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Thomas Poinot, Alexandre Govin, Philippe Grosseau

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1 Impact of hydroxypropylguars on the early age hydration

2 of portland cement

3 4 Thomas Poinot —Alexandre Govin* — Philippe Grosseau 5 6 7 Ecole Nationale Supérieure des Mines, SPIN-EMSE, CNRS:FRE3312, LPMG, F-42023 8 Saint-Etienne, France 9 10 * Corresponding author: 11 Tel: +33 4 77 42 02 53 12 E-mail address: govin@emse.fr

ABSTRACT

14	Hydroxypropylguars (HPG) are used as admixtures in factory-made mortars. These molecules
15	present water retention properties comparable to those obtained with commonly used
16	cellulosic water-retaining agent.
17	The influence of HPG on cement hydration was investigated in order to improve
18	understanding on the delayed effect induced by polysaccharides. Hydration kinetics were
19	characterized by means of conductivity and isothermal calorimetry measurements. The
20	influence of polymer concentration and predissolution was studied. A weak influence of HPG
21	on the germination of hydrates was observed. In contrast, HPG induced a significant decrease
22	in the hydrates growth rate. Strong effects of the polymer concentration and predissolution
23	were noticed too. From these results, we supported the hypothesis that HPG adsorption on
24	hydrated phases via polar interactions should be responsible for the delayed effect observed.
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27	KEYWORDS: polysaccharide (D), hydroxypropylguars (D), retardation (A), hydration (A),
28	water retention (C)

1 Introduction

31	Traditionally, mortars are based on a mixture of sand, a binder such as cement or lime, and
32	water. Nowadays, modern factory-made mortars are complex materials, in which are added
33	some kinds of admixtures used to exhibit various properties, from the fresh state to the
34	hardened material.
35	Polysaccharides are one of these admixtures. They are frequently introduced into mortar
36	formulations in order to improve water retention capacity of the freshly-mixed materials,
37	which enhances cement hydration and adhesion to the substrate [1-4]. These products are also
38	expected to act as viscosity-enhancing admixtures to prevent segregation and thus improve
39	the homogeneity and workability of the mortar [5–8].
40	Among all polysaccharides, Cellulose Ethers (CE) are the most widely used when high water
41	retention capacity is expected. Nevertheless, H ydroxy P ropyl G uars (HPG) were recently
42	presented as a promising new class of water-retaining agent [9]. HPG are already used in
43	various industrial fields, such as textile printing, oil production or paper manufacturing, due to
44	their thickening effect [10]. HPG were also the subject of some patents as admixture for
45	mortars.
46	The effect of saccharides has been largely studied these fifty last years, in particular from a
47	cement hydration delay point of view. In the first time, the delayed effect of monosaccharides
48	was investigated [11-19]. It appears that sugars could be adsorbed to cement phases by a
49	chelation process. It can thereby form a temporary barrier to further hydration. In broad
50	agreement with Young [11], Thomas and Birchall [12] proposed that sugars would be able to
51	poison the surfaces of the CH and CSH by complexation onto these phases, which inhibit
52	their growth and therefore would be responsible for the delay observed. According to Taplin
53	[13], sugars could bind to the cement phases if they have a HO-C=O group, or it could be
54	formed in alkaline media, such as cement paste, by hydrolyze [14].

55 Then, due to the use of polysaccharides in modern factory-made mortars, interactions between 56 polysaccharides and cement have been reported recently. It is established that polysaccharides 57 induce a more or less important delay of Portland cement hydration [20–25], which depends 58 on the nature of the polysaccharide [26]. Pourchez et al. [27,28] have established a 59 mechanism of interaction between CE and cement. 60 However, HPG have received scant attention by the academic community although they are 61 already used industrially. As far as we know, only Izaguirre et al. [29] was interested on the 62 impact of HPG, but in lime-based mortars. Thus, the aim of this work is to study the influence of HPG on the Portland cement hydration kinetics at early age. 63 64 Firstly, the water-retaining effect induced by the HPG in Portland cement-based mortars will be checked. Secondly, cement hydration kinetics in the presence of HPG will be presented. 65 66 Hydration kinetics have been monitored by conductivity and isothermal calorimetry 67 measurements. Finally, a special focus on the influence of the polymer predissolution has

69 2 Materials

been performed.

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2.1 Mineral product

The investigated ordinary Portland cement (OPC) was a CEM I 52.5 R CE CP2 NF type

cement according to the EN 197-1 standard. Its chemical and phase compositions are given in

Table 1. Oxide composition was determined by X-ray fluorescence spectroscopy (SRS3400,

Bruker-AXS). XRD analysis (D5000, Siemens) also allowed quantifying the phase

composition of the given cement by means of Rietveld refinement method (Siroquant V2.5 software).

