



HAL
open science

Non-quadratic local stabilization for continuous-time Takagi-Sugeno models

Thierry-Marie Guerra, Miguel Bernal, Kevin Guelton, Salim Labiod

► **To cite this version:**

Thierry-Marie Guerra, Miguel Bernal, Kevin Guelton, Salim Labiod. Non-quadratic local stabilization for continuous-time Takagi-Sugeno models. *Fuzzy Sets and Systems*, 2012, 201, pp.40-54. 10.1016/j.fss.2011.12.003 . hal-00793244

HAL Id: hal-00793244

<https://hal.science/hal-00793244>

Submitted on 21 Feb 2013

HAL is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers.

L'archive ouverte pluridisciplinaire **HAL**, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d'enseignement et de recherche français ou étrangers, des laboratoires publics ou privés.

Non-quadratic local stabilization for continuous-time Takagi-Sugeno models

Thierry Marie Guerra⁽¹⁾, Miguel Bernal⁽²⁾, Kevin Guelton^{(3),*}, Salim Labiod⁽⁴⁾

⁽¹⁾LAMIH FRE CNRS 3304,
University of Valenciennes Hainaut-Cambrésis, France
phone: +33 3 27 51 14 87; email: guerra@univ-valenciennes.fr

⁽²⁾Sonora Institute of Technology
5 de febrero 818 Sur, Col. Centro, C.P. 85000. Ciudad Obregón, Mexico.
email: miguel.bernal@itson.edu.mx

*Corresponding author
⁽³⁾CRéSTIC EA 3804,
University of Reims Champagne-Ardenne,
Moulin de la Housse, BP 1039, 51687 Reims cedex 2, France.
Phone : +33 3 26 91 32 61 ; email : kevin.guelton@univ-reims.fr

⁽⁴⁾ University of Jijel,
LAMEL,
BP 98, Ouled Aissa Jijel 18000, Algérie.

Abstract :

This paper is concerned with non-quadratic stabilization of continuous-time Takagi-Sugeno (TS) models. The well-known problem of handling time-derivatives of membership functions (MFs) as to obtain conditions in the form of linear matrix inequalities (LMIs) is overcome by reducing global goals to the estimation of a region of attraction. Instead of parallel distributed compensation (PDC), a non-PDC control law is proposed according to the non-quadratic nature of the Lyapunov function. Examples are provided to show the advantages over the quadratic and some non-quadratic approaches.

Keywords :

Linear Matrix Inequalities, Non-quadratic Lyapunov function, Stabilization, Takagi-Sugeno models.

1. Introduction

Since they were proposed in [1] the control community has intensively studied Takagi-Sugeno (TS) models due to the fact that they can exactly represent a nonlinear model **in a compact subset of the domain of the state variables**. A TS model is a nonlinear blending of linear models via membership functions (MFs) which hold the convex-sum property [2]. The stabilization problem is usually addressed via the so-called parallel distributed compensation (PDC) control law [3], which is a nonlinear blending of linear-state feedbacks which uses the same MFs as the TS model.

The direct Lyapunov method altogether with quadratic Lyapunov functions has been usually employed to investigate the stability and stabilization of TS models. This method usually leads to conditions formulated in terms of linear matrix inequalities (LMIs) [4], which can be efficiently solved by convex optimization techniques. Quadratic analysis and design has produced a remarkable number of results regarding robustness, performance, observer design, output feedback and time delay systems (see e.g. [5-9] and references therein). Nonetheless, the quadratic approach presents serious limitations because its solutions are inherently pessimistic, i.e., there are stable or stabilizable models which do not have a quadratic solution (see [10] and references therein). Conservativeness comes from different sources: the type of TS model [11,12], the way the membership functions are dropped-off to obtain LMI expressions [13-15], the integration of membership-function information [16,17], or the choice of Lyapunov function [18,19]. This work is concerned with a relaxation in the latter sense which demands a change of perspective from global to local conditions.

Several Lyapunov functions have been proposed in the literature. Piecewise Lyapunov functions (PWLF) [18,20] have been straightforwardly applied to those TS models that induce state-space partitions from the fact that not all their linear components are simultaneously activated; unfortunately, TS models constructed via the sector nonlinearity approach lack this property. Various kinds of non-quadratic Lyapunov functions

(NQLF) have been also employed; they depend on the same MFs of the model, hereby taking into account structural information otherwise ignored by the quadratic approach. However, NQLF-based results have not triggered the same developments for continuous-time TS models [21] than for discrete-time ones [22,26]. This asymmetry is explained by the difficulty of dealing with time-derivatives of the MFs that emerge while applying the direct Lyapunov method to obtain global conditions.

Some palliative solutions have been proposed to the aforementioned problem. In [21,27] the authors bound the time-derivatives of the MFs assuming that they do not depend on the input, which turns out to be very restrictive. Moreover, the proposed control law makes use of the time-derivatives of the MFs through a classical PDC scheme, thus ignoring the non-quadratic nature of the involved Lyapunov function. In [28] a line-integral Lyapunov function is proposed to circumvent the MFs' time-derivative obstacle, though the line integral is asked to be path-independent thus significantly reducing its applicability [29]. A change of perspective for non-quadratic stability analysis of TS models has been proposed in [30]. This approach reduces global goals to less exigent conditions, thereby showing that an estimation of the region of attraction can be found (local stability); this solution parallelizes nonlinear analysis and design for models that do not admit a global solution [31]. Said in another words, classical linear parameter varying (LPV) models do not capture the nonlinear behavior of models [32] whereas TS ones, also known as quasi-LPV models, can do it exactly [33]. In the LPV case it is therefore reasonable to deal with global stability (under the constraints due to the bounds on the variables) [32], whereas obviously global stability is very often unreachable for nonlinear systems and therefore for their TS representation. This paper extends the previous results so they can be applied for controller design. A non-PDC control law is employed to fully exploit the non-quadratic properties of the Lyapunov function.

The contents are organized as follows: Section II introduces TS models, sector nonlinearity approach, the NQLF this work is based on and the proposed non-PDC control law; a problem statement is made. Section III **summarizes** the work presented in [30] and extends it for stabilization purposes, thus establishing new

local conditions for controller design. Section IV presents some illustrative examples to stress the fact that the few existent solutions on the subject are clearly outperformed by the new approach. Finally, section V gathers some conclusions and perspectives.

2. Definitions and Notation

Consider a nonlinear model of the form:

$$\dot{x}(t) = f(z(t))x(t) + g(z(t))u(t) \quad (1)$$

with $f(\cdot)$, $g(\cdot)$ nonlinear functions, $x(t) \in \mathbb{R}^n$ the state vector, $u(t) \in \mathbb{R}^m$ the input vector, and $z(x(t)) \in \mathbb{R}^p$ the premise vector assumed to be bounded and smooth in a compact set C of the state space including the origin.

Let $nl_j(t) \in [\underline{nl}_j, \overline{nl}_j]$, $j \in \{1, \dots, p\}$ be the set of bounded nonlinearities in (1) belonging to C . Employing the sector nonlinearity approach [5], the following weighting functions can be constructed

$$w_0^j(\cdot) = \frac{\overline{nl}_j - nl_j(\cdot)}{\overline{nl}_j - \underline{nl}_j}, \quad w_1^j(\cdot) = 1 - w_0^j(\cdot), \quad j \in \{1, \dots, p\}. \quad (2)$$

From the previous weights, the following MFs are defined:

$$h_i = h_{1+i_1+i_2 \times 2 + \dots + i_p \times 2^{p-1}} = \prod_{j=1}^p w_{i_j}^j(z_j), \quad (3)$$

with $i \in \{1, \dots, 2^p\}$, $i_j \in \{0, 1\}$. These MFs satisfy the convex sum property $\sum_{i=1}^r h_i(\cdot) = 1$, $h_i(\cdot) \geq 0$ in C .

Where convenient, convex sums will be denoted as $\Upsilon_z = \sum_{i=1}^r h_i(z(t))\Upsilon_i$ and their inverse as

$$\Upsilon_z^{-1} = \left(\sum_{i=1}^r h_i(z(t)) \Upsilon_i \right)^{-1}.$$

Based on the previous definitions, an exact representation of (1) in C is given by the following TS model:

$$\dot{x}(t) = \sum_{i=1}^r h_i(z(t)) (A_i x(t) + B_i u(t)) = A_z x(t) + B_z u(t), \quad (4)$$

with $r = 2^p \in \mathbb{N}$ representing the number of linear models and (A_i, B_i) , $i = 1, \dots, r$ a set of controllable pairs of proper dimensions directly obtained from the new representation.

