

Impact of hydroxypropylguars on the early age hydration of Portland cement

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1	Impact of hydroxypropylguars on the early age hydration
2	of portland cement
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13 ABSTRACT

14	Hydroxypropylguars (HPG) are used as admixtures in factory-made mortars. These molecules
15	present water retention properties comparable to those obtained with commonly used
16	cellulosic water-retaining agent.
17	The influence of HPG on cement hydration was investigated in order to improve
18	understanding on the delayed effect induced by polysaccharides. Hydration kinetics were
19	characterized by means of conductivity and isothermal calorimetry measurements. The
20	influence of polymer concentration and predissolution was studied. A weak influence of HPG
21	on the germination of hydrates was observed. In contrast, HPG induced a significant decrease
22	in the hydrates growth rate. Strong effects of the polymer concentration and predissolution
23	were noticed too. From these results, we supported the hypothesis that HPG adsorption on
24	hydrated phases via polar interactions should be responsible for the delayed effect observed.
25	
26	

KEYWORDS: polysaccharide (D), hydroxypropylguars (D), retardation (A), hydration (A), water retention (C)

30 1 Introduction

31

32 water. Nowadays, modern factory-made mortars are complex materials, in which are added 33 some kinds of admixtures used to exhibit various properties, from the fresh state to the 34 hardened material. 35 Polysaccharides are one of these admixtures. They are frequently introduced into mortar 36 formulations in order to improve water retention capacity of the freshly-mixed materials, 37 which enhances cement hydration and adhesion to the substrate [1-4]. These products are also 38 expected to act as viscosity-enhancing admixtures to prevent segregation and thus improve 39 the homogeneity and workability of the mortar [5-8]. 40 Among all polysaccharides, Cellulose Ethers (CE) are the most widely used when high water 41 retention capacity is expected. Nevertheless, HydroxyPropylGuars (HPG) were recently 42 presented as a promising new class of water-retaining agent [9]. HPG are already used in 43 various industrial fields, such as textile printing, oil production or paper manufacturing, due to 44 their thickening effect [10]. HPG were also the subject of some patents as admixture for 45 mortars. 46 The effect of saccharides has been largely studied these fifty last years, in particular from a 47 cement hydration delay point of view. In the first time, the delayed effect of monosaccharides 48 was investigated [11-19]. It appears that sugars could be adsorbed to cement phases by a 49 chelation process. It can thereby form a temporary barrier to further hydration. In broad 50 agreement with Young [11], Thomas and Birchall [12] proposed that sugars would be able to 51 poison the surfaces of the CH and CSH by complexation onto these phases, which inhibit 52 their growth and therefore would be responsible for the delay observed. According to Taplin 53 [13], sugars could bind to the cement phases if they have a HO-C=O group, or it could be 54 formed in alkaline media, such as cement paste, by hydrolyze [14].

Traditionally, mortars are based on a mixture of sand, a binder such as cement or lime, and

55 Then, due to the use of polysaccharides in modern factory-made mortars, interactions between 56 polysaccharides and cement have been reported recently. It is established that polysaccharides 57 induce a more or less important delay of Portland cement hydration [20–25], which depends 58 on the nature of the polysaccharide [26]. Pourchez et al. [27,28] have established a 59 mechanism of interaction between CE and cement. 60 However, HPG have received scant attention by the academic community although they are 61 already used industrially. As far as we know, only Izaguirre et al. [29] was interested on the 62 impact of HPG, but in lime-based mortars. Thus, the aim of this work is to study the influence of HPG on the Portland cement hydration kinetics at early age. 63 64 Firstly, the water-retaining effect induced by the HPG in Portland cement-based mortars will be checked. Secondly, cement hydration kinetics in the presence of HPG will be presented. 65 66 Hydration kinetics have been monitored by conductivity and isothermal calorimetry 67 measurements. Finally, a special focus on the influence of the polymer predissolution has 68 been performed.

69 2 Materials

70 2.1 Mineral product

The investigated ordinary Portland cement (OPC) was a CEM I 52.5 R CE CP2 NF type
cement according to the EN 197-1 standard. Its chemical and phase compositions are given in
Table 1. Oxide composition was determined by X-ray fluorescence spectroscopy (SRS3400,
Bruker-AXS). XRD analysis (D5000, Siemens) also allowed quantifying the phase
composition of the given cement by means of Rietveld refinement method (Siroquant V2.5
software).

