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Phase-resolved heterodyne holographic vibrometry with a strobe local oscillator

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We report a demonstration of phase-resolved vibrometry, in which out-of-plane sinusoidal motion is assessed by heterodyne holography. In heterodyne holography, the beam in the reference channel is an optical local oscillator (LO). It is frequency-shifted with respect to the illumination beam to enable frequency conversion within the sensor bandwidth. The proposed scheme introduces a strobe LO, where the reference beam is frequency-shifted and modulated in amplitude, to alleviate the issue of phase retrieval. The strobe LO is both tuned around the first optical modulation side band at the vibration frequency, and modulated in amplitude to freeze selected mechanical vibration states sequentially. The phase map of the vibration can then be derived from the demodulation of successive vibration states.

Time-averaged holography is an efficient detection method for mapping sinusoidal out-of-plane vibration amplitudes. Homodyne [1–3] and heterodyne [4, 5] modalities were investigated. However, achieving a robust mechanical phase mapping remains an important issue. In holography, the local phase retardation of the scattered optical field impinging onto each pixel of a sensor array is used for image reconstruction. Nevertheless, it is not exploited straightforwardly for the determination of the local mechanical phase of an object in sinusoidal motion unless if a high framerate sensor is used [3]. A stroboscopic approach can alleviate this issue. Several holographic and interferometric approaches have been proposed and validated for mechanical phase retrieval from sequences of intensity images under phase-stepped stroboscopic illumination [6–8]

In this letter, we report the use of a stroboscopic scheme in conjunction with frequency-shifted modulation sideband detection to map mechanical phase shifts with respect to the excitation signal at a given vibration frequency. Detuning the strobe frequency with respect to the mechanical excitation signal by a fraction of the sampling frequency can be used to freeze m linearly-spaced vibration states over a vibration period. Each of these states can then be measured, from sequentially-acquired frames. Furthermore, detuning the carrier frequency of the reference beam with respect to the object beam will enable phase-shifting holography with optimal accuracy [9]. Appropriate LO carrier frequency will provoke n -phase modulation of the optical signal from each of the m vibration states. The purpose of this scheme is to recover a phase map of the vibration from the demodulation of m intensity holographic images, each of which will be derived from the demodulation of n raw interferograms. Hence a phase map measurement

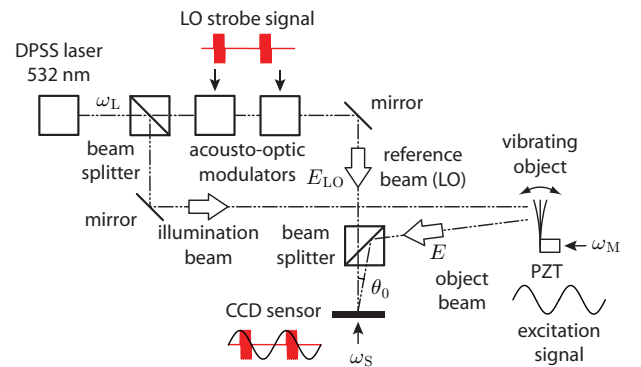


FIG. 1: Sketch of the optical setup.

will require $m \times n$ sequentially recorded frames.

The optical acquisition set-up, sketched in Fig. 1, consists of an off-axis heterodyne Mach-Zehnder interferometer allowing detection of modulation sidebands of the optical radiation scattered by a vibrating object. This holographic interferometer is used for the detection of an object field E in reflective geometry, beating against a LO field E_{LO} . The optical radiation is provided by a 100 mW, single-mode, doubled Nd:YAG laser (Oxxius SLIM 532) at wavelength $\lambda = 532$ nm, and optical frequency $\omega_L/(2\pi) = 5.6 \times 10^{14}$ Hz. The LO field is shaped by two acousto-optic modulators (AA-electronics, MT80-A1.5-VIS). It has the form $E_{LO} = \mathcal{E}_{LO} e^{i(\omega_L + \Delta\omega)t} H_{AM}(t)$, where \mathcal{E}_{LO} is its complex amplitude. The frequency shift of the carrier is $\Delta\omega$, and $H_{AM}(t)$ is the amplitude modulation (AM) function of the LO pulses : a square signal with a cyclic ratio of 25%; its angular frequency is ω_P . The studied objects are attached to a piezo-electric actuator (Thorlabs AE0505D08F), vibrating sinusoidally, at angular frequency ω_M . The out-of-plane vibration $z \sin(\omega_M t + \psi)$,

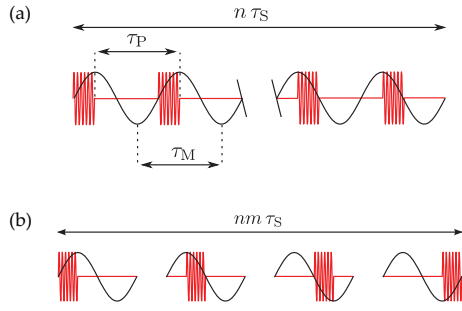


FIG. 2: (Color on-line) Chronogram of signal acquisition over n and $m \times n$ successive frames, (a) and (b), respectively. Black: mechanical excitation signal, red: strobe LO signal.

