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Hanna Lönnberg, Linda Fogelström, Qi Zhou, Anders Hult, Lars Berglund, et al.. Investigation of the graft length impact on the interfacial toughness in a cellulose/poly(ϵ -caprolactone) bilayer laminate. Composites Science and Technology, 2010, 71 (1), pp.9. 10.1016/j.compscitech.2010.09.007. hal-00702322

HAL Id: hal-00702322

https://hal.science/hal-00702322

Submitted on 30 May 2012

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Accepted Manuscript

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PII: S0266-3538(10)00352-0

DOI: 10.1016/j.compscitech.2010.09.007

Reference: CSTE 4810

To appear in: Composites Science and Technology

Received Date: 26 March 2010
Revised Date: 8 September 2010
Accepted Date: 13 September 2010



Please cite this article as: Lönnberg, H., Fogelström, L., Zhou, Q., Hult, A., Berglund, L., Malmström, E., Investigation of the graft length impact on the interfacial toughness in a cellulose/poly(ε-caprolactone) bilayer laminate, *Composites Science and Technology* (2010), doi: 10.1016/j.compscitech.2010.09.007

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Investigation of the graft length impact on the interfacial toughness in a cellulose/poly(- caprolactone) bilayer laminate

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ABSTRACT

Interfacial adhesion between immiscible cellulose-polymer interfaces is a crucial property for fibrous biocomposites. To tailor the interfacial adhesion, the grafting of polymers from cellulose films was studied using ring-opening polymerization of -caprolactone. The poly(-caprolactone) (PCL) grafted cellulose was analyzed with FTIR, AFM and *via* water CA measurements. The graft length was varied by the addition of a free initiator, enabling tailoring of the interfacial toughness. Films of microfibrillated cellulose were grafted with PCL and hot-pressed together with a PCL film to form a bilayer laminate. Interfacial peeling toughness correlates very strongly with PCL degree of polymerization (DP). PCL

grafts form physical entanglements in the PCL matrix and promote significant plastic deformation in the PCL bulk, thus increasing interfacial peeling energy.

KEYWORDS: microfibrillated cellulose grafted with polycaprolactone

- A. Polymer-matrix composites
- A. Laminate
- A. Wood
- B. Interfacial strength
- B. Delamination

INTRODUCTION

Cellulose in the form of high-strength nanofibers is the main load-bearing constituent in the cell wall of plant structures. The biosynthetic origin combined with exceptional physical properties and nanoscale lateral dimension makes cellulose a highly desirable constituent in new nanostructured material systems such as nanopaper, aerogels, biofoams, and high-strength biocomposites.

Fibrous plant cells, typically 30 µm in diameter and several mm in length, are already used as reinforcement in biocomposite materials. Such systems are very complex, and their end properties are difficult to predict. However, one of the most important issues for fully taking advantage of the excellent mechanical properties of cellulosic plant fibers in composite materials, is the creation of a strong interfacial adhesion between the reinforcing fiber and the polymer matrix. Different approaches have been utilized to improve fiber dispersion as well as strengthen the interface between fiber and matrix e.g. fiber-surface

modification attaching silanes, isocyanates etc. to the hydroxyl group on the surface of cellulose.^{7,8} There are also a number of studies on the improvement of the mechanical properties by grafting polymers to or from the cellulose surface.^{9,10-12}

The effect of chain entanglements on the interfacial toughness has been reviewed by Creton *et al.*¹³ At high areal density of high molar mass polymer molecules crossing an immiscible interface, entanglements can be highly successful during interface separation and promote extensive plastic deformation in polymer regions surrounding the interface. As a consequence, significant improvement in the interfacial toughness can be achieved.¹⁴

In the present study, we use the ideas reviewed by Creton *et al.* for fracture of interfaces between immiscible polymers,¹³ and apply them to the equally immiscible interface between cellulose nanofibers and a polymer matrix. For this reason, we graft PCL chains of various chain lengths from the cellulose surface in a step towards molecular design of grafts for interfacial toughness. High interface toughness often enhances composites strength; however, low toughness of the fiber/matrix interface may also be advantageous in certain fibrous polymer composites. Extensive fiber pull-out is then promoted, and consumes considerable energy so that composite toughness is increased.¹⁵