77 2.2 Organic admixtures

78 Guar gum is a polysaccharide extracted from the seed endosperm of *Cyamopsis*

79 *tetragonolobus*, a native plant from India. This is a galactomannan consisting of a (1-4)-

80 linked β -D-mannopyranose backbone, with random branchpoints of galactose via an α -(1-6)

81 linkage [30] (Fig. 1a). The ratio of mannose to galactose is about 1.8. Unlike the

82 manufacturing of cellulose, the extraction does not require chemical process, but a thermo-

83 mechanical one. So, guar gum is produced without producing any effluent. Moreover, because

84 of the presence of hydroxyl groups in its structure, guar gum exhibits a high chemical

85 reactivity and is soluble in cold water. Thus, the chemical modification of this polysaccharide

86 does not require hard reaction conditions of temperature and pressure, does not generate large

87 quantity of by-products and needs weak purification procedure [31].

HPG are obtained from the native guar gum via an irreversible nucleophilic substitution,

using propylene oxide in the presence of an alkaline catalyst (Fig. 1b). Table 2 gives a

90 qualitative description of the six HPG samples from Lamberti S.p.A which were studied. All

91 the samples have similar molecular weight. The only difference between HPG 1, 2 and 3 is

92 the Degree of Substitution (DS). The only difference between HPG 4, 5 and 6 is the presence

93 of additional substitution (short or long alkyl chains).

94 In order to compare with classical polysaccharide admixtures, three CE were also tested

95 (Table 2): two HydroxyPropylMethyl Cellulose (HPMC) named HPMC1 and HPMC2, and

96 one HydroxyEthyl Cellulose (HEC).

97 **3** Experimental methods of investigation

98 **3.1** Water retention measurements

Water retention capacity of mortars was characterized according to ASTM C1506-09 standard
[32]. This test is based on a measurement of the removed water after depression and was
previously described by Patural et al. [3]. Water retention, noted WR, was calculated using
the following equation:

103
$$WR(\%) = \frac{W_0 - W_1}{W_0} \times 100$$
 (1)

 W_0 represents the initial mass of mixing water; W_1 is the loss of water mass after aspiration. 104 105 Mortars were prepared according to the following mixture proportions: 30% of cement, 65% 106 of sand and 5% of limestone filler (by weight). This mixture design was adapted from the 107 CEReM (european consortium for study and research on mortars) mortars formulation [3]. 108 Admixture amount (0.3 wt%) was in addition to the total dry mixture (*i.e.* cement, sand and 109 filler). Dry mixture was blended in a shaker (Turbula, Wab) for 15 min. Deionized water was 110 added in order to obtain a water to cement ratio W/C = 1. Mixing procedure was in 111 accordance with EN 196-1 [33]. All tests were carried out in triplicate and at controlled 112 temperature of 23°C because water retention is temperature-dependent. A control test was 113 performed with a mortar without admixture.

114 **3.2** Characterization of the cement hydration delay

115 *3.2.1 Conductivity measurements on diluted suspensions*

116 Characterization of the delay induced by the studied polymers on the cement hydration was

- 117 performed by conductivity measurements. This method appears as a powerful and
- reproducible tool to monitor the hydration kinetics [34,35].
 - 6

119 Conductivity measurements could be achieved in lime suspension. This allows obtaining 120 hydration kinetics close to that observed in cement pastes, in spite of a high liquid to solid 121 weight ratio (noted L/S). Nevertheless, monitoring hydration kinetics in an artificial system of 122 lime water is complicated because the dissolution rate of calcium from the cement could be 123 modified due to the initial high concentration of calcium ions in solution. Thus, conductivity 124 curves were interpreted according to the explanation proposed by Comparet et al. [36]. As 125 soon as cement was put in contact with liquid, the electrical conductivity increased as a 126 consequence of the dissolution of the anhydrous phases. Then, germination of hydrates on the 127 grain surface leads to a period, called "low conductivity increasing period", where the 128 conductivity evolves weakly. Conductivity then accelerated more quickly. The conductimetric 129 slope is related to the growth rate of the hydration products. Meanwhile, cement dissolution 130 still continued. The conductivity increased to the critical supersaturation point with respect to 131 portlandite and decreased rapidly due to its precipitation. Thus, an electrical conductivity drop 132 is caused by the portlandite precipitation. This phenomenon was used to determine the 133 hydration delay. Therefore, in this study, the portlandite precipitation time (noted t_{CH}) is a 134 benchmark to classify and to quantify the relative retardation ability of admixtures on cement 135 hydration.

