies   | $\operatorname{CR}$ | 261        | 494       | 415.5             | 0.060            | 0.067       | 0.066                  | 0.064                     | 25.4                      |
| Southern Rockies  | SR                  | 799        | 1413      | 1329.0            | 0.232            | 0.232       | 0.218                  | 0.207                     | 82.5                      |
| Totals            |                     | 7906       | 20304     | 26585.5           | 6.214            | 7.378       | 6.506                  | 5.826                     | 2317.7                    |

Table 7. Summary of sources of error and estimates of error magnitude. Ocean area is taken as  $3.62 \times 10^8 \,\mathrm{km^2}$  with  $\rho = 910 \,\mathrm{kg \,m^{-3}}$ , and  $\rho_\mathrm{w} = 1000 \,\mathrm{kg \,m^{-3}}$ . Thus  $1 \,\mathrm{km^3}$  ice volume corresponds to  $2.51 \,\mu\mathrm{m}$  of sea-level rise and  $1 \,\mathrm{mm \, SLE}$  corresponds to  $398 \,\mathrm{km^3}$  ice volume. For the error estimates the total area of ice cover is taken as  $26586 \,\mathrm{km^2}$  (the 2005 value from Table 6) and the total ice volume as  $5.8 \,\mathrm{mm \, SLE}$  (from Table 5).

| Error source   | Comments  | Error ran | ge (mm SL |
|--|---|-----------|-----------|
|  |   | Lower     | Upper     |
| Potential systematic errors  |   |           |           |
| Ice flow law coefficient, $\mathcal{A}$                                  | We assume that the flow law coefficient is $A=2.4\pm0.5\times10^{-24}\mathrm{Pa^{-3}s^{-1}}$ and apply Equation 20 to obtain a fractional volume error of $\pm4.5\%$ .  | -0.3      | +0.3      |
| Flow partitioning, $\xi$   | We assume $\xi=1$ (no sliding), an upper limit on $\xi$ that would overestimate ice volume. Applying Equation 20, the likely volume error is less than 5%.  | -0.3      | 0         |
| Shallow ice approximation and shape factor, $f$                          | We take $f=1$ which is an upper limit. With $f=0.75$ applied universally, thickness estimates would increase the volume by 33%. Overall a 20% increase cannot be discounted.  | 0         | +1.5      |
| Tradeoff parameter, $\chi$   | $\chi \to 0$ causes underestimates because of oversmoothing. For $\chi = 0.4$ this effect is small. For $\chi \to 1$ (much larger than desirable) the volume increase is $\sim 0.5$ mm.   | 0         | +0.3      |
| Ice mask, $I_{i,j}$  | Total mask areas for SE+NC subregions is $2\%$ less than those of Bolch et al. (2010).  | 0         | +0.1      |
| Random errors  |   |           |           |
| DEM elevation, $S_{i,j}$   | 9 m absolute error for SRTM elevations in North America (Farr et al., 2007) has no effect. Contribution from random elevation errors should cancel.   | -0.001    | +0.001    |
| Ice mask, $I_{i,j}$  | Estimated area error from erroneous classification of debris-covered glacier cells as non-ice is $-0.5\%$ ( $\delta A^- = -154 \mathrm{km}^2$ ); estimated area error from erroneous classification of snow-covered non-ice cells as ice is $+1.4\%$ ( $\delta A^+ = 430 \mathrm{km}^2$ ). Taking $H^- = 25 \mathrm{m}$ and $H^+ = 10 \mathrm{m}$ gives $\delta V^- = -3.8 \mathrm{km}^3$ and $\delta V^+ = +4.3 \mathrm{km}^3$ . | -0.01     | +0.01     |
| Thinning rate, $\dot{H}_{i,j}$ , and mass balance model, $\dot{b}_{i,j}$ | Flowshed balancing removes the effect of bias errors in surface melt and accumulation fields. Schieffer et al. (2007) give the thinning rate error as $\pm 0.19 \mathrm{myr^{-1}}$ . Random errors of magnitude $\pm 0.2 \mathrm{myr^{-1}}$ give a volume change of $\sim 0.1 \mathrm{mm}$ when thickness inversion is rerun with these errors added.   | -0.1      | +0.1      |
| Flowshed delineation   | Potentially important for individual flowsheds but small cumulative effect.   | -0.01     | +0.01     |
| Balance adjustment   | Not applying flowshed balance adjustment causes $\sim 0.03\mathrm{mm}$ volume change but we consider this correction necessary.   | -0.03     | +0.03     |