Instead of PDC [3], the following generalization of the non-quadratic control law in [22] is proposed:

$$u(t) = \sum_{i=1}^r \sum_{j=1}^r h_i h_j \left(F_i + \sum_{k=1}^p \frac{\partial w_0^k}{\partial z_k} \left(\frac{\partial z_k(t)}{\partial x(t)} A_j x \right) \cdot G_i^k \right) \left(\sum_{l=1}^r h_l P_l \right)^{-1} x(t) = (F_z + \delta(z)) P_z^{-1} x(t) \quad (5)$$

with $F_i, G_i^k \in \mathbb{R}^{m \times n}$ the controller gains, $P_i \in \mathbb{R}^{n \times n}$, $P_i = P_i^T > 0$, and $\delta(z) = \sum_{k=1}^p \frac{\partial w_0^k}{\partial z_k} \left(\frac{\partial z_k(t)}{\partial x(t)} A_z x \right) \cdot G_z^k$.

The closed-loop TS model is thence written as

$$\dot{x}(t) = \sum_{i=1}^r h_i(z(t)) (A_i x(t) + B_i u(t)) = (A_z + B_z (F_z + \delta(z)) P_z^{-1}) x(t). \quad (6)$$

Triple convex sums $\Upsilon_{zzz} = \sum_{i=1}^r \sum_{j=1}^r \sum_{l=1}^r h_i(z(t)) h_j(z(t)) h_l(z(t)) \Upsilon_{ijl}$ arise along matrix manipulations and their negative-definiteness is usually examined after dropping the MFs to obtain LMI conditions in terms of Υ_{ijl} . The way the MFs are dropped from the triple sum above is called a sum-relaxation; several of them are available in the literature for double [13] and multiple sums [14]. In this work, a relaxation derived from Proposition 2 of the latter work has been adopted because it combines computational efficiency and does

not need slack variables:

Relaxation Lemma [14]: Let Υ_{ijl} be matrices of proper dimensions. Then

$$\sum_{i=1}^r \sum_{j=1}^r \sum_{l=1}^r h_i(z(t)) h_j(z(t)) h_l(z(t)) \Upsilon_{ijl} < 0 \quad (7)$$

holds if for a given $q \geq 3$

$$\tilde{\Upsilon}_{\mathbf{a}} = \sum_{\substack{\mathbf{b} \in \mathbf{A}(\mathbf{a}) \\ ij^l = b_1 b_2 b_3}} \Upsilon_{ijl} < 0, \quad \forall \mathbf{a} \in \mathbf{I}_q^+, \quad (8)$$

with $\mathbf{I}_q = \{ \mathbf{a} = (a_1, \dots, a_q) \in \mathbb{R}^q : 1 \leq a_b \leq r, \forall b = 1, \dots, q \}$, $\mathbf{I}_q^+ = \{ \mathbf{a} \in \mathbf{I}_q : a_b \leq a_{b+1}, \forall b = 1, \dots, q-1 \}$, and $\mathbf{A}(\mathbf{a})$

being the set of permutations (with possibly repeated elements) of multi-index \mathbf{a} in \mathbf{I}_q .

Quadratic Lyapunov function $V = x(t)^T P x(t)$ has been originally employed for stabilization purposes. TS

model (4) is stabilized by the PDC control law $u(t) = \sum_{i=1}^r h_i(z(t)) F_i x(t)$ if there exist matrices $X = P^{-1} > 0$

and $M_i = F_i X$, $i \in \{1, \dots, r\}$ such that (8) holds with $\Upsilon_{ij} = X A_i^T + A_i X + M_j^T B_i^T + B_i M_j$ [5]. This result

presents a serious inconvenient: as the number of rules increases the existence of a matrix P as a common

solution of the aforementioned set of LMIs gets harder to satisfy. In other words, asking for a global

common Lyapunov function is a source of conservatism which can be reduced considering non-quadratic

Lyapunov function (NQLF) candidates. **NQLFs increase the flexibility by enlarging the choice of matrices**

that solve the LMI problem (8) [19, 22, 27]. In this framework, let us consider the following non-quadratic

Lyapunov function candidate:

$$V(x(t)) = x(t)^T \left(\sum_{i=1}^r h_i(z(t)) P_i \right)^{-1} x(t) = x(t)^T P_z^{-1} x(t) \quad (9)$$

with $P_z = P_z^T > 0$ (therefore $P_z^{-1} > 0$).

Its time-derivative along the trajectories of TS model (6) is given by

$$\dot{V}(x(t)) = x^T(t) \left(P_z^{-1} (A_z + B_z (F_z + \delta(z))) P_z^{-1} + (A_z + B_z (F_z + \delta(z))) P_z^{-1} \right)^T P_z^{-1} + \dot{P}_z^{-1} \Big) x(t). \quad (10)$$

Via elementary properties and taking into account that $P_z \dot{P}_z^{-1} P_z = -\dot{P}_z$, it is verified that

$$\begin{aligned} \dot{V}(x(t)) < 0 &\Leftrightarrow P_z^{-1} (A_z + B_z (F_z + \delta(z))) P_z^{-1} + (A_z + B_z (F_z + \delta(z))) P_z^{-1} \Big)^T P_z^{-1} + \dot{P}_z^{-1} < 0 \\ &\Leftrightarrow A_z P_z + B_z (F_z + \delta(z)) + (A_z P_z + B_z (F_z + \delta(z)))^T + P_z \dot{P}_z^{-1} P_z < 0 \\ &\Leftrightarrow A_z P_z + B_z (F_z + \delta(z)) + (A_z P_z + B_z (F_z + \delta(z)))^T - \dot{P}_z < 0 \end{aligned} \quad (11)$$

Global conditions in the form of LMIs are normally derived from expressions similar to the previous one in the quadratic case. Unfortunately, obtaining non-conservative LMIs from (11) for global stabilization is no

longer possible since the terms $\dot{P}_z = \sum_{i=1}^r \dot{h}_i P_i$ and $\delta(z) = \sum_{k=1}^p \frac{\partial w_0^k}{\partial z_k} \left(\frac{\partial z_k(t)}{\partial x(t)} \right)^T A_z x \Big) \cdot G_z^k$ depend on the time-

derivatives of the MFs, which do not convey to readily available bounds. This situation raises some questions:

- Should the quadratic case fail, what can be done?
- Can expression (11) be handled to avoid conditions of the sort $\|\dot{P}_z\| < \phi_z$ [19,21,27]?

The previous works intended to derive global asymptotic conditions. In contrast, in [30] the previous questions were answered for stability analysis via a local approach. It was shown that reducing global goals responds better to stability problems, since the stability domain of a TS model can be estimated via local asymptotic conditions. This kind of estimation is customary for numerous nonlinear models whose global stability cannot be reached [31] and will be extended to the closed-loop TS model in the following section.

3. Main results

Theorem 1 (Local stabilizability): If there exist matrices of the proper size $P_i = P_i^T > 0$, F_i , and G_i^k , $i \in \{1, \dots, r\}$, $k \in \{1, \dots, p\}$ such that $A_z P_z + B_z (F_z + \delta(z)) + (A_z P_z + B_z (F_z + \delta(z)))^T < 0$, then there exists a domain D , $0 \in D$, such that TS model (4) is locally asymptotically stabilizable under control law (5).