Experiments were performed in diluted suspensions, thermostated at 25°C and continuously stirred. Each experiment was carried out in triplicate. The liquid to solid weight ratio (L/S) used was equal to 20. Polymer to cement weight ratios (P/C) equal to 0.5, 1.0, 1.5 and 2.0 % were studied. Cement and admixture powders were blended in a shaker (Turbula, Wab) for 10 min before contact with the liquid phase. The liquid used was a 20 mM lime solution or deionized water. The control used was the neat cement.

142 *3.2.2 Isothermal calorimetry on cement pastes*

143 Calorimetry is another technique useful to characterize the exothermic hydration process of 144 cement. The hydration process can be followed continuously at realistic water/cement ratios 145 (W/C) in situ and aims at giving an indication of the overall rate of reaction. Thus, 146 calorimetry can be used as a complementary method to conductivity in order to monitor the 147 kinetics of cement hydration and to observe hydration delay induced by retarders [37]. 148 The tests were performed with an isothermal calorimeter (C80, Setaram) at 25°C. The weight 149 ratios used were W/C = 0.4, with deionized water, and P/C = 0.3 %. Ex-situ mixing was 150 preferred to in-situ mixing to improve the homogeneity of the sample, and thus 151 reproducibility. Mixing procedure, with 100g of cement, was in accordance with standard EN 152 196-1 [33]. 10 min after the beginning of the batch, about 2g of paste are introduced in the 153 calorimeter. The control used was the neat cement.

154 *3.2.3 Predissolution of the admixture*

The influence of the polymer predissolution was studied by means of conductivity and
isothermal calorimetry measurements. Admixtures were previously dissolved in the liquid
phase, deionized water or 20 mM lime solution, for 24h by magnetic stirring. Then, cement
was added.

In case of conductivity experiments, the effect of the predissolution has been highlighted by calculating the increase percentage in the portlandite precipitation time t_{CH} as followed (in gray in Fig. 10):

162 Increase of
$$t_{CH}$$
 (%) = $\frac{t_{CH}(with \ prediss) - t_{CH}(without \ prediss)}{t_{CH}(without \ prediss)} \times 100$ (2)

163 **3.3** Calcium binding capacity

164 The ability of HPG and also sugars (sucrose which is known to complex calcium ions,165 galactose and mannose which constitute HPG's molecule) to form complexes with calcium

166 ions was studied. Sugars are valuable insights in order to compare the behavior of HPG and to

167 validate the relevance of this protocol, developed by Thomas and Birchall [12].

168 Each sample (2 g per liter) was introduced into a volume of water (1L) containing a large

169 excess of solid lime (6 g per liter). After 48 hours of stirring at a controlled temperature of

 $170 \quad 23^{\circ}$ C, the suspension was filtered through a 0.7 μ m glass fiber filter. The filtrates were diluted

and acidified. Then, a quantification of the calcium ion content by ionic chromatography was

172 performed on a Dionex apparatus composed of a GP 50 gradient pump, a CS 12A cation-

173 exchange column and a CD 20 conductometric detector. The eluent was a solution of

metasulfonic acid at 20 mM with isocratic mode. The flow was fixed at 1 mL/min. The results
correspond to an average of 3 experiments.

As the solid calcium hydroxide is in large excess, calcium ions consumed by complexation do not affect the "stock" of calcium ions in solution, which thus remains equal to 23 mM during the experiment. However, once the filtrate diluted and acidified, the complexes are destroyed, thus freeing the complexed calcium ions. So, if the calcium concentration is about 23 mM (solubility of lime), no significant complexation has taken place. Instead, a calcium concentration above 23 mM indicates a significant complexation of calcium ions.

182 **3.4** Kinetic of dissolution

HPG absorb in the ultraviolet as evidenced by the absorption spectra (Fig. 2a), and the
concentration of HPG in solution is proportional to the absorbance at the maximum of the
band (266 nm) as shown in Fig. 2b.