## 903 List of Figures

| 904 | 1 | Surface elevation digital elevation model (DEM), ice mask and automatically-            |    |
|-----|---|---|----|
| 905 |   | delineated glacier flowsheds for study region BC2 synthetic example. (a)                |    |
| 906 |   | Surface topography. (b) Ice mask. (c) Glacier flowsheds (each flowshed is               |    |
| 907 |   | represented by a different colour).   | 50 |
| 908 | 2 | Ice masks for synthetic glaciation of test regions. The columns correspond              |    |
| 909 |   | to the "H" forcings for each of the regions in Table 1 starting from the low-           |    |
| 910 |   | est ELA value and ending with the highest. (a1–a4) Region BC1 (centered                 |    |
| 911 |   | at 55.4635°N, 124.8151°W). (b1–b4) Region BC2 (centered at 58.9000°N,                   |    |
| 912 |   | 125.8714°W). (c1–c4) Region BC3 (centered at 59.4545°N, 130.3566°W).                    |    |
| 913 |   | (d1–d4) Region YT1 (centered at 61.6014°N, 133.3684°W).                                 | 51 |
| 914 | 3 | Ice thickness estimation error for Model YT1·1700H. This is an example of               |    |
| 915 |   | below-average performance of the inversion model rather than a selected ex-             |    |
| 916 |   | ample of good performance. (a) Plot of estimated thickness $\widetilde{H}$ against true |    |
| 917 |   | thickness $H$ generated by a numerical glaciation model. (b) Histogram of ice           |    |
| 918 |   | thickness estimation error. Note that the distribution is somewhat skewed               |    |
| 919 |   | because ice thickness cannot be negative. (c) Distribution functions for true           |    |
| 920 |   | (solid line and open circles) and estimated (dashed line and $+$ signs) ice thick-      |    |
| 921 |   | ness.   | 52 |
| 922 | 4 | Maps of assigned basal stress, estimated ice thickness, thickness error, and            |    |
| 923 |   | subglacial topography for Model YT1·1700H. This is an example of below-                 |    |
| 924 |   | average performance of the inversion model rather than a selected example of            |    |
| 925 |   | good performance. (a) Assigned basal stress. (b) Estimated ice thickness. (c)           |    |
| 926 |   | Thickness estimation error. (d) Bed surface elevation.                                  | 53 |

Measured and estimated ice thickness for sites on Athabasca, Peyto, and
Salmon Glaciers. Measurements were taken decades previously (ca. 1960 for
Athabasca, ca. 1984 for Peyto, and 1956 for Salmon). The estimated thickness is based on elevation data and ice masks from ca. 2005. (a) Results
without correction for surface lowering. (b) Results corrected for estimated
surface lowering that occurred between the measurement date and the thickness estimation date.

54

55

Glacierization and sub-regions within western Canadian study area. The labeled arrows indicate the locations of Athabasca (A), Peyto (P), and Salmon (S) glaciers for which there are published measurements of ice thickness.

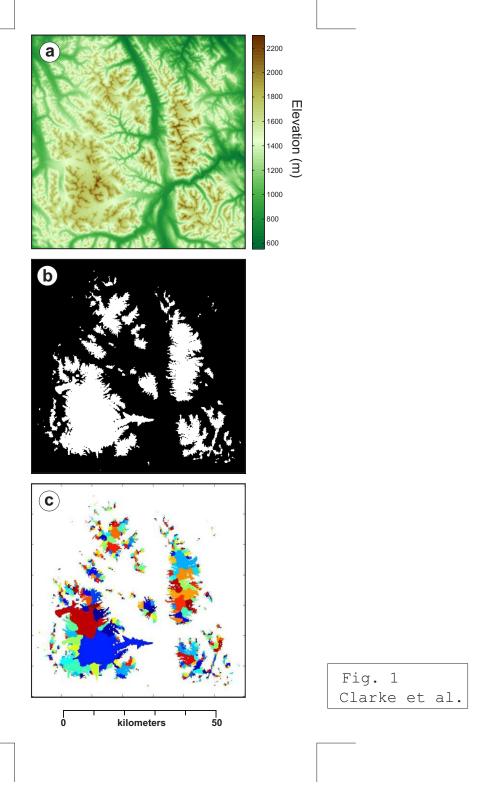


FIG. 1. Surface elevation digital elevation model (DEM), ice mask and automatically-delineated glacier flowsheds for study region BC2 synthetic example. (a) Surface topography. (b) Ice mask. (c) Glacier flowsheds (each flowshed is represented by a different colour).

