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A partitioning strategy for the coupled hygromechanical analysis with application to wood structures of Cultural Heritage

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Abstract

One of the main causes for damage of panel paintings of cultural heritage is due to the environmental micro-climatic variations. Wood science and numerical modeling may help to analyze and calibrate restoration interventions, to predict the behavior of the artwork, taking into account the individual painted panels and the conservation environment. In this article, a partitioning numerical strategy is proposed to predict by simulation the behavior of such artworks. It is based on a multi-physics partition focusing on the interactions between the different physics that are described in a thermodynamical framework. It is applied to the case study of Mona Lisa, modeled as a strongly coupled hygromechanical structure. The strategy is designed to couple two different modelings: a plate model for the mechanical behavior of the panel, and one-dimensional transverse diffusion for the moisture evolution.

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Keywords: fluid-structure interaction; multiphysics; hygroscopic; anisotropy; thermomechanics; Jacobi; paintings, Mona Lisa

1 INTRODUCTION

Wood mechanical behavior is strongly dependent on moisture, and this hygromechanical coupled phenomena is itself dependent on temperature. Therefore, painted wood panels of cultural heritage (furniture, musical instruments, paintings...) are often sensitive to several loadings such as mechanical restraint, as well as humidity and temperature cycles due to the hygrothermal variations of the surrounding environment [1, 2, 3]. To improve preventive conservation and to guide restoration acts on wooden artworks, virtual testing via numerical simulation is necessary to assess a risk analysis, in order to predict if the object will remain safe under various scenarios.

In this article, we focus on a numerical strategy to solve the coupled problem of interactions between the panel support and the pictorial layer and we consider humidity variations only as a first step, with isothermal evolutions. Of course, the long term goal of such studies also requires interdisciplinary experiments, at least to nurture the model with information on the initial state of the artwork. For the application we use in this article, the case of *Mona Lisa*, we rely on the study reported in [4]. In all of the following, the small perturbation assumption is used for the structural model.

More sophisticated models are available in the literature, especially for wood drying [5, 6, 7, 8]. We choose a simpler one herein in order to focus on the numerical strategy to solve the hygromechanical coupled problem via a partitioning strategy. Nevertheless, to design such a strategy, we need for a consistent thermodynamics approach, especially for selecting the couples of dual variables involved in the model. Apart from the coupled physics, the second difficulty lies in the anisotropy arising from the wood underlying micro-structure.

A three-dimensional hygromechanical model is therefore stated within the framework of thermomechanics of materials. This study is afterwards dedicated to one-sided painted panels for which main moisture gradient is along the thickness of the panel. The panel itself is modeled as a plate. The final hygromechanical coupled problem is solved with a partitioning approach relying on a structural solver on one hand, and a diffusion code on the other hand. For this strongly coupled problem, an inner iteration loop is used to recover the coupling effects.

This article is organized as follows: Section 2 recalls the basic behavior and notations for hygromechanical problems, and Section 3 details the model we are interested in. The computational strategy is designed in Section 4 in the case of identical 3D meshes for the elastic and for the diffusion problems, while Section 5 couples two dedicated models and discretizations for the application to one-sided painted wood panels, and displays the numerical results. The influence of the discretization parameters on the accuracy of the solution and on the convergence of the partitioning scheme is studied.

w	moisture content (dimensionless)
Δw	variation of moisture content w.r.t. the reference state (dimensionless)
H	relative humidity (dimensionless)
μ	massic chemical potential of water (J.kg^{-1})
$\Delta\mu$	variation of massic chem. pot. of water w.r.t. the reference state (J.kg^{-1})
\underline{J}	water mass flux ($\text{kg.m}^{-2}.\text{s}^{-1}$)
\underline{F}	gradient of moisture content (m^{-1})
\underline{Z}	gradient of massic chemical potential ($\text{J.kg}^{-1}.\text{K}^{-1}.\text{m}^{-1}$)
$\boldsymbol{\sigma}$	stress field (Pa)
$\boldsymbol{\varepsilon}$	strain field (dimensionless)
\underline{U}	displacement field w.r.t. the reference configuration (m)
\underline{D}	diffusivity tensor or matrix ($\text{m}^2.\text{s}^{-1}$)
ρ_o	specific density of oven-dry wood (kg.m^{-3})
\underline{C}	elasticity tensor (Pa)
E_α	Young modulus (Pa)
$\nu_{\alpha\beta}$	Poisson coefficient (dimensionless)
$G_{\alpha\beta}$	shear modulus (Pa)

Main notations

2 HYGROMECHANICAL BEHAVIOR

2.1 Water in wood

Water in wood material can occur at different levels:

- chemical water that cannot be extracted without transforming the material constituents;
- bound (or hygroscopic) water in cell walls;
- water vapor in lumens;
- free (or capillary) water in liquid form in the voids of the wood.

The moisture content w is the mass of water contained in the last three forms, in an elementary representative volume, expressed as a fraction of its oven-dry mass. Using apparent water specific density ρ_w and specific density of the oven-dry wood ρ_o , one gets

$$w = \frac{\rho_w}{\rho_o} \quad (1)$$

Wood panels of cultural heritage are usually loaded within hygroscopic regime, for which water mainly occurs as bound water and water vapor. In such cases, the moisture content is below the fiber saturation point (FSP) for which it is approximately $w_{\text{FSP}} = 30\%$ [9, 10].

Variations of humidity are supposed to be sufficiently slow for bound water to be in local equilibrium with the relative humidity of the air, defined as $H = p/p_s$, where p is the partial water vapor pressure in the air, and p_s is the saturated vapor pressure (therefore, one gets $0 \leq H \leq 1$).

In this study, the material behavior will be described at macroscopic scale, and only diffusion is considered as a water transfer mechanism (no pressure gradients are involved that can lead to a bulk viscous flow).

$E_L = 10.06 \text{ GPa}$	$E_R = 1.19 \text{ GPa}$	$E_T = 0.58 \text{ GPa}$
$G_{RT} = 0.20 \text{ GPa}$	$G_{TL} = 0.64 \text{ GPa}$	$G_{LR} = 0.86 \text{ GPa}$
$\nu_{RT} = 0.70$	$\nu_{LT} = 0.47$	$\nu_{LR} = 0.36$
$w_m = 7.0 \%$	$K = 0.76$	$C = 6.0$
$a_L = 0.8 \%$	$a_R = 9.5 \%$	$a_T = 48 \%$
$D_L = 30.10^{-10} \text{ m}^2 \cdot \text{s}^{-1}$	$D_R = 2.510^{-10} \text{ m}^2 \cdot \text{s}^{-1}$	$D_T = 0.5410^{-10} \text{ m}^2 \cdot \text{s}^{-1}$
$c_L = -1.74$	$c_R = -0.66$	$c_T = -0.16$

Table 1: Elastic parameters at reference state (after [11, 13]); sorption and shrinkage parameters; diffusivity parameters (after [14])

2.2 Elastic behavior

Concerning the elastic behavior, the stress field $\boldsymbol{\sigma}$ and the strain field $\boldsymbol{\varepsilon}$ are linked via the Hooke tensor. The elastic behavior is orthotropic; moreover in a wood piece, due to the radial growth of the tree, the directions of anisotropy are heterogeneous (roughly with a cylindrical symmetry). These directions are usually denoted with L, R and T for the longitudinal, radial and tangential directions, respectively.

The elastic part of the material behavior is represented with Hooke tensor \mathbf{C} . The compliant tensor \mathbf{S} is classically expressed in the orthotropic base (L,R,T) with Voigt notations:

$$\mathbf{S} = \mathbf{C}^{-1} = \begin{bmatrix} 1/E_L & -\nu_{LR}/E_L & -\nu_{LT}/E_L & 0 & 0 & 0 \\ -\nu_{RL}/E_R & 1/E_R & -\nu_{RT}/E_R & 0 & 0 & 0 \\ -\nu_{TL}/E_T & -\nu_{TR}/E_T & 1/E_T & 0 & 0 & 0 \\ 0 & 0 & 0 & 1/G_{RT} & 0 & 0 \\ 0 & 0 & 0 & 0 & 1/G_{TL} & 0 \\ 0 & 0 & 0 & 0 & 0 & 1/G_{LR} \end{bmatrix}_{(L,R,T)} \quad (2)$$

with symmetry, positiveness and definiteness conditions. E_α are Young modulus in direction $\alpha = \text{L,R,T}$, $\nu_{\alpha\beta}$ are Poisson coefficients, $G_{\alpha\beta}$ are the shear modulus.

For wooden structures of cultural heritage, it is often impossible to extract a specimen of wood and perform a tensile test; only measurements without contact are allowed. Therefore, estimations of material characteristic parameters are useful. Concerning the case of poplar wood (*Populus sp.*), which is under concern herein, [11] provides estimation of elastic parameters for the reference state, as functions of density. Density can be obtained in a non destructive manner. We consider here a specific density $\rho = 0.45 \pm 0.025 \text{ g/cm}^3$ [12], and the reference state $w = 12 \%$, that leads to the estimations of Table 1. They proved to reproduce experimental observations [13].

2.3 Sorption curve, swelling and shrinkage

The basic test for the hygromechanical behavior consists in placing an elementary representative volume (or a specimen with homogeneous properties) in a humidity-controlled and temperature-regulated air. Increasing slowly the humidity H to get an equilibrium with the moisture content w in all the body of the specimen allows to get the value of this moisture content by monitoring the weight of the specimen. This isothermal sorption curve is usually obtained under null stress. If not, an additional mechanism known as mechano-sorption is involved [15, 16, 17]; this mechanism is not taken into account herein. Usually an hysteresis is obtained between adsorption and desorption, due to chemical interactions [18, 19]. We will not take this effect into account here, and we will consider the average curve of Figure 1. This Figure plots data obtained from different sources, and the Guggenheim, Anderson and Boer-Dent (GAB) model is identified to obtain an average curve, from data in [20]:

$$w = w_m \frac{CKH}{(1 - KH)(1 - KH + CKH)} \quad (3)$$

The parameter values are referenced in Table 1.

To derive a constitutive model, we do need to define a reference state, on a reference configuration, from which the displacement of the structure \underline{U} is measured (i.e. $\boldsymbol{\varepsilon}_{\text{ref}} = 0$). We choose here the standard state at a temperature of 25°C , and a relative humidity $H_{\text{ref}} = 65 \%$ (corresponding approximately to $w_{\text{ref}} = 12 \%$, in the isothermal sorption curve of Figure 1). Moreover, we assume that for the same

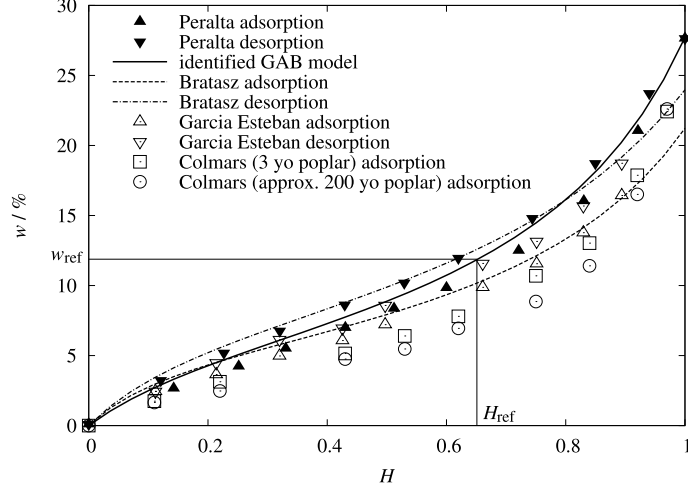


Figure 1: Isothermal sorption-desorption curve (after [20, 21, 22, 23])

reference configuration, the stress is null: $\sigma_{\text{ref}} = 0$. Concerning the sorption test, the relationship between moisture content and relative humidity (3) can be written as

$$\Delta w = f(H/H_{\text{ref}}) \quad (4)$$

where $\Delta w = w - w_{\text{ref}}$.

During the same test, measurements of dimension variations of the specimen may characterize the swelling and shrinkage effect, that mainly appears during the hygroscopic regime. Since this effect is also anisotropic, all the principal components of the corresponding free strain ε have to be measured. A linear model is usually satisfactory, and the fitting leads to

$$\varepsilon = \mathbf{A}\Delta w \quad (\text{when } \sigma = 0) \quad (5)$$

where, in the orthotropic basis,

$$\mathbf{A} = \begin{bmatrix} a_L & 0 & 0 \\ 0 & a_R & 0 \\ 0 & 0 & a_T \end{bmatrix} \quad (6)$$

with constant adimensional coefficients a_α . To estimate these coefficients, the approach in [24] is used: for a large set of wood species, $\mathbf{A} = \mathbf{S}\beta\mathbf{1}$ where $\mathbf{1}$ is the identity tensor and $\beta = K_\beta\rho_o^2$ with $K_\beta \approx 2.15 \text{ GPa}/(\text{g}/\text{cm}^3)^2$. This leads to the values reported in Table 1 (for instance, with $\Delta w = 10\%$ the free tangential strain is $a_T\Delta w = 4.8\%$).

