

# **Thermodynamic modeling of the NbeB system**

Rockfeller Maciel Peçanha, Flàvio Ferreira, Gilberto Carvalho Coelho, Carlos

## Angelo Nunes, Bo Sundman

## **To cite this version:**

Rockfeller Maciel Peçanha, Flàvio Ferreira, Gilberto Carvalho Coelho, Carlos Angelo Nunes, Bo Sundman. Thermodynamic modeling of the NbeB system. Intermetallics, 2007, vol. 15, pp.999-1005.  $10.1016/j.intermet.2006.10.054$  .  ${\it hal}\textrm{-}00806040$ 

# **HAL Id: hal-00806040 <https://hal.science/hal-00806040v1>**

Submitted on 29 Mar 2013

**HAL** is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers.

L'archive ouverte pluridisciplinaire **HAL**, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d'enseignement et de recherche français ou étrangers, des laboratoires publics ou privés.



# Open Archive Toulouse Archive Ouverte (OATAO)

OATAO is an open access repository that collects the work of Toulouse researchers and makes it freely available over the web where possible.

This is an author-deposited version published in: http://oatao.univ-toulouse.fr/ Eprints ID : 2404

> **To link to this article** : URL : http://dx.doi.org/10.1016/j.intermet.2006.10.054

**To cite this version** : Peçanha, Rockfeller Maciel and Ferreira, Flàvio and Carvalho Coelho, Gilberto and Nunes, Carlos Angelo and Sundman, B. ( 2007) *[Thermodynamic modeling of the NbeB system.](http://oatao.univ-toulouse.fr/2404/)* Intermetallics, vol. 15 (n° 8). pp. 999-1005. ISSN 0966-9795

Any correspondence concerning this service should be sent to the repository administrator: staff-oatao@inp-toulouse.fr

## Thermodynamic modeling of the  $Nb-B$  system

Rockfeller Maciel Peçanha<sup>a</sup>, Flávio Ferreira<sup>b,\*</sup>, Gilberto Carvalho Coelho<sup>a</sup>, Carlos Angelo Nunes<sup>a</sup>, Bo Sundman<sup>c</sup>

<sup>a</sup> Departamento de Engenharia de Materiais, DEMAR-EEL-USP, CP116, 12600-970, Lorena, SP, Brazil

 $b$  Escola de Engenharia Industrial Metalúrgica de Volta Redonda-UFF-TMC, Av. dos Trabalhadores,<br>420, CEP 27255-125, Volta Redonda, RJ, Brazil

 $\degree$  Division of Physical Metallurgy, Royal Institute of Technology, S-10044, Stockholm 70, Sweden

#### Abstract

In the present work, the Nb-B binary system was thermodynamically optimized. The stable phases in this system are BCC (niobium),  $Nb_3B_2$ , NbB, Nb<sub>3</sub>B<sub>4</sub>, Nb<sub>5</sub>B<sub>6</sub>, NbB<sub>2</sub>, B (boron) and liquid L. The borides  $Nb_3B_2$ , NbB,  $Nb_3B_4$  and  $Nb_5B_6$  and the B (boron) were modeled as stoichiometric phases and the liquid L, BCC (niobium) and NbB2 as solutions, using the sublattices model, with their excess terms described by the Redlich-Kister polynomials. The Gibbs energy coefficients were optimized based on the experimental values of enthalpy of formation, low temperature specific heat, liquidus temperatures and temperatures of invariant transformations. The calculated Nb-B diagram reproduces well the experimental values from the literature.

Keywords: A. Intermetallics, miscellaneous; B. Phase diagrams; B. Thermodynamic and thermochemical properties; E. Phase diagram, prediction

#### 1. Introduction

The development of new high-temperature materials is essential for future generations of both aircraft engines and landbased gas turbines. Nb-silicide-based composites are potential alloy candidates because they present a good balance of properties required for high-temperature applications [1,2]. Among the information for alloy design and potential evaluation for use as structural material, the phase equilibrium is one of the most important. The present thermodynamic optimization of the  $Nb-B$  system is part of a research project, which studies the phase relations in the Nb-rich corner of the  $Nb-Si-B$ system.