2.2 Organic admixtures

78	Guar gum is a polysaccharide extracted from the seed endosperm of Cyamopsis
79	tetragonolobus, a native plant from India. This is a galactomannan consisting of a (1-4)-
80	linked β -D-mannopyranose backbone, with random branchpoints of galactose via an α -(1-6)
81	linkage [30] (Fig. 1a). The ratio of mannose to galactose is about 1.8. Unlike the
82	manufacturing of cellulose, the extraction does not require chemical process, but a thermo-
83	mechanical one. So, guar gum is produced without producing any effluent. Moreover, because
84	of the presence of hydroxyl groups in its structure, guar gum exhibits a high chemical
85	reactivity and is soluble in cold water. Thus, the chemical modification of this polysaccharide
86	does not require hard reaction conditions of temperature and pressure, does not generate large
87	quantity of by-products and needs weak purification procedure [31].
88	HPG are obtained from the native guar gum via an irreversible nucleophilic substitution,
89	using propylene oxide in the presence of an alkaline catalyst (Fig. 1b). Table 2 gives a
90	qualitative description of the six HPG samples from Lamberti S.p.A which were studied. All
91	the samples have similar molecular weight. The only difference between HPG 1, 2 and 3 is
92	the Degree of Substitution (DS). The only difference between HPG 4, 5 and 6 is the presence
93	of additional substitution (short or long alkyl chains).
94	In order to compare with classical polysaccharide admixtures, three CE were also tested
95	(Table 2): two HydroxyPropylMethyl Cellulose (HPMC) named HPMC1 and HPMC2, and
96	one HydroxyEthyl Cellulose (HEC).

3 Experimental methods of investigation

3.1 Water retention measurements

Water retention capacity of mortars was characterized according to ASTM C1506-09 standard [32]. This test is based on a measurement of the removed water after depression and was previously described by Patural et al. [3]. Water retention, noted WR, was calculated using the following equation:

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$$WR(\%) = \frac{W_0 - W_1}{W_0} \times 100 \tag{1}$$

 W_0 represents the initial mass of mixing water; W_1 is the loss of water mass after aspiration. Mortars were prepared according to the following mixture proportions: 30% of cement, 65% of sand and 5% of limestone filler (by weight). This mixture design was adapted from the CEReM (european consortium for study and research on mortars) mortars formulation [3]. Admixture amount (0.3 wt%) was in addition to the total dry mixture (*i.e.* cement, sand and filler). Dry mixture was blended in a shaker (Turbula, Wab) for 15 min. Deionized water was added in order to obtain a water to cement ratio W/C = 1. Mixing procedure was in accordance with EN 196-1 [33]. All tests were carried out in triplicate and at controlled temperature of 23°C because water retention is temperature-dependent. A control test was performed with a mortar without admixture.

3.2 Characterization of the cement hydration delay

3.2.1 Conductivity measurements on diluted suspensions

Characterization of the delay induced by the studied polymers on the cement hydration was performed by conductivity measurements. This method appears as a powerful and reproducible tool to monitor the hydration kinetics [34,35].

Conductivity measurements could be achieved in lime suspension. This allows obtaining hydration kinetics close to that observed in cement pastes, in spite of a high liquid to solid weight ratio (noted L/S). Nevertheless, monitoring hydration kinetics in an artificial system of lime water is complicated because the dissolution rate of calcium from the cement could be modified due to the initial high concentration of calcium ions in solution. Thus, conductivity curves were interpreted according to the explanation proposed by Comparet et al. [36]. As soon as cement was put in contact with liquid, the electrical conductivity increased as a consequence of the dissolution of the anhydrous phases. Then, germination of hydrates on the grain surface leads to a period, called "low conductivity increasing period", where the conductivity evolves weakly. Conductivity then accelerated more quickly. The conductimetric slope is related to the growth rate of the hydration products. Meanwhile, cement dissolution still continued. The conductivity increased to the critical supersaturation point with respect to portlandite and decreased rapidly due to its precipitation. Thus, an electrical conductivity drop is caused by the portlandite precipitation. This phenomenon was used to determine the hydration delay. Therefore, in this study, the portlandite precipitation time (noted t_{CH}) is a benchmark to classify and to quantify the relative retardation ability of admixtures on cement hydration. Experiments were performed in diluted suspensions, thermostated at 25°C and continuously stirred. Each experiment was carried out in triplicate. The liquid to solid weight ratio (L/S) used was equal to 20. Polymer to cement weight ratios (P/C) equal to 0.5, 1.0, 1.5 and 2.0 % were studied. Cement and admixture powders were blended in a shaker (Turbula, Wab) for 10 min before contact with the liquid phase. The liquid used was a 20 mM lime solution or deionized water. The control used was the neat cement.

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3.2.2 Isothermal calorimetry on cement pastes

gray in Fig. 10):

Calorimetry is another technique useful to characterize the exothermic hydration process of cement. The hydration process can be followed continuously at realistic water/cement ratios (W/C) in situ and aims at giving an indication of the overall rate of reaction. Thus, calorimetry can be used as a complementary method to conductivity in order to monitor the kinetics of cement hydration and to observe hydration delay induced by retarders [37]. The tests were performed with an isothermal calorimeter (C80, Setaram) at 25° C. The weight ratios used were W/C = 0.4, with deionized water, and P/C = 0.3 %. Ex-situ mixing was preferred to in-situ mixing to improve the homogeneity of the sample, and thus reproducibility. Mixing procedure, with 100g of cement, was in accordance with standard EN 196-1 [33]. 10 min after the beginning of the batch, about 2g of paste are introduced in the calorimeter. The control used was the neat cement.