The shrinkage tensor \mathbf{A} is indeed a coupling between mechanical behavior and hygrometry.

3 REFERENCE PROBLEM

3.1 Admissibility conditions

Concerning the structural problem on the domain Ω , a given displacement field \underline{U}_d is prescribed on a first part $\partial_1\Omega$ of the boundary $\partial\Omega$. A surface force density \underline{F}_d on the complementary part $\partial_2\Omega$, and a bulk force density \underline{f}_d are also prescribed. The conservation of momentum gives the static admissibility conditions on the stress field σ :

$$\text{div } \sigma + \underline{f}_d = 0 \quad \text{in } \Omega, \quad \sigma \underline{n} = \underline{F}_d \quad \text{on } \partial_2\Omega \quad (7)$$

\underline{n} is the outward normal unitary vector at the boundary. The strain field ε should be compatible with a kinematically admissible displacement field \underline{U} :

$$\varepsilon = (\text{Grad } \underline{U})_{\text{sym}} \quad \text{in } \Omega, \quad \underline{U} \in \mathcal{U}, \quad \underline{U} = \underline{U}_d \quad \text{on } \partial_1\Omega \quad (8)$$

where \mathcal{U} is the set of finite energy displacement field, typically: $\mathcal{U} = H^1(\Omega)$.

The conservation of fluid mass leads to

$$\frac{\partial \rho_w}{\partial t} = -\operatorname{div} \underline{J} \quad (9)$$

where \underline{J} is the water mass flux. With the expression (1) of the moisture content, this reads

$$\rho_o \frac{\partial w}{\partial t} = -\operatorname{div} \underline{J} \quad (10)$$

The boundary conditions corresponding to the fluid quantities may be of several types depending on the problem. They are usually of one of the forms (Dirichlet, Neumann, or Robin-type):

$$w = w_d, \quad \underline{J} \cdot \underline{n} = j_d, \quad \rho_o k(w - w_d) = \underline{J} \cdot \underline{n} \quad (11)$$

where w_d is a prescribed moisture content, j_d is a given normal flux, and k is a surface emissivity (the inverse of an hydraulic resistance), where \underline{n} is the normal to the boundary.

3.2 Strongly coupled constitutive model

The Young modulus are known to be dependent on the moisture content, i.e. $\mathbf{C} = \mathbf{C}(\Delta w)$.

On the other hand, the diffusion of water in hygroscopic wood depends on diffusion of bound water through cell walls and of water vapor in the lumens, both being in equilibrium [25, 9, 26, 27]. At the macroscopic scale, the overall effect is often modeled as a global diffusion with a unique diffusivity tensor \mathbf{D} [28, 29], and a Fick equation, for which

$$\underline{J} = -\rho_o \mathbf{D} \operatorname{grad} \Delta w \quad (12)$$

To keep the constitutive model consistent, a thermodynamics framework is compulsory. The state of the material in each elementary representative volume is described by a certain number of variables. For instance, for the structural part, the strain $\boldsymbol{\varepsilon}$ accounts for the deformation phenomena. The fluid part can also be described by a variable, the amount of water $\rho_o \Delta w$. We restrict ourselves here to these two variables, as sufficient ones to describe the internal material state.

To derive the state laws of the constitutive model, the Gibbs free energy is expressed as a function of the state of the material: $\Psi(\boldsymbol{\varepsilon}, \rho_o \Delta w)$. Following this description, the state laws can be derived as

$$\boldsymbol{\sigma}_r := \frac{\partial \Psi}{\partial \boldsymbol{\varepsilon}} \quad (13)$$

$$A_w := \frac{\partial \Psi}{\partial \rho_o \Delta w} \quad (14)$$

where $\boldsymbol{\sigma}_r$ is defined as a reversible stress, and A_w is the thermodynamic dual variable of $\rho_o \Delta w$.

The dissipation is derived from the Clausius-Duhem inequality, see [30] for instance, as

$$d = \boldsymbol{\sigma} : \dot{\boldsymbol{\varepsilon}} + \Delta \mu \rho_o \Delta \dot{w} - \dot{\Psi} - \underline{J} \cdot \underline{Z} \geq 0 \quad (15)$$

where μ is the massic chemical potential of water [9, 31], and \underline{Z} is its spatial gradient: $\underline{Z} = \operatorname{grad} \Delta \mu$. At local equilibrium, μ is also the chemical potential of the water vapor, that can be linked to the relative humidity H , with the assumption of perfect gas,

$$\mu = \mu_0 + \frac{RT}{M} \ln H \quad (16)$$

μ_0 is the value of the massic chemical potential for a saturated vapor, $R = 8.31 \text{ J K}^{-1} \text{ mol}^{-1}$ is the perfect gas constant, T is the absolute temperature, here $T = T_{\text{ref}} = 298 \text{ K}$, and $M = 18 \text{ g/mol}$ is the molar mass of water. The corresponding value at the reference state is μ_{ref} , and

$$\Delta \mu = \mu - \mu_{\text{ref}} = \frac{RT}{M} \ln \frac{H}{H_{\text{ref}}} \quad (17)$$

Using the previous state laws, the dissipation reads

$$d = (\boldsymbol{\sigma} - \boldsymbol{\sigma}_r) : \dot{\boldsymbol{\varepsilon}} + (\Delta \mu - A_w) \rho_o \Delta \dot{w} - \underline{J} \cdot \underline{Z} \geq 0 \quad (18)$$

This dissipation is assumed to be expressed from the gradient of a potential, here chosen as

$$\Phi(\underline{Z}) = \frac{1}{2} \underline{Z} \cdot \underline{L} \underline{Z} \quad (19)$$

where \underline{L} is a diffusion tensor for chemical potential (homogeneous to $\text{kg.m}^{-3}.\text{s}^2$). This choice is made to recover a Fick-like diffusion behavior. Indeed, with $d = (\partial\Phi/\partial\underline{Z}) \cdot \underline{Z}$, one gets the evolution laws:

$$\underline{\sigma} = \underline{\sigma}_r \quad (20)$$

$$\Delta\mu = A_w \quad (21)$$

$$-\underline{J} = \underline{L} \underline{Z} \quad (22)$$

The fact that the moisture flux can be driven by the moisture gradient (12) or the chemical potential gradient (22) depends on the modeling, and on the fact that the corresponding diffusivity tensors may depend on the current state. For instance, with the state description with the couple $(\underline{\varepsilon}, \rho_o \Delta w)$, (22) can be written as

$$\underline{J} = -\underline{L} \text{grad } A_w = -\underline{L} \frac{\partial A_w}{\partial \Delta w} \text{grad } \Delta w - \underline{L} \frac{\partial A_w}{\partial \underline{\varepsilon}} : \text{Grad } \underline{\varepsilon} \quad (23)$$

where the last term (dependence on the stress strain, similar to the Gorsky effect with the stress gradient [32, 33]) is usually neglected for the present application. Then one gets the relationship:

$$\rho_o \underline{D} = \underline{L} \frac{\partial A_w}{\partial \Delta w} \quad (24)$$

with emphasize the possible dependence of the diffusivity on the current state.

We now have to precise the constitutive model. First, we propose the modeling choice for the Gibbs potential:

$$\Psi(\underline{\varepsilon}, \rho_o \Delta w) = \frac{1}{2} \underline{\varepsilon} : \underline{C}(\Delta w) \underline{\varepsilon} - \underline{B}_0(\Delta w) : \underline{C}(\Delta w) \underline{\varepsilon} + \Psi_0(\Delta w) \quad (25)$$

for which the state laws are

$$\underline{\sigma}_r = \frac{\partial \Psi}{\partial \underline{\varepsilon}} = \underline{C}(\underline{\varepsilon} - \underline{B}_0) \quad (26)$$

$$A_w = \frac{\partial \Psi}{\partial \rho_o \Delta w} = \frac{1}{\rho_o} \left(\frac{1}{2} \underline{\varepsilon} : \underline{C}' \underline{\varepsilon} - \underline{B}'_0 : \underline{C} \underline{\varepsilon} - \underline{B}_0 : \underline{C}' \underline{\varepsilon} + \Psi'_0 \right) \quad (27)$$

\underline{B}_0 is homogeneous to a strain tensor, coupling elasticity and moisture, corresponding to the swelling / shrinkage phenomenon; Ψ_0 is a potential to be identified. Indeed, when considering an evolution at null stress, $\underline{\varepsilon}|_{\underline{\sigma}=0} = \underline{B}_0(\Delta w)$ and the fitting (5) gives

$$\underline{B}_0(\Delta w) = \underline{A} \Delta w \quad (28)$$

With the isothermal sorption curve at null stress (4) and the expression (17), one gets

$$\Psi'_0(\Delta w) = \rho_o \frac{RT}{M} \ln[f^{-1}(\Delta w)] + \frac{1}{2} \Delta w (\underline{A} : \underline{C}' \underline{A}) \Delta w + (\underline{A} : \underline{C} \underline{A}) \Delta w \quad (29)$$

Note that the inverse function f^{-1} is required. With the GAB model used herein, this inversion can be done analytically (at least on the range $-\frac{1}{(C-1)K} < H < \frac{1}{K}$; to be able to use the logarithm, one may restrict himself to $0 < H < \frac{1}{K}$, which corresponds to $w > 0$). If not, it is still possible to represent the sorption curve as a tabulated function, given by experimental values, that can be inverted by switching entries of the table, with an interpolation between experimental points and a suitable management of out-of-range values. The first term is indeed the variation of chemical potential during the sorption test, see Figure 2.

3.3 Choice of the coupling parameters

To express the dependency of Hooke operator with respect to the moisture content, a practical approach consists in considering the components of the 6×6 compliant matrix with Voigt notations S_{ij} , $i = 1, \dots, 6$, $j = 1, \dots, 6$. Each of them is usually linked to the moisture content w as follows:

$$\frac{1}{S_{ij}} = \frac{1}{S_{ij}^{\text{ref}}} (1 - b_{ij} \Delta w) \quad (30)$$

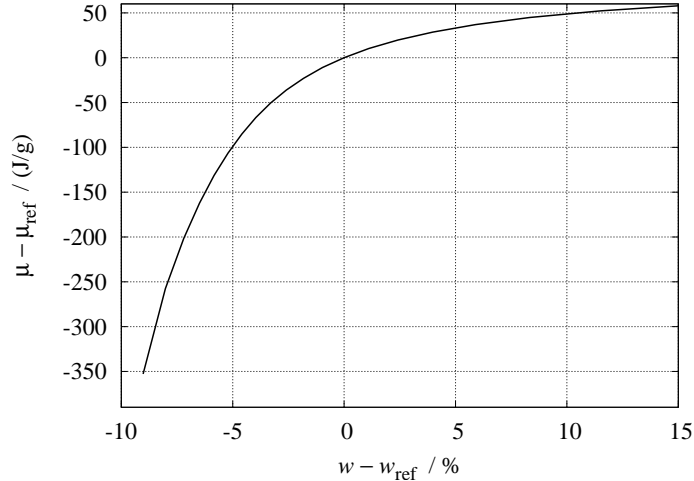


Figure 2: Evolution of massic chemical potential vs. moisture content

where S_{ij}^{ref} is the corresponding component at reference state, and b_{ij} is an adimensional parameter. The values obtained in [34, 35, 36] are used here: with the same notation as in Section 2.2, these parameters are stored in the matrix \mathbf{b} :

$$\mathbf{b} = \begin{bmatrix} 1.0 & 1.2 & 1.2 & 0 & 0 & 0 \\ 1.2 & 3.0 & 3.0 & 0 & 0 & 0 \\ 1.2 & 3.0 & 3.0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 2 \times 2.0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 2 \times 2.0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 2 \times 2.0 \end{bmatrix}_{(L,R,T)} \quad (31)$$

This model is consistent for a limited range of moisture content values, especially to maintain the positive definiteness of the Hooke tensor. For the considered values, one can check that this is the case up to $\Delta w \approx 25\%$, i.e. far within the range of the variation of moisture content for our application (see Figure 1). It is nevertheless checked in the code that intermediate solutions during the iterations do not exceed this value.

As a consequence, $\mathbf{C} = \mathbf{S}^{-1}$ is a non linear function of the moisture content: It decreases when the moisture content increases; therefore the following notation is useful for subsequent developments:

$$\mathbf{C}(\Delta w) = \mathbf{C}_{\text{ref}} - \tilde{\mathbf{C}}(\Delta w) \quad (32)$$

where $\mathbf{C}_{\text{ref}} = \mathbf{C}(\Delta w = 0)$.