The currently accepted  $Nb-B$  phase diagram [3], shown in Fig. 1, presents the following stable phases: BCC (niobium),  $Nb<sub>3</sub>B<sub>2</sub>$ , NbB,  $Nb<sub>3</sub>B<sub>4</sub>$ ,  $Nb<sub>5</sub>B<sub>6</sub>$ ,  $NbB<sub>2</sub>$ , B (boron) and liquid L. This phase diagram is mainly based on the experimental data of Nowotny et al. [4] and shows some divergences with the diagram proposed by Rudy and Windisch [5], which is shown in Fig. 2. The main divergences are (i) Massalski proposes a peritectic formation for the  $Nb<sub>3</sub>B<sub>2</sub>$ , while Rudy and Windisch suggest that this phase is formed peritectoidically; (ii) Massalski proposes the stability of  $Nb<sub>5</sub>B<sub>6</sub>$ , based on results reported by Bolmgren and Lundström [6], while Rudy and Windisch do not mention the presence of this phase in the microstructures of their samples; (iii) Massalski proposes a homogeneity range for NbB<sub>2</sub> much wider than the  $65-70$  at% B reported in Refs.  $[5,7-9]$ ; and (iv) Massalski suggests the composition of the liquid in the B-rich eutectic to be located at approximately 90 at% B, while Rudy and Windisch propose 98 at% B. To solve these discrepancies, an experimental re-investigation of the Nb-B system was performed by Borges et al. [10,11], which confirmed the stability of  $Nb_5B_6$  and the phase relation in the Nb-rich region proposed by Rudy and Windisch, except for the composition of the liquid in

<sup>\*</sup> Corresponding author. Tel.: þ55 24 3344 3013; fax: þ55 24 3344 3020. E-mail address: [flavio@metal.eeimvr.uff.br](mailto:flavio@metal.eeimvr.uff.br) (F. Ferreira).



Fig. 1. Nb-B phase diagram, as assessed by Massalski [3].

the Nb-rich eutectic, located at 16 at % B instead of at 19 at % B. The composition of the B-rich eutectic was informed to be above 96 at% B.

The experimental phase diagram data available in the literature for this system are (i) the congruent melting points of  $NbB<sub>2</sub>$  [4,5,12] and NbB [4,5]; (ii) the temperatures and compositions of the phases for the invariant reactions [4,5,10]; and (iii) the solubility range of the phase  $NbB<sub>2</sub>$  [4,5,7,9,10].

The thermodynamic data available for this system are (i) the entropy of  $NbB_2$  [13],  $Nb_3B_2$ ,  $NbB$  and  $Nb_3B_4$  phases [14]; (ii) the enthalpy of formation of  $NbB_2$  [15-19]; and (iii) the temperature dependence of the enthalpy,  $H(T) - H(298 \text{ K})$ , for the phases  $Nb_3B_2$ , NbB,  $Nb_3B_4$  and NbB<sub>2</sub> in the 1200–2350 K range [20].

The only optimization of the  $Nb-B$  system available in the literature is due to Kaufman et al. [21]. In the modeling of the Me-Si-B systems, we have been using the Stable Element



Fig. 2. Nb-B phase diagram proposed by Rudy and Windisch [5].

Reference (SER), adopted by the SGTE (Scientific Group Thermodata Europe) in their databases, which is not compatible with the reference state adopted by Kaufman. Furthermore, in Kaufman's work on the Nb-B system: (i) all solid phases are modeled as stoichiometric; (ii) the stability of the phase  $Nb<sub>5</sub>B<sub>6</sub>$  is not considered; (iii) NbB is predicted to be formed peritectically; and (iv) more recent experimental information  $[6,9-11,19]$  were not considered. Therefore, the aim of the present work is to provide a new set of thermodynamic coefficients for the Nb-B system.

### 2. Thermodynamic models

The Nb-B phase diagram proposed by Rudy and Windisch (Fig. 2) is plotted with all intermetallic phases showing some solubility of Nb and B in their crystal structures. Except for the  $NbB<sub>2</sub>$ , there are no quantitative experimental evidences for these phase boundaries, which would allow their modeling as solution phases. Therefore, the borides  $Nb_3B_2$ ,  $NbB$ ,  $Nb_3B_4$ and  $Nb<sub>5</sub>B<sub>6</sub>$  and the B (boron) were modeled as stoichiometric phases and the liquid L, BCC (niobium) and  $NbB<sub>2</sub>$  as solution phases, using the Compound Energy Formalism (CEF).

