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Self-Powered Ultra-low Power DC-DC Converter for RF Energy Harvesting

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Abstract—In this paper, an autonomous low voltage and ultra-low power DC-DC converter is presented. This novel topology is inspired from the classical Armstrong oscillator structure. In addition to be self-powered and autonomous, this converter is suitable for high-impedance sources. Theoretical and simulation-based optimizations are used in order to design the converter. A fabricated prototype is tested. It harvests RF energy from a low power rectenna (rectifying antenna). High output voltage and good performances are achieved in the range of $4\mu\text{W}$ to 1mW of input power.

Keywords- ultra-low power, low voltage, self-oscillating DC-DC converter, RF energy harvesting, rectenna.

I. INTRODUCTION

Nowadays, energy harvesting is an emerging topic that electronic researchers are increasingly interested in. It is based on collecting very small amounts of energy from the environment using small scale transducers. The harvested energy is used in order to feed low power circuits such as Wireless Sensor Nodes (WSNs). There are various sources for energy harvesting [1]: solar, organic, vibration, thermal, near-field electromagnetic and far-field electromagnetic (or Radio-Frequency RF). Most energy harvesting transducers deliver a very low voltage (below 1V) and a very low power (below 1mW). A voltage level of few volts is essential in order to supply conventional electronic circuits (wireless sensors in particular). Voltage step-up can be achieved with power electronics, but again, conventional commercial DC/DC converters need at least 1V of input voltage and require a minimum power in order to start-up functioning. Specific new circuit architectures are therefore necessary. For this purpose, various topologies of low voltage and low power DC-DC converters have emerged these last years from both industrial and academic research. Fig. 1 and Tab. I show an overview of those converters.

Most low-voltage and low-power converters need an external power source (A on Fig. 1). It can be either the external output rechargeable battery or a storage capacitor charged to a sufficient level. In [2] a DC/DC boost converter powered by the external output battery is presented. It harvests low RF energy ($>10\mu\text{W}$). Another ultra-low power boost

converter is presented in [3]; output capacitor has to be charged to 650mV in order to supply the control circuit.

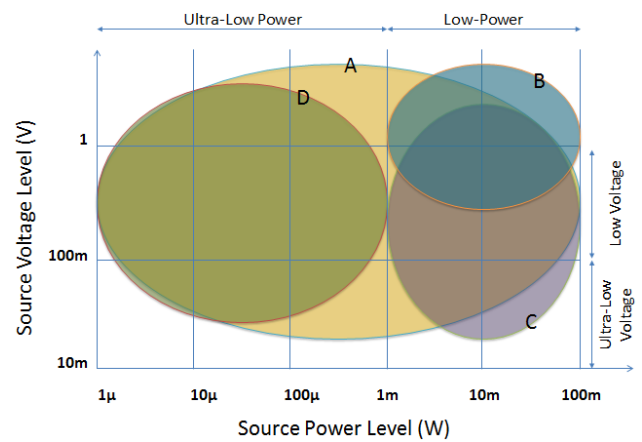


Figure 1. State of the art of low voltage and low power converters

TABLE I. LOW VOLTAGE AND LOW POWER CONVERTERS CATEGORIES

Battery-Powered Converters		Battery-less Converters	
A	Wide range of input voltage and power [2-3]	B	Special low voltage integrated circuit based on: <ul style="list-style-type: none"> • Sub-threshold CMOS design [4] • Silicon-On-Insulator (SOI) technology [5]
		C	Classical Armstrong-oscillator-based converters (ultra-low voltage) [6-9]
		D	Novel Armstrong-oscillator-based converter (ultra-low power) [this work]

Self-powered converter topologies (B, C and D on Fig. 1) are more adapted for autonomous WSNs. Unlike a battery system in which batteries have limited charge/discharge cycles, a battery-less system does not require any maintenance. Furthermore, energy harvesting systems do not contribute to a good battery health because of the non-regulated available energy for most sources. Batteries are space consuming and they take a large part of the system size. For these reasons, a self-powered system is more reliable and offers more application opportunities.

There are two major types of self-powered converters. First type is based on special low power integrated circuit techniques, i.e. the use of sub-threshold design [4] and also the use of low-power and low-voltage fabrication technologies such as Silicon-On-Insulator (SOI) [5].

The second category of self-powered converter is based on the use of self-oscillating circuits. Armstrong oscillator [6-9] is commonly used in this field. Major benefit of such structure is ultra-low input voltage and also high voltage stepping-up abilities. Oscillating circuits are often used as a start-up part of a principal converter because of the need of an external regulated voltage. Most self-oscillating circuits operate for milli-watts power levels. In [7] a 100mW boost converter using the Armstrong oscillator as a start-up stage is presented. Similar topologies are presented in [8-9] for 17mW and 1mW respectively.