The diffusivity dependence on the current state is usually determined with a phenomenological identification. Within the orthotropic basis,

$$\mathbf{D}_{\text{ref}} = \begin{bmatrix} D_L & 0 & 0 \\ 0 & D_R & 0 \\ 0 & 0 & D_T \end{bmatrix} \quad (33)$$

For the dependence on moisture, under null stress, we choose to reuse the values obtained for European beech in [14, 37], for which $D_\alpha = D_{\text{ref}\alpha} \exp(c_\alpha \Delta w)$, $\alpha = L, R, T$, and the diffusivity values are recalled in Table 1. For the dependence on stress, we rely again on a phenomenological identification, though it is difficult to perform here due to the neglected mechano-sorptive effects, that nevertheless may occur when applying a prescribed stress on the specimen. According to the relationship between different expressions of the diffusion driving gradient that can be obtained (83), we use herein the following model:

$$D_\alpha = \frac{\exp(c_\alpha \Delta w)}{1 + \left| \frac{1}{\sigma_0} \mathbf{A} : \boldsymbol{\sigma} \right|} D_{\text{ref}\alpha} \quad (34)$$

The value of σ_0 can be identified from experiments as those in [29] (for Douglas Fir), and we use the corresponding value of $\sigma_0 = 1.9$ MPa.

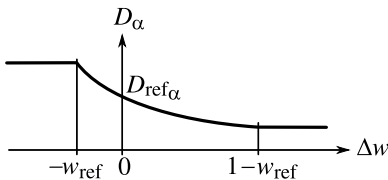


Figure 3: Evolution of diffusivity vs. moisture content

Note that, with an iterative scheme, the diffusivity may have to be evaluated for non physical values of moisture content (i.e. values for non converged quantities during iterations). In order to increase the robustness of the approach, the exponential form is cutted out over the physical window of moisture content values, i.e. Δw is replaced in the previous expression (34) with $\min[\max(\Delta w, -w_{\text{ref}}), 1 - w_{\text{ref}}]$, $(-w_{\text{ref}})$ and $(1 - w_{\text{ref}})$ being the extrema for the allowable values of moisture content Δw . This lead to use a dependence on the moisture content of the form described in Figure 3.

4 PARTITIONING STRATEGY FOR 3D PROBLEM

The main interest in using a partitioning scheme rather than a monolithic solver when dealing with multiphysics problems lies in (see [38, 39, 40, 41, 42, 43] for instance):

- the possibility to couple different numerical codes (for the different physics);
- the increase in flexibility (useful when adding a new physics, or for code maintenance and evolution).

The main difficulties concern the case of strong coupling for which

- iterations are mandatory to recover the coupling effects;
- the robustness is not ensured, which may lead to a lack of convergence.

Herein, we focus on a class of partitioning schemes that promote the interactions between subsystems, i.e. the local coupled equations between the different physics, by emphasizing on material fields that participate to the interactions. Within this class of solvers, one may find the Large Time Increment (LATIN) approach [44, 45, 46], and for coupling different bodies with contact and friction, the Non Smooth Contact Dynamics (NSCD) approach [47, 48].

These approaches lead to isolate the treatment of the interactions from the behavior of the subsystems themselves for which adequate techniques can be used in a modular fashion. Indeed, they deal with iterations involving a local coupled resolution when expressing the coupled constitutive equations on one hand, and admissibility conditions on the other hand, as does the proposed approach.

4.1 Splitting the constitutive relations

To focus on coupled and non-linear equations, constitutive relations are partitioned according to the following splitting:

$$\boldsymbol{\sigma} = \mathbf{C}_{\text{ref}} \boldsymbol{\varepsilon} + \tilde{\boldsymbol{\sigma}} \quad (35)$$

where the pair $(\tilde{\boldsymbol{\sigma}}, \boldsymbol{\varepsilon})$ is linked with Δw :

$$\tilde{\boldsymbol{\sigma}} = -\tilde{\mathbf{C}}(\Delta w) \boldsymbol{\varepsilon} - \mathbf{C}(\Delta w) \mathbf{A} \Delta w \quad (36)$$

On the other hand,

$$\Delta \mu = c \Delta w + \tilde{\mu} \quad (37)$$

with $c = \frac{1}{\rho_o} \mathbf{A} : \mathbf{C}_{\text{ref}} \mathbf{A}$ and the pair $(\tilde{\mu}, \Delta w)$ is linked with $\boldsymbol{\varepsilon}$:

$$\tilde{\mu} = \mu_1(\boldsymbol{\varepsilon}, \Delta w) + \mu_2(\Delta w) \quad (38)$$

where $\mu_2(\Delta w)$ collects nonlinear terms, and $\mu_1(\boldsymbol{\varepsilon}, \Delta w)$ the coupling terms:

$$\mu_1(\boldsymbol{\varepsilon}, \Delta w) = \frac{1}{\rho_o} \left[-\frac{1}{2} \boldsymbol{\varepsilon} : \tilde{\mathbf{C}}' \boldsymbol{\varepsilon} - \mathbf{A} : \mathbf{C} \boldsymbol{\varepsilon} + \mathbf{A} : \tilde{\mathbf{C}}' \boldsymbol{\varepsilon} \Delta w \right] \quad (39)$$

$$\mu_2(\Delta w) = \frac{RT}{M} \ln[f^{-1}(\Delta w)] - \frac{1}{\rho_o} \left[(\mathbf{A} : \tilde{\mathbf{C}} \mathbf{A}) \Delta w + \frac{1}{2} (\mathbf{A} : \tilde{\mathbf{C}}' \mathbf{A}) (\Delta w)^2 \right] \quad (40)$$

Finally for the diffusion part, using a constant diffusivity \mathbf{D}_0 as a parameter for the approach,

$$\underline{J} = -\rho_o \mathbf{D}_0 \underline{F} + \tilde{\underline{J}} \quad (41)$$

where $\underline{F} = \underline{\text{grad}} \Delta w$. The pair $(\tilde{\underline{J}}, \underline{F})$ is linked with $\boldsymbol{\sigma}$ and Δw :

$$\tilde{\underline{J}} = -\rho_o [\mathbf{D}(\boldsymbol{\sigma}, \Delta w) - \mathbf{D}_0] \underline{F} \quad (42)$$

4.2 Admissibility closure equations

The admissibility conditions arise from the conservation principles. They are linear when a suited choice of variables is used, and they will be used here to close the problem by adding equations linking the unknown couples $(\tilde{\boldsymbol{\sigma}}, \boldsymbol{\varepsilon})$ on one side, independently of $(\tilde{\boldsymbol{\mu}}, \Delta w)$ and $(\tilde{\underline{J}}, \underline{F})$ on the other side, while being kept linear (but global on the studied spatial domain).

4.2.1 Solid part.

This structural problem is close to an elastic analysis, modeled with elliptic partial differential equations. Therefore, finite elements are a suited discretization tool, and they will be used in the following [49]. With a displacement-oriented approach, the displacement field is described with a finite number of values, defined at the nodes of the finite element mesh, while strain and stress fields are evaluated at integration points within each element.

The conservation of momentum is

$$\mathbf{B}_\sigma^T \boldsymbol{\sigma} = f_d \quad (43)$$

where $\boldsymbol{\sigma}$ is here the column vector of values of the stress tensor field $\boldsymbol{\sigma}$, defined at integration points of the solid mesh, and f_d are the generalized external forces. The operator \mathbf{B}_σ is classically defined as

$$\forall \underline{u}, \int_{\Omega} \boldsymbol{\varepsilon}(\underline{u}) : \boldsymbol{\sigma} \, d\Omega = \underline{u}^T \mathbf{B}_\sigma^T \boldsymbol{\sigma}$$

where \underline{u} is the column vector of nodal displacement \underline{u} . On the other hand, the strain column vector is

$$\boldsymbol{\varepsilon} = \mathbf{B}_\varepsilon \underline{u} \quad (44)$$

With the previous constitutive-like relation (35), the previous admissibility equations give

$$\underbrace{[\mathbf{B}_\sigma^T \mathbf{C}_{\text{ref}} \mathbf{B}_\varepsilon]}_{\mathbf{K}} \underline{u} + \mathbf{B}_\sigma^T \tilde{\boldsymbol{\sigma}} = f_d \quad (45)$$

where \mathbf{K} is the stiffness matrix. With appropriate boundary conditions on the displacement field, this problem is regular, and the strain is

$$\boldsymbol{\varepsilon} = \mathbf{B}_\varepsilon \mathbf{K}^{-1} f_d - \mathbf{X}_S \tilde{\boldsymbol{\sigma}} \quad (46)$$

with $\mathbf{X}_S = \mathbf{B}_\varepsilon \mathbf{K}^{-1} \mathbf{B}_\sigma^T$. Note that, from a computational point of view, \mathbf{X}_S should not be assembled explicitly, due to the large cost of producing the inverse of the stiffness matrix; on the other hand, its product with a stress requires a global elastic solve.

4.2.2 Fluid part.

This fluid problem is a transient diffusion problem, modeled with parabolic partial differential equations. Finite elements (unless stabilized [50, 51]) are less suited to such a problem, but they will nevertheless be used in the following. Using more dedicated discretization tools, such as finite differences, finite volumes or even discrete elements and discontinuous Galerkin approach, would lead to different discrete matrices, but the coupling terms would be similar as those used herein. Coupling different discretization schemes

is not under the scope of this article, but is currently under development. Here, the discretization of the moisture content field lead to select its values at the nodes of the mesh as primary unknowns. The integration points are the support of several dual fields: the moisture gradient associated to the water mass flux, and the chemical potential associated to the moisture content itself. Concerning time evolutions, a classical incremental scheme is used.

The conservation of mass for the fluid phase (10) is written at the discretized level as

$$-\mathbf{B}_q^T \rho_o \mathbf{B}_w \Delta \dot{w} + \mathbf{B}_J^T J = g_d \quad (47)$$

The column vector of nodal moisture content is Δw , and the vector of moisture gradient values is $F = \mathbf{B}_F \Delta w$. These last values are expressed at the integration points of the fluid mesh, as for the vector of water mass flux J . By a simple extrapolation with finite element shape functions, the moisture content itself can be expressed at the same integration points: $W = \mathbf{B}_w \Delta w$. Finally, the operators \mathbf{B}_q and \mathbf{B}_J are defined as

$$\forall \Delta w, \int_{\Omega} \Delta w q d\Omega = (\Delta w)^T \mathbf{B}_q^T q \quad \text{and} \quad \int_{\Omega} \underline{\text{grad}}(\Delta w) \cdot \underline{J} d\Omega = (\Delta w)^T \mathbf{B}_J^T J$$

With (42) and after algebraic manipulations, one gets

$$\underbrace{[\mathbf{B}_q^T \rho_o \mathbf{B}_w]}_{\mathbf{M}} \Delta \dot{w} + \underbrace{[\mathbf{B}_J^T \rho_o \mathbf{D}_0 \mathbf{B}_F]}_{\mathbf{H}} \Delta w - \mathbf{B}_J^T \tilde{J} = -g_d \quad (48)$$

\mathbf{M} is a ‘capacity’-like matrix, and \mathbf{H} is the diffusivity matrix. A time integration scheme is needed (here the θ -method): $\Delta \dot{w} = \frac{1}{\theta \delta t} (\Delta w - \Delta w_i) - \frac{1-\theta}{\theta} \Delta \dot{w}_i$, where δt is the time step and $\theta \in [0, 1]$ is the parameter of the scheme, Δw_i and $\Delta \dot{w}_i$ being the values at the previous time step. Therefore,

$$\underbrace{\left(\frac{1}{\theta \delta t} \mathbf{M} + \mathbf{H} \right)}_{\tilde{\mathbf{M}}} \Delta w = - \underbrace{\left(g_d - \frac{1}{\theta \delta t} \mathbf{M} [\Delta w_i + (1-\theta) \delta t \Delta \dot{w}_i] \right)}_{\tilde{g}_d} + \mathbf{B}_J^T \tilde{J} \quad (49)$$

$\tilde{\mathbf{M}}$ is sometimes referred to as a ‘dynamical’ matrix. It is regular, and one gets

$$F = -\mathbf{B}_F \tilde{\mathbf{M}}^{-1} \tilde{g}_d + \mathbf{X}_F \tilde{J} \quad (50)$$

with $\mathbf{X}_F = \mathbf{B}_F \tilde{\mathbf{M}}^{-1} \mathbf{B}_J^T$. As previously, \mathbf{X}_F is not explicitly assembled, and its product with a flux requires the solve of a global diffusion problem.