Proof: The NQLF candidate (9) satisfies $V(0) = 0$ and $V(x) \geq 0$ in \square^n . Its time-derivative (10) holds $\dot{V}(0) = 0$. Provided that $A_z P_z + B_z (F_z + \delta(z)) + (A_z P_z + B_z (F_z + \delta(z)))^T < 0$ it is implied that there exists a sufficiently small $\lambda > 0$ such that $A_z P_z + B_z (F_z + \delta(z)) + (A_z P_z + B_z (F_z + \delta(z)))^T + \lambda I < 0$ which can be used to define $D = \{x : x \in B, \|\dot{P}_z\| < \lambda\}$. The origin belongs to domain D since

$$\dot{P}_z = \sum_{i=1}^r \dot{h}_i P_i = \sum_{i=1}^r \left(\frac{\partial h_i}{\partial z} \right)^T \frac{\partial z^T}{\partial x} \dot{x} P_i = \sum_{i=1}^r \left[\left(\frac{\partial h_i}{\partial z} \right)^T \frac{\partial z^T}{\partial x} (A_z + B_z (F_z + \delta(z))) P_z^{-1} x(t) \right] P_i$$

depends on the state vector $x(t)$ in such a way that $x(t) = 0$ is a trivial solution of $\|\dot{P}_z\| < \lambda$. Since $V(x) > 0$ and $\dot{V}(x) < 0$ in $D - \{0\}$, the equilibrium point $x = 0$ is locally asymptotically stable, thus concluding the proof. \square

In [30] it has been shown that \dot{P}_z can be written as

$$\dot{P}_z = \sum_{k=1}^p \frac{\partial W_0^k}{\partial z_k} (P_{g_1(z,k)} - P_{g_2(z,k)}) \dot{z}_k = \sum_{j=1}^r \sum_{k=1}^p h_j \frac{\partial W_0^k}{\partial z_k} (P_{g_1(j,k)} - P_{g_2(j,k)}) \dot{z}_k \quad (12)$$

with $g_1(j, k) = \lfloor (j-1) / 2^{p+1-k} \rfloor \times 2^{p+1-k} + 1 + (j-1) \bmod 2^{p-k}$ and $g_2(j, k) = g_1(j, k) + 2^{p-k}$.

Substituting (12) in (11) and recalling that $\dot{z}_k = \frac{\partial z_k(t)}{\partial x(t)} (A_z x(t) + B_z u(t))$ and

$$\delta(z) = \sum_{k=1}^p \frac{\partial w_0^k}{\partial z_k} \cdot \left(\frac{\partial z_k(t)}{\partial x(t)} A_z x \right) \cdot G_z^k, \text{ gives}$$

$$\begin{aligned} & A_z P_z + B_z (F_z + \delta(z)) + (A_z P_z + B_z (F_z + \delta(z)))^T - \sum_{k=1}^p \frac{\partial w_0^k}{\partial z_k} (P_{g_1(z,k)} - P_{g_2(z,k)}) \dot{z}_k \\ &= A_z P_z + P_z A_z^T + B_z F_z + F_z^T B_z^T + B_z \delta(z) + \delta^T(z) B_z^T - \sum_{k=1}^p \frac{\partial w_0^k}{\partial z_k} \cdot \frac{\partial z_k(t)}{\partial x(t)} (A_z x(t) + B_z u(t)) (P_{g_1(z,k)} - P_{g_2(z,k)}) \\ &= A_z P_z + B_z F_z + P_z A_z^T + F_z^T B_z^T - \sum_{k=1}^p \frac{\partial w_0^k}{\partial z_k} \cdot \frac{\partial z_k(t)}{\partial x(t)} B_z u(t) (P_{g_1(z,k)} - P_{g_2(z,k)}) \\ &\quad - \sum_{k=1}^p \frac{\partial w_0^k}{\partial z_k} \cdot \frac{\partial z_k(t)}{\partial x(t)} A_z x(t) (P_{g_1(z,k)} - P_{g_2(z,k)}) + \sum_{k=1}^p \frac{\partial w_0^k}{\partial z_k} \cdot \frac{\partial z_k(t)}{\partial x(t)} A_z x (B_z G_z^k + (B_z G_z^k)^T) \\ &= A_z P_z + B_z F_z + P_z A_z^T + F_z^T B_z^T - \sum_{k=1}^p \frac{\partial w_0^k}{\partial z_k} \cdot \frac{\partial z_k(t)}{\partial x(t)} B_z u(t) (P_{g_1(z,k)} - P_{g_2(z,k)}) \\ &\quad - \sum_{k=1}^p \frac{\partial w_0^k}{\partial z_k} \cdot \frac{\partial z_k(t)}{\partial x(t)} A_z x(t) (P_{g_1(z,k)} - P_{g_2(z,k)} - B_z G_z^k - (G_z^k)^T B_z^T) \\ &= A_z P_z + B_z F_z + P_z A_z^T + F_z^T B_z^T - \sum_{k=1}^p \sum_{v=1}^n \sum_{e=1}^m \frac{\partial w_0^k}{\partial x_v} u_e (B_z)_{ve} (P_{g_1(z,k)} - P_{g_2(z,k)}) \\ &\quad - \sum_{k=1}^p \sum_{v=1}^n \sum_{s=1}^n (A_z)_{vs} \frac{\partial w_0^k}{\partial x_v} x_s (P_{g_1(z,k)} - P_{g_2(z,k)} - B_z G_z^k - (G_z^k)^T B_z^T) < 0 \end{aligned} \tag{13}$$

Therefore, knowing the bounds $\left| \frac{\partial w_0^k}{\partial x_v} x_s \right|$ and $\left| \frac{\partial w_0^k}{\partial x_v} u_e \right|$ allows (13) to be verified as an LMI constraint, thence

guaranteeing $\dot{V}(x(t)) < 0$ in the region thus defined.

To guarantee $\|u\|_2 < \mu$ (so as to bound $\left| \frac{\partial w_0^k}{\partial x_v} u_e \right|$), let us assume $|x(0)| < c$. Note that $P_z \geq c^2 I$ (or

$P_z^{-1} \leq c^{-2} I$) altogether with the fact that $x^T(t) P_z^{-1} x(t) \leq x^T(0) P_z^{-1} x(0)$ for $t \geq 0$, means that $V(x(t)) \leq 1$;

then, condition $\|u\|_2 \leq \mu$ is implied by

$$\frac{1}{\mu^2} \|u\|_2^2 = \frac{1}{\mu^2} x^T(t) P_z^{-1} (F_z + \delta(z))^T (F_z + \delta(z)) P_z^{-1} x(t) \leq x^T(t) P_z^{-1} x(t) \leq x^T(0) P_z^{-1} x(0) \leq 1,$$

from which the following stems using the Schur complement and replacing $\delta(z)$ by its value

$$\begin{aligned} & x^T(t) \left(\frac{1}{\mu^2} P_z^{-1} (F_z + \delta(z))^T (F_z + \delta(z)) P_z^{-1} - P_z^{-1} \right) x(t) \leq 0 \\ & \Leftrightarrow \frac{1}{\mu^2} (F_z + \delta(z))^T (F_z + \delta(z)) - P_z \leq 0 \\ & \Leftrightarrow \begin{bmatrix} P_z & (F_z + \delta(z))^T \\ F_z + \delta(z) & \mu^2 I_m \end{bmatrix} > 0 \Leftrightarrow \begin{bmatrix} P_z & F_z^T \\ F_z & \mu^2 I_m \end{bmatrix} + \begin{bmatrix} 0 & \delta^T(z) \\ \delta(z) & 0 \end{bmatrix} > 0 \\ & \Leftrightarrow \begin{bmatrix} P_z & F_z^T \\ F_z & \mu^2 I_m \end{bmatrix} + \sum_{k=1}^p \frac{\partial w_0^k}{\partial z_k} \cdot \begin{pmatrix} \frac{\partial z_k(t)}{\partial x(t)} A_z x \end{pmatrix} \begin{bmatrix} 0 & (G_z^k)^T \\ G_z^k & 0 \end{bmatrix} > 0 \end{aligned} \quad (14)$$

Inequality (14) is therefore implied by

$$\begin{bmatrix} P_z & F_z^T \\ F_z & \mu^2 I_m \end{bmatrix} + \sum_{k=1}^p \sum_{v=1}^n \sum_{s=1}^n (A_z)_{vs} \frac{\partial w_0^k}{\partial x_v} x_s \begin{bmatrix} 0 & (G_z^k)^T \\ G_z^k & 0 \end{bmatrix} > 0 \quad (15)$$

which as expression (13) depends on bounding terms $\left| \frac{\partial w_0^k}{\partial x_v} x_s \right|$ to yield LMI expressions.