186 The dissolution process was monitored by acquisition of UV-Vis absorption spectra. The procedure was the following: a dispersion of HPG (final concentration: 2g.L⁻¹) in deionized 187 188 water or 20 mM lime solution was prepared in a sealed reactor (1L of solution) thermostated 189 at 25°C. HPG was introduced through a sieve in order to have a good dispersion of the sample 190 into the vortex created by the mechanic stirrer. Thus, the aggregation of particles was 191 minimized and a homogeneous polymer solution was produced. The experiment was done 192 under continuous flow of nitrogen to avoid carbonation of lime. At different times, an aliquot 193 of approximately 5 mL was taken from the batch solution and centrifuged by means of a 194 micro-centrifuge (Eppendorf MiniSpin Plus, 14500 rpm) for 5 min in order to remove 195 undissolved particles. The supernatant was collected and homogenized by vortex-stirring. The 196 absorbance of this solution was measured between 200 and 400 nm using an UV/Visible 197 spectrophotometer (Cary 300 Scan, Varian). A degree of progress of the dissolution reaction 198 $\lambda(t)$ was used, which is equal to the absorption at time t divided by the absorption at the end 199 of the dissolution reaction (*i.e.* 24 h). This number is adimensional and its value is between 0 200 and 1.

201 **4 Results and discussions**

202 4.1 Impact of HPG on water retention in fresh mortar

Water retention is a very sensitive mortar property. Indeed, it must be important enough to not
disturb the hydration of the cement. It also limits the absorption of the mixing water by the
substrate and thus provides good mechanical and adhesive properties to the mortar.
DTU 26.1 [38] specifies three classes of water retention of a fresh mortar. The first one
represents mortars which water retention is lower than 86%; they belong to the low water
retention category. The second class (intermediate water retention) corresponds to values

ranging from 86% to 94%. The last one is defined by water retention higher than 94%. This

210 class is related to strong water retention mortar and is desired by formulators of industrial

211 mortars.

212 Water retention capacity of the studied mortars according to the admixture used is shown in

Fig. 3. With this formulation, mortars containing HPG 2 to 6 and HPMC 2 could be

considered as high WR capacity according to the DTU 26.1. Mortars containing HPG 1,

215 HPMC 1 and HEC are in the intermediate category.

216 Thus, HPG improve considerably the water retention capacity of the mortar compared to the

217 control without water-retention admixture, as announced by Plank [9]. In addition, the results

are quite comparable to those obtained with the CE of reference.

Therefore, HPG can be considered as promising water-retention agents for dry-mix Portlandcement-based mortars.

221 4.2 Impact of HPG on hydration kinetics of cement

222 4.2.1 Delayed effect

223 The delayed effect of HPG on cement hydration kinetics was monitored by conductivity in a 224 20 mM lime solution, for ratios L/S = 20 and P/C = 2%. To have a clear and readable 225 analysis, all the conductimetric curves will not be presented on the same figure. Thus, Table 3 226 regroups the conductimetric data obtained (i.e. portlandite precipitation times, delays 227 compared to the control and conductimetric slopes). Fig. 4 presents the influence of the DS on 228 the conductimetric curves by studying HPG 1, 2 and 3 which are the same molecules, except 229 the DS (DSHPG1>DSHPG2>DSHPG3). The influence of the alkyl substitution was studied 230 by comparison of HPG 4, 5 and 6 (see Table 2). The conductimetric curves obtained are 231 shown in Fig. 5.

The conductimetric data (Table 3) highlights the impact of HPG on the kinetics of hydration.
By focusing on the portlandite precipitation time (conductivity drop) and delays, it appears a
wide range of delays induced by the admixtures studied. HPG 5 and 6 exhibit superposed
conductimetric curves and the weaker delay (+71% and +66% respectively). The most
important delay is observed for HPG 1 (+329%). It also appears that delays induced by HPG
are between those obtained for the CE studied (+40% to +405%).
Some polysaccharides (dextrines for example [26]) or other admixtures (setting retarding