3.2.3 Predissolution of the admixture

The influence of the polymer predissolution was studied by means of conductivity and isothermal calorimetry measurements. Admixtures were previously dissolved in the liquid phase, deionized water or 20 mM lime solution, for 24h by magnetic stirring. Then, cement was added. In case of conductivity experiments, the effect of the predissolution has been highlighted by calculating the increase percentage in the portlandite precipitation time t_{CH} as followed (in

Increase of
$$t_{CH}$$
 (%) = $\frac{t_{CH}(with\ prediss) - t_{CH}(without\ prediss)}{t_{CH}(without\ prediss)} \times 100$ (2)

3.3 Calcium binding capacity

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The ability of HPG and also sugars (sucrose which is known to complex calcium ions, galactose and mannose which constitute HPG's molecule) to form complexes with calcium ions was studied. Sugars are valuable insights in order to compare the behavior of HPG and to validate the relevance of this protocol, developed by Thomas and Birchall [12]. Each sample (2 g per liter) was introduced into a volume of water (1L) containing a large excess of solid lime (6 g per liter). After 48 hours of stirring at a controlled temperature of 23°C, the suspension was filtered through a 0.7 µm glass fiber filter. The filtrates were diluted and acidified. Then, a quantification of the calcium ion content by ionic chromatography was performed on a Dionex apparatus composed of a GP 50 gradient pump, a CS 12A cationexchange column and a CD 20 conductometric detector. The eluent was a solution of metasulfonic acid at 20 mM with isocratic mode. The flow was fixed at 1 mL/min. The results correspond to an average of 3 experiments. As the solid calcium hydroxide is in large excess, calcium ions consumed by complexation do not affect the "stock" of calcium ions in solution, which thus remains equal to 23 mM during the experiment. However, once the filtrate diluted and acidified, the complexes are destroyed, thus freeing the complexed calcium ions. So, if the calcium concentration is about 23 mM (solubility of lime), no significant complexation has taken place. Instead, a calcium concentration above 23 mM indicates a significant complexation of calcium ions.

3.4 Kinetic of dissolution

HPG absorb in the ultraviolet as evidenced by the absorption spectra (Fig. 2a), and the concentration of HPG in solution is proportional to the absorbance at the maximum of the band (266 nm) as shown in Fig. 2b.

The dissolution process was monitored by acquisition of UV-Vis absorption spectra. The procedure was the following: a dispersion of HPG (final concentration: $2g.L^{-1}$) in deionized water or 20 mM lime solution was prepared in a sealed reactor (1L of solution) thermostated at 25° C. HPG was introduced through a sieve in order to have a good dispersion of the sample into the vortex created by the mechanic stirrer. Thus, the aggregation of particles was minimized and a homogeneous polymer solution was produced. The experiment was done under continuous flow of nitrogen to avoid carbonation of lime. At different times, an aliquot of approximately 5 mL was taken from the batch solution and centrifuged by means of a micro-centrifuge (Eppendorf MiniSpin Plus, 14500 rpm) for 5 min in order to remove undissolved particles. The supernatant was collected and homogenized by vortex-stirring. The absorbance of this solution was measured between 200 and 400 nm using an UV/Visible spectrophotometer (Cary 300 Scan, Varian). A degree of progress of the dissolution reaction $\lambda(t)$ was used, which is equal to the absorption at time t divided by the absorption at the end of the dissolution reaction (*i.e.* 24 h). This number is adimensional and its value is between 0 and 1.

4 Results and discussions

4.1 Impact of HPG on water retention in fresh mortar

Water retention is a very sensitive mortar property. Indeed, it must be important enough to not disturb the hydration of the cement. It also limits the absorption of the mixing water by the substrate and thus provides good mechanical and adhesive properties to the mortar.

DTU 26.1 [38] specifies three classes of water retention of a fresh mortar. The first one represents mortars which water retention is lower than 86%; they belong to the low water retention category. The second class (intermediate water retention) corresponds to values

ranging from 86% to 94%. The last one is defined by water retention higher than 94%. This class is related to strong water retention mortar and is desired by formulators of industrial mortars. Water retention capacity of the studied mortars according to the admixture used is shown in Fig. 3. With this formulation, mortars containing HPG 2 to 6 and HPMC 2 could be considered as high WR capacity according to the DTU 26.1. Mortars containing HPG 1, HPMC 1 and HEC are in the intermediate category. Thus, HPG improve considerably the water retention capacity of the mortar compared to the control without water-retention admixture, as announced by Plank [9]. In addition, the results are quite comparable to those obtained with the CE of reference. Therefore, HPG can be considered as promising water-retention agents for dry-mix Portland

4.2 Impact of HPG on hydration kinetics of cement

222 4.2.1 Delayed effect

cement-based mortars.

The delayed effect of HPG on cement hydration kinetics was monitored by conductivity in a 20 mM lime solution, for ratios L/S = 20 and P/C = 2%. To have a clear and readable analysis, all the conductimetric curves will not be presented on the same figure. Thus, Table 3 regroups the conductimetric data obtained (i.e. portlandite precipitation times, delays compared to the control and conductimetric slopes). Fig. 4 presents the influence of the DS on the conductimetric curves by studying HPG 1, 2 and 3 which are the same molecules, except the DS (DSHPG1>DSHPG2>DSHPG3). The influence of the alkyl substitution was studied by comparison of HPG 4, 5 and 6 (see Table 2). The conductimetric curves obtained are shown in Fig. 5.