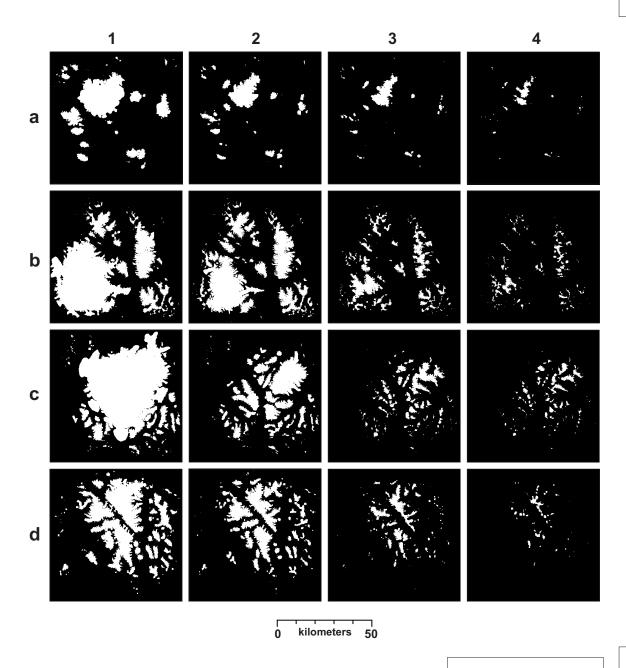


Fig. 2 Clarke et al.

FIG. 2. Ice masks for synthetic glaciation of test regions. The columns correspond to the "H" forcings for each of the regions in Table 1 starting from the lowest ELA value and ending with the highest. (a1–a4) Region BC1 (centered at 55.4635°N, 124.8151°W). (b1–b4) Region BC2 (centered at 58.9000°N, 125.8714°W). (c1–c4) Region BC3 (centered at 59.4545°N, 130.3566°W). (d1–d4) Region YT1 (centered at 61.6014°N, 133.3684°W).

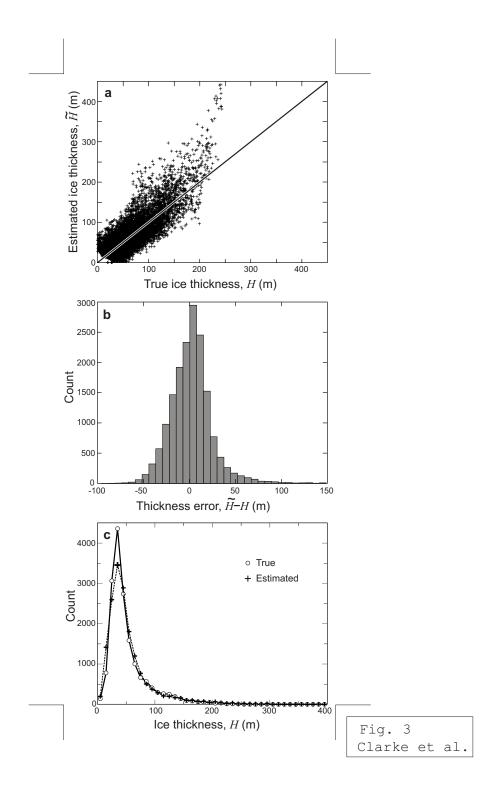


FIG. 3. Ice thickness estimation error for Model YT1·1700H. This is an example of below-average performance of the inversion model rather than a selected example of good performance. (a) Plot of estimated thickness  $\widetilde{H}$  against true thickness H generated by a numerical glaciation model. (b) Histogram of ice thickness estimation error. Note that the distribution is somewhat skewed because ice thickness cannot be negative. (c) Distribution functions for true (solid line and open circles) and estimated (dashed line and + signs) ice thickness.