The CEF is described in detail by Sundman and Agren [22] as well as by Hillert [23]. It allows an adequate description of the thermodynamic properties of phases taking the existence of sublattices into account. The sublattices are basically given by the different Wyckoff positions of the atoms in the crystal structure of the phase. Empty positions are also considered as sublattices if they are eventually occupied by atoms such as in interstitial solutions. A helpful reference for modeling intermetallic compounds is the compilation of Villars and Calvert [24]. Table 1 shows the crystal structure data of the stable solid phases in the Nb-B system, in their ideal stoichiometry [24,25]. A phase is modeled as a stoichiometric compound when it exists in a very limited composition range,

for example close to its ideal stoichiometry, and therefore one may consider each sublattice being always occupied by a unique component. When a phase exists over a not negligible composition range, the knowledge of the specific lattice defect structure is essential for the correct choice of the model, which is the case of the  $NbB<sub>2</sub>$  compound in the present work. In such a case, a random mixture of species, which includes vacancies, occurs in at least one of the phase sublattices. Stable or metastable end-member compounds are formed in the limiting cases of occupation of the solution sublattices. Considering the case where the species are not complex constituents such as ions, the Gibbs energy for each individual phase  $\phi$ ,  $G_m^{\phi}$ , is described by the CEF with the following equation expressed per mole of formula unity [23] (note that the upper suffix "s" is not a power and its meaning will become clear later in the text):

$$
G_{\rm m}^{\phi} = \sum_{\rm s} n^{\rm s} (1 - y_{\rm Va}^{\rm s}) \sum_{i} x_i^{\circ} G_i^{\rm stat} + \sum_{\rm end} \Delta_{\rm f}^{\circ} G_{\rm end}^{\phi} H y_i^{\rm s} + RT \sum_{\rm s} n^{\rm s} \sum_{i} y_i^{\rm s} \ln(y_i^{\rm s}) + {}^{E} G_{\rm m}^{\phi} \tag{1}
$$

which can also be written in the form as shown below [22]

$$
G_{\rm m}^{\phi} = \sum_{\rm end} {}^{o}G_{\rm end}^{\phi} \Pi y_i^{\rm s} + RT \sum_{\rm s} n^{\rm s} \sum_{i} y_i^{\rm s} \ln(y_i^{\rm s}) + {}^{E}G_{\rm m}^{\phi} \tag{2}
$$

with

$$
{}^{o}G^{\phi}_{end} = \Delta_{f}{}^{o}G^{\phi}_{end} + \sum_{i} {}^{o}G^{\text{stst}}_{i} n^{s}
$$
\n(3)

Table 1



The symbols in Eqs.  $(1)$ – $(3)$  have the following meaning:

- $n<sup>s</sup>$  is the stoichiometric coefficient of sublattice "s";
- $y_{Va}^s$  is the site fraction of vacancy in the sublattice "s";
- 
- $x_i$  is the mole fraction of component "*i*" in the compound;  $^oG_i^{\text{stst}}$  is the Gibbs free energy of component "*i*" at standard state;
- end is an array with ''end-member compounds'';

 $\Delta_f^{\circ} G_{end}^{\phi}$  is the Gibbs free energy of formation of an end-member of phase  $\phi$ :

- $y_i^s$  is the site fraction of component "*i*" in the sublattice  $``s"$ :
- $^{E}G_{\text{m}}^{\phi}$  is the excess Gibbs energy of phase  $\phi$ .

The summations are performed for arrays whose elements are sublattices (s), components (i) or end-members (end), and the product  $\varPi y_i^s$  contains the site fractions corresponding to the components present in each end-member. As mentioned before, the end-members are formed when each sublattice is occupied by a single component at a time. Therefore, the first right-hand term of Eq. (2) describes a surface of reference in which the interaction energies between neighboring components in different sublattices are essentially considered. The second right-hand term of Eq. (2) accounts for the ideal entropy of mixing, under the assumption of random mixing of components within the solution sublattices. The excess term basically takes into account the interaction energies between different components in the solution sublattices, which are given by interaction parameters  $L_{\text{xs}}^{\phi}$ . A general expression for the excess term is given in Ref. [22]. For the present



<sup>a</sup> ip stands for octahedral interstitial positions.<br><sup>b</sup> Data taken from Ref. [25].<br><sup>c</sup> Wyckoff positions and their coordinates were intentionally suppressed for B-Rhom. The complete list can be found in Ref. [24].

work, it is sufficient to take the case of interaction energies within ''excess solutions'' formed under the consideration of mixing of different components " $i1$ " and " $i2$ " in each solution sublattice at a time while the other sublattices are occupied by single components "i". Using Redlich-Kister polynomials for the interaction parameters [26], the excess term may be described by:

$$
{}^{E}G_{\mathbf{m}}^{\phi} = \sum_{\mathbf{x}\mathbf{s}} II y_i^s \sum_{\mathbf{v}} {}^{\mathbf{v}} L_{\mathbf{x}\mathbf{s}}^{\phi} (y_{i1}^s - y_{i2}^s)^{\mathbf{v}} \tag{4}
$$

where  $^vL_{xs}^{\phi}$  is the interaction parameter of order "v". The first summation is performed for an array whose elements are all possible "excess solutions" (xs) and the product  $\pi y_i^s$  contains the site fractions corresponding to the components present in each ''excess solution''.