We have previously confirmed that ring-opening polymerization (ROP) is a versatile technique in order to covalently graft polymers directly from cellulose substrates, *via* a grafting-from approach.^{16,17} Surface characterizations of the PCL-grafted substrates with different graft lengths, as well as various prefunctionalization of the cellulosic surfaces, have shown significant impact on the surface composition, the surface morphology as well as the hydrophobic properties.¹⁶ In addition, for PCL-grafted nanosized cellulose, longer grafts gradually improved the dispersion in non-polar solvent and showed a gradual change

in the thermal properties and in the crystallization behavior of the PCL grafts, which verified an increase in graft length with higher target DP, i.e., ratio of added monomer to initiator. Habibi *et al.*¹¹ studied nanocomposite materials reinforced with different compositions of PCL-grafted cellulose nanocrystals that were obtained via a grafting-from approach. They reported a significant improvement in mechanical properties of biocomposites based on PCL-grafted cellulose nanocrystals in comparison to neat cellulose nanocrystals. However, no investigation of the graft length impact on the mechanical properties was performed.

In the present study PCL of different molecular weights is grafted from a cellulose surface and thereafter we analyze the effect of graft length on the interfacial adhesion in a bilayer laminate. The aim is to investigate if chain entanglements across a PCL grafted cellulose fiber/ polymer matrix interface can be utilized to strengthen the interfacial toughness between the reinforcement and the matrix in a biocomposite material.

EXPERIMENTAL

Materials. ε -Caprolactone (ε -CL), benzyl alcohol, tin octoate (SnOct₂), tetrahydrofuran (THF), methanol (MeOH) and poly(ε -caprolactone) (PCL) (Sigma-Aldrich, MW 80 000 g/mol) were used as received. Microfibrillated cellulose films (MFC-films) were prepared according to a procedure described by Henrikssson *et al.* The MFC-films were dried in vacuum oven at 50 °C for 24 h prior to use.

Characterization. Nuclear magnetic resonance (NMR) spectra were recorded at 400 MHz on a Bruker AM 400 using CDCl₃ as solvent. The TMS signal was used as an internal standard. Fourier transform infrared spectroscopy (FTIR) was performed on a Perkin-Elmer

Spectrum 2000 FTIR equipped with a MKII Golden Gate, Single Reflection ATR system from Specac Ltd, London, U.K. All spectra were normalized against a specific ATR crystal adsorption. Size exclusion chromatography (SEC) of the free, ungrafted, polymer formed was performed using a TDA Model 301 equipped with one or two GMH_{HR}-M columns with TSK-gel (Tosoh Biosep), a VE 5200 GPC Autosampler, a VE 1121 GPC Solvent pump and a VE 5710 GPC Degasser, from Viscotek Corp. THF was used as the mobile phase (1.0 ml min⁻¹). The measurement was performed at 35 °C. The SEC apparatus was calibrated with linear polystyrenes standards, and toluene was used as flow rate marker. Peel tests were performed on a dynamic mechanical analysis (DMA) TA-instrument Q800 equipped with a film fixture for tensile testing. The measurements were performed on rectangular laminates samples (20x4mm) at room temperature. The tests were performed in a controlled stressstrain mode with a preload force of 0.0010N and force ramp of 0.100N/min. The instrument set-up allowed for a maximum displacement of 20 mm. Four samples were used to characterize each PCL-MFC laminate. Atomic Force Microscopy (AFM) was performed using a Nanoscope III-a system (Digital Instruments) equipped with an EV-type vertically engaged piezoelectric scanner operating in tapping mode in air. Silicon AFM probes from Veccon (Nanosensors) were used with a resonance frequency of 275-348 kHz.

Synthesis of MFC-films grafted with PCL (MFC-PCL). In total, six different samples of the MFC-films were prepared: blank and MFC-PCL with target DP 75, 150, 300, and 600. The target DP was based on the amount of monomer, ε -CL, and the initiator, benzyl alcohol, added to the systems. The polymerizations were performed similarly to previously described procedures. Pre-dried MFC-films (2 pieces of 2*3 cm² and 1 piece of 2*1 cm²) were immersed in ε -CL (12 g) and toluene (20 ml). Thereafter benzyl alcohol was added to

the solution, corresponding to the targeted DP. To remove a majority of the remaining water, part of the solvent (15 ml) was distilled off before the catalyst, Sn(Oct)₂ (0.36 g), was added to the system under argon flow at 100 °C. The polymerizations were allowed to proceed16–18 h. Subsequently, the free PCL was dissolved in THF and precipitated in cold MeOH. In order to remove physically adsorbed but ungrafted PCL, the PCL grafted MFC films were thoroughly washed using soxhlet extraction in THF before characterization. The blank sample was treated in the same manner as the other samples with the exception that no catalyst was added in the ROP step.