Two choices are offered to deal with these bounds, based respectively on the following properties:

$$X + \begin{pmatrix} \frac{\partial w_0^k}{\partial x_v} x_s \end{pmatrix} Y + \begin{pmatrix} \frac{\partial w_0^k}{\partial x_v} u_e \end{pmatrix} Z \leq 0 \quad \Leftrightarrow \quad X \pm \lambda_{ksv} \times Y \pm \eta_{kv} \times \mu Z \leq 0 \quad (16)$$

or

$$\begin{aligned}
Q &= Q^T > 0, \quad S = S^T > 0, \\
X + \left(\frac{\partial w_0^k}{\partial x_v} x_s \right) Y + \left(\frac{\partial w_0^k}{\partial x_v} u_e \right) Z &\leq X + \frac{1}{2} (\lambda_{kvs}^2 Q + Y Q^{-1} Y) + \frac{1}{2} (\eta_{kv}^2 S + \mu^2 Z S^{-1} Z) < 0.
\end{aligned} \tag{17}$$

By means of property (16) the following result is obtained:

Theorem 2: If there exist matrices of proper size $P_j = P_j^T \geq c^2 I$, F_j , G_j^k , $\forall j \in \{1, \dots, r\}$, $k \in \{1, \dots, p\}$ such that LMIs

$$\tilde{\Lambda}_{\mathbf{a}}^\alpha = \sum_{\substack{\mathbf{b} \in \mathbf{A}(\mathbf{a}) \\ ij1=b_1 b_2 b_3}} \Lambda_{ijl}^\alpha < 0, \quad \forall \mathbf{a} \in \mathbf{I}_q^+, \quad \alpha \in \{1, \dots, 2^{pn(m+n)}\} \tag{18}$$

hold for a given $q \geq 3$ with

$$\Lambda_{ijl}^\alpha = \text{block-diag} \left[\Upsilon_{ijl}^\alpha, \Omega_{ij}^\alpha \right],$$

$$\begin{aligned}
\Upsilon_{ijl}^\alpha &= A_i P_j + B_i F_j + P_j A_i^T + F_j^T B_i^T \\
&\quad - \sum_{k=1}^p \sum_{v=1}^n \sum_{e=1}^m (-1)^{d_{kv(e+n)}^\alpha} \eta_{kv} \mu (B_i)_{ve} (P_{g_1(j,k)} - P_{g_2(j,k)}) \\
&\quad - \sum_{k=1}^p \sum_{v=1}^n \sum_{s=1}^n (-1)^{d_{kvs}^\alpha} \lambda_{kvs} (A_i)_{vs} (P_{g_1(j,k)} - P_{g_2(j,k)} - B_l G_j^k - (G_j^k)^T B_l^T)
\end{aligned}$$

$$\Omega_{ij}^\alpha = - \begin{bmatrix} P_j & F_j^T \\ F_j & \mu^2 I_m \end{bmatrix} - \sum_{k=1}^p \sum_{v=1}^n \sum_{s=1}^n (-1)^{d_{kvs}^\alpha} \lambda_{kvs} (A_i)_{vs} \begin{bmatrix} 0 & (G_j^k)^T \\ G_j^k & 0 \end{bmatrix},$$

$d_{kv(e+n)}^\alpha$, d_{kvs}^α defined from $\alpha - 1 = d_{pn(n+m)}^\alpha + d_{pn(n+m-1)}^\alpha \times 2 + \dots + d_{111}^\alpha \times 2^{pn(n+m)-1}$, and $g_1(j, k)$, $g_2(j, k)$

defined as in (12), then $x(t)$, $|x(0)| < c$ tends to zero exponentially for any trajectory satisfying (6) in the

outermost Lyapunov level contained in $R_o \subseteq (R \cap C)$ with $R = \bigcap_{e,k,s,v} \left\{ x : \left| \frac{\partial w_0^k}{\partial x_v} u_e \right| \leq \mu \eta_{kv}, \left| \frac{\partial w_0^k}{\partial x_v} x_s \right| \leq \lambda_{kvs} \right\}$.

Proof: From relaxation Lemma in (8), LMIs in (18) imply $\Lambda_{zzz}^\alpha = \text{block-diag}[\Upsilon_{zzz}^\alpha, \Omega_{zzz}^\alpha] < 0$, or equivalently,

$$\begin{aligned} \Upsilon_{zzz}^\alpha &= A_z P_z + B_z F_z + P_z A_z^T + F_z^T B_z^T - \sum_{k=1}^p \sum_{v=1}^n \sum_{e=1}^m (-1)^{d_{kv}(e+n)} \eta_{kv} \mu (B_z)_{ve} (P_{g_1(z,k)} - P_{g_2(z,k)}) \\ &\quad - \sum_{k=1}^p \sum_{v=1}^n \sum_{s=1}^n (-1)^{d_{kvs}} \lambda_{kvs} (A_z)_{vs} (P_{g_1(z,k)} - P_{g_2(z,k)} - B_z G_z^k - (G_z^k)^T B_z^T) < 0, \end{aligned}$$

$$\Omega_{zz}^\alpha = - \begin{bmatrix} P_z & F_z^T \\ F_z & \mu^2 I_m \end{bmatrix} - \sum_{k=1}^p \sum_{v=1}^n \sum_{s=1}^n (-1)^{d_{kvs}} \lambda_{kvs} (A_z)_{vs} \begin{bmatrix} 0 & (G_z^k)^T \\ G_z^k & 0 \end{bmatrix} < 0.$$

Given that all the possible sign combinations of the terms involving η_{kv} and λ_{kvs} are taken into account in

the previous expressions by means of parameter α , and provided that $\left| \frac{\partial w_0^k}{\partial x_v} u_e \right| \leq \mu \eta_{kv}$, $\left| \frac{\partial w_0^k}{\partial x_v} x_s \right| \leq \lambda_{kvs}$ in R_o ,

it follows that:

$$\begin{aligned} A_z P_z + B_z F_z + P_z A_z^T + F_z^T B_z^T - \sum_{k=1}^p \sum_{v=1}^n \sum_{e=1}^m \frac{\partial w_0^k}{\partial x_v} u_e (B_z)_{ve} (P_{g_1(z,k)} - P_{g_2(z,k)}) \\ - \sum_{k=1}^p \sum_{v=1}^n \sum_{s=1}^n (A_z)_{vs} \frac{\partial w_0^k}{\partial x_v} x_s (P_{g_1(z,k)} - P_{g_2(z,k)} - B_z G_z^k - (G_z^k)^T B_z^T) < \Upsilon_{zzz}^\alpha < 0 \end{aligned} \quad (19)$$

$$- \begin{bmatrix} P_z & F_z^T \\ F_z & \mu^2 I_m \end{bmatrix} - \sum_{k=1}^p \sum_{v=1}^n \sum_{s=1}^n (A_z)_{vs} \frac{\partial w_0^k}{\partial x_v} x_s \begin{bmatrix} 0 & (G_z^k)^T \\ G_z^k & 0 \end{bmatrix} < \Omega_{zz}^\alpha < 0. \quad (20)$$

The time-derivative (10) of the non-quadratic Lyapunov function candidate (9) is negative if (11) holds, which is implied by condition (19). Moreover, $\|u\|_2 < \mu$ holds if (15) does so, which is guaranteed by condition (20), thus concluding the proof. \square

A similar result is now presented via property (17):

$$\Omega_{ij} = \begin{bmatrix} - \begin{bmatrix} P_j & F_j^T \\ F_j & \mu^2 I_m \end{bmatrix} + \frac{1}{2} \sum_{k=1}^p \sum_{v=1}^n \sum_{s=1}^n \lambda_{kvs}^2 T_{ij}^{kvs} & (*) & \cdots & (*) & \cdots & (*) \\ (A_i)_{11} \begin{bmatrix} 0 & -(G_j^1)^T \\ -G_j^1 & 0 \end{bmatrix} & -2T_{ij}^{111} & \cdots & 0 & \cdots & 0 \\ \vdots & \vdots & \ddots & \vdots & \ddots & \vdots \\ (A_i)_{11} \begin{bmatrix} 0 & -(G_j^p)^T \\ -G_j^p & 0 \end{bmatrix} & 0 & \cdots & -2T_{ij}^{p11} & \cdots & 0 \\ \vdots & \vdots & \ddots & \vdots & \ddots & \vdots \\ (A_i)_{nn} \begin{bmatrix} 0 & -(G_j^p)^T \\ -G_j^p & 0 \end{bmatrix} & 0 & \cdots & 0 & \cdots & -2T_{ij}^{pnn} \end{bmatrix},$$