#### 2.1. Gibbs energy for pure components

The temperature dependent Gibbs energy of each pure element is described by an equation of the general form:

$$
{}^{o}G_{\mathbf{m}}^{\phi} - H_{i}^{\text{SER}} = a + bT + cT \ln(T) + dT^{2} + eT^{3} + fT^{-1}
$$
 (5)

where  $H_i^{\text{SER}}$  is the enthalpy of stable element "*i*" at 298.15 K.

#### 2.2. Solution phase liquid

The liquid phase was modeled as a single sublattice substitutional solution. Therefore, the site fractions in Eq. (2) are equivalent to the molar fractions and the end-members are coincident with the pure elements, i.e.  ${}^oG_{\text{end1}}^{\text{L}} = {}^oG_{\text{Nb}}^{\text{L}}$  and  ${}^oG_{\text{end2}}^{\text{L}} = {}^oG_{\text{B}}^{\text{L}}$ , yielding the following expression for its Gibbs free energy:

$$
G_{\rm m}^{\rm L} = x_{\rm Nb} {}^{o}G_{\rm Nb}^{\rm L} + x_{\rm B} {}^{o}G_{\rm B}^{\rm L} + RT[x_{\rm Nb}\ln(x_{\rm Nb}) + x_{\rm B}\ln(x_{\rm B})] + x_{\rm Nb}x_{\rm B}[{}^{o}L_{\rm Nb,B}^{\rm L} + {}^{1}L_{\rm Nb,B}^{\rm L}(x_{\rm B} - x_{\rm Nb}) + {}^{2}L_{\rm Nb,B}^{\rm L}(x_{\rm B} - x_{\rm Nb})^{2}] \tag{6}
$$

### 2.3. Solution phase BCC

The Body Centered Cubic (BCC) crystal structure may be modeled as a phase with two sublattices, namely the sublattice corresponding to Wyckoff positions 2a (substitutional) and that corresponding to octahedral interstitial positions 6b (Table 1). Due to compatibility reasons within thermodynamic databases, this model is usually adopted even if no interstitial solution is formed in the specific system. For the BCC phase in the Nb-B system there is no experimental information about the type of solution of B, whether interstitial or substitutional. However, it is known that the boron atoms occupy the interstitial sublattice in metals of BCC structure like Nb [27]. Therefore, also for the Nb-B system, the model  $(Nb)(B,Va)$ <sub>3</sub> was chosen yielding the following expression for its Gibbs energy:

$$
G_{m}^{BCC} = y_{Nb}^{s1} y_{Va}^{s2} G_{Nb:Va}^{BCC} + y_{Nb}^{s1} y_{B}^{s2} G_{Nb:B}^{BCC} + 3RT \left[ y_{B}^{s2} \ln(y_{B}^{s2}) + y_{Va}^{s2} \ln(y_{Va}^{s2}) \right] + y_{B}^{s2} y_{Va}^{s2} \left[ {}^{0}L_{Nb:Bya}^{BCC} + {}^{1}L_{Nb:B,Va}^{BCC}(y_{B}^{s2} - y_{Va}^{s2}) + \cdots \right]
$$
\n(7)

where  ${}^oG_{Nb:Va}^{BCC}$  and  ${}^oG_{Nb:B}^{BCC}$  correspond to:

$$
{}^{o}G_{Nb:Va}^{BCC} = {}^{o}G_{Nb}^{BCC} + 3{}^{o}G_{Va} + \Delta_f{}^{o}G_{Nb:Va}^{BCC}
$$
  

$$
{}^{o}G_{Nb:B}^{BCC} = {}^{o}G_{Nb}^{BCC} + 3{}^{o}G_{B}^{Rhom} + \Delta_f{}^{o}G_{Nb:B}^{BCC}
$$
  

$$
(8)
$$

The BCC phase is described within the limits of  $(Nb)(Va)_{3}$ and  $(Nb)(B)_3$ , which correspond to the pure BCC-Nb, when the interstitial sublattice is empty, and to the metastable compound BCC-NbB<sub>3</sub>, when the interstitial sublattice is completely filled with B atoms. Therefore, the Gibbs energy of the first end-member compound,  ${}^{o}\text{GBCC}_{Nb:Va}$ , corresponds to that of the pure component Nb,  ${}^oG_{Nb}^{BCC}$ .