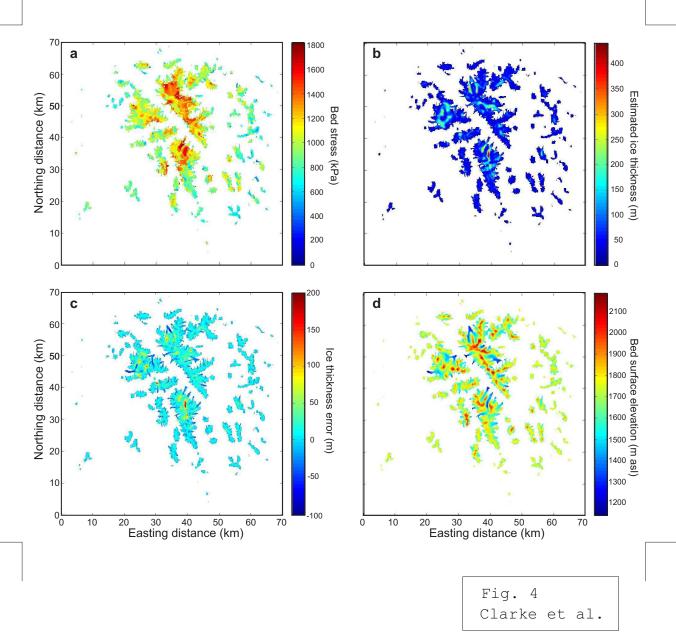


Fig. 4. Maps of assigned basal stress, estimated ice thickness, thickness error, and subglacial topography for Model YT1·1700H. This is an example of below-average performance of the inversion model rather than a selected example of good performance. (a) Assigned basal stress. (b) Estimated ice thickness. (c) Thickness estimation error. (d) Bed surface elevation.

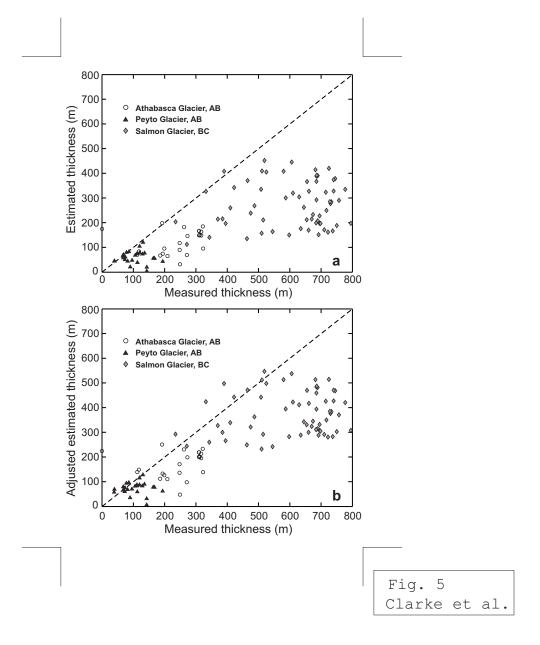


FIG. 5. Measured and estimated ice thickness for sites on Athabasca, Peyto, and Salmon Glaciers. Measurements were taken decades previously (ca. 1960 for Athabasca, ca. 1984 for Peyto, and 1956 for Salmon). The estimated thickness is based on elevation data and ice masks from ca. 2005. (a) Results without correction for surface lowering. (b) Results corrected for estimated surface lowering that occurred between the measurement date and the thickness estimation date.

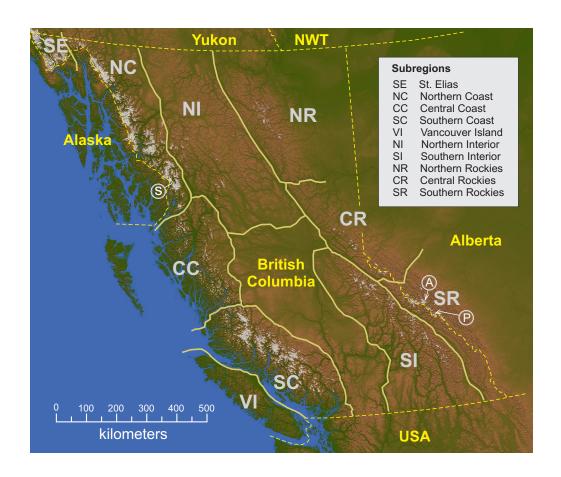


Fig. 6 Clarke et al.

Fig. 6. Glacierization and sub-regions within western Canadian study area. The labeled arrows indicate the locations of Athabasca (A), Peyto (P), and Salmon (S) glaciers for which there are published measurements of ice thickness.