4.3 A non linear Jacobi-like iterative partitioned scheme

At each time step of the incremental scheme, the reference problem consists in finding the fields $(\tilde{\boldsymbol{\sigma}}, \tilde{\mu}, \tilde{J}; \boldsymbol{\varepsilon}, \Delta w, \underline{F})$ satisfying:

- the linear global solid structure behavior (46),
- the linear global fluid behavior (50) and (37),
- the nonlinear coupled local constitutive behaviors (36), (38), (42).

To derive a partitioning scheme, we propose to split the global operators into $\mathbf{X}_S = \mathbf{X}_S^D + (\mathbf{X}_S - \mathbf{X}_S^D)$, and $\mathbf{X}_F = \mathbf{X}_F^D + (\mathbf{X}_F - \mathbf{X}_F^D)$.

The operators \mathbf{X}_S^D and \mathbf{X}_F^D are supposed to play the role of search directions, and to keep the coupled non-linearities local in space variables: they should be decoupled from each integration point to the other. They can be viewed as ‘diagonals’ of initial operators, or more simply, one can choose $\mathbf{X}_S^D = \mathbf{C}_{\text{ref}}^{-1}$ and $\mathbf{X}_F^D = \frac{1}{\rho_o} \mathbf{D}_0^{-1}$. Concerning the parameter \mathbf{D}_0 , one can choose the value of diffusivity for null stress and $\Delta w = 0$, i.e. \mathbf{D}_{ref} .

An iterative procedure consists in updating an iterate $(\tilde{\boldsymbol{\sigma}}, \tilde{J})^{(k-1)}$ following (50), (46), such that:

$$\boldsymbol{\varepsilon}^{(k)} + \mathbf{X}_S^D \tilde{\boldsymbol{\sigma}}^{(k)} = \mathbf{B}_\varepsilon \mathbf{K}^{-1} f_d - (\mathbf{X}_S - \mathbf{X}_S^D) \tilde{\boldsymbol{\sigma}}^{(k-1)} \quad (51)$$

$$F^{(k)} - \mathbf{X}_F^D \tilde{J}^{(k)} = -\mathbf{B}_F \tilde{\mathbf{M}}^{-1} \tilde{g}_d + (\mathbf{X}_F - \mathbf{X}_F^D) \tilde{J}^{(k-1)} \quad (52)$$

together with the constitutive relations (36), (42). No admissibility condition involve the pair $(\tilde{\mu}, \Delta w)$: Once ε and Δw are known, $\Delta\mu$ can be evaluated with (37) and (38).

This leads to the following (coupled but local at each integration point) system:

$$[(\mathbf{X}_S^D)^{-1} - \tilde{\mathbf{C}}(W^{(k)})]\varepsilon^{(k)} = \sigma_d + \mathbf{C}(W^{(k)})\mathbf{A}W^{(k)} \quad (53)$$

$$[(\mathbf{X}_F^D)^{-1} + \rho_o(\mathbf{D}(\sigma^{(k)}, W^{(k)}) - \mathbf{D}_0)]F^{(k)} = J_d \quad (54)$$

$$\sigma^{(k)} = \mathbf{C}(W^{(k)})(\varepsilon^{(k)} + \mathbf{A}W^{(k)}) \quad (55)$$

$$\tilde{\mu}^{(k)} = \mu_1(\varepsilon^{(k)}, W^{(k)}) + \mu_2(W^{(k)}) \quad (56)$$

where

$$\sigma_d = (\mathbf{X}_S^D)^{-1}[\mathbf{B}_\varepsilon \mathbf{K}^{-1} f_d - (\mathbf{X}_S - \mathbf{X}_S^D)\tilde{\sigma}^{(k-1)}] \quad (57)$$

$$J_d = (\mathbf{X}_F^D)^{-1}[-\mathbf{B}_F \tilde{\mathbf{M}}^{-1} \tilde{g}_d + (\mathbf{X}_F - \mathbf{X}_F^D)\tilde{J}^{(k-1)}] \quad (58)$$

$$W^{(k)} = \mathbf{B}_w \Delta w^{(k-1)} \quad (59)$$

are constant during an iteration. Note that their evaluations require to solve two decoupled global and linear equations: one for an elastic structure problem, one for a linear diffusion problem.

This problem is easily solved with a given $(\tilde{\sigma}, \Delta w, \tilde{J})^{(k-1)}$: first, $(\sigma_d, J_d, W^{(k)})$ are computed with (57), (58), (59); second, (53) is solved to get $\varepsilon^{(k)}$; third, (54), (55) are used to get $F^{(k)}$, and finally, if needed, $\tilde{\mu}^{(k)}$ is obtained from (56). Algorithm 1 gives the overall procedure. Note that, apart from the incremental scheme, this algorithm requires independent solves for each physics (a classical elastic problem and a classical diffusion problem), and local computations to recover the coupled effects. If the previous parameters \mathbf{X}_S^D and \mathbf{X}_F^D are selected as before, the global problems to be solved have constant left hand sides, and are factorized only once during the initialization phase.

Note that due to a strong coupling between fluid and structure, there is a need for an iterative scheme between the two physics for each time step, contrary to staggered schemes [52, 53, 54, 55, 43]. At convergence for each time step, the produced solution is the same as for a full coupled solution scheme. The stability of the proposed partitioning approach is therefore entirely inherited from the time integration scheme that is used, and is not degraded.

For the termination criteria, apart from a classical stationary criteria, we proposed to use the following error estimators: the error indicators η_S for the elastic (solid) part, and η_F for the diffusion (fluid) part:

$$\eta_F^{(k)} = \frac{\|F^{(k)} - \tilde{F}^{(k)}\|_F}{\|F^{(k)} + \tilde{F}^{(k)}\|_F} \quad \text{and} \quad \eta_S^{(k)} = \frac{\|\varepsilon^{(k)} - \tilde{\varepsilon}^{(k)}\|_S}{\|\varepsilon^{(k)} + \tilde{\varepsilon}^{(k)}\|_S} \quad (60)$$

with the energy norms:

$$\|\bullet\|_S = \left(\frac{1}{2} \int_{\Omega} \bullet \mathbf{C}_{\text{ref}} \bullet d\Omega \right)^{1/2} \quad \text{and} \quad \|\bullet\|_F = \left(\frac{1}{2} \int_{\Omega} \bullet \rho_o \mathbf{D}_0 \bullet d\Omega \right)^{1/2} \quad (61)$$

Indeed, if fluxes $\tilde{F}^{(k)}$ and $F^{(k)}$ are equal ($\tilde{F}^{(k)} = F^{(k)} = F$), as well as strain fields $\tilde{\varepsilon}^{(k)}$ and $\varepsilon^{(k)}$ ($\tilde{\varepsilon}^{(k)} = \varepsilon^{(k)} = \varepsilon$), with the local coupled problem solving, the fields satisfying the constitutive behaviors, $\tilde{J}^{(k)}$ and $\tilde{\sigma}^{(k)}$ are computed as functions of F and ε . Then, with the global solid problem, the new flux satisfying the admissibility conditions with $\tilde{\sigma}^{(k)}$ is again F . The global fluid problem ensures as well that ε is admissible with $\tilde{\sigma}^{(k)}$. Therefore the set $(F, \tilde{J}^{(k)}; \varepsilon, \tilde{\sigma}^{(k)})$ satisfies both the constitutive relations and the admissibility conditions. If the reference problem is well posed, it is therefore the solution.

The convergence is declared when $\eta_S < \varepsilon_S$ and $\eta_F < \varepsilon_F$ with the user-given thresholds ε_S and ε_F .

4.4 Test case and performance comparisons

In this Section, the proposed strategy is compared to a monolithic scheme with a direct coupled solid-fluid solver. In the following simplified case, we implement a classical modified Newton resolution in a standard 3D finite element code, namely Cast3M [56]. For testing purposes, we simplify the geometry with an homogeneous 3D block of size 531 mm \times 787 mm \times 13 mm, and an orthotropic material with a local basis defined with a uniform angle α , Figure 4. We also consider simplified couplings: (i) a constant

Algorithm 1 Main algorithm

```
1: Initialization (first time step,  $i \leftarrow 1$ , initial conditions)
2:   Set  $\Delta w_i \leftarrow 0$ ,  $\Delta \dot{w}_i \leftarrow 0$ 
3:   Set  $\tilde{\sigma}_i \leftarrow 0$ 
4:   Set  $\tilde{J}_i \leftarrow 0$ 
5: {Loop on time steps}
6: for  $i = 2, \dots, n$  do
7:   Compute right-hand sides  $f_{d_i}$  and
8:      $\Delta \tilde{w}_{i-1} \leftarrow \Delta w_{i-1} + (1 - \theta)\delta t \Delta \dot{w}_{i-1}$ 
9:      $\tilde{g}_{d_i} \leftarrow g_{d_i} - \frac{1}{\theta \delta t} \mathbf{M} \Delta \tilde{w}_{i-1}$ 
10:  Initial guess ( $k \leftarrow 1$ )
11:    Initiate  $\tilde{\sigma}^{(k)} \leftarrow \tilde{\sigma}_{i-1}$ 
12:    Initiate  $\tilde{J}^{(k)} \leftarrow \tilde{J}_{i-1}$ 
13:  {Loop on inner iterations}
14:  repeat
15:     $k \leftarrow k + 1$ 
16:    Global solid problem
17:    Solve  $\mathbf{K}u^{(k)} = f_{d_i} - \mathbf{B}_\sigma^T \tilde{\sigma}^{(k-1)}$  to get  $u^{(k)}$ 
18:    Compute  $\tilde{\varepsilon}^{(k)} \leftarrow \mathbf{B}_\varepsilon u^{(k)}$ 
19:    Compute  $\sigma_d \leftarrow (\mathbf{X}_S^D)^{-1} \tilde{\varepsilon}^{(k)} + \tilde{\sigma}^{(k-1)}$ 
20:    Global fluid problem
21:    Solve  $\tilde{\mathbf{M}} \Delta w^{(k)} = -\tilde{g}_{d_i} + \mathbf{B}_J^T \tilde{J}^{(k-1)}$  to get  $\Delta w^{(k)}$ 
22:    Compute  $W^{(k)} \leftarrow \mathbf{B}_w \Delta w^{(k)}$ 
23:    Compute  $\tilde{F}^{(k)} \leftarrow \mathbf{B}_F \Delta w^{(k)}$ 
24:    Compute  $J_d \leftarrow (\mathbf{X}_F^D)^{-1} \tilde{F}^{(k)} - \tilde{J}^{(k-1)}$ 
25:    Local coupled problem (at each integration point)
26:    Set  $\tilde{\sigma}_d \leftarrow \sigma_d + \mathbf{C}(W^{(k)}) \mathbf{A} W^{(k)}$ , and
27:    Solve  $[(\mathbf{X}_S^D)^{-1} - \tilde{\mathbf{C}}(W^{(k)})] \varepsilon^{(k)} = \tilde{\sigma}_d$  to get  $\varepsilon^{(k)}$ 
28:    Update  $\tilde{\sigma}^{(k)} \leftarrow -(\mathbf{X}_S^D)^{-1} (\varepsilon^{(k)} - \tilde{\varepsilon}^{(k)}) + \tilde{\sigma}^{(k-1)}$ 
29:    Set  $\hat{\sigma} \leftarrow \mathbf{C}_{\text{ref}} \varepsilon^{(k)} + \tilde{\sigma}^{(k)}$  and  $\tilde{\mathbf{D}} \leftarrow \mathbf{D}(\hat{\sigma}, W^{(k)})$  and
30:    Solve  $[\rho_o(\tilde{\mathbf{D}} - \mathbf{D}_0) + (\mathbf{X}_F^D)^{-1}] F^{(k)} = J_d$  to get  $F^{(k)}$ 
31:    Update  $\tilde{J}^{(k)} \leftarrow (\mathbf{X}_F^D)^{-1} (F^{(k)} - \tilde{F}^{(k)}) + \tilde{J}^{(k-1)}$ 
32:    Compute  $\eta_S^{(k)}$  and  $\eta_F^{(k)}$ 
33:    {Convergence criteria}
34:    if  $(\eta_S^{(k)} < \epsilon_S$  and  $\eta_F^{(k)} < \epsilon_F)$  then
35:      Set  $\Delta w_i \leftarrow \Delta w^{(k)}$ ,  $\Delta \dot{w}_i \leftarrow \frac{1}{\theta \delta t} (\Delta w_i - \Delta \tilde{w}_{i-1})$ 
36:      Set  $\tilde{\sigma}_i \leftarrow \tilde{\sigma}^{(k)}$ 
37:      Set  $\tilde{J}_i \leftarrow \tilde{J}^{(k)}$ 
38:    end if
39:  until  $(\eta_S^{(k)} \geq \epsilon_S$  or  $\eta_F^{(k)} \geq \epsilon_F)$ 
40: end for
```

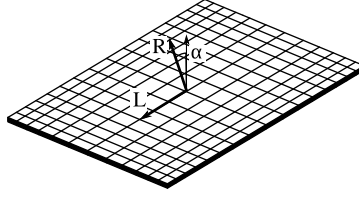


Figure 4: Simplified test case

σ_0 / MPa	500	100	50	10	5
n_N	4.2	5.1	5.8	9.8	no convergence
n_P	4.0	5.5	5.8	9.6	no convergence

Table 2: Average number of inner iterations per time step, n_N for the Newton solver, n_P for the proposed partitioned solver, with respect to the coupling strength (and $\alpha = 20^\circ$).