The conductimetric data (Table 3) highlights the impact of HPG on the kinetics of hydration. By focusing on the portlandite precipitation time (conductivity drop) and delays, it appears a wide range of delays induced by the admixtures studied. HPG 5 and 6 exhibit superposed conductimetric curves and the weaker delay (+71% and +66% respectively). The most important delay is observed for HPG 1 (+329%). It also appears that delays induced by HPG are between those obtained for the CE studied (+40% to +405%). Some polysaccharides (dextrines for example [26]) or other admixtures (setting retarding admixtures such as sugars [19], sodium gluconate [39] or some superplasticizers [36]) induce a blocking effect or an inhibition of the hydration. Here, from the shape of the conductimetric curves obtained, HPG involve a small increase in the duration of the "low conductivity increasing period". Therefore, this indicates a weak influence of the HPG on the germination of cement hydrates. The delay of portlandite precipitation time seems to be mainly due to a slope decrease (Table 3). Indeed, the slope obtained with the control is almost six times higher than that obtained for HPG 1. The slope of the conductimetric curve is linked to the growth rate of the hydrated cement phases. HPG seem to act preferentially on the growth of hydrates phases, rather than on their germination. This could explain the delays observed and is in agreement with results obtained with CE [40]. In addition, delay increases when DS decreases (Fig. 4). Nevertheless, the alkyl substitution seems to have a slight effect (Fig. 5) because the delay slightly decreases in the presence of

4.2.2 Calcium binding capacity

alkyl chains. The effect of the chain length is negligible.

The calcium complexation is often advanced as assumption to explain the effect of retarders [41]. It seemed important to check if HPG complex with calcium ions. The calcium binding capacity at alkaline pH of the 6 HPG and 3 sugars were conducted and the results are presented in Fig. 6. It appears clearly that the complexation of calcium ions by HPG is null or

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very weak, like with CE [42]. Indeed, the value of calcium ions concentration found for the HPG samples was close to the reference sample and is only due to the lime solubility. Instead, sugars studied present higher calcium ion concentration due to a greater binding capacity, which is coherent according to the data of the literature [12,42]. Therefore, calcium ion complexation is clearly not responsible for the delay of cement hydration induced by HPG.

4.2.3 Influence of polymer concentration

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The influence of the amount of polymer is studied by conductivity in 20mM lime solution by varying P/C ratio with a constant L/S ratio (equal to 20) for each HPG. The effect of polymer concentration is considerable and results in a drastic decrease in the slope (Fig. 7). Thus, a small increase in the amount of polymer leads to a huge increase in the portlandite precipitation time, and so in the delay of hydration. Fig. 8 presents the portlandite precipitation time for each polymer and concentration. The effect of the concentration is similar whatever the molecule. For each polymer, the more the concentration increases, the more the delay increases. As the retarding effect is effective at very low HPG concentrations, it confirms that calcium complexation cannot be responsible for the delay mechanism. It is generally admitted that cement hydration delay induced by admixtures is due to adsorption of these molecules to surfaces of the hydrating cement particles and/or surfaces of hydration products [41,43]. The concentration dependent behavior of the delay suggests also that HPG delay cement hydration via adsorption on the cement phases. The mechanism responsible for the delay induced by CE is the adsorption of the molecule on the hydrate cement phases. Indeed, Pourchez et al. have shown evidence of the adsorption of CE on calcium hydroaluminates [44] and CSH/CH [40]. Polysaccharides are molecules which contain a lot of polar functional groups (-OH). Therefore, strong interactions, through electrostatic forces and hydrogen-bonding, can occur between polysaccharides and the highly polar hydrated phases [43]. The relationship between adsorption and retardation was

previously shown [25,40]. It results that the higher the substituent content is, the weaker the retardation ability is, because of lower amount of free hydroxyls and so lower adsorption ability. For HPG, the phenomena could be very close, due to the similarity of the molecules used, in particular the high content of hydroxyl groups. Wang et al. [45,46] have shown that the adsorption mechanism of galactomannose polysaccharides at solid-liquid interfaces involves strong hydrogen bonding. Results obtained are in broad agreement with the relationship between adsorption and retardation described above. Indeed, qualitative data of DS are coherent with the delay observed. For example, the comparison of the HPG with different DS shows that $t_{CH}(HPG1) > t_{CH}(HPG2) > t_{CH}(HPG3)$ with DS(HPG1) < DS(HPG2) < DS(HPG3). Moreover, delay induced by HPG 4 is slightly higher compared to HPG 5 and 6. The only difference between these HPG is the substitution of the alkyl chains which could cause steric hindrance and increase the lipophilic character of the polymer. The presence of alkyl chains could reduce slightly the adsorption and so the delay. Effectively, t_{CH}(HPG4) is higher than t_{CH}(HPG5,6). Nevertheless, the length of the alkyl chains seems to not affect the adsorption because the difference on hydration delay is negligible. Indeed, the portlandite precipitation times for HPG 5 and HPG 6 are very close.