#### 2.4. Solution phase  $NbB<sub>2</sub>$

The  $NbB<sub>2</sub>$  phase exhibits a hexagonal structure ( $hP3$ , space group  $P6/mmm$ , prototype  $AIB_2$ ) with two sublattices, with Nb and B atoms occupying 1a and 2d positions, respectively. As mentioned before, this phase shows an extensive homogeneity range  $(65-70 \text{ at} \%)$  [5,7-9]. Post et al. [28] compared the structural characteristics of several diborides and proposed substitutional vacancies in both Nb and B positions as defect mechanisms to explain the homogeneity range of  $NbB<sub>2</sub>$ . Muzzy et al. [29], while studying  $AlB_2$ -type, B-rich  $(Mo,Zr)<sub>x</sub>B<sub>2</sub>$  by neutron diffraction, reported that the metal vacant positions would accommodate the excess of boron in its structure. More recently, Nunes et al. [9] investigated the homogeneity range of  $NbB<sub>2</sub>$ , also by neutron diffraction experiments, and confirmed Post's hypothesis. Therefore, the model  $(Nb, Va)<sub>1</sub>(B, Va)<sub>2</sub>$  was adopted for  $NbB<sub>2</sub>$  in the present work with its Gibbs energy described by the following equation:

$$
G_{\rm m}^{\rm NbB_2} = y_{\rm Nb}^{\rm sl} y_{\rm B}^{\rm s2o} G_{\rm Nb:B}^{\rm NbB_2} + y_{\rm Nb}^{\rm sl} y_{\rm Va}^{\rm s2o} G_{\rm Nb:Va}^{\rm NbB_2} + y_{\rm Na}^{\rm sl} y_{\rm B}^{\rm s2o} G_{\rm Va:B}^{\rm NbB_2} + y_{\rm Va}^{\rm sl} y_{\rm va}^{\rm v2o} G_{\rm Va:Va}^{\rm NbB_2} + RT \{y_{\rm Nb}^{\rm sl} \ln(y_{\rm Nb}^{\rm sl}) + y_{\rm va}^{\rm sl} \ln(y_{\rm Va}^{\rm sl})\} + 2 \left[ y_{\rm B}^{\rm s2} \ln(y_{\rm B}^{\rm s2}) + y_{\rm va}^{\rm s2} \ln(y_{\rm Va}^{\rm s2}) \right] \} + ^E G_{\rm Nb, Va:B,Va}^{\rm NbB_2} \tag{9}
$$

where

$$
{}^{o}G_{NbB2}^{NbB2} = {}^{o}G_{Nb}^{BCC} + 2{}^{o}G_{B}^{Rhom} + \Delta_{f}{}^{o}G_{NbB2}^{NbB2}
$$
  
\n
$$
{}^{o}G_{Nb;Va}^{NbB2} = {}^{o}G_{Nb}^{BCC} + 2{}^{o}G_{Va} + \Delta_{f}{}^{o}G_{Nb;Va}^{NbB2}
$$
  
\n
$$
{}^{o}G_{Va:B}^{NbB2} = {}^{o}G_{Va} + 2{}^{o}G_{B}^{Rhom} + \Delta_{f}{}^{o}G_{Va:B}^{NbB2}
$$
  
\n
$$
{}^{o}G_{Va:Va}^{NbB2} = {}^{o}G_{Va} + 2{}^{o}G_{Va} + \Delta_{f}{}^{o}G_{Va:Va}^{NbB2}
$$
  
\n(10)

and the excess term is given as follows:

$$
\begin{split} ^E G^{\text{NbB}_2}_{\text{Nb},\text{Va:B},\text{Va}} = &\; y_{\text{Nb}}^{\text{sl}} y_{\text{Va}}^{\text{sl}} y_{\text{S}}^{\text{SO}} L^{\text{NbB}_2}_{\text{Nb},\text{Va:B},\text{Va}} + y_{\text{Nb}}^{\text{sl}} y_{\text{Va}}^{\text{sl}} y_{\text{Va}}^{\text{S2}} \, \Omega^{\text{NbB}_2}_{\text{Nb},\text{Va}:\text{Va}} \\ &\;+ y_{\text{Nb}}^{\text{sl}} y_{\text{B}}^{\text{S2}} y_{\text{Va}}^{\text{2}} L^{\text{NbB}_2}_{\text{Nb:B},\text{Va}} + y_{\text{Va}}^{\text{sl}} y_{\text{B}}^{\text{S2}} y_{\text{Va}}^{\text{2}} L^{\text{NbB}_2}_{\text{Va:B},\text{Va}} \end{split} \tag{11}
$$

In Eq. (10),  ${}^oG_{Nb:Va}^{\text{NbB}_2}$  and  ${}^oG_{Va:B}^{\text{NbB}_2}$  correspond to the Gibbs energy of pure Nb and B with hexagonal  $hp3$  structure, respectively.