$g_1(\alpha, k)$, $g_2(\alpha, k)$ defined as in (12), then $x(t)$ tends to zero exponentially for any trajectory satisfying

$$(6) \text{ in the outermost Lyapunov level } R_o \subseteq (R \cap C) \text{ with } R = \bigcap_{e,k,s,v} \left\{ x : \left| \frac{\partial w_0^k}{\partial x_v} u_e \right| \leq \mu \eta_{kv}, \left| \frac{\partial w_0^k}{\partial x_v} x_s \right| \leq \lambda_{kvs} \right\}.$$

Proof: From (17) it is clear that

$$\begin{aligned} & A_z P_z + B_z F_z + P_z A_z^T + F_z^T B_z^T - \sum_{k=1}^p \sum_{v=1}^n \sum_{e=1}^m \frac{\partial w_0^k}{\partial x_v} u_e (B_z)_{ve} (P_{g_1(z,k)} - P_{g_2(z,k)}) \\ & - \sum_{k=1}^p \sum_{v=1}^n \sum_{s=1}^n (A_z)_{vs} \frac{\partial w_0^k}{\partial x_v} x_s (P_{g_1(z,k)} - P_{g_2(z,k)} - B_z G_z^k - (G_z^k)^T B_z^T) \\ & = A_z P_z + B_z F_z + P_z A_z^T + F_z^T B_z^T \\ & + \sum_{k=1}^p \sum_{v=1}^n \sum_{e=1}^m \frac{\partial w_0^k}{\partial x_v} u_e (B_z)_{ve} (P_{g_2(z,k)} - P_{g_1(z,k)}) \\ & + \sum_{k=1}^p \sum_{v=1}^n \sum_{s=1}^n (A_z)_{vs} \frac{\partial w_0^k}{\partial x_v} x_s (P_{g_2(z,k)} - P_{g_1(z,k)} + B_z G_z^k + (G_z^k)^T B_z^T) \end{aligned}$$

$$\begin{aligned}
& - \begin{bmatrix} P_z & F_z^T \\ F_z & \mu^2 I_m \end{bmatrix} - \sum_{k=1}^p \sum_{v=1}^n \sum_{s=1}^n (A_z)_{vs} \frac{\partial w_0^k}{\partial x_v} x_s \begin{bmatrix} 0 & (G_z^k)^T \\ G_z^k & 0 \end{bmatrix} \\
& = - \begin{bmatrix} P_z & F_z^T \\ F_z & \mu^2 I_m \end{bmatrix} + \sum_{k=1}^p \sum_{v=1}^n \sum_{s=1}^n (A_z)_{vs} \frac{\partial w_0^k}{\partial x_v} x_s \begin{bmatrix} 0 & -(G_z^k)^T \\ -G_z^k & 0 \end{bmatrix} \\
& \leq - \begin{bmatrix} P_z & F_z^T \\ F_z & \mu^2 I_m \end{bmatrix} + \frac{1}{2} \sum_{k=1}^p \sum_{v=1}^n \sum_{s=1}^n \left[\lambda_{kvs}^2 T_{zz}^{kvs} + (A_z)_{vs}^2 \begin{bmatrix} 0 & -(G_z^k)^T \\ -G_z^k & 0 \end{bmatrix} [T_{zz}^{kvs}]^{-1} \begin{bmatrix} 0 & -(G_z^k)^T \\ -G_z^k & 0 \end{bmatrix} \right] < 0
\end{aligned}$$

gives

$$\Omega_{zz} = \begin{bmatrix} - \begin{bmatrix} P_z & F_z^T \\ F_z & \mu^2 I_m \end{bmatrix} + \frac{1}{2} \sum_{k=1}^p \sum_{v=1}^n \sum_{s=1}^n \lambda_{kvs}^2 T_{zz}^{kvs} & (*) & \dots & (*) & \dots & (*) \\ (A_z)_{11} \begin{bmatrix} 0 & -(G_z^1)^T \\ -G_z^1 & 0 \end{bmatrix} & -2T_{zz}^{111} & \dots & 0 & \dots & 0 \\ \vdots & \vdots & \ddots & \vdots & \ddots & \vdots \\ (A_z)_{11} \begin{bmatrix} 0 & -(G_z^p)^T \\ -G_z^p & 0 \end{bmatrix} & 0 & \dots & -2T_{zz}^{p11} & \dots & 0 \\ \vdots & \vdots & \ddots & \vdots & \ddots & \vdots \\ (A_z)_{nn} \begin{bmatrix} 0 & -(G_z^p)^T \\ -G_z^p & 0 \end{bmatrix} & 0 & \dots & 0 & \dots & -2T_{zz}^{pnn} \end{bmatrix},$$

which allows defining $\Lambda_{zzz} = \text{block-diag}[\Upsilon_{zzz}, \Omega_{zz}]$.

Applying Relaxation Lemma (8) to Λ_{zzz} leads to LMIs (21), thus concluding the proof. \square

Remark 1: Theorems 2 and 3 provide LMI conditions for local non-quadratic controller design of continuous-time TS models. The control law thus designed is guaranteed to stabilize the TS model in the outermost Lyapunov level of region R , whose bounds depend on those of the compact set C , the designed bound μ of the input, and the inherited bounds of the partial derivatives $\partial w_0^k / \partial x_v$. Let us recall that, in many previous studies, see e.g. [13,19,21-25,27], **controller design conditions** have been obtained by

making very restrictive assumptions of the sort $\|\dot{P}_z\| < \phi_z$. It means that these bounds cannot be known in advance since they depend on the time-derivative of the state, which cannot be assured to be a priori stable.

Therefore, all these previous methods fail to give a solution to this problem whereas the parameters

$\left| \frac{\partial w_0^k}{\partial x_v} x_s \right|$ and $\left| \frac{\partial w_0^k}{\partial x_v} u_e \right|$, which are used in the above proposed theorems, are always known. Indeed, it is well-

known that the quasi-LPV (or TS) description is only validated in a compact set of the state space, therefore

x_s is known and the functions w_0^k being smooth, their derivative $\partial w_0^k / \partial x_v$ limits are easy to compute.

Moreover, considering any practical application, conditions (15) allows to guarantee $\|u\|_2 < \mu$ so as to

bound $\left| \frac{\partial w_0^k}{\partial x_v} u_e \right|$. The parameter μ (which can be obtained from the actuators technical characteristics)

ensure that, with the obtained solution to LMIs, the control signal will always be bounded while the initial

conditions belong inside the domain of attraction D . Therefore, the proposed study provides an answer to

previous non-quadratic approaches where unknown parameters had to be assumed for the LMI

computation. **At last, it is important to point out that most of the previous studies dealing with TS systems**

tend to explore global stability regardless of their local nature. By contrast, local analysis and controller

design for nonlinear systems are widely used; in this sense the proposed approach better fits the nonlinear

spirit by reducing global objectives to local stability conditions for TS models.

Remark 2: Conditions in Theorems 2 and 3 reduce to those of the quadratic global controller design if

$P_i = P$, $G_i^k = 0$, $i \in \{1, \dots, r\}$, $k \in \{1, \dots, p\}$. For Theorem 2 it cancels the last two triple sums of Υ_{ijl}^α and

the last triple sum of Ω_{ij}^α in (18), allowing λ_{kvs} and η_{kv} to grow arbitrarily large (global controller). As for

Theorem 3, it makes zero all the non-diagonal terms of Υ_{ijl} and Ω_{ij} in (21), so matrices $Q_{ijl}^{ksv} > 0$, $S_{ijl}^{kve} > 0$,

and $T_{ij}^{ksv} > 0$ can always be found to fulfill conditions (21) despite the values of λ_{kvs} and η_{kv} .

Remark 3: Even if conditions in Theorems 2 or 3 fail to be fulfilled for a given set of constants $\lambda_{kvs}, \eta_{kv} > 0$

(i.e., for a given region), the largest region of attraction can still be found via linear programming by testing conditions in these theorems for successively larger values of a common factor $\lambda > 0$ multiplying both sets of constants, assuming that conditions in Theorem 1 hold.

Remark 4: Notice that compared with the quadratic case, theorem 2 increases the number of LMI constraints from $r+1$ to $r+r^2 \times 2^{pn-1}$ whereas theorem 3 increases them from $r+1$ to $r+r^2$ while increasing the size of each LMI from $\square^{n \times n}$ to $\square^{(n \times k \times u) \times (n \times k \times u)}$.