of amplitude z and phase retardation ψ , provokes a modulation of the optical path length of the object field. It induces a phase modulation of the backscattered light $\phi(t) = \phi_0 \sin(\omega_M t + \psi)$, where $\phi_0 = 4\pi z/\lambda$ is the modulation depth. This phase modulation generates radiofrequency optical modulation side bands at harmonics of ω_M . For each mechanical phase map retrieval at a given excitation frequency, a set of $m \times n$ optical interferograms \mathcal{I}_k ($k = 1, \dots, mn$) is recorded by an Andor EMCCD sensor array of 1002×1004 pixels. Throughout the experiments, raw frames are sampled at a frame rate of $\omega_S/(2\pi) = 24$ Hz. Holographic image rendering from the recorded interferograms \mathcal{I}_k at times $2\pi k/\omega_S$ involves a scalar diffraction calculation. It is performed with a numerical Fresnel transform \mathcal{F} , a special case of linear canonical transform, whose digital computing is studied in detail in [10]. Its implementation in off-axis holographic conditions [11] yields holograms I_k reconstructed in the object plane.

Signal modulation consists in choosing appropriate LO pulse and carrier frequencies, ω_P and $\Delta\omega$, respectively. We want the LO pulse pattern of period $\tau_P = 2\pi/\omega_P$, shown in fig. 2(a) and fig. 2(b), to be shifted by one m -th of the mechanical signal pattern (of period $\tau_M = 2\pi/\omega_M$) after n consecutive images. This implies $\tau_P - \tau_M = \tau_M^2/(nm\tau_S)$, where $\tau_S = 2\pi/\omega_S$ is the time elapsed from-frame-to-frame recording. For pulse frequencies close to the excitation frequency $\tau_P - \tau_M \ll \tau_M$, to provoke the desired drift between the optical and the mechanical signal pattern (Fig.2(a)), the pulse frequency is set to

$$\omega_P = \omega_M + \omega_S/(nm) \quad (1)$$

Furthermore, the LO carrier is detuned by $\Delta\omega = \omega_M + \omega_S/n$ to provoke a beat of the first optical modulation side band component in the recorded interferogram at ω_S/n . Following these guidelines, signal demodulation is made in two steps. First, a set of $m \times n$ consecutive raw intensity images I_k ($k = 1, \dots, mn$) is acquired (Fig. 2(b)), from which m states M_p ($p = 1, \dots, m$) within the

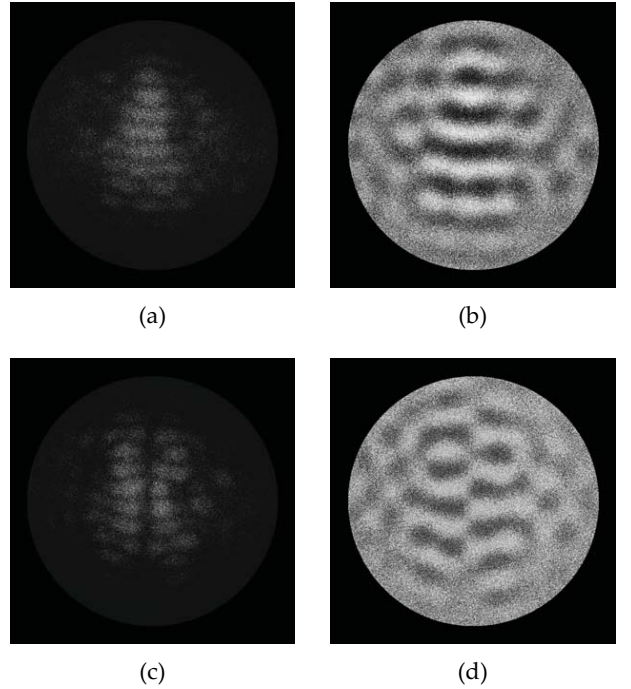


FIG. 3: Out-of-plane vibration maps of a silicon wafer excited at 142 kHz (a,b), 151 kHz (c,d). Amplitude maps (a,c), in arbitrary units ; black: nodes, white: antinodes. Phase maps (b,d). Black : 0 rad, white : π rad.

mechanical excitation period are derived

$$M_p = \sum_{k=1}^n I_{k+(p-1)n} \exp\left(-\frac{2i\pi k}{n}\right). \quad (2)$$

Then, a local vibration map Q is demodulated from the m states.

$$Q = \sum_{p=1}^m |M_p|^2 \exp\left(-\frac{2i\pi p}{m}\right). \quad (3)$$

For small vibrations ($z \ll \lambda$), the magnitude of the quantity derived in eq. 3 is proportional to the local out-of-plane vibration amplitude $|Q| \propto z$. Its argument yields the local phase retardation with respect to the excitation signal $\psi \equiv \arg(Q) [2\pi]$.