239 admixtures such as sugars [19], sodium gluconate [39] or some superplasticizers [36]) induce 240 a blocking effect or an inhibition of the hydration. Here, from the shape of the conductimetric 241 curves obtained, HPG involve a small increase in the duration of the "low conductivity 242 increasing period". Therefore, this indicates a weak influence of the HPG on the germination 243 of cement hydrates. The delay of portlandite precipitation time seems to be mainly due to a 244 slope decrease (Table 3). Indeed, the slope obtained with the control is almost six times 245 higher than that obtained for HPG 1. The slope of the conductimetric curve is linked to the 246 growth rate of the hydrated cement phases. HPG seem to act preferentially on the growth of 247 hydrates phases, rather than on their germination. This could explain the delays observed and 248 is in agreement with results obtained with CE [40].

In addition, delay increases when DS decreases (Fig. 4). Nevertheless, the alkyl substitution seems to have a slight effect (Fig. 5) because the delay slightly decreases in the presence of alkyl chains. The effect of the chain length is negligible.

252 4.2.2 Calcium binding capacity

The calcium complexation is often advanced as assumption to explain the effect of retarders [41]. It seemed important to check if HPG complex with calcium ions. The calcium binding capacity at alkaline pH of the 6 HPG and 3 sugars were conducted and the results are presented in Fig. 6. It appears clearly that the complexation of calcium ions by HPG is null or very weak, like with CE [42]. Indeed, the value of calcium ions concentration found for the
HPG samples was close to the reference sample and is only due to the lime solubility. Instead,
sugars studied present higher calcium ion concentration due to a greater binding capacity,
which is coherent according to the data of the literature [12,42]. Therefore, calcium ion
complexation is clearly not responsible for the delay of cement hydration induced by HPG.

262

4.2.3 Influence of polymer concentration

263 The influence of the amount of polymer is studied by conductivity in 20mM lime solution by 264 varying P/C ratio with a constant L/S ratio (equal to 20) for each HPG. The effect of polymer 265 concentration is considerable and results in a drastic decrease in the slope (Fig. 7). Thus, a 266 small increase in the amount of polymer leads to a huge increase in the portlandite 267 precipitation time, and so in the delay of hydration. Fig. 8 presents the portlandite 268 precipitation time for each polymer and concentration. The effect of the concentration is 269 similar whatever the molecule. For each polymer, the more the concentration increases, the 270 more the delay increases. As the retarding effect is effective at very low HPG concentrations, 271 it confirms that calcium complexation cannot be responsible for the delay mechanism. 272 It is generally admitted that cement hydration delay induced by admixtures is due to 273 adsorption of these molecules to surfaces of the hydrating cement particles and/or surfaces of 274 hydration products [41,43]. The concentration dependent behavior of the delay suggests also 275 that HPG delay cement hydration via adsorption on the cement phases. 276 The mechanism responsible for the delay induced by CE is the adsorption of the molecule on 277 the hydrate cement phases. Indeed, Pourchez et al. have shown evidence of the adsorption of 278 CE on calcium hydroaluminates [44] and CSH/CH [40]. Polysaccharides are molecules which 279 contain a lot of polar functional groups (-OH). Therefore, strong interactions, through 280 electrostatic forces and hydrogen-bonding, can occur between polysaccharides and the highly 281 polar hydrated phases [43]. The relationship between adsorption and retardation was

282 previously shown [25,40]. It results that the higher the substituent content is, the weaker the 283 retardation ability is, because of lower amount of free hydroxyls and so lower adsorption 284 ability.

285 For HPG, the phenomena could be very close, due to the similarity of the molecules used, in 286 particular the high content of hydroxyl groups. Wang et al. [45,46] have shown that the 287 adsorption mechanism of galactomannose polysaccharides at solid-liquid interfaces involves 288 strong hydrogen bonding. Results obtained are in broad agreement with the relationship 289 between adsorption and retardation described above. Indeed, qualitative data of DS are 290 coherent with the delay observed. For example, the comparison of the HPG with different DS 291 shows that $t_{CH}(HPG1) > t_{CH}(HPG2) > t_{CH}(HPG3)$ with DS(HPG1) < DS(HPG2) < DS(HPG3). 292 Moreover, delay induced by HPG 4 is slightly higher compared to HPG 5 and 6. The only 293 difference between these HPG is the substitution of the alkyl chains which could cause steric 294 hindrance and increase the lipophilic character of the polymer. The presence of alkyl chains 295 could reduce slightly the adsorption and so the delay. Effectively, t_{CH}(HPG4) is higher than 296 t_{CH}(HPG5,6). Nevertheless, the length of the alkyl chains seems to not affect the adsorption 297 because the difference on hydration delay is negligible. Indeed, the portlandite precipitation 298 times for HPG 5 and HPG 6 are very close.