4. Examples

Example 1: Consider the following TS model [28]

$$\dot{x} = \sum_{i=1}^2 h_i(x_1)(A_i x + B_i u) \quad (22)$$

$$\text{with } h_1(x_1) = \frac{1 - \sin(x_1)}{2}, \quad h_2(x_1) = \frac{1 + \sin(x_1)}{2}, \quad A_1 = \begin{bmatrix} 2 & -10 \\ 2 & 0 \end{bmatrix}, \quad A_2 = \begin{bmatrix} a & -5 \\ 1 & 2 \end{bmatrix}, \quad B_1 = \begin{bmatrix} 1 \\ 1 \end{bmatrix}, \quad B_2 = \begin{bmatrix} b \\ 2 \end{bmatrix},$$

$$|x_i| < \frac{\pi}{2}, \quad -20 \leq a \leq 10, \quad 0 \leq b \leq 25.$$

Figure 1 shows the effects of parameter μ in a single stabilization case ($a = 4.6, b = 0$). Conditions in Theorem 2 and linear programming have been combined to find local controllers maximizing the region of attraction for $\mu = 30$ (bounded by the dashed closed curve) and $\mu = 100$ (bounded by the solid closed curve). As expected, the latter provides the biggest region and includes the former one. The bounds of

$$R = \bigcap_{e,k,s,v} \left\{ x : \left| \frac{\partial w_0^k}{\partial x_v} u_e \right| \leq \mu \eta_{kv}, \left| \frac{\partial w_0^k}{\partial x_v} x_s \right| \leq \lambda_{kvs} \right\} \text{ for } \mu = 100 \text{ are shown in dotted lines.}$$

Figure 2 shows the advantages of using gains G_i^k for the previous case ($a = 4.6, b = 0$). Theorem 2 and linear programming have been used again to find local controllers maximizing the region of attraction

without G_i^k (bounded by a dashed closed curve) and including G_i^k (bounded by the solid closed curve). It is clear that the new control law (5) outperforms the existing non-quadratic ones [22]. As in Figure 1, the bounds of region R for the case including G_i^k are shown in dotted lines.

Conditions in [21] are unfeasible for this model in any point of the considered grid. The proposed approach is therefore compared with that in [28], for which the following pole placement LMIs for a D-region must be included:

$$\begin{bmatrix} -\bar{r}P_i & \bar{G}_{ij}^\alpha \\ (*) & -\bar{r}P_i \end{bmatrix} < 0, \begin{bmatrix} \sin \theta \left(\bar{G}_{ij}^\alpha + (\bar{G}_{ij}^\alpha)^T \right) & \cos \theta \left(\bar{G}_{ij}^\alpha - (\bar{G}_{ij}^\alpha)^T \right) \\ \cos \theta \left(\bar{G}_{ij}^\alpha - (\bar{G}_{ij}^\alpha)^T \right) & \sin \theta \left(\bar{G}_{ij}^\alpha + (\bar{G}_{ij}^\alpha)^T \right) \end{bmatrix} < 0, \bar{G}_{ij}^\alpha + (\bar{G}_{ij}^\alpha)^T + \beta P_i < 0, \quad (23)$$

with $\bar{G}_{ij}^\alpha = A_i P_i + B_i \left(F_i + \sum_{k=1}^p \sum_{v=1}^n \sum_{s=1}^n (A_j)_{vs} (-1)^{d_{ksv}^\alpha} \lambda_{ksv} G_i^k \right) < 0$, $i, j \in \{1, \dots, r\}$, $\alpha \in \{1, \dots, 2^{pn^2}\}$, and \bar{r} , θ and

β as parameters defining the D-region.

The proposed approach is μ -dependent ($|\mu| < \mu$). Figure 3 shows the effect of this parameter on the stabilizability region size for $-20 \leq a \leq 10$, $0 \leq b \leq 25$. As μ increases, more feasible points (“+” marks) are found via conditions in Theorem 1 and (23); these points are then compared with those of the quadratic approach (“o” marks) and those of the line integral approach in [28] (“x” marks). Note that with $\mu = 500$, the new approach includes any feasible point of the other approaches considered.

Example 2: Consider the following TS model [21]:

$$\dot{x} = \sum_{i=1}^2 h_i(x_1) (A_i x + B_i \mu), \quad (24)$$

with $h_1(x_1) = \frac{1 + \sin(x_1)}{2}$, $h_2(x_1) = \frac{1 - \sin(x_1)}{2}$, $A_1 = \begin{bmatrix} -5 & -4 \\ -1 & -2 \end{bmatrix}$, $A_2 = \begin{bmatrix} -2 & -4 \\ 20 & -2 \end{bmatrix}$, $B_1 = \begin{bmatrix} 0 \\ 10 \end{bmatrix}$, $B_2 = \begin{bmatrix} 0 \\ 3 \end{bmatrix}$,

$$|x_i| < \frac{\pi}{2}.$$

The approach in [21] has several drawbacks, none of which is shared by the proposed one: it only applies for TS models whose membership functions have strictly state-dependent time-derivatives (like (24)); its conditions are not LMIs unless some parameters are given; its proposed control law includes time-derivatives of the membership functions which are not always available. For the sake of comparison between Theorems 2 and 3, they have been applied for stabilization of TS model (24) for different values of μ and c , with $|u| < \mu$, $|x(0)| < c$; the resulting maxima λ_{kvs} and η_{kv} are summarized in Table 1. Figure 4 illustrates the states evolution of TS model (24) under a control law (5) whose gains have been obtained via Theorem 3 with $\mu = 0.1$, $c = \sqrt{2} \pi/2$; correspondingly, Figure 5 shows the control law evolution corresponding to this case.

5. Conclusions and Perspectives

A novel approach for local non-quadratic stabilization of continuous-time TS models has been presented. Thanks to the information provided by the MFs and a proper manipulation of their time-derivatives, a new non-PDC control law has been proposed which locally stabilizes a continuous-time TS model through straightforward LMI conditions. It has been shown that reducing global goals to the estimation of a region of attraction constitutes a good way-out from the quadratic framework, since **it provides new basis** to overcome old issues on stabilization of continuous-time TS models while incorporating former results as particular cases. Two examples have been provided **that clearly show** that the proposed approach **outperforms the palliative solutions of the previous non-quadratic studies.**

6. Acknowledgment

The present research work has been supported by International Campus on Safety and Intermodality in

Transportation, the Nord-Pas-de-Calais Region, the European Community, the Regional Delegation for Research and Technology, the Ministry of Higher Education and Research, and the National Center for Scientific Research. The authors gratefully acknowledge the support of these institutions.

7. References

- [1] T. Takagi and M. Sugeno, Fuzzy identification of systems and its application to modeling and control, *IEEE Trans. on System Man and Cybernetics*. 15(1) (1985) 116-132.
- [2] T. Taniguchi, K. Tanaka, H.O. Wang, Model construction, rule reduction and robust compensation for generalized form of Takagi-Sugeno fuzzy systems, *IEEE Trans. on Fuzzy Systems*. 9(4) (2001) 525-537.
- [3] H.O. Wang, K. Tanaka, M. Griffin, An approach to fuzzy control of nonlinear systems: Stability and Design Issues, *IEEE Trans. on Fuzzy Systems*. 4(1) (1996) 14-23.
- [4] S. Boyd, L. El Ghaoui, E. Féron, V. Balakrishnan, Linear matrix inequalities in system and control theory. *Studies in Applied Mathematics*; Philadelphia, USA, 1994.
- [5] K. Tanaka and H.O. Wang, Fuzzy control systems design and analysis. A linear matrix inequality approach. John Wiley and Sons, New York. 2001.
- [6] T. Senthilkumar, P. Balasubramaniam, Delay-dependent robust H_∞ control for uncertain stochastic T-S fuzzy systems with time-varying state and input delays, *International Journal of Systems Science*. 42 (5) (2011) 877-887.
- [7] T. Senthilkumar, P. Balasubramaniam, Robust H_∞ control for nonlinear uncertain stochastic T-S fuzzy systems with time-delays, *Applied Mathematics Letters*. 24(12) (2011) 1986-1994.
- [8] M. Zerar, K. Guelton, N. Manamanni, Linear Fractional Transformation Based H-infinity Output Stabilization for Takagi-Sugeno Fuzzy Models, *Mediterranean Journal of Measurement and Control*. 4(3) (2008) 111-121.