The aim of this article is to present a novel topology of self-oscillating converter that is suitable for ultra-low power applications (several μW to 1mW). This converter is suitable in particular for RF energy harvesting. For such system, the energy source which is a rectenna has a large internal impedance (several $\text{k}\Omega$), resulting in ultra-low available current.

Rectennas are introduced in part II. The converter topology, the design procedure as well as the performances are presented in part III. In the part IV, the converter is powered by the rectenna in order to evaluate the global performances of the system.

II. LOW-POWER RECTENNA

The association of a receiving antenna and an RF-DC rectifier circuit is called a rectenna (rectifying antenna). A rectenna usually operates in the range of UHF ($f > 1\text{GHz}$) enabling long range wireless energy transfer with relatively compact antennas.

Rectenna operation principle is illustrated in Fig. 2. The incident RF power is captured by an antenna under the form of a high frequency sine wave. This is then transformed into DC power by the diode-based converter. A HF filter ensures impedance adaptation between the antenna and the diode rectifier around work-frequency (2.45GHz) for optimal power transfer. The output DC filter smooths the output DC voltage and current by attenuating high frequency harmonics present in the RF signal or generated by the rectification process itself.

In the case of low incident power levels (below 1mW), rectifier is often based on series-mounted diode. This structure offers the best compromise between DC output voltage level and conversion efficiency at those low incident power levels [10]. Furthermore, zero bias Schottky diodes are often used in this case due to their low threshold voltage (around 150 mV) and their low junction capacitance (0.18 pF) [11].

A prototype of a single series-mounted diode rectenna was fabricated on a low-cost 1.6 mm FR4 substrate. In order to evaluate the rectenna output characteristic, the fabricated prototype was tested under wide range of input RF power and output load resistance. RF power is directly supplied by a

power source through a SMA cable. Current-Voltage (I-V) and Efficiency-Load (η -R) characteristics are shown in Fig. 3.

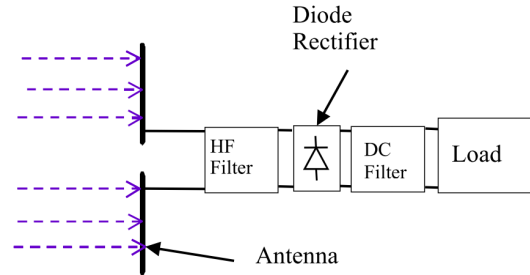


Figure 2. Block diagram of a rectenna circuit

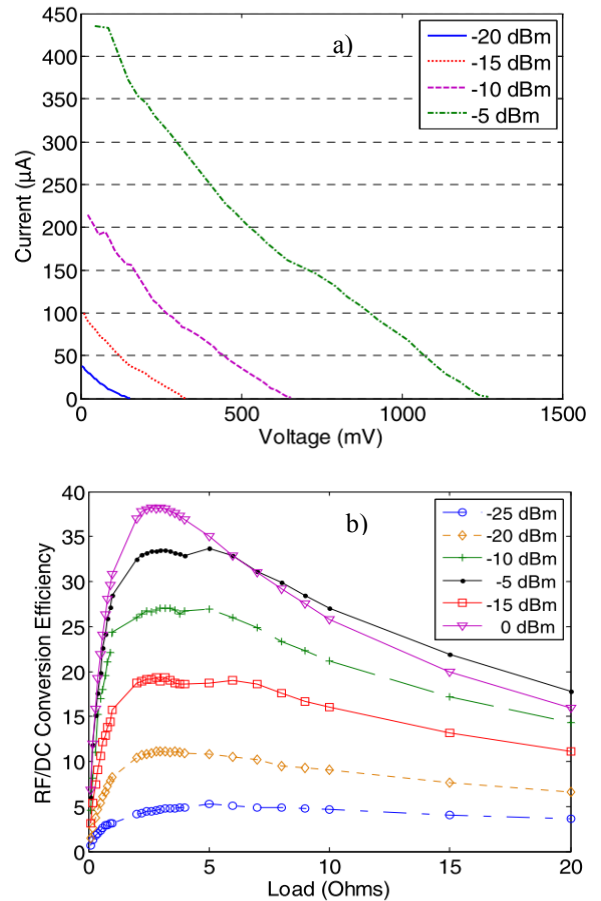


Figure 3. Series-mounted rectenna output characteristic: a) Current-Voltage, b) Efficiency-Load

I-V characteristic are almost parallel straight lines. In addition, conversion efficiency is maximal for a specific fixed output load value. Therefore, rectenna output DC model is a voltage source in series with its internal impedance. This internal impedance is equal to the optimal load value (2.4k Ω in this case). For a -15dBm (30 μW) level of injected RF power, output open-circuit voltage is equal to 300mV. In this case, the maximum DC power is around 10 μW . In order to be able to use this energy, a specific DC-DC converter topology would be needed in order to provide a conventional over 1V voltage level.