4.2.4 Influence of admixture predissolution

The effect of the admixture predissolution on the cement hydration kinetics has also been observed. Firstly, this effect in concentrated paste was studied by isothermal calorimetry. Heat evolutions within 24h for cement pastes without and with admixtures are presented in Fig. 9. For admixed cement pastes, HPG 1 (a), HPG 2 (b) and HPG 3 (c) were predissolved or not.

Two significant heat flow maxima are observed at early age for the neat cement paste.

According to many authors [47-50], the main peak is attributed to the alite hydration reaction.

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The second peak, only visible as a shoulder, corresponds to renewed dissolution of C₃A once the solid gypsum has been exhausted. For the cement pastes admixed with HPG and without predissolution, the main peak is delayed, whatever the admixture. Thus, HPG retard cement hydration at early age, as well in concentrated cement pastes as in diluted suspensions. The polymer predissolution seems to allow the separation of the main peak into two peaks. This separation is more easily visible in the case of the HPG 1 (Fig. 9a). For HPG 4, 5 and 6, which have a high DS, the effect is very weak, as for the HPG 3 (Fig. 9c). For HPG 2 (Fig. 9b), which has an intermediate DS, separation of the peak is less pronounced than in the case of HPG 1, but it is clearly visible. This suggests that the effect is all the more significant since the DS is low. Thus, HPG act preferentially either on the alite hydration or on the exhaustion of the solid gypsum, which is highlighted when HPG are already in the solution. In diluted suspensions, negligible impact of predissolution is observed in water whatever the admixture considered (Fig. 10a). However, in lime suspension (Fig. 10b), the impact of predissolution is very strong for HPG 1, with a huge increase in portlandite precipitation time of 77%. As observed by isothermal calorimetry, the effect decreases when the DS increases: + 19% for HPG 2 and +10% for HPG 3. The impact of predissolution is negligible for HPG 4 and 5. For CE, no impact of predissolution is observed too, which is coherent with results of Pourchez [51]. For HPG, the delay caused by the polymer is more important after predissolution in 20 mM lime solution than in water (no effect), mainly when DS is low. It is therefore an effect of the alkalinity of the medium. Different hypotheses can be considered. The polymer could be degraded due to the high alkalinity reached when cement dissolves. This degradation could lead to the formation of carboxylates by peeling reaction, molecules known to have a strong retarding effect [52]. The predissolution in lime would promote this degradation, resulting in an increase in the delay.

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Ultra-violet spectroscopy allows highlighting alkaline degradation. Indeed, the alkaline degradation of sugars leads to the formation of a large peak in the UV range, between 250 and 300 nm, due to the formation of saccharinic acids or the enolization of the sugars [12]. To investigate this effect, HPG and sugars (samples tested in calcium binding experiments) were stirred in water and lime solution. UV-Vis absorption spectra were carried out over time. Fig. 11 shows these results in case of HPG 1 and galactose, representing HPG and sugars respectively. In the case of HPG 1, the absorption spectra are different in water and in lime solution. Nevertheless, the difference is almost instantaneous and then remains stable over time. Therefore, it cannot be due to alkaline degradation. The difference in intensity is only due to HPG dissolution. For the other 5 HPG, no difference was observed between UV-Vis absorption spectra of polymer dissolved in water and in lime solution. On the contrary, sugars exhibit actually alkaline degradation. A new peak appears and grows with time when they are dissolved in lime solution. Moreover, an infrared investigation was made to determine if carboxylates are formed after dissolution of HPG in alkaline media. As above, HPG were stirred in water and lime solution. After 24h, solutions were neutralized and then placed in an oven until evaporation of the liquid phase. Solid residues were analyzed by infrared spectrometry. No band at 1590 cm⁻¹, corresponding to carboxylates functions, was observed, neither in water nor in lime solution. Thus, experiments on HPG indicate their alkaline stability. This is consistent with the hypotheses of many authors. A reduction in intrinsic viscosity has been observed for galactomannans under alkaline conditions [53–55]. However, according to these authors, this reduction is not due to degradation by a peeling reaction, but to inhibition of intermolecular interactions (hyperentanglement) because of ionization of hydroxyl groups. Izaguirre et al. reached the same conclusion with HPG [29]. Furthermore, similar results of polysaccharide alkaline stability were observed with CE [42].

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A second hypothesis would be slower dissolution kinectis of the polymer in lime solution than in water. In that case, in lime solution, the polymer is not fully active to delay the cement hydration without predissolution because the dissolution would be slowdown. On the contrary, predissolution leads to the complete dissolution of the polymer and therefore a maximum delay. In water, if the dissolution is fast, predissolution could have no effect. Fig. 12 presents the effect of the media on the dissolution kinetics for HPG 1. Dissolution is very fast, both in water and in 20 mM lime solution. The polymer seems to be completely dissolved after 40 min, whatever the dissolution media. Same results are obtained for the other HPG. Thus, dissolution kinetics cannot be responsible for the predissolution effect on cement hydration kinetics. Moreover, guar gum is known to be easily soluble [56]. According to some authors, hydroxyl groups of galactomannans [53–55] and HPG [29] would ionize in alkaline media. It seems very probable that predissolving the polymer in the lime solution would ionize a maximum of hydroxyl groups and thus enhance the adsorption of polysaccharide on the cement phases. So, the delayed effect is greater after predissolution in lime solution, but there is no change after predissolution in water. That would explain why HPG 1, which is the polymer with the lower DS, thus higher amount of polysaccharidic backbone hydroxyl groups, is the most sensitive to predissolution. Furthermore, this hypothesis is coherent with the adsorption mechanism via the hydroxyl sites proposed to explain hydration delay induced by HPG. This is consistent with the effect of HPG predissolution in water observed by isothermal calorimetry too. Indeed, calorimetry experiments were made in concentrated pastes. The paste is quickly saturated in lime and the pH increases almost instantly. Thus, even if the polymer is predissolved in water, phenomena occurring are closer to what was observed in conductivity experiments after predissolution in lime solution.