- [9] T. Bouarar, K. Guelton, N. Manamanni, LMI stability conditions for Takagi-Sugeno uncertain descriptors, In Proc. in Proc. of the IEEE International Fuzzy Systems Conference, FUZZ-IEEE 2007, London, UK, 2007.
- [10] A. Sala, T.M. Guerra, R. Babuska, Perspectives of fuzzy systems and control, *Fuzzy Sets & Systems*. 156 (2005) 432-444.
- [11] T.M. Guerra, M. Bernal, A. Kruszewski, M. Afroun, A way to improve results for the stabilization of continuous-time fuzzy descriptor models. In Proc. of 46th IEEE CDC, 5960-5964, New Orleans, USA, 2007.
- [12] T. Bouarar, K. Guelton, N. Manamanni, Robust fuzzy Lyapunov stabilization for uncertain and disturbed Takagi-Sugeno descriptors, *ISA Transactions*. 49(4) (2010) 447-461.
- [13] H.D. Tuan, P. Apkarian, T. Narikiyo, Y. Yamamoto, Parameterized linear matrix inequality techniques in fuzzy control system design, *IEEE Trans. on Fuzzy Systems*. 9(2) (2001) 324–332.
- [14] A. Sala, C. Ariño, Asymptotically necessary and sufficient conditions for stability and performance in fuzzy control: Applications of Polya's theorem; *Fuzzy Sets and Systems*. 158(24) (2007) 2671-2686.
- [15] A. Sala, C. Ariño, Relaxed stability and performance conditions for Takagi-Sugeno fuzzy systems with knowledge on membership-function overlap, *IEEE Trans. SMC(B)*. 37(3) (2007) 727–732.
- [16] A. Sala, T.M. Guerra, Stability Analysis of Fuzzy Systems: membership-shape and polynomial approaches, In Proc. of IFAC World Congress, Seoul, South Korea, 5605-5610, 2008.
- [17] M. Bernal, T.M. Guerra, A. Kruszewski, A membership-function-dependent approach for stability analysis and controller synthesis of Takagi-Sugeno models, *Fuzzy Sets & Systems*. 160(19) (2009) 2776-2795.
- [18] M. Johansson, A. Rantzer, K. Arzen, Piecewise quadratic stability of fuzzy systems, *IEEE Trans. on Fuzzy Systems*. 7 (1999) 713-722.

- [19] K. Tanaka, T. Hori, H.O. Wang, A fuzzy Lyapunov approach to fuzzy control systems design, in Proc. American Control Conference, Arlington, USA, 4790-4795, 2001.
- [20] G. Feng, C.L. Chen, D. Soun, Y. Zhu, H_∞ controller synthesis of fuzzy dynamic systems based on piecewise Lyapunov functions and bilinear matrix inequalities. *IEEE Trans. on Fuzzy Systems*. 13(1) (2005) 94–103.
- [21] K. Tanaka, T. Hori, H.O. Wang, A multiple Lyapunov function approach to stabilization of fuzzy control systems, *IEEE Trans. on Fuzzy Systems*. 11(4) (2003) 582-589.
- [22] T.M. Guerra, L. Vermeiren, LMI-based relaxed non-quadratic stabilization conditions for nonlinear systems in Takagi-Sugeno's form, *Automatica*. 40(5) (2004) 823-829.
- [23] W.J. Wang, C.H. Sun, Relaxed stability and stabilization conditions for a T-S fuzzy discrete system, *Fuzzy Sets & Systems*. 156(2) (2005) 208-225.
- [24] B.C. Ding, H.X. Sun, P. Yang, Further studies on LMI-based relaxed stabilization conditions for nonlinear systems in Takagi-Sugeno's form, *Automatica*. 42 (2006) 503-508.
- [25] A. Kruszewski, R. Wang, T.M. Guerra, Non-quadratic stabilization conditions for a class of uncertain non linear discrete-time T-S fuzzy models: a new approach, *IEEE Trans. on Automatic Control*. 53(2) (2008) 606-611.
- [26] T.M. Guerra, A. Kruszewski, M. Bernal, Control Law Proposition for the Stabilization of Discrete Takagi-Sugeno Models, *IEEE Trans. on Fuzzy Systems*. 17(3) (2009) 724-731.
- [27] Y. Blanco, W. Perruquetti, P. Borne, Stability and stabilization of nonlinear systems and Tanaka-Sugeno fuzzy models, in Proc. of the European Control Conference, Lisbon, Portugal, 2001.
- [28] B.J. Rhee, S. Won, A new fuzzy Lyapunov function approach for a Takagi–Sugeno fuzzy control system design, *Fuzzy Sets & Systems*. 157(9) (2006) 1211-1228.

- [29] K. Guelton, T.M. Guerra, M. Bernal, T. Bouarar, N. Manamanni, Comments on Fuzzy Control Systems Design via Fuzzy Lyapunov Functions, *IEEE Trans. on Systems, Man, and Cybernetics (B)*. 40(3) (2010) 970-973.
- [30] T.M. Guerra, M. Bernal, A way to escape from the quadratic framework, in *Proc. FUZZ-IEEE Conference, Jeju, Korea, 2009*.
- [31] H. Khalil, *Nonlinear Systems*, 3rd edition. Prentice Hall, New Jersey, USA. 2002.
- [32] G. Chesi, A. Garulli, A. Tesi, A. Vicino, *Homogeneous Polynomial Forms for Robustness Analysis of Uncertain Systems*, *Lecture Notes in Control and Information Sciences*, volume 390, Springer, 2009.
- [33] M. Bernal, T.M. Guerra, Generalized Nonquadratic Stability of Continuous-Time Takagi-Sugeno Models, *IEEE Trans. on Fuzzy Systems*. 18(4) (2010) 815-822.

Figures and table

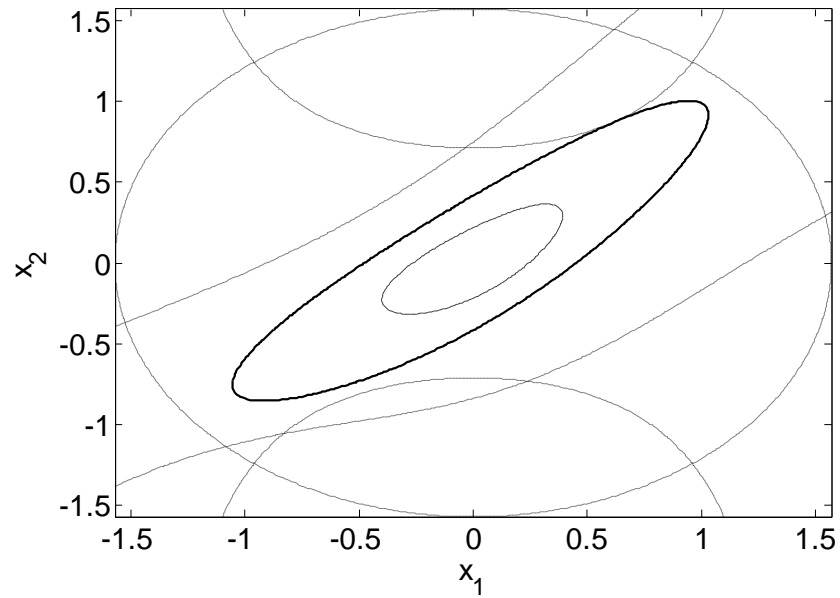


Figure 1: Stabilized domains: with $\mu = 30$ (dashed closed curve); with $\mu = 100$ (solid closed curve).