299 4.2.4

Influence of admixture predissolution

300 The effect of the admixture predissolution on the cement hydration kinetics has also been 301 observed. Firstly, this effect in concentrated paste was studied by isothermal calorimetry. 302 Heat evolutions within 24h for cement pastes without and with admixtures are presented in 303 Fig. 9. For admixed cement pastes, HPG 1 (a), HPG 2 (b) and HPG 3 (c) were predissolved or 304 not.

305 Two significant heat flow maxima are observed at early age for the neat cement paste.

306 According to many authors [47-50], the main peak is attributed to the alite hydration reaction. 307 The second peak, only visible as a shoulder, corresponds to renewed dissolution of C₃A once 308 the solid gypsum has been exhausted. For the cement pastes admixed with HPG and without 309 predissolution, the main peak is delayed, whatever the admixture. Thus, HPG retard cement 310 hydration at early age, as well in concentrated cement pastes as in diluted suspensions. 311 The polymer predissolution seems to allow the separation of the main peak into two peaks. 312 This separation is more easily visible in the case of the HPG 1 (Fig. 9a). For HPG 4, 5 and 6, 313 which have a high DS, the effect is very weak, as for the HPG 3 (Fig. 9c). For HPG 2 (Fig. 314 9b), which has an intermediate DS, separation of the peak is less pronounced than in the case 315 of HPG 1, but it is clearly visible. This suggests that the effect is all the more significant since 316 the DS is low. Thus, HPG act preferentially either on the alite hydration or on the exhaustion 317 of the solid gypsum, which is highlighted when HPG are already in the solution. 318 In diluted suspensions, negligible impact of predissolution is observed in water whatever the 319 admixture considered (Fig. 10a). However, in lime suspension (Fig. 10b), the impact of 320 predissolution is very strong for HPG 1, with a huge increase in portlandite precipitation time 321 of 77%. As observed by isothermal calorimetry, the effect decreases when the DS increases: + 322 19% for HPG 2 and +10% for HPG 3. The impact of predissolution is negligible for HPG 4 323 and 5. For CE, no impact of predissolution is observed too, which is coherent with results of 324 Pourchez [51]. For HPG, the delay caused by the polymer is more important after 325 predissolution in 20 mM lime solution than in water (no effect), mainly when DS is low. It is 326 therefore an effect of the alkalinity of the medium. 327 Different hypotheses can be considered. The polymer could be degraded due to the high 328 alkalinity reached when cement dissolves. This degradation could lead to the formation of 329 carboxylates by peeling reaction, molecules known to have a strong retarding effect [52]. The

330 predissolution in lime would promote this degradation, resulting in an increase in the delay.

331 Ultra-violet spectroscopy allows highlighting alkaline degradation. Indeed, the alkaline 332 degradation of sugars leads to the formation of a large peak in the UV range, between 250 and 333 300 nm, due to the formation of saccharinic acids or the enolization of the sugars [12]. To 334 investigate this effect, HPG and sugars (samples tested in calcium binding experiments) were 335 stirred in water and lime solution. UV-Vis absorption spectra were carried out over time. Fig. 336 11 shows these results in case of HPG 1 and galactose, representing HPG and sugars 337 respectively. In the case of HPG 1, the absorption spectra are different in water and in lime 338 solution. Nevertheless, the difference is almost instantaneous and then remains stable over 339 time. Therefore, it cannot be due to alkaline degradation. The difference in intensity is only 340 due to HPG dissolution. For the other 5 HPG, no difference was observed between UV-Vis 341 absorption spectra of polymer dissolved in water and in lime solution. On the contrary, sugars 342 exhibit actually alkaline degradation. A new peak appears and grows with time when they are 343 dissolved in lime solution.