Hooke stiffness $\mathbf{C} = \mathbf{C}_{\text{ref}}$ (but still the same swelling / shrinkage \mathbf{A}), such that the solid equilibrium reads

$$\mathbf{K}u - \mathbf{N}\Delta w = f_d \quad (62)$$

with $\mathbf{N} = \mathbf{B}_\sigma^T \mathbf{C}_{\text{ref}} \mathbf{A}$, and (ii) for not a too strong coupling, we linearized the dependence of the diffusion coefficients on the stress, and we neglect the dependence on the current moisture content, as:

$$\rho_o \mathbf{D}(\boldsymbol{\sigma}) = \left(1 - \left| \frac{1}{\sigma_0} \mathbf{A} : \boldsymbol{\sigma} \right| \right) \rho_o \mathbf{D}_{\text{ref}} \quad (63)$$

With a modified Newton scheme as a monolithic solver, the tangent operator has to be computed at the beginning of each time step, but is kept constant for the inner loops. Due to the norm in (63), this expression is not differentiable at $\boldsymbol{\sigma} = 0$, and so is the left-hand-side contribution $\mathbf{H}(\boldsymbol{\sigma}) = \mathbf{B}_J^T \rho_o \mathbf{D} \mathbf{B}_F$. We therefore use a generalized Newton approach [57, 58] for systems that are piecewise differentiable, for which

$$\partial_\sigma \mathbf{H} : \boldsymbol{\sigma}^* = -\mathbf{B}_J^T \left| \frac{1}{\sigma_0} \mathbf{A} : \boldsymbol{\sigma}^* \right| \rho_o \mathbf{D}_{\text{ref}} \mathbf{B}_F \quad (64)$$

The upper surface is prescribed to a null moisture flux (impervious boundary condition), while the remaining part of the boundary is subjected to a prescribed moisture content $\Delta w_d(t) = f(H(t)/H_{\text{ref}})$ with $H(t) = H_{\text{ref}} - 0.2 \sin(2\pi t/T)$ and $H_{\text{ref}} = 65\%$. The studied time interval $[0, T]$ with $T = 20$ days is discretized in 10 time steps. No external forces are considered, and only 6 displacement dofs are clamped to avoid rigid body motions.

The comparisons are performed for different values of σ_0 (expected to change the strength of the coupling). The spatial discretization uses 1152 8-node hexahedral elements. The termination criteria for the partitioned approach uses $\epsilon_S = \epsilon_F = \epsilon = 10^{-6}$, and for the Newton solver, for both solid and fluid, the relative residual should not exceeds $\epsilon = 10^{-6}$ as well. Both the monolithic and the partitioned approach lead to the same solution (up to the convergence precision ϵ).

In each case, the cost is expected to be driven by the linear global solves. The linear problem to solve at each Newton iteration is half decoupled (the fluid problem can be solved first, then the solid problem can be solved in a second hand). This is therefore optimistic for the Newton approach, since then, the cost is equivalent for both the two approaches, at each global solve. Nevertheless, the tangent linear operator is updated at each time step for the modified Newton scheme (that requires as many factorizations as time steps, and as many forward-backward solves as inner Newton iterations), but the left-hand-side is constant for the partitioned approach (that requires only one factorization for each physics, and as many forward-backward solves as inner fixed-point iterations).

Table 2 compares the number of inner iterations for both approaches with respect to the value of the coupling strength σ_0 (decreasing its value leads to a stronger coupling). In the convergence domain, both approaches require roughly the same number of inner iterations. Since left-hand-sides for the partitioned approaches are factorized only once, this approach is therefore the most efficient. There is indeed a domain where the fixed-point like approach failed to converge when the coupled non-linearities become larger, but this convergence failure appears at the same time as for the Newton solver.

5 MODEL COUPLING

Due to the nature of the application, a full 3D model is not required. The aim of this Section is to adapt the previous approach to a particular case of plate model for elasticity and 1D model for diffusion. Therefore, this Section emphasizes the modularity of the proposed approach, since the only modification concerns the solver black-box. The same modularity feature could be used when different finite element meshes are used for each physics.

5.1 Structural model

Painted panels of cultural heritage often exhibit a small thickness to in-plane length ratio. For instance, in the case of *Mona Lisa*, the thickness e of the poplar panel ranges between 12.4 mm and 13.8 mm, its width between 53.3 cm and 53.4 cm, and its height h between 79.1 cm and 79.4 cm [13]. Therefore, neglecting also the curvature effects, the structure is usually modeled as a plate satisfying Kirchhoff-Love assumptions [59]. The 3D displacement field is therefore described with the displacement of the average surface displacement denoted with \underline{u} for the displacement in the plane directions, and v for the transverse displacement, as

$$\underline{U} = \underline{u} + v\mathbf{e}_3 - z \text{grad } v \quad (65)$$

\mathbf{e}_3 is the normal vector along the thickness, and z is the associated coordinate. Here, the derivatives are performed with respect to the planar coordinates. The corresponding generalized strains are $(\mathbf{e}, \boldsymbol{\chi})$, with

$$\begin{aligned} \mathbf{e} &= (\text{Grad } \underline{u})_{\text{sym}} \\ \boldsymbol{\chi} &= -\text{Grad}(\text{grad } v) \end{aligned} \quad (66)$$

which allow to recover the plane part of the strain as

$$[\boldsymbol{\varepsilon}] = \mathbf{e} + z\boldsymbol{\chi} \quad (67)$$

Moreover, the plane stress state is also assumed. Using Hellinger-Reissner variational formulation allows to define (i) the consistent generalized stresses (\mathbf{N}, \mathbf{M}) :

$$\begin{aligned} \mathbf{N} &= \langle [\boldsymbol{\sigma}] \rangle \\ \mathbf{M} &= \langle z[\boldsymbol{\sigma}] \rangle \end{aligned} \quad (68)$$

where $[\bullet]$ and $\langle \bullet \rangle$ denote the planar part and the average with respect to thickness, respectively; and (ii) the generalized constitutive relation, considering (35):

$$\begin{aligned} \mathbf{N} &= \langle \mathbf{C}_{\text{ref}}^{\text{cp}} \rangle \mathbf{e} + \langle z\mathbf{C}_{\text{ref}}^{\text{cp}} \rangle \boldsymbol{\chi} + \tilde{\mathbf{N}} \\ \mathbf{M} &= \langle z\mathbf{C}_{\text{ref}}^{\text{cp}} \rangle \mathbf{e} + \langle z^2\mathbf{C}_{\text{ref}}^{\text{cp}} \rangle \boldsymbol{\chi} + \tilde{\mathbf{M}} \end{aligned} \quad (69)$$

where $\mathbf{C}_{\text{ref}}^{\text{cp}}$ is the elastic tensor that links the plane parts of stress and strain tensors with the plane stress assumption: $(\mathbf{C}_{\text{ref}}^{\text{cp}})^{-1} = [\mathbf{C}_{\text{ref}}^{-1}]$, and $\tilde{\mathbf{N}} = \langle [\tilde{\boldsymbol{\sigma}}] \rangle$, $\tilde{\mathbf{M}} = \langle z[\tilde{\boldsymbol{\sigma}}] \rangle$.

To adapt the previous algorithm to this model, the most modular approach consists in using the discretized operators $\tilde{\mathbf{K}}$, $\tilde{\mathbf{B}}_\sigma$, $\tilde{\mathbf{B}}_\varepsilon$ corresponding to the discretized plate model, here with DKT plate elements [60]. u now denotes the column vector of plate degrees of freedom.

The previous global solid box is replaced with the plate solver of algorithm 2, where the generalized forces for the plate problem are computed with (68), and by reciprocity, the plane strain $\boldsymbol{\varepsilon}$ is computed from (67), (66). The corresponding structural operator is $\mathbf{X}_S = \tilde{\mathbf{B}}_\varepsilon \mathbf{K}^{-1} \tilde{\mathbf{B}}_\sigma^T$. Since the eventual out-of-plane components of stresses and strains are not taken into account in the plate model resolution, \mathbf{X}_S is not invertible. Nevertheless the partition $\mathbf{X}_S^D = \mathbf{C}_{\text{ref}}^{-1}$ is still regular. Finally, for the termination criteria, $\mathbf{C}_{\text{ref}}^{\text{cp}}$ is used in (61).

5.2 Moisture evolution model

Concerning the moisture content evolution, on the present studied case, only one side of the panel is painted. This side will exhibit a much lower emissivity than the other side. Therefore, apart from some edge effects on the lateral sides, the main moisture gradient occurs along the thickness and neglecting the other directions lead to consider only 1D diffusion along the thickness, and the 1D mesh is a vertical segment. The scalar diffusivity for this problem is then $D = \underline{e}_3^T \mathbf{D} \underline{e}_3$, \underline{e}_3 being the normal to the plate. All the previous developments still hold for the fluid part in this case; the in-plane components of $\tilde{\mathbf{F}}$ are null. The previous global fluid box is therefore replaced with the 1D diffusion solver of algorithm 3.

The overall model coupling uses therefore the diagram of Table 3.

Algorithm 2 Global solid problem for the plate model

- 1: Compute plate loading $\tilde{N}^{(k-1)}, \tilde{M}^{(k-1)}$ from 3D stress $\tilde{\sigma}^{(k-1)}$
 - 2: Solve plate problem $\bar{\mathbf{K}}\mathbf{u}^{(k)} = f_{d_i} - \bar{\mathbf{B}}_{\sigma}^T[\tilde{N}^{(k-1)}, \tilde{M}^{(k-1)}]$ to get $u^{(k)}$
 - 3: Compute plate generalized strains $[\tilde{\epsilon}^{(k)}, \tilde{\chi}^{(k)}] \leftarrow \bar{\mathbf{B}}_{\epsilon}^T u^{(k)}$
 - 4: Compute 3D strain $\epsilon^{(k)}$ from plate generalized strains $\tilde{\epsilon}^{(k)}, \tilde{\chi}^{(k)}$
 - 5: Compute $\sigma_d \leftarrow (\mathbf{X}_S^D)^{-1} \tilde{\epsilon}^{(k)} + \tilde{\sigma}^{(k-1)}$
-

Algorithm 3 Global fluid problem for the 1D diffusion model

- 1: Compute normal component of flux $\tilde{J}_n^{(k-1)}$ from 3D flux $\tilde{J}^{(k-1)}$
 - 2: Solve 1D diffusion problem $\tilde{\mathbf{M}}\Delta w^{(k)} = -\tilde{g}_{d_i} + \bar{\mathbf{B}}_J^T \tilde{J}_n^{(k-1)}$ to get $\Delta w^{(k)}$
 - 3: Compute $W^{(k)} \leftarrow \mathbf{B}_w \Delta w^{(k)}$
 - 4: Compute normal component of moisture gradient $\tilde{F}_n^{(k)} \leftarrow \bar{\mathbf{B}}_F \Delta w^{(k)}$
 - 5: Compute 3D moisture gradient $\tilde{F}^{(k)}$ from its normal component $\tilde{F}_n^{(k)}$
 - 6: Compute $J_d \leftarrow (\mathbf{X}_F^D)^{-1} \tilde{F}^{(k)} - \tilde{J}^{(k-1)}$
-

Solid (plate model)	Interface (3D)	Fluid (1D)
generalized strains $(\mathbf{e}, \boldsymbol{\chi})$	ϵ	
	projection	
generalized stresses $(\tilde{\mathbf{N}}, \tilde{\mathbf{M}})$	$\tilde{\sigma}$	
	restriction	
	W	W
	identity	
	\underline{F}	F_n
	projection	
	\underline{J}	J_n
	restriction	

Table 3: Overall sketch of the model coupling strategy

5.3 Pictural layer

With aging, the pictural layer often became fragile, and a network of fine cracks (*craquelures*) usually developed and hopefully became stable during the past history of the painting [61]. This coating possesses its own permittivity to moisture. Here, we assume the pictural layer to be homogeneous at macro scale (homogenized from the *craquelure* network), and the thickness of the layer negligible when compared to the thickness of the panel, therefore, without adding additional mechanical stiffness.