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5 Conclusions

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381 Based upon this study, it appears that HPG delayed cement hydration with an influence on the 382 growth of the hydrates, rather than on the germination of hydrates. Complexation of calcium 383 ions does not explain this effect. A strong impact of the concentration on the hydration 384 kinetics was observed. The results and the molecular similarity with CE suggest that the delay 385 effect is due to the adsorption of the HPG via the interaction between hydroxyl groups and the 386 highly polar hydrated phases. This hypothesis is coherent with the qualitative data of DS. 387 An increase in portlandite precipitation time was noticed after predissolution of HPG in lime 388 solution. It was shown that no alkaline degradation of HPG occurs. Moreover, no difference 389 of admixture dissolution kinetics in water or lime solution was observed. Thus, these two 390 phenomena are not responsible for the increase in the delay. We put forward that the 391 ionization of hydroxyl groups in alkaline media enhances the delay. This is consistent with 392 the adsorption theory. In addition, calorimetric investigations on predissolution effect show 393 that the delayed effect induced by HPG would be more specific on silicate or aluminate 394 reaction. 395 Finally, this paper initiates the study of the interaction between cement and HPG. This 396 polymer, whose study is very scarce in literature, presents very interesting properties. 397 Especially, water retention properties are comparable to those obtained with CE, with the 398 advantage of producing lower pollution during the manufacturing. Therefore, it is very 399 important to improve knowledge of the impact of HPG on cement hydration kinetics.

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402 **References**

- 403 [1] L. Bertrand, S. Maximilien, R. Guyonnet, Wedge Splitting Test: A test to measure the
- 404 polysaccharide influence on adhesion of mortar on its substrate, Proceedings of the 11th
- 405 International Congress on Polymers in Concrete, Berlin, Germany (2004) 569-576.
- 406 [2] A. Jenni, L. Holzer, R. Zurbriggen, M. Herwegh, Influence of polymers on microstructure
- and adhesive strength of cementitious tile adhesive mortars, Cem. Concr. Res. 35 (1) (2005)
- 408 35-50.
- 409 [3] L. Patural, P. Marchal, A. Govin, P. Grosseau, B. Ruot, O. Devès, Cellulose ethers
- influence on water retention and consistency in cement-based mortars, Cem. Concr. Res.
- 411 41(1) (2011) 46-55.
- 412 [4] H. B. Wagner, Polymer modification of portland-cement systems, Chemtech 3 (2) (1973),
- 413 105–108
- 414 [5] V. A. Ghio, P. J. M. Monteiro, L. A. Demsetz, The rheology of fresh cement paste
- containing polysaccharide gums, Cem. Concr. Res. 24 (2) (1994) 243-249.
- 416 [6] K. H. Khayat, Effect of antiwashout admixtures on fresh concrete properties, ACI Mater.
- 417 J. 92 (2) (1995) 164-171.
- 418 [7] K. H. Khayat, A. Yahia, Effect of welan gum-high-range water reducer combinations on
- 419 rheology of cement grout, ACI Mater. J. 94 (5) (1997) 365-372.
- 420 [8] H. Paiva, L. M. Silva, J. A. Labrincha, V. M. Ferreira, Effects of a water-retaining agent
- on the rheological behaviour of a single-coat render mortar, Cem. Concr. Res. 36 (7) (2006)
- 422 1257-1262.
- 423 [9] J. Plank, Applications of biopolymers and other biotechnological products in building
- materials, Appl. Microbiol. Biotechnol. 66 (1) (2004) 1-9.