Table 2 Optimized Gibbs energy coefficients for all phases of the Nb-B system

Phase	Model	Parameter	Coefficient		
			a	b	$\mathcal{C}_{0}$
L	(Nb,B)	${}^{0}L^{\rm L}_{\rm Nb,B}$ $L_{\text{Nb,B}}^{\text{L}}$ $^2L^{\rm L}_{\rm Nb,B}$	$-158000$ $-21,500$ $+147500$	$+19.5$	
<b>BCC</b>	$(Nb)(B, Va)$ <sub>3</sub>	$\Delta_f{}^oG_{Nb:B}^{BCC}$ ${}^{0}L_{\text{Nb:B,Va}}^{BCC}$	$+20000$ $-74000$		
Nb <sub>3</sub> B <sub>2</sub>	$(Nb)_{3}(B)_{2}$	$\Delta_{\text{f}}{}^o G^{\text{Nb}_3\text{B}_2}_{\text{Nb}: \text{B}}$	$-295300$	$-24.4$	$+6.65$
NbB	$(Nb)$ $(B)$	$\Delta_f{}^oG_{Nb:B}^{NbB}$	$-128150$	$-7.7$	$+1.75$
$Nb_5B_6$	$(Nb)_{5}(B)_{6}$	$\Delta_{\rm f}{}^o G_{{\rm Nb: B}}^{{\rm Nb_5B_6}}$	$-727900$	$-73.6$	$+14.0$
$Nb_3B_4$	$(Nb)_{3}(B)_{4}$	$\Delta_{\text{f}}{}^o G^{\text{Nb}_3\text{B}_4}_{\text{Nb:B}}$	$-469900$	$-65.3$	$+11.34$
NbB <sub>2</sub>	$(Nb, Va)$ $(B, Va)2$	$\Delta_{\rm f}{}^oG^{\rm NbB_2}_{\rm Nb:B}$ $\Delta_{\rm f}{}^oG_{\rm Va:B}^{\rm NbB_2}$ $\Delta_{\rm f}{}^oG^{\rm NbB_2}_{\rm Nb;Va}$ ${}^{0}L_{\text{Nb,Va:B}}^{\text{NbB}_2}$ ${}^{0}L_{\text{Nb:B,Va}}^{\text{NbB}_2}$ ${}^{0}L_{\rm Va:B,Va}^{\rm NbB_2}$ 0I NbB <sub>2</sub> "Nb,Va:Va	$-196200$ $+100416$ $+10000$ $-106000$ $+180000$ $+200000$ $+200000$	$+7.54$ $-19.412$ $+2.4$ $+33.0$	$+0.25$

#### 2.5. Stoichiometric phases

The crystal structures of the stoichiometric borides (Table 1) suggest the use of multiple sublattices for their modeling, as follows: (1) for  $Nb_3B_2$ ,  $Nb_2Nb_4$ ,  $B_4$ ; (2) for NbB,  $Nb_4$ ,  $B_4$ ; (3) for  $Nb_5B_6$ ,  $(Nb)_2(Nb)_4(Nb)_4(B)_4(B)_4(B)_4$ ; and (4) for  $Nb<sub>3</sub>B<sub>4</sub>$ ,  $Nb<sub>2</sub>(Nb)<sub>4</sub>(B)<sub>4</sub>(B)<sub>4</sub>$ . However, in the present work, positions occupied by the same element were considered energetically equivalent, reducing their description to 2-sublattices, using the smallest integers as stoichiometric indices. For each stoichiometric phase, there is only one possible arrangement



Fig. 3. Phase diagram of the Nb-B system calculated with the coefficients of the present work.



Fig. 4. Calculated enthalpy differences  $[H(T) - H(298)]$  (continuous lines) for  $Nb<sub>3</sub>B<sub>2</sub>$ , NbB,  $Nb<sub>3</sub>B<sub>4</sub>$  and  $NbB<sub>2</sub>$  and the values measured by Bolgar et al. [20] (symbols).

of the pure elements in the crystal structure of the compound. Therefore, the ideal and excess contributions to their Gibbs energies are equal to zero, leading to the following expressions for their Gibbs energies:

 $Nb<sub>3</sub>B<sub>2</sub>$ 

$$
G_{\rm m}^{\rm Nb_3B_2} = 3^o G_{\rm Nb}^{\rm BCC} + 2^o G_{\rm B}^{\rm Rhom} + \Delta_{\rm f}^{\,o} G_{\rm NbB}^{\rm Nb_3B_2} \tag{12}
$$