III. SELF-OSCILLATING DC-DC CONVERTER TOPOLOGY

A. Topology Presentation and Operation

This converter is inspired from the classical Armstrong oscillator topology [6-9]. In addition to its self-powering capability (neither external energy source nor external control are needed), this converter was optimized in order to accept very high source impedance (up to several k Ω). Fig. 4 shows the converter topology.

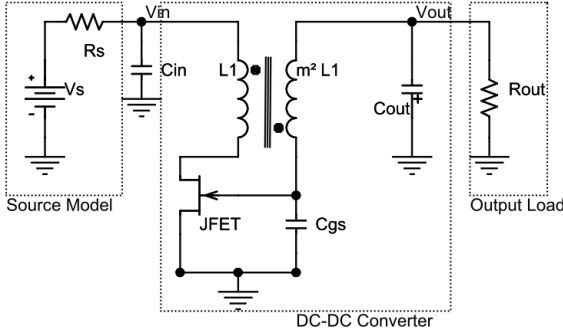


Figure 4. Self-oscillating DC-DC converter circuit

This converter contains three blocks which are essentials for its well-functioning:

- The oscillator: it is composed by the JFET which amplifies the gate's input signal. The oscillator return loop is formed by the two coupled-inductors and by the gate-source capacitor C_{gs} (which includes main parasitic capacitors).
- Voltage stepping-up: standard over 1V level is obtained from a very low source voltage level (some hundreds of mV) via a high step-up ratio transformer.
- The rectifier: in order to rectify JFET's gate oscillating voltage, the gate-source PN junction of the transistor is used. When the voltage of the gate becomes superior to the diode threshold voltage, the diode is turned ON and the circuit supplies the output load.

When the converter is connected to energy source, the current increases in the primary winding; the secondary winding applies then a positive voltage on the normally-on N-channel JFET's gate. The gate-source PN junction of the JFET is conducting, and the output capacitor is charged with a negative voltage. The output voltage is therefore negative. When the primary current reaches saturation, the voltage across the primary winding cancels and the negative voltage of the output capacitor is applied on the gate of the JFET pinching it off. The current in the primary winding decreases and a negative voltage is applied by the secondary winding on the gate of the JFET, which leads to its switching off. This peak voltage that switched off the JFET falls back to zero and the oscillation process starts again.

This circuit topology is very similar to those how are already present in the literature. However, there is a main advantageous of this structure in ultra-low current applications. Classical structure has a Flyback mode of operation, while this topology is based on a Forward mode. Energy is transferred to

the output during the on-phase which avoids the collapse of the switch gate voltage oscillations during the off-phase (case of Flyback operation mode).

B. DC-DC Converter Design and optimization

Theoretical as well as simulation optimizations have been performed. The source is characterized by a low voltage (several hundreds of mV) and by a very high internal impedance (several k Ω). Theoretical calculations on oscillations start-up conditions show that in order for the converter to work properly with such low input voltage and such high source impedance, JFET cutoff voltage V_p as well as its zero-gate voltage drain current I_{DSS} have to be minimized. Furthermore, transformer turn ration is a compromise between efficiency and start-up capability.

Regarding to optimization results, best commercially available JFET is the J201 ($I_{DSS}=583\mu A$; $V_p=-0.6V$). The optimal transformer turn ratio is around 1:20 (Coilcraft LPR6235-253PMB). The high-frequency transformer model has been established (from 40Hz to 1MHz) using an impedance meter (Agilent 4294A) and using the model described in [12]. This model includes: serial coils resistances, coupling coefficient and stray capacitances. The DC/DC converter was simulated using Pspice with the parameters indicated in Tab. II.

TABLE II. SIMULATION MODEL PARAMETERS

	Symbol	description	value	Unit
JFET	I_{DSS}	Zero-gate voltage drain current	583	μA
	V_p	Gate-source cutoff voltage	-0.6	V
	C_{gs}, C_{gd}	JFET capacitances	3; 4	pF
Transformer	$L1$	Primary inductance	23.74	μH
	m	Turn ratio	1:20	-
	C_p	Primary stray capacitance	3.13	nF
	C_s	Secondary stray capacitance	13.9	pF
	C_{ps}	Prim. to secon. stray capacitance	50.9	pF
	$RL1, RL2$	Primary coil resistance	155	m Ω
	Secondary coil resistance	54.8	Ω	

C. Simulation and experimental results

A prototype was fabricated in order to evaluate the real performances and to make comparison with simulations results. In this first step, the rectenna model ($R_s=2.4k\Omega$) is used and the source power is controlled via the voltage source V_s .