344 Moreover, an infrared investigation was made to determine if carboxylates are formed after 345 dissolution of HPG in alkaline media. As above, HPG were stirred in water and lime solution. 346 After 24h, solutions were neutralized and then placed in an oven until evaporation of the 347 liquid phase. Solid residues were analyzed by infrared spectrometry. No band at 1590 cm⁻¹, 348 corresponding to carboxylates functions, was observed, neither in water nor in lime solution. 349 Thus, experiments on HPG indicate their alkaline stability. This is consistent with the 350 hypotheses of many authors. A reduction in intrinsic viscosity has been observed for 351 galactomannans under alkaline conditions [53–55]. However, according to these authors, this 352 reduction is not due to degradation by a peeling reaction, but to inhibition of intermolecular 353 interactions (hyperentanglement) because of ionization of hydroxyl groups. Izaguirre et al. reached the same conclusion with HPG [29]. Furthermore, similar results of polysaccharide 354 355 alkaline stability were observed with CE [42].

356 A second hypothesis would be slower dissolution kinectis of the polymer in lime solution than 357 in water. In that case, in lime solution, the polymer is not fully active to delay the cement 358 hydration without predissolution because the dissolution would be slowdown. On the 359 contrary, predissolution leads to the complete dissolution of the polymer and therefore a 360 maximum delay. In water, if the dissolution is fast, predissolution could have no effect. Fig. 361 12 presents the effect of the media on the dissolution kinetics for HPG 1. Dissolution is very 362 fast, both in water and in 20 mM lime solution. The polymer seems to be completely 363 dissolved after 40 min, whatever the dissolution media. Same results are obtained for the 364 other HPG. Thus, dissolution kinetics cannot be responsible for the predissolution effect on 365 cement hydration kinetics. Moreover, guar gum is known to be easily soluble [56]. 366 According to some authors, hydroxyl groups of galactomannans [53–55] and HPG [29] would 367 ionize in alkaline media. It seems very probable that predissolving the polymer in the lime 368 solution would ionize a maximum of hydroxyl groups and thus enhance the adsorption of 369 polysaccharide on the cement phases. So, the delayed effect is greater after predissolution in 370 lime solution, but there is no change after predissolution in water. That would explain why 371 HPG 1, which is the polymer with the lower DS, thus higher amount of polysaccharidic backbone hydroxyl groups, is the most sensitive to predissolution. Furthermore, this 372 373 hypothesis is coherent with the adsorption mechanism via the hydroxyl sites proposed to 374 explain hydration delay induced by HPG. This is consistent with the effect of HPG 375 predissolution in water observed by isothermal calorimetry too. Indeed, calorimetry 376 experiments were made in concentrated pastes. The paste is quickly saturated in lime and the 377 pH increases almost instantly. Thus, even if the polymer is predissolved in water, phenomena 378 occurring are closer to what was observed in conductivity experiments after predissolution in 379 lime solution.

380 **5** Conclusions

381 Based upon this study, it appears that HPG delayed cement hydration with an influence on the 382 growth of the hydrates, rather than on the germination of hydrates. Complexation of calcium 383 ions does not explain this effect. A strong impact of the concentration on the hydration 384 kinetics was observed. The results and the molecular similarity with CE suggest that the delay 385 effect is due to the adsorption of the HPG via the interaction between hydroxyl groups and the 386 highly polar hydrated phases. This hypothesis is coherent with the qualitative data of DS. 387 An increase in portlandite precipitation time was noticed after predissolution of HPG in lime 388 solution. It was shown that no alkaline degradation of HPG occurs. Moreover, no difference 389 of admixture dissolution kinetics in water or lime solution was observed. Thus, these two 390 phenomena are not responsible for the increase in the delay. We put forward that the 391 ionization of hydroxyl groups in alkaline media enhances the delay. This is consistent with 392 the adsorption theory. In addition, calorimetric investigations on predissolution effect show 393 that the delayed effect induced by HPG would be more specific on silicate or aluminate 394 reaction.

Finally, this paper initiates the study of the interaction between cement and HPG. This
polymer, whose study is very scarce in literature, presents very interesting properties.
Especially, water retention properties are comparable to those obtained with CE, with the
advantage of producing lower pollution during the manufacturing. Therefore, it is very
important to improve knowledge of the impact of HPG on cement hydration kinetics.

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