NbB

$$
G_{\rm m}^{\rm NbB} = {}^oG_{\rm Nb}^{\rm BCC} + {}^oG_{\rm B}^{\rm Rhom} + \Delta_{\rm f} {}^oG_{\rm Nb:B}^{\rm NbB} \tag{13}
$$

 $Nb<sub>5</sub>B<sub>6</sub>$ 

$$
G_{\rm m}^{\rm Nb_5B_6} = 5^{\circ}G_{\rm Nb}^{\rm BCC} + 6^{\circ}G_{\rm B}^{\rm Rhom} + \Delta_{\rm f}^{\circ}G_{\rm Nb_2B_6}^{\rm Nb_5B_6}
$$
 (14)

 $Nb<sub>3</sub>B<sub>4</sub>$ 

$$
G_{\rm m}^{\rm Nb_3B_4} = 3^{\circ} G_{\rm Nb}^{\rm BCC} + 4^{\circ} G_{\rm B}^{\rm Rhom} + \Delta_{\rm f}^{\circ} G_{\rm NbB}^{\rm Nb_3B_4} \tag{15}
$$

Table 3





Table 4 Entropies at 298.15 K for the stable Nb-borides

Phase	Entropy at $298.15$ K (kJ/mol of phase. K)		
	Calculated	Experimental	
NbB <sub>2</sub>	38.7	38.1 [13]	
Nb <sub>3</sub> B <sub>2</sub>	99.4	102.0 [14]	
NbB	38.1	38.0 [14]	
$Nb_5B_6$	196.5		
Nb <sub>3</sub> B <sub>4</sub>	121.7	121.1 [14]	

#### 3. Optimization procedure (results and discussion)

The  ${}^nL_{ij}^{\phi}$  parameters in Eqs. (6), (7) and (11) ( $\phi = L$ ,  $BCC$  or  $NbB_2$ ) as well as the Gibbs energy of formation of the end-members in Eqs. (8) and (10) and of the stoichiometric compounds in Eqs.  $(12)$ – $(15)$  are described according to Eq.  $(5)$ . Their coefficients a, b and c correspond to the adjustable variables in the optimization procedure (see Table 2).

The temperature dependent Gibbs energies of the pure elements in their stable and metastable states were taken from SGTE database [30] and are given in Appendix.

The model  $(Nb)<sub>1</sub>(B,Va)<sub>3</sub>$  chosen for the BCC leads to the definition of the end-member NbB<sub>3</sub>, with its Gibbs energy of formation given by  $\Delta_f^{\circ}G_{\text{Nb:B}}^{\text{BCC}}$ , for which no experimental value is available. A positive value of 5000 J/mol of atoms has been often used, e.g. Ref. [31], for the Gibbs energy of formation of such metastable compounds, thus, a value of 20 000 J/mol of phase was adopted here for  $\Delta_f^o G_{Nb:B}^{BCC}$ .

The SGTE descriptions for hcp-Nb and hcp-B were adopted for the parameters  $\Delta_f^o G_{Nb:Va}^{NbB_2}$  and  $\Delta_f^o G_{Va:B}^{NbB_2}$  in Eq. (10), respectively. The Gibbs energy of the end-member with vacancies in both sublattices of the phase  $NbB<sub>2</sub>$  was assumed to be zero  $({}^oG_{\text{Va}: \text{Va}}^{\text{NbB}_2}=0)$ .

The liquidus line and the temperatures of the invariant reactions measured by Rudy and Windisch [5] with the modifications proposed in Refs. [10,11] were adopted in the optimization procedure. However, to make the stability of  $Nb<sub>5</sub>B<sub>6</sub>$  compatible with the measurements of Rudy and Windisch, the 3133 K reported for the eutectic  $L \leftrightarrow NbB + Nb_3B_4$ was assumed to be valid for the eutectic  $L \leftrightarrow NbB + Nb_5B_6$ , with the composition of the liquid at  $52 \text{ at } \%$  B [10]. The temperature for the peritectic formation of  $Nb_5B_6$  (L +  $Nb_3B_4 \leftrightarrow Nb_5B_6$ ) was assumed to be 3170 K, which is a mean value between the temperatures given by Rudy and Windisch for the immediate neighbor invariant transformations. Furthermore, all thermodynamic data available were used in the optimization procedure.

The optimized Gibbs energy coefficients for the phases of the  $Nb-B$  system are presented in Table 2. The calculated phase diagram is shown in Fig. 3, where a good agreement between the experimental and calculated values can be observed. The calculated enthalpy differences,  $H(T) - H(298)$ , for the phases  $Nb_3B_2$ ,  $Nb_3B_4$  and  $Nb_2$  reproduce well the values measured by Bolgar et al. [20], as shown in Fig. 4. The calculated and experimental data for the enthalpies and the entropies of the intermediate compounds at 298.15 K are compared in Tables 3 and 4, respectively, also showing a good agreement.