- 425 [10] Y. Chen, X. Wu, X. Miao, J. Luo, B. Jiang, Determination of the degree of substitution
- of hydroxypropyl guar gum at C-6 by Pyrolysis-Gas Chromatography spectrometry,
- 427 Carbohyd. Polym. 82 (3) (2010) 829-832.
- 428 [11] J. F. Young, A review of the mechanisms of the set-retardation in portland cement pastes
- 429 containing organic admixtures, Cem. Concr. Res. 2 (4) (1972) 415-433.
- 430 [12] N. L. Thomas, J. D. Birchall, The retarding action of sugars on cement hydration, Cem.
- 431 Concr. Res. 13 (6) (1983) 830-842.
- 432 [13] J. H. Taplin, Discussion of "Some chemical additions and admixtures in cement paste
- and concrete" by H.E. Vivian, Proceedings of the 4th Internationnal Congress on the
- 434 Chemistry of Cement, Washington, 7 (1) (1962) 909-926.
- 435 [14] G. M. Bruere, Set-retarding effects of sugars in Porland cement pastes, Nature 212
- 436 (1966) 502-503.
- 437 [15] N. B. Singh, Effect of gluconates on the hydration of cement, Cem. Concr. Res. 6 (1976)
- 438 455-460.
- [16] J. D. Birchall, N. L. Thomas, The mechanism of retardation of setting of OPC by sugars,
- 440 Proceedings of British Ceramic Proceedings, London, 35 (1984) 305-315.
- 441 [17] M. C. Garci Juenger, H. M. Jennings, New insights into the effects of sugar on the
- 442 hydration and microstructure of cement pastes, Cem. Concr. Res. 32 (3) (2002) 393-399.
- 443 [18] V. K. Peterson, M. C. Garci Juenger, Time-resolved quasielastic neutron scattering study
- of the hydration of tricalcium silicate: effects of CaCl2 and sucrose, Phys. Rev. B 385-386 (1)
- 445 (2006) 222-224.
- 446 [19] L. Zhang, L. J. J. Catalan, R. J. Balec, A. C. Larsen, H. H. Esmaeili, S. D. Kinrade,
- Effects of saccharide set retarders on the hydration of ordinary portland cement and pure
- 448 tricalcium silicate, J. Am. Ceram. Soc. 93 (1) (2010) 279-287.

- 449 [20] M. Alesiani, S. Capuani, R. Giorgi, B. Maraviglia, I. Pirazzoli, F. Ridi, P. Baglioni,
- 450 Influence of cellulosic additives on tricalcium silicate hydration: nuclear magnetic resonance
- 451 relaxation time analysis, J. Phys. Chem. B 108 (15) (2004) 4869-4874.
- 452 [21] A. M. Betioli, P. J. P. Gleize, D. A. Silva, V. M. John, R. G. Pileggi, Effect of HMEC on
- 453 the consolidation of cement pastes: Isothermal calorimetry versus oscillatory rheometry, Cem.
- 454 Concr. Res. 39 (5) (2009) 440-445.
- 455 [22] E. Knapen, D. Van Gemert, Cement hydration and microstructure formation in the
- presence of water-soluble polymers, Cem. Concr. Res. 39 (1) (2009) 6-13.
- 457 [23] F. Ridi, E. Fratini, F. Mannelli, P. Baglioni, Hydration process of cement in the presence
- of a cellulosic additive. A calorimetric investigation, J. Phys. Chem. B 109 (30) (2005)
- 459 14727-14734.
- 460 [24] D. A. Silva, P. J. M. Monteiro, The influence of polymers on the hydration of portland
- 461 cement phases analyzed by soft X-ray transmission microscopy, Cem. Concr. Res. 36 (8)
- 462 (2006) 1501-1507.
- 463 [25] H. J. Weyer, I. Müller, B. Schmitt, D. Bosbach, A. Putnis, Time-resolved monitoring of
- 464 cement hydration: Influence of cellulose ethers on hydration kinetics, Nucl. Instrum. Meth. B
- 465 238 (1-4) (2005) 102-106.
- 466 [26] A. Peschard, A. Govin, P. Grosseau, B. Guilhot, R. Guyonnet, Effect of polysaccharides
- on the hydration of cement paste at early ages, Cem. Concr. Res. 34 (11) (2004) 2153-2158.
- 468 [27] J. Pourchez, A. Peschard, P. Grosseau, R. Guyonnet, B. Guilhot, F. Vallée, HPMC and
- 469 HEMC influence on cement hydration, Cem. Concr. Res. 36 (2) (2006) 288-294.
- 470 [28] J. Pourchez, P. Grosseau, R. Guyonnet, B. Ruot, HEC influence on cement hydration
- 471 measured by conductometry, Cem. Concr. Res. 36 (9) (2006) 1777-1780.

- 472 [29] A. Izaguirre, J. Lanas, J. I. Álvarez, Characterization of aerial lime-based mortars
- 473 modified by the addition of two different water-retaining agents, Cem. Concr. Comp. 33 (2)
- 474 (2011) 309-318.
- 475 [30] D. Risica, M. Dentini, V. Crescenzi, Guar gum methyl ethers. Part I. Synthesis and
- 476 macromolecular characterization, Polymer 46 (26) (2005) 12247-12255.
- 477 [31] B. Biasotti, M. Giudici, V. Langella, U. Pfeiffer, Highly substituted hydroxypropylguar:
- a strong contribution to construction chemistry, Proceedings of the Third International
- 479 Drymix Mortar Conference, Nürnberg, Germany (2011).
- 480 [32] Standard C1506-09, Standard test Method for Water Retention of Hydraulic Cement-
- 481 Based Mortars and Plasters. Am. Soc. Test. Mat. (2009).
- 482 [33] EN 196-1, Methods of testing cement Part 1: Determination of strength (2006).
- 483 [34] A. Nonat, J. C. Mutin, X. Lecoq, S. P. Jiang, Physico-chemical parameters determining
- 484 hydration and particle interactions during the setting of silicate cements, Solid State Ionics
- 485 101-103 (2) (1997) 923-930.
- 486 [35] D. Damidot, A. Nonat, P. Barret, Kinetics of Tricalcium Silicate Hydration in Diluted
- Suspensions by Microcalorimetric Measurements, J. Am. Ceram. Soc. 73 (11) (1990) 3319-
- 488 3322.
- 489 [36] C. Comparet, A. Nonat, S. Pourchet, J. P. Guicquero, E. Gartner, Chemical interaction of
- 490 di-phosphonate terminated monofunctional polyoxethylene superplasticizer with hydrating
- 491 tricalcium silicate, Proceedings of the 6th CANMET/ACI International Conference on
- 492 Superplasticizers and Other Chemical Admixtures in Concrete (1997) 61-74.
- 493 [37] V. S. Ramachandran, M. S. Lowery, Conduction calorimetric investigation of the effect
- of retarders on the hydration of Portland cement, Thermochim. Acta 195 (1992) 373-387.
- 495 [38] NF DTU 26.1, Travaux d'enduits de mortiers (2008).