As for the bulk diffusion, there are several modeling choices for the diffusion through the thin pictural layer. The normal massic flux $j = \underline{J} \cdot \underline{n}$ is linked to the jump in the state variable from one side (the wood panel side) to the other (the environmental air) [62]. Denoting with $[\![\bullet]\!]$ the jump of a quantity, i.e. its value at point \underline{M}_2 minus its value at point \underline{M}_1 , Figure 6, and since there is a water vapor on both sides, one can model the flux as $j = -l[\![\Delta\mu]\!]$ or $j = -m[\![H/H_{\text{ref}}]\!]$ or, when using the sorption curve for the wood side, and a same fictitious wood on the other side, $j = -\rho_o k[\![\Delta w]\!]$. The difference in all these models is the dependency of the material parameter l , m or k on the current state of the layer.

Note that within the framework of the proposed algorithm, each model can be implemented quite easily. For the problem we consider here, the state value at point \underline{M}_2 is prescribed, usually in term of relative humidity: at $z = e/2$, $H = H_d(t)$. Therefore the flux can be split into a prescribed value and a value depending on the state at point \underline{M}_1 : $j = -j_d + mH_1/H_{\text{ref}}$, where $j_d(t) = mH_d(t)/H_{\text{ref}}$, or $j = -j_d + l\Delta\mu_1$ or $j = -j_d + \rho_o k\Delta w_1$. The last case, with a constant parameter k is the simplest one, since it directly depends on the primal unknown $\Delta w_1 = \Delta w(z = e/2)$; therefore the flux $j_d = -\rho_o k\Delta w_d$, with $\Delta w_d(t) = f(H_d(t)/H_{\text{ref}})$, is added to the right hand side, and the diffusion matrix on the left hand side is summed up with $\rho_o k$ for the suited degree of freedom at $z = e/2$. The other cases can be implemented as well. The easiest way to implement this pictural layer effect is to add a special element to the diffusion mesh: an element with a null length (similar to a joint element for 2D or 3D problems), that will add a degree of freedom for moisture content (the one to be prescribed to Δw_d), and for which the gradient F is the jump in moisture content $[\Delta w_d - \Delta w_1]$. There is an additional unique integration point for this element, and provided that operators \mathbf{B}_J , \mathbf{B}_F and \mathbf{D} take into account this additional element, the framework is unchanged.

Here, we consider the model using the moisture content jump, with a parameter k dependent on the surface strain $\epsilon_s = \text{Tr}[\boldsymbol{\varepsilon}(z = \frac{e}{2})] = \text{Tr}(\mathbf{e} + \frac{e}{2}\boldsymbol{\chi})$. In this case, we proceed to the splitting (similar to (41), (42)):

$$j = -\rho_o k(\epsilon_s)[\Delta w_d(t) - \Delta w_1] = -\rho_o k_0[\Delta w_d - \Delta w_1] + \tilde{j} \quad (70)$$

where

$$\tilde{j} = -\rho_o [k(\epsilon_s) - k_0][\Delta w_d - \Delta w_1] \quad (71)$$

which is computed during the local coupled problem as $\tilde{j}^{(k)}$, and added to the right hand side during the global fluid problem, while the left hand side is added to $\rho_o k_0$.

The evaluation of surface emissivity $\rho_o k$ is the most difficult part. Since each workpiece of cultural heritage is a unique object, and due to the difficulty to proceed to tests on these masterpieces, experiments can be conducted on mockups, designed as close as possible to the original studied object. In the scope of this article, we restrict ourselves to an estimation of its value considering the available data in the literature, and some crude micromechanical scenarios.

To get the form of the phenomenological model linking the emissivity k and the strain on the painted surface, we therefore consider a thin layer of either paint and varnish or only varnish (at the fine crack positions), with a given crack density. With a one-dimensional normal diffusion assumption (which is not the case due to the 3D diffusion at the layer thickness scale, but which is sufficient to derive the searched expression), a mixture law gives $k = (1 - \eta_s)k_1 + \eta_s k_2$ where k_1 (resp. k_2) is the emissivity of the painted surface, of area S_1 (resp. the cracked area S_2), and the surface ratio $\eta_s = S_2/(S_1 + S_2)$. The surface area modification due to the strain is ϵ_s . If there is a perfect mechanical link between the pictural layer and the panel, $S_i = S_i^0(1 + \epsilon_s)$, where S_i^0 is the area at reference configuration ($i = 1, 2$); therefore η_s and the emissivity are constant: $\eta_s = \eta_s^0$ and $k = k^0$. The other extreme alternative considers that the deformation is localized in the varnish only: $S_1 = S_1^0$ while $S_1 + S_2 = (S_1^0 + S_2^0)(1 + \epsilon_s)$. In this case, one gets $\eta_s = \eta_s^0 + \epsilon_s$ and $k = k^0(1 + \kappa\epsilon_s)$, with $\kappa = (k_2 - k_1)/k_0$. Therefore, we propose the following dependency expression

$$k = k^0(1 + \omega_s \kappa \epsilon_s) \quad (72)$$

with $0 < \omega_s < 1$. In the following, we choose $\omega_s = 0.5$, $\kappa = 0.2$.

With this dependency, a second kind of coupling between moisture and elasticity occurs: a structural coupling via boundary conditions, in addition to the previous state and evolution coupled constitutive equations.

In [63], for spruce (*Picea abies*) and a water based white acrylic paint (60 g/cm²), the coefficient m is identified: $m = 2.84 \cdot 10^{-6} \text{ kg m}^{-2} \text{ s}^{-1}$. Since it is obtained from a single state point ($H_1 = 82\%$ and $H_2 = 93\%$), the corresponding value at that point of the other parameter is $\rho_o k = 8.8 \cdot 10^{-6} \text{ kg m}^{-2} \text{ s}^{-1}$. Note that, in [14, 37], on a straight wood surface without treatment, for Scots pine wood (*Pinus sylvestris* L), a surface emissivity is nevertheless measured on a whole range of relative humidity (from $H_1 = 40\%$ to $H_1 = 75\%$, while $H_2 = 75\%$) and the corresponding parameter is $\rho_o k = 2 \cdot 10^{-4} \text{ kg m}^{-2} \text{ s}^{-1}$, i.e. an hydraulic resistance of 4% of the previous value. Therefore, we neglect the hydraulic resistance of back panel side in all of the following. Finally, [64] reports for a cellulose acetate coating with a thickness of 0.5 mm, an equivalent to the parameter $\rho_o k$ with a value approx. $1.7 \cdot 10^{-7} \text{ kg m}^{-2} \text{ s}^{-1}$. Several typical painted layer replica have been tested in [65, 66] for which the values of $\rho_o k_0$ range between $1.6 \cdot 10^{-6} \text{ kg m}^{-2} \text{ s}^{-1}$ and $8 \cdot 10^{-5} \text{ kg m}^{-2} \text{ s}^{-1}$. In the following computations, we select the average value $\rho_o k_0 = 4 \cdot 10^{-6} \text{ kg m}^{-2} \text{ s}^{-1}$.

5.4 Problem settings

The case of *Mona Lisa* is used here to test the proposed solving strategy. The material coefficients are those given in the previous sections and, to avoid numerical ill-conditioning, a particular unit system is used. Concerning the fluid part, the goal is to have the three following values close to unity (these last two quantities lead to have the same magnitude for the diagonals of the mass matrix and of the diffusion matrix):

- the diffusion characteristic time $\tau = \frac{1}{D_R} \frac{e^2}{\pi^2}$,
- the characteristic surface mass density $m = \frac{1}{3} \rho_o e$,
- the characteristic diffusivity $d = \frac{\rho_o}{e} D_R$.

The length unity has been chosen to be $L_F = 1$ meter, the mass unity, $M_F = 1$ kilogram, and the duration unity $T_F = 12$ hours. In such a way, $\tau \approx 1.59 T_F$, $m \approx 1.95 M_F L_F^{-2}$, $d \approx 0.37 M_F L_F^{-2} T_F^{-1}$. Unfortunately, this system is not suited to the solid part. Since solvers are decoupled, a different system could be used for each physics. To keep the same geometry and loading time evolution, we choose $L_S = L_F$ and $T_S = T_F$. Moreover we expect the characteristic stiffness $r = E_L/h$ to be close to unity. This leads to choose the unity for pressure equals to 1 GPa, to get $r \approx 1.27 M_S L_S^{-2} T_S^{-2}$. Finally, some care must be taken when coupling the physics, with different unit systems. For the concerned case, this is not an issue, since only the moisture content (adimensional) is needed for the solid part coupling. For the fluid part coupling, σ/σ_0 (adimensional) is required for the body diffusion and ε (adimensional) for the painting diffusion.

Concerning the geometrical parameters, we choose here to use a constant thickness $e = 13$ mm. A stabilized crack in the upper left part of the panel is taken into account (but not the double-dovetail walnut braces performed during an early restoration act [4]). Note that the plate model coupled with the 1D diffusion model are unable to take into account 3D effects that may appear at the crack tip. Since the stability of this crack is not the goal of the present analysis, this is not an issue for the following results. Figure 6 depicts the diffusion problem, with associated boundary conditions. Figure 5 illustrates the position the single wide poplar panel has been initially sawn in the trunk [67], and the current shape at reference state (outside the frame) [68]. Figure 7 depicts the elastic problem, for which the loading is prescribed displacements to model the interaction of the painting panel with its housing frame (considered as rigid). The contact areas have been located with examining the real workpiece and are either due to contact with the frame itself, or with the backside crosspieces that squeeze (up to a certain point) the distorted panel. The values of the prescribed displacement have been identified from force measurements [12] and an elastic analysis.

The studied time interval is $[0, T]$ with $T = 24$ h. Two loading parameters are involved: the first one is related to the prescribed displacement at contacts with the housing frame and with the horizontal crosspieces; the second parameter is the time evolution of the relative external humidity $H(t)$, see Figure 8. The first stage consists in a drying evolution, as happens when a climatic regulation is set up. This stage ends with a rapid variation in relative humidity, similar to a failure in the regulation system. When the system is reconnected, the drying begins again, and two short-time increase in relative humidity mimic two inspections of the panel, for which it is getting out of the regulation system. No surface tractions are considered, $\underline{F}_d = 0$, and the body forces are specific gravity.

The initial form of the panel is taken into account from measurements performed with shadow Moiré [68], Figure 9.

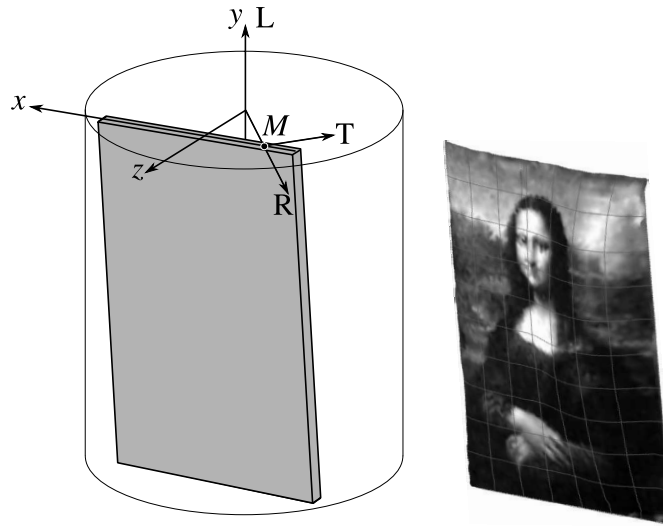


Figure 5: *Mona Lisa* panel sawing within the trunk, local material basis (R,T,L) at a current point \underline{M} , and initial deformed shape (amplified 5 times)