Amplitude and phase maps of the vibration modes of a silicon wafer excited at 142 kHz (a,b) and 151 kHz (c,d), are reported in Fig.3. Each couple of maps is calculated according to eq.3, from the recording of 16 consecutive interferograms ($m = 4$ and $n = 4$). Phase maps (b,d) exhibit phase oppositions between adjacent bellies (antinodes), in agreement with the modal distribution of the amplitude maps (a,c).

The validity of the phase measurement was achieved by estimating the average phase within one antinode of a vibrating sheet of paper, whose lateral dimensions

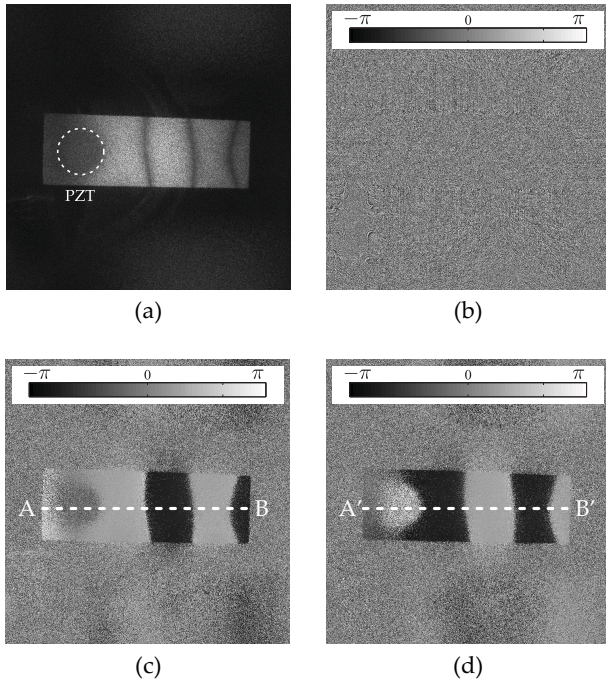


FIG. 4: Amplitude (a) (black: nodes, white: antinodes) and phase maps (b-d) of a vibrating sheet of paper with no phase shift (c), and π phase shift between the excitation and the strobe illumination (d). The phase image rendered without strobe demodulation does not exhibit the vibration phase retardation (b). Dark and light gray regions within the object in (c) and (d) are in phase opposition, as shown in cuts reported in fig5.

are 9×26 mm, excited at 10 kHz. At this frequency, the steady-state vibrational mode, whose amplitude is reported in Fig.4(a), is composed of rectilinear nodes and bellies oriented vertically [11]. Amplitude and phase maps measured for a strobe signal phase-shifted by 0 and π radians with respect to the mechanical excitation, respectively, are reported in Fig.4(c) and Fig.4(d). Once again, each couple of maps was calculated according to eq.3, from 16 raw frames ($m = 4$ and $n = 4$). To avoid any ambiguity of the mechanical phase determination, bursts of camera frames and strobe LO signal patterns $H_{AM}(t)$ were triggered by a clock signal, derived from frequency-division of the mechanical excitation signal. As expected, reconstructed mechanical phases in (e) and (f) exhibit inverted contrast from-antinode-to-antinode within the same map. The phase contrast is also inverted between (e) and (f) within the same area of the object, which corresponds to phase opposition. These phase oppositions are also visible in the cuts reported in Fig. 5(a). Twelve phase shifts between the strobe illumination and the mechanical excitation signal, linearly-spaced between 0 and 2π radians are set and measured sequentially. Measures are reported in Fig.5(b). They are in agreement with the set of imposed

phase shifts.

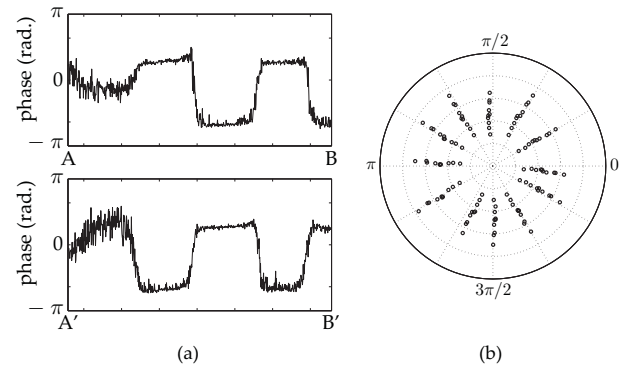


FIG. 5: (a) Cuts of the vibrating object, along AB and A'B' in Figs. 4(c,d). (b) Measured phase of an antinode in fig. 4 (circles) versus phase detuning between the the excitation and the illumination patterns (lines).

In conclusion, we demonstrated that quantitative phase maps from sinusoidal out-of-plane vibration can be measured by frequency-shifted holography tuned for first modulation side band detection in conjunction with a stroboscopic illumination. In the reported approach, phase maps are derived from sequences of hologram intensity measures. Its robustness and accuracy lies in the continuous drift of the optical pulses with respect to the mechanical excitation signal, throughout image sequence acquisition. With this method, sequential shifting of strobe pulse is circumvented.

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