### Acknowledgements

The authors gratefully acknowledge the financial support of FAPESP through grants  $#97/06348-4$  (Nb-B-Si),  $#99/06160-$ 0, and #00/08062-5.

#### Appendix: Gibbs energies of the pure elements in their stable and metastable states (in J/mol).



### References

- [1] Bewlay BP, Jackson MR, Zhao J-C, Subramanian PR. Metallurgical and Materials Transactions A  $2003;34:2043-52$ .
- [2] Zhao J-C, Westbrook JH. MRS Bulletin  $2003:28:622-30$ .
- [3] Massalski TB, editor. Binary alloy phase diagrams. 2nd ed., 3 vols.. Materials Park, OH: ASM International; 1990.
- [4] Nowotny H, Benesovsky F, Kieffer R. Zeitschrift für Metallkunde  $1959.50.417 - 23$
- [5] Rudy E, Windisch St. Ternary phase equilibria in transition metalboron-carbon-silicon systems, AFML-TR-65-2, part I, vol. X. OH: Wright-Patterson Air Force Base; 1966.
- [6] Bolmgren H, Lundstroem T. Journal of the Less-Common Metals 1990;  $159: L25 - 7.$
- [7] Nowotny H, Benesovsky F, Rudy E, Wittmann A. Monatshefte für Chemie 1960;91:975-90.
- [8] Rudy E, Benesovsky F, Toth L. Zeitschrift für Metallkunde 1963;  $54:345 - 53$ .
- [9] Nunes CA, Kaczorowski D, Rogl P, Baldissera MR, Suzuki PA, Coelho GC, et al. Acta Materialia 2005;53:3679-87.
- [10] Borges Jr. LA. MSc. thesis, FAENQUIL, Brazil; 2001.
- [11] Borges Jr LA, Coelho GC, Nunes CA, Suzuki PA. Journal of Phase Equilibria 2003;24:140-6.
- [12] Glaser FW. Transactions of the American Institute of Mining and Metallurgical Engineers 1952;194:391-6.
- [13] Westrum EF, Clay GA. Journal of Physical Chemistry 1963;67:2385-7.
- [14] Blinder AV, Bolgar AS. Soviet Powder Metallurgy and Metal Ceramics 1991;30:1053-6.
- [15] Huber Jr. EJ. 5th Quarterly report, AVCO-SR-63-183; 1963.
- [16] Johnson GK, Greenberg E, Margrave JL, Hubbard WN. Journal of Chemical and Engineering Data  $1967;12:597-600$ .
- [17] Reznitskii LA. Russian Journal of Physical Chemistry  $1967;41:612-4$ .
- [18] Kirpichev EP, Rubtsov YuI, Sorokina TV, Prokudina VK. Russian Journal of Physical Chemistry 1979;53:1128-30.
- [19] Meschel SV, Kleppa OJ. Metallurgical Transactions A  $1993;24:947-50$ .
- [20] Bolgar AS, Serbova MI, Serebryakova TI, Isaeva LP, Fesenko VV. Soviet Powder Metallurgy and Metal Ceramics 1983;243:57-62.
- [21] Kaufman L, Uhrenius B, Birnie D, Taylor K. CALPHAD 1984;8:25-66.
- [22] Sundman B, Ågren J. Journal of Physics and Chemistry of Solids 1981;42:297-301.
- [23] Hillert M. The compound energy formalism. Journal of Alloys and Compounds 2001;320:161-76.
- [24] Villars P, Calvert LD. Pearson's handbook of crystallographic data for intermetallic phases. 2nd ed., 4 vols.. Materials Park, OH: ASM International; 1991.
- [25] Bolmgren H, Lundström T, Tergenius L-E. Journal of the Less-Common Metals 1990:161:341-5.
- [26] Redlich O, Kister AT. Journal of Industrial and Engineering Chemistry 1948:40:345-8.
- [27] Kiessling R. Acta Chemica Scandinavica 1949;3:603-15.
- [28] Post B, Glaser FW, Moskowitz D. Acta Metallurgica 1954;2:20-5.
- [29] Muzzy LE, Avdeev M, Lawes G, Haas MK, Zandbergen HW, Ramirez AP, et al. Physica C 2002;382:153-65.
- [30] Dinsdale AT. CALPHAD 1991;15:317-425.
- [31] Neto JGC, Fries SG, Lukas HL, Gama S, Effenberg G. CALPHAD 1993;17:219-28.