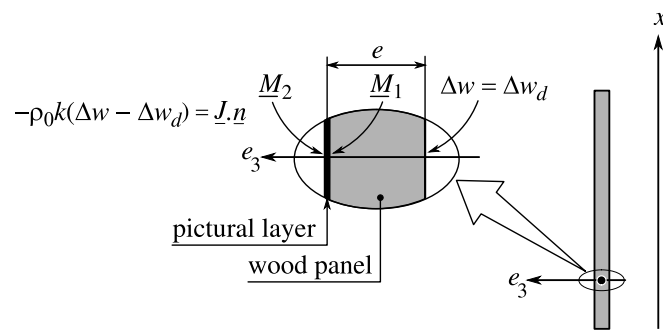


Figure 6: Diffusion problem, \underline{e}_3 being the normal to the panel

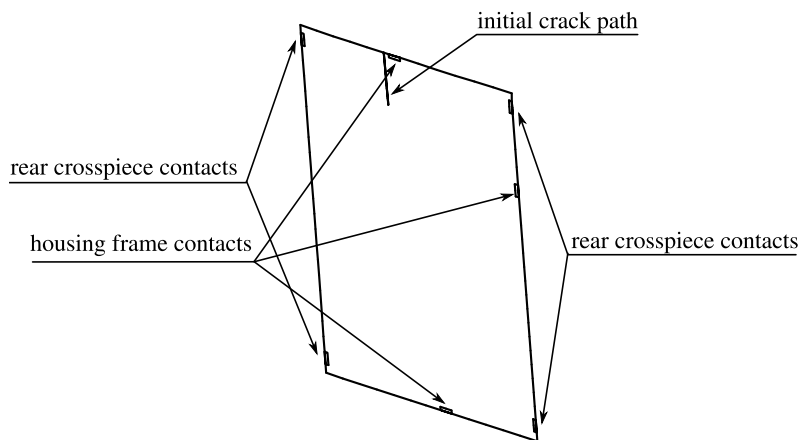


Figure 7: Elastic plate problem

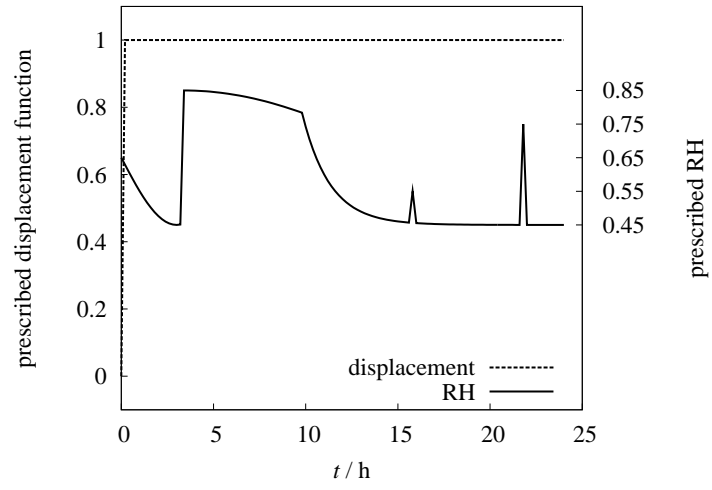


Figure 8: Loading parameter evolutions

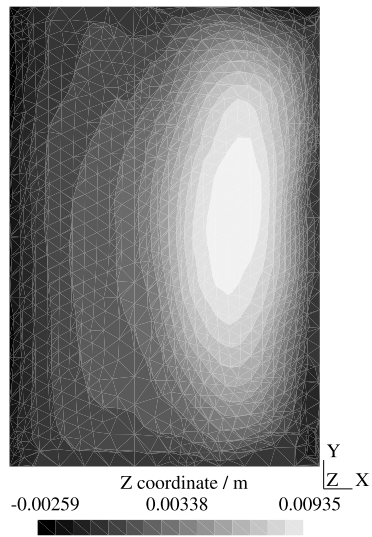


Figure 9: Initial form of the panel, after [68]

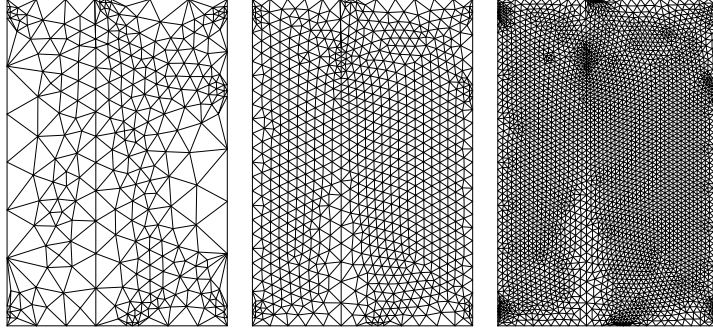


Figure 10: Different meshes for the plate problem; from left to right: $n_S = 509$, $n_S = 1697$ and $n_S = 6788$ DKT elements

6 NUMERICAL RESULTS

All the simulations are performed with an explicit Euler method ($\theta = 1$) as a time integration scheme, and the time discretization is the same for both the solid and the fluid physics.

The mesh for the solid problem uses DKT plate elements with Hammer integration points (for bending, and the associated 3-node triangle for in-plane behavior).

For the fluid problem, the 1D discretization in the thickness of the plate uses linear elements. There are as many 1D ‘segments’ as there are integration points for the solid problem (i.e. 3 times the number of plate elements) and the same transverse mesh is used to perform averages in the thickness (for instance, for the plate behavior deduced from the 3D Hooke tensor field). Though the diffusion problem is a parabolic system, the problem is solved with finite elements. In such a case, it requires an ‘accuracy condition’ [69, 70]

$$\frac{\Delta t}{(\Delta l)^2} \geq \frac{1}{6\theta D} \quad (73)$$

where Δl is a characteristic element size, and Δt the time step. With the previous expression of τ , the number of time steps n_τ per characteristic time τ is limited by the number of elements in the thickness n_F as $n_\tau \leq 6\theta n_F^2 / \pi^2$.

Concerning the splitting in the proposed strategy, the simplest choice is selected: $\mathbf{X}_S^D = \mathbf{C}_{\text{ref}}^{-1}$ and $\mathbf{X}_F^D = \frac{1}{\rho_o} \mathbf{D}_{\text{ref}}^{-1}$ (and the corresponding k_0 for the pictural layer). The termination thresholds for the inner iterations are chosen as $\epsilon_S = \epsilon_F = 10^{-6}$.

To assess the performances of the proposed strategy, the influence of the discretization parameters are tested, both on the solution and on the behavior of the algorithm.

Pre-processing is performed with the finite element code Cast3M [56], processing uses two codes (elastic, and diffusion) implemented within matlabTM platform, post-processing is performed with gmsh [71].

6.1 Influence of the fluid spatial discretization

Considering first the plate discretization with $n_S = 509$ finite elements (Figure 10, on the left); 4 different discretizations for the moisture diffusion in the thickness are tested: $n_F = 4, 6, 8$ or 10 elements of regular size, with a linear interpolation, for a fixed time discretization with $n_T = 120$ time steps.

The numerical results are reported first as the evolution of the deflection at the central point on the panel, measured from the initial position of the reference state, Figure 11, for the different discretizations. The different stages in the humidity loading are clearly visible. The scheme is indeed convergent with respect to the fluid discretization. With few fluid elements, the moisture profile in the thickness tends to overestimate the water penetration, and the swelling/shrinkage is itself overestimated: This is why the central deflection is larger with a coarse fluid discretization. With these results, a fluid discretization with $n_F = 8$ elements is selected as sufficiently accurate and will be used in the following.

Table 4 reports the average number of iterations per time step, and the cumulative number of iterations n_{it} , to declare the convergence of the partitioning scheme at each time step. The number of iterations hardly depends on the fluid discretization. It is almost constant for all the tested cases.

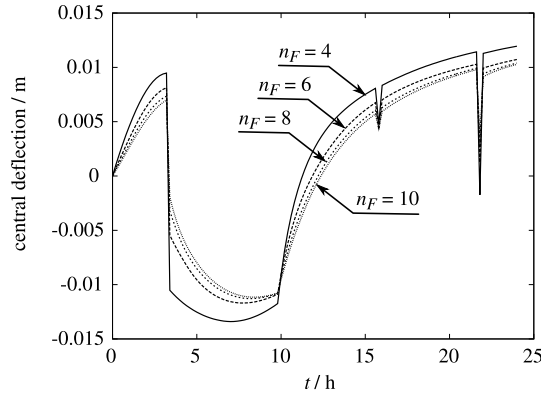


Figure 11: Influence of the moisture diffusion discretization on the central panel deflection evolution ($n_S = 509$, $n_T = 120$)

n_S	n_F	n_T	n_{it}/n_T	n_{it}
509	4	120	16.7	2009
509	6	120	16.9	2030
509	8	120	17	2040
509	10	120	17	2037
509	8	63	18.2	1166
509	8	120	17	2040
509	8	240	15.2	3646
509	4	120	16.7	2009
1697	4	120	17	2034
6788	4	120	16.7	2006
1697	8	120	17	2039

Table 4: Convergence indicators (average number of iterations per time step and cumulative number of iterations n_{it}) as functions of the parameter discretizations (number of elements for the diffusion through the thickness n_F , number of time steps n_T , number of plate elements n_S)

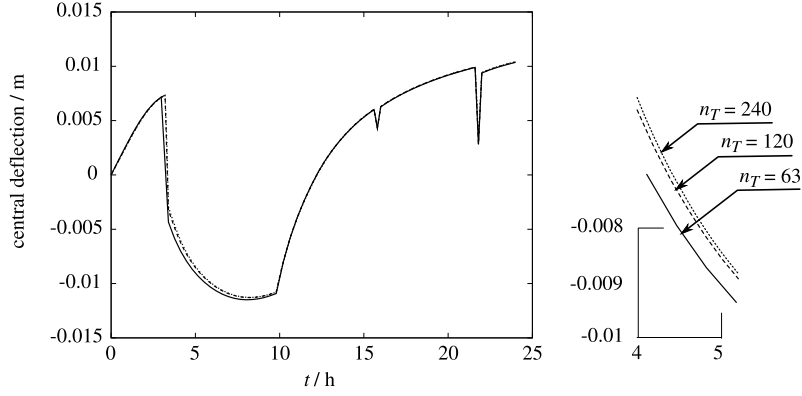


Figure 12: Influence of the time discretization on the central panel deflection evolution ($n_F = 8$, $n_S = 509$)

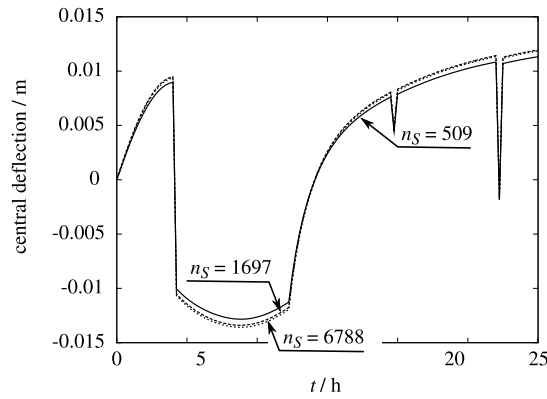


Figure 13: Influence of the solid discretization on the central panel deflection evolution ($n_F = 4$, $n_T = 120$)

6.2 Influence of the time discretization

With a fixed number of fluid elements ($n_F = 8$) for moisture diffusion, and still $n_S = 509$ elements for the plate discretization, 3 different time discretizations were tested: $n_T = 63$, 120 and 240 time steps, with as regular time-step lengths as possible while consistent with the occurrences of the different loading stages.

The obtained central deflection is reported in Figure 12. Few dependence is observed; therefore the time step length is already sufficiently small for the precision criteria ($n_T = 120$ will be used in the following).

Nevertheless, for the previously mentioned criteria for the time step length selection with a parabolic equation (73), this time step length should not be too small with respect to the spatial discretization. With $\theta = 1$ and the initial value $D \approx D_R = 30.10^{-10} \text{ m}^2.\text{s}^{-1}$, this criteria leads to $\Delta t/(\Delta l)^2 > 5.55 \cdot 10^7 \text{ s.m}^{-2}$. which is the case here ($\Delta t = 12 \text{ min}$ for $n_T = 120$ and $\Delta l = 1.625 \text{ mm}$ for $n_F = 8$, for which $\Delta t/(\Delta l)^2 \approx 27.3 \cdot 10^7 \text{ s.m}^{-2}$). Note that due to the coupled model, if the diffusion coefficients decrease, the characteristic time increases; therefore, the accuracy condition may be violated. This is also an indication of the interest for using an adaptive time step (this feature is not implemented here).

The convergence in terms of iteration count is also reported in Table 4. Obviously, this iteration number per time step decreases when decreasing the time step length, but not in large proportions.

6.3 Influence of the solid spatial discretization

Finally, several discretizations for the plate problem are now considered, with $n_S = 509$, 1697 and 6788 elements, using $n_F = 4$ finite elements for the fluid, and $n_T = 120$ time steps, Figure 10. Again, Figure 13 reports the central deflection, and convergence of the iterations are given in the same Table 4.