First step of experimental tests consists of varying the output load resistance for a fixed value of the input power. This test shows that maximum output power is reached with a 600k Ω load resistance. This is an optimal value that is kept in the following measurement. Afterwards, converter input and output voltages are measured for each value of input power. The simulation results are compared to experimental data. Fig. 5 shows input and output voltages as a function of input power level. Simulation results are close to the experimental data, which proves that simulation model is quite accurate. In addition, the voltage step-up ratio (up to 9) is almost constant over all input voltage range. Fig. 6 shows the efficiency of the converter as a function of input power level.

Converter efficiency reaches a maximum of 25% for input power levels between 60 μW and 200 μW . For power levels from 5 μW to 1mW, efficiency is between 10% and 25%.

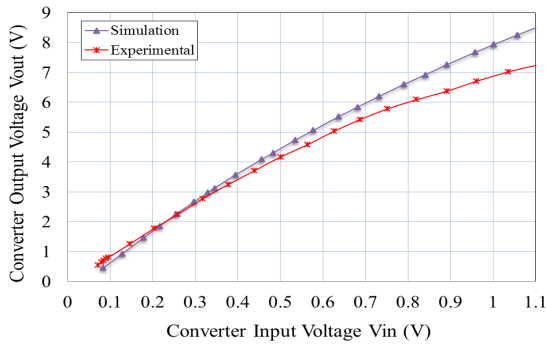


Figure 5. DC-DC converter input and output voltages

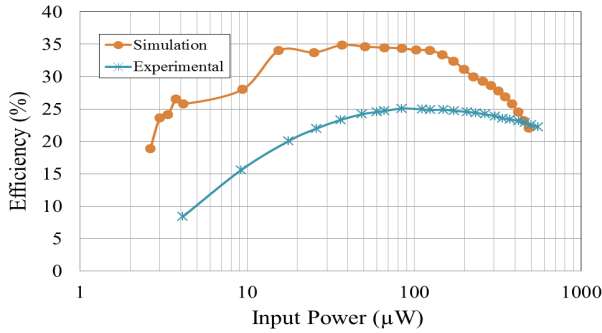


Figure 6. DC-DC converter efficiency vs. input power

Most losses are due to the JFET on-resistance which is high because of the low gate-cutoff voltage V_p (the drain-source channel is weakly doped). A low V_p and a low I_{DSS} are essential in order to satisfy the oscillations start-up conditions (for low source voltage and high source impedance). However, this leads to increase losses in the steady state. There is a compromise between start-up capability and steady state efficiency.

IV. SELF-OSCILLATING DC-DC CONVERTER POWERED BY A RECTENNA

In order to evaluate the global performances, the self-oscillating converter is associated with the previously described rectenna. A power RF signal generator is used to feed the RF-DC rectifier (power signal frequency is 2.45GHz).

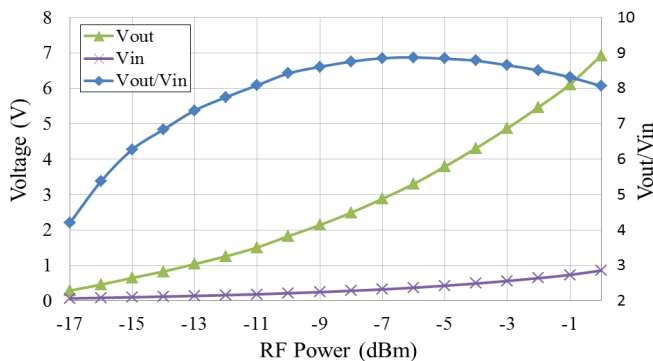


Figure 7. The converter powered by a rectenna: converter input and output voltages Vs. rectenna input power

Input power is varied from -20dBm to 0dBm. The external load is equal to the optimal load resistance of 600k Ω . Fig. 7 shows the converter input and output voltage and the stepping-up ratio with respect to the input power at rectenna level.

Whilst input voltage at converter level is under 1V for the entire range of input power, the output voltage rises to 7V for 0dBm. Furthermore, output voltage is above 1V for input power levels higher than -13dBm.

V. CONCLUSION

A self-powered, low voltage and ultra-low power DC-DC converter has been presented in this paper. It is suitable for high-impedances sources which provide ultra-low current. The converter performances were demonstrated using experimental tests. The fabricated prototype harvests low RF power (4 μ W-1mW) from a low power rectenna. 25% efficiency is achieved as well as a high voltage step-up ratio (up to 9). Furthermore, this converter is very compact (<0.5cm³) and has a very low cost (<1 USD for 1k units), which is suitable for industrial applications. Although it was designed for RF energy harvesting, this converter could be adapted and used with other energy-harvesting transducers.

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