- 496 [39] S. Garrault, A. Nonat, Y. Sallier, L. Nicoleau, On the origin of the dormant period of
- cement hydration », Proceedings of the 13th International Congress on the Chemistry of
- 498 Cement, Madrid, Spain (2011).
- 499 [40] J. Pourchez, P. Grosseau, B. Ruot, Changes in C3S hydration in the presence of cellulose
- 500 ethers, Cem. Concr. Res. 40 (2) (2010) 179-188.
- 501 [41] J. Cheung, A. Jeknavorian, L. Roberts, D. Silva, Impact of admixtures on the hydration
- 502 kinetics of Portland cement, Cem. Concr. Res. 41 (12) (2011) 1289-1309.
- 503 [42] J. Pourchez, A. Govin, P. Grosseau, R. Guyonnet, B. Guilhot, B. Ruot, Alkaline stability
- of cellulose ethers and impact of their degradation products on cement hydration, Cem.
- 505 Concr. Res. 36 (7) (2006) 1252-1256.
- 506 [43] C. Jolicoeur, M. A. Simard, Chemical admixture-cement interactions: Phenomenology
- and physico-chemical concepts, Cem. Concr. Comp. 20 (2-3) (1998) 87-101.
- 508 [44] J. Pourchez, P. Grosseau, B. Ruot, Current understanding of cellulose ethers impact on
- the hydration of C3A and C3A-sulphate systems, Cem. Concr. Res. 39 (8) (2009) 664-669.
- 510 [45] J. Wang, P. Somasundaran, D. R. Nagaraj, Adsorption mechanism of guar gum at solid-
- 511 liquid interfaces, Min. Eng. 18 (1) (2005) 77-81.
- 512 [46] J. Wang, P. Somasundaran, Study of galactomannose interaction with solids using AFM,
- 513 IR and allied techniques, J. Colloid Interf. Sci. 309 (2) (2007) 373-383.
- 514 [47] H. Minard, S. Garrault, L. Regnaud, A. Nonat, Mechanisms and parameters controlling
- 515 the tricalcium aluminate reactivity in the presence of gypsum, Cem. Concr. Res. 37 (10)
- 516 (2007) 1418-1426.
- 517 [48] C. Hesse, F. Goetz-Neunhoeffer, et J. Neubauer, A new approach in quantitative in-situ
- XRD of cement pastes: Correlation of heat flow curves with early hydration reactions, Cem.
- 519 Concr. Res. 41 (1) (2011) 123-128.

- 520 [49] J. W. Bullard, H. M. Jennings, R. A. Livingston, A. Nonat, G. W. Scherer, J. S.
- 521 Schweitzer, K. L. Scrivener, J. J. Thomas, Mechanisms of cement hydration, Cem. Concr.
- 522 Res. 41 (12) (2011) 1208-1223.
- 523 [50] A. Quennoz, K. L. Scrivener, Hydration of C3A–gypsum systems, Cem. Concr. Res. 42
- 524 (7) (2012) 1032-1041.
- 525 [51] J. Pourchez, « Aspects physico-chimiques de l'interaction des éthers de cellulose avec la
- 526 matrice cimentaire », PhD Thesis, Ecole Nationale Supérieure des Mines de Saint-Etienne
- 527 (2006) 285 p.
- 528 [52] Y. Ohama, Polymer-based admixtures, Cem. Concr. Comp. 20 (2-3) (1998) 189-212.
- 529 [53] E. R. Morris, A. N. Cutler, S. B. Ross-Murphy, D. A. Rees, J. Price, Concentration and
- shear rate dependence of viscosity in random coil polysaccharide solutions, Carbohyd. Polym.
- 531 1 (1) (1981) 5-21.
- [54] F. M. Goycoolea, E. R. Morris, M. J. Gidley, Viscosity of galactomannans at alkaline
- and neutral pH: evidence of 'hyperentanglement' in solution, Carbohyd. Polym. 27 (1) (1995)
- 534 69-71.
- [55] J. P. Doyle, G. Lyons, E. R. Morris, New proposals on "hyperentanglement" of
- 536 galactomannans: Solution viscosity of fenugreek gum under neutral and alkaline conditions,
- 537 Food Hydrocolloid. 23 (6) (2009) 1501-1510.
- [56] P. A. Dakia, B. Wathelet, M. Paquot, Influence de la teneur en galactose sur les
- 539 interactions moléculaires et sur les propriétés physico-chimiques des galactomannanes en
- 540 solution, Biotechnol. Agron. Soc. Environ. 14 (1) (2010) 213-223.