Only a weak influence is exhibited. Indeed, in the case $n_S = 6788$, the minimum size of the elements is already smaller than the panel thickness. Therefore, as a plate model, the previous discretization is

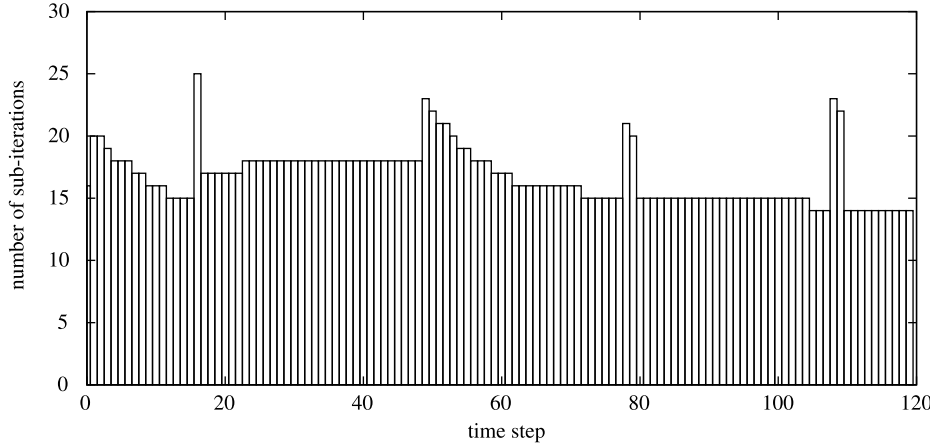


Figure 14: Number of iterations to reach convergence ($\epsilon_S = \epsilon_F = 10^{-6}$) along the time steps ($n_S = 1697$, $n_F = 8$, $n_T = 120$)

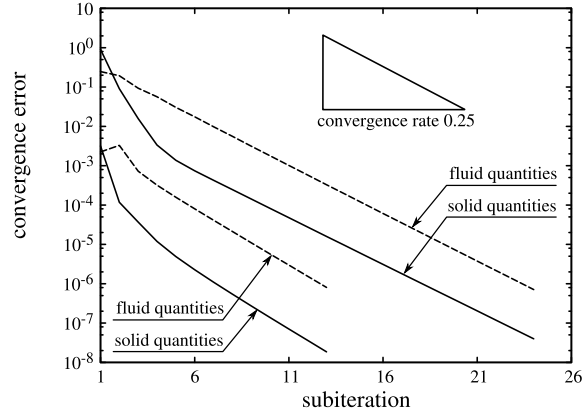


Figure 15: Convergence of the error indicators n_S (for the solid) and n_F (for the fluid) at two time increments, corresponding to the faster and slower convergences ($n_S = 1697$, $n_F = 8$, $n_T = 120$)

already sufficient. In the following, the discretization parameters $n_T = 120$, $n_F = 8$ and $n_S = 1697$ are therefore selected.

As a general remark, the average convergence rate is only weakly dependent on the element size of the solid discretization. The number of iterations required to reach the convergence with the criteria $\epsilon_S = \epsilon_F = 10^{-6}$ are not constant with respect to the time step, but their distribution is always similar to the case depicted in Figure 14. The main convergence difficulties (the largest number of iterations per time step) happen when the moisture content does vary rapidly, and for its highest amplitude, i.e. when the coupling is maximum.

The convergence of the error indicators η_S and η_F , for the same case, are reported in Figure 15, for the time steps corresponding to the smallest and the largest number of iterations to converge. Asymptotic convergence rate is close to 0.25 (i.e. $\log(\eta^{(k)}/\eta^{(k+1)}) \approx 0.25$) both for the fluid and the solid quantities; The previous definitions of the error nevertheless lead to a higher value for the fluid error than for the solid one. When the number of iterations at convergence is larger, the same convergence rate was obtained, but the initial levels of both errors were larger. Therefore, a possible improvement would consist in a better initialization of the iterations. Nevertheless, this is not under the scope of this article.

6.4 Interpretation of the numerical results

Considering the results obtained with the discretization parameters $n_S = 1697$, $n_F = 8$ and $n_T = 120$, the distributions of moisture Δw in the panel thickness are depicted on Figure 16, at different time steps. Each integration point of the plate model has its own evolution, and each plot reports the ranges between the minimum and maximum values. The jump in the values at the right end of the curves are due to the pictorial layer with its own permeability, modeled as a zero thickness layer.

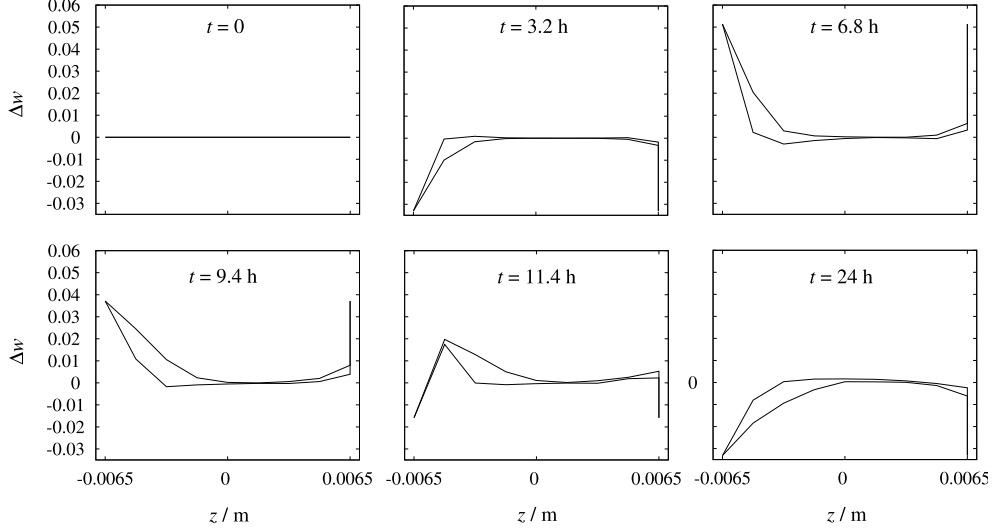


Figure 16: Distributions of moisture variations in the panel thickness at various time steps ($n_S = 1697$, $n_F = 8$, $n_T = 120$)

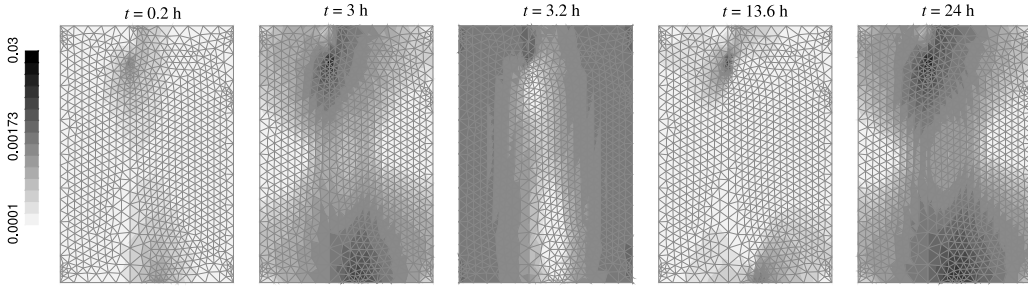


Figure 17: Norm of the minimal surface principal strain (negative) at various time steps

Finally, the minimum principal surface strain on the painted side (eventually compressive, which is the most dangerous for the pictural layer) is depicted on Figure 17, at several time steps. These values are obtained for low moisture content which are therefore the most penalizing.

6.5 Other versions of the proposed strategy

Slightly different choices can be made for the design of the previous scheme. Apart from different splittings in (35), (37) and (41) that can be chosen, the choice of \mathbf{D}_0 could be made as a uniform value.

Additionally, a relaxation can be added to the previous algorithm 1: With an additional relaxation parameter γ in the same way the classical Jacobi algorithm can be relaxed in the linear case (if $0 < \gamma < 1$, this is an under-relaxed scheme; if $1 < \gamma < 2$, this is an over-relaxed scheme; $\gamma = 1$ recovers the previous algorithm). To do so, the lines 18 and 19 have to be modified as follows:

$$\tilde{\varepsilon}^{(k)} \leftarrow \gamma \mathbf{B}_\varepsilon u^{(k)} + (1 - \gamma) \tilde{\varepsilon}^{(k-1)} \quad (74)$$

$$\sigma_d \leftarrow (\mathbf{X}_S^D)^{-1} \tilde{\varepsilon}^{(k)} + \gamma \tilde{\sigma}^{(k-1)} + (1 - \gamma) \tilde{\sigma}^{(k-2)} \quad (75)$$

and the lines 22, 23 and 24 as

$$W^{(k)} \leftarrow \gamma \mathbf{B}_w \Delta w^{(k)} + (1 - \gamma) W^{(k-1)} \quad (76)$$

$$\tilde{F}^{(k)} \leftarrow \gamma \mathbf{B}_F \Delta w^{(k)} + (1 - \gamma) \tilde{F}^{(k-1)} \quad (77)$$

$$J_d \leftarrow (\mathbf{X}_F^D)^{-1} \tilde{F}^{(k)} - \gamma \tilde{J}^{(k-1)} - (1 - \gamma) \tilde{J}^{(k-2)} \quad (78)$$

A relaxation parameter slightly less than 1 is usually suited to improve the performance. The Table 5 reports the total number of iterations for the reference case when changing the relaxation parameter. Best improvement has been found to be close to 30% with $\gamma = 0.95$.

γ	0.7	0.8	0.9	0.95	0.975	1	1.1
n_{it}	3284	2353	1674	1379	1532	2039	8125

Table 5: Cumulative number of iterations n_{it} as a function of the relaxation parameter γ ($n_S = 1697$, $n_F = 8$ and $n_T = 120$)

7 CONCLUSIONS AND PROSPECTS

The partitioning framework that is proposed in this article is well suited to multiphysics problems, for which it focuses on the interactions between the different physics. The modularity of such an approach allows to couple different models for the different physics, and is expected to cope with different discretizations as well [72]. Its convergence properties were little influenced by the discretization parameters, for the non linear coupled problem of hygroelasticity in wood structures under study. The extension of this approach to other coupled multiphysics problems is on development.

Apart from the multimodel management ability of the proposed scheme, exemplified on the coupling of a plate problem with a monodimensional diffusion problem, work is on progress on its usage to couple two different discretization schemes, for instance finite volumes and finite elements. In each case, an adaptive discretization scheme (eventually independently for each physics) would be an interesting feature.

Concerning virtual testing of wooden artworks of cultural heritage, the material behavior used here mainly couples elasticity and hygrometry with the simplest model. For such applications, a meaningful model would take into account moisture-dependent visco-elasticity, mechano-sorption, and eventually their dependency on temperature. Additionally, more details of interest can be taken into account. For instance the crack tip may require a finer 3D discretization, and the previous approach could be coupled with a structural zooming technique, such as in [73]. Concerning the contact points with the housing frame, due to the movements of the panel, their location may evolve on the panel edges. These unilateral interactions are expected to be integrated as well in the framework proposed in this article, similarly as in the NSCD approach [47, 48].

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A Constitutive behavior

Other choices can be made to express the constitutive behavior; for instance, the material state can be described with other state variables, such as the stress $\boldsymbol{\sigma}$ and the chemical potential $\Delta\mu$. The same reversible part of the model can be obtained with a Fenchel transform of the previous potential $\Psi(\boldsymbol{\varepsilon}, \rho_o \Delta w)$ (25), or with a direct modeling such as:

$$\Psi^*(\boldsymbol{\sigma}, \Delta\mu) = \frac{1}{2} \boldsymbol{\sigma} : \mathbf{C}^{-1} \boldsymbol{\sigma} + \mathbf{B}_1(\Delta\mu) : \boldsymbol{\sigma} + \Psi_1(\Delta\mu) \quad (79)$$

Once the state laws are derived, an identification can be also performed as:

$$\Psi_1'(\Delta\mu) = \rho_o f \left(\exp \frac{M \Delta\mu}{RT} \right) \quad \text{and} \quad \mathbf{B}_1(\Delta\mu) = \frac{1}{\rho_o} \mathbf{A} \Psi_1'(\Delta\mu) \quad (80)$$

Concerning the dissipative part of the model, the counterpart of (23) reads:

$$\underline{J} = -\rho_o \mathbf{D} \text{grad} \Delta w = -\rho_o \mathbf{D} \left(\frac{\partial \Delta w}{\partial \Delta\mu} \text{grad} \Delta\mu + \frac{\partial \Delta w}{\partial \boldsymbol{\sigma}} \text{Grad} \boldsymbol{\sigma} \right) \quad (81)$$

With

$$\rho_o \frac{\partial \Delta w}{\partial \Delta\mu} = \Psi_1'' + \mathbf{B}_1'' : \boldsymbol{\sigma} = \Psi_1'' + \frac{1}{\rho_o} \Psi_1''' \mathbf{A} : \boldsymbol{\sigma} \quad (82)$$

¹<http://www.woodculther.org>

and neglecting the effect of the stress gradient, one gets:

$$\mathbf{D} = \frac{\mathbf{L}}{\Psi_1'' + \frac{1}{\rho_o} \Psi_1''' \mathbf{A} : \boldsymbol{\sigma}} \quad (83)$$

This expression can be used to select a form of coupling between the different diffusion tensors.

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