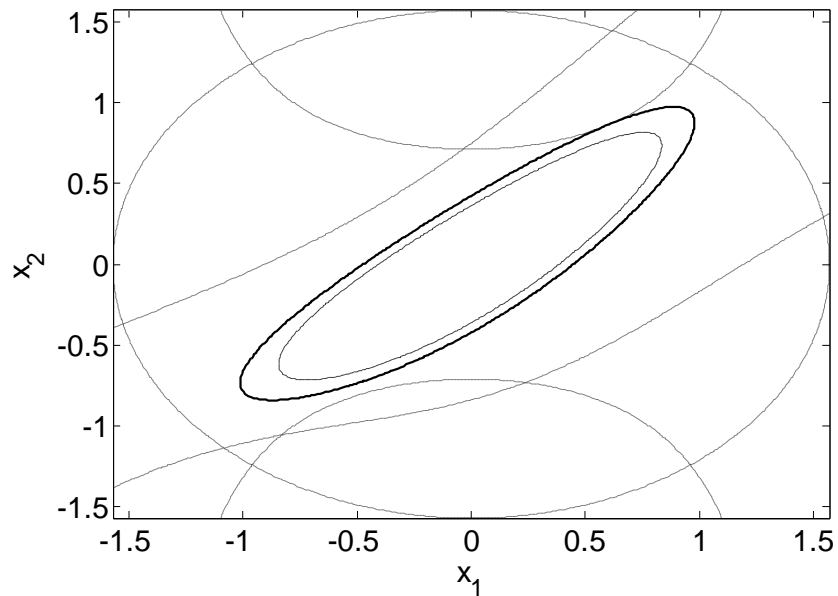


Figure 2: Stabilized domains: without gains G_i^k (dashed closed curve); with gains G_i^k (solid closed curve).

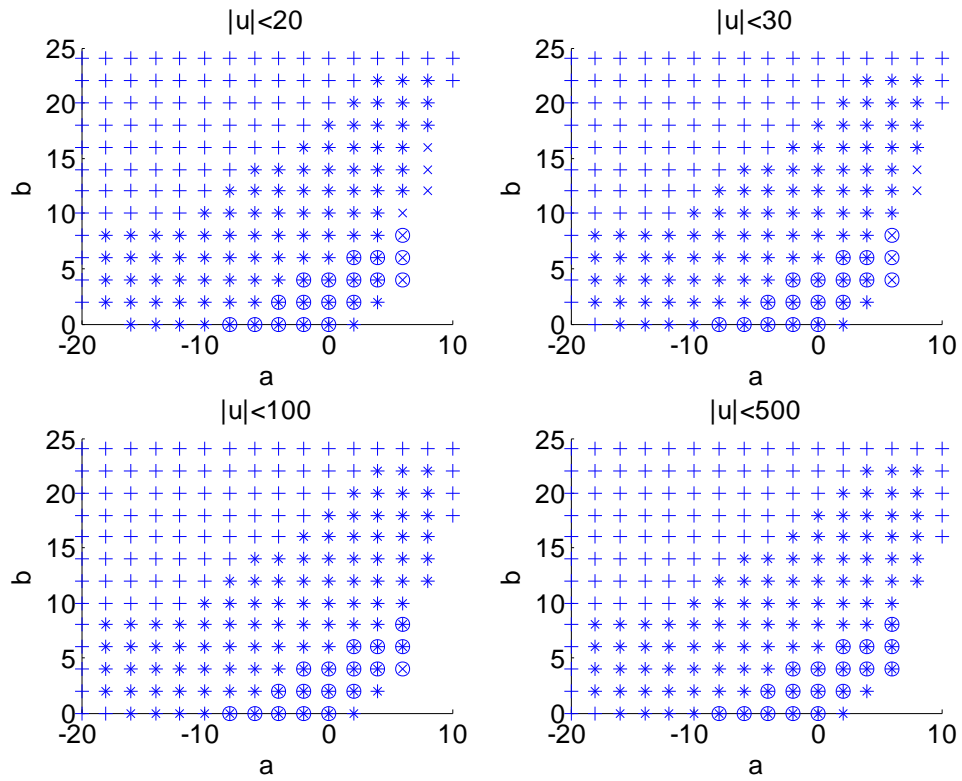


Figure 3: Stabilizability regions (quadratic-“o”, line integral-“x”, proposed approach-“+”).

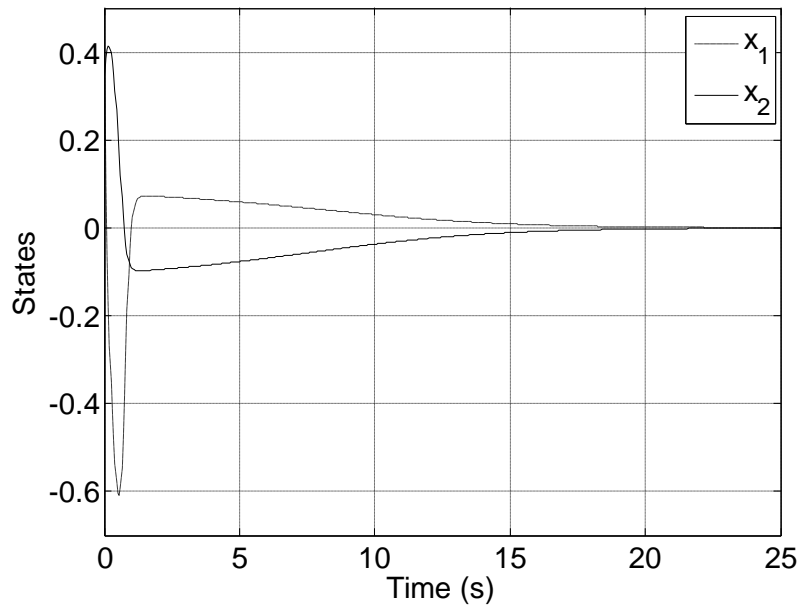


Figure 4: States evolution of TS model (24) under control law (5) obtained via Theorem 3 with $\mu = 0.1$,

$$c = \sqrt{2} \pi / 2 .$$

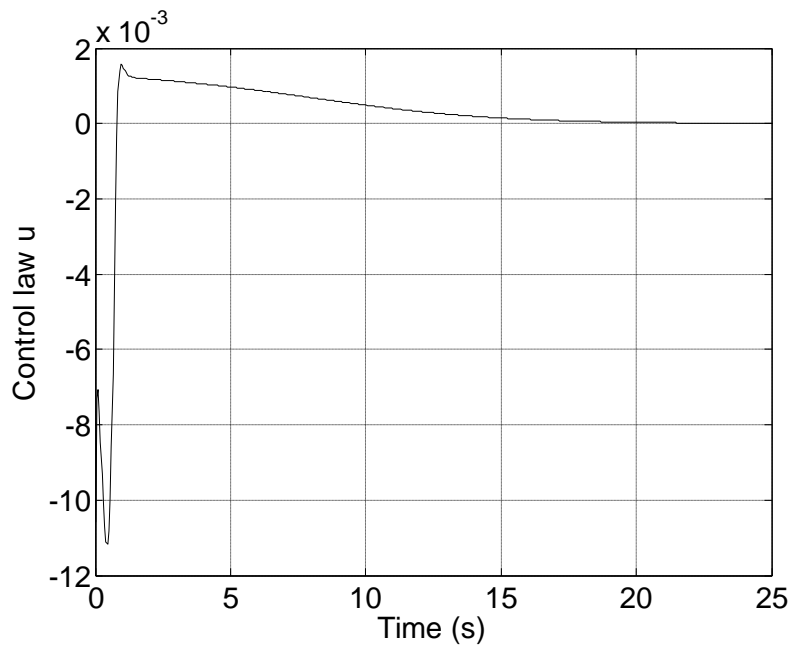


Figure 5: Control law evolution with gains obtained via Theorem 3 with $\mu = 0.1$, $c = \sqrt{2} \pi/2$.

Table 1: Comparison between Theorems 2 and 3.

Approach	$\mu = 0.01, c = \pi/2$	$\mu = 0.01, c = \sqrt{2} \pi/2$	$\mu = 0.1, c = \pi/2$	$\mu = 0.1, c = \sqrt{2} \pi/2$
Theorem 2	$\lambda_{kvs} = 0.8836$ $\eta_{kv} = 0.5625$	$\lambda_{kvs} = 0.8713$ $\eta_{kv} = 0.5547$	$\lambda_{kvs} = 1.4603$ $\eta_{kv} = 0.9297$	$\lambda_{kvs} = 1.2149$ $\eta_{kv} = 0.7734$
Theorem 3	$\lambda_{kvs} = 0.8836$ $\eta_{kv} = 0.5625$	$\lambda_{kvs} = 0.8713$ $\eta_{kv} = 0.5547$	$\lambda_{kvs} = 1.4481$ $\eta_{kv} = 0.9219$	$\lambda_{kvs} = 1.2026$ $\eta_{kv} = 0.7656$