Preparation of PCL-film and PCL-MFC bilayer laminates. PCL-films were prepared by solvent casting from THF. The bilayer laminates of MFC-PCL films and PCL-films were prepared by hot-pressing at 120 °C, 2 min 1 unit pressure and then 5 min 4 unit pressure.

RESULTS AND DISCUSSION

In this study ring-opening polymerization (ROP) is performed to graft poly(ε -caprolactone) (PCL) from a film of microfibrillated cellulose (MFC) derived from wood pulp. Subsequently, the PCL-grafted MFC films (MFC-PCL), are hot-pressed together with neat PCL film to form a PCL-MFC bilayer laminate. During the hot press stage the grafted molecules can diffuse across the interface.

In an attempt to gradually improve the interfacial peeling toughness of the PCL-MFC laminates the MFC-films were grafted with PCL to several different polymer lengths. We have previously demonstrated that the length of the polymer grafts, and the graft layer thickness, can be varied by the addition of a free (sacrificial) initiator (benzyl alcohol) to the polymerization mixture in a grafting-from approach, Scheme 1. The sacrificial

initiator also gives rise to a free polymer that can be isolated and subsequently characterized.

The samples prepared in this study are outlined in Table 1. The molar masses of the ungrafted, free PCL formed during ROP were determined by SEC and ¹H NMR spectroscopy. The determined molar masses (M_n), and corresponding (DP), were found to be lower than the theoretical values. This is somewhat expected since the ROP is initiated both from the added free initiator as well as from available OH-groups on the cellulose surface. However, the estimated molar masses of the free PCL were found to increase with increasing monomer-to-initiator ratio, i.e. target DP, Table 1.

FTIR spectroscopy was used to compare the amount of grafted PCL on the MFC-film surfaces for the different targeted DPs, Figure 1. In agreement with the previous studies^{16,17} a gradually increasing peak intensity of the carbonyl peak (at 1725 cm-1) was observed for higher target DP, thus indicating that more polymer is bound to the surface when higher DPs were targeted, which is also in agreement with the results from the characterization of the free, ungrafted PCL analyzed via ¹H-NMR and SEC analysis.

Atomic force microscopy (AFM) was used to study the change in surface morphology due to grafting, Figure 2. The MFC-film shows a defined fibrillar structure, whereas the images of MFC-PCL reveal an increasingly more polymer-covered surface with less defined fibrillar structure. Thus, there is a good agreement between the results from the FTIR analysis and the AFM images that indicate a gradual increase of the grafted polymer layers, or graft lengths, on the MFC-film surfaces with higher target DPs.

Contact angle (CA) against water was measured to investigate the change in hydrophobicity of the MFC-films as an effect of the grafting of PCL from the surface,

Table 1. It can be observed that the PCL grafting increased the hydrophobicity of all MFC-films. The MFC-PCL75 to MFC-PCL300 exhibits similar CA (91-94°), whereas a significantly higher CA was observed for the MFC-PCL600 (105°). Thus, all CAs of the PCL-grafted MFC-films are significantly higher than for both the reference materials, PCL and casted MFC-films. So despite the fact that the longer PCL grafts have a more smoothening effect on the surface morphology, observed with AFM, the higher surface coverage of hydrophobic PCL in combination with the present of surface roughness is accompanied by a higher hydrophobicity. The results are in good agreement with a previous study of PCL-grafted filter papers where high surface coverage of PCL grafts, obtained after pre-functionalization and grafting with long PCL grafts, significantly increased the CA to 105° for the PCL-grafted filter paper surface.

The graft length impact on the interfacial toughness in a bilayer laminate of the PCL grafted MFC-films was evaluated in a peel test, using a DMA instrument. The MFC-PCL films with different target DPs were laminated against thin films of pure PCL-forming bilayer laminates, which thereafter were subjected to the peel test. Figure 3 presents the peeling energy as a function of displacement; the values are also reported in Table 1. As seen, the sample grafted with short PCL chains, MFC-PCL75, does not show any improvement of the interfacial adhesion as compared to the neat MFC-film. This suggests that albeit the hydrophobicity of the surface is increased, as verified by CA measurements, the grafts are too short to substantially affect the interfacial adhesion. The samples MFC-PCL150 to MFC-PCL600, however, require a significantly higher peeling energy. Since the energy is very high, plastic deformation in the PCL matrix is the only plausible explanation caused by significant contribution from chain entanglements. In addition, interfacial

peeling toughness correlates very strongly with increasing chain length of PCL. This clearly demonstrates the importance of physical entanglements to promote plastic deformation in the PCL layer, and this represents the first study where the potential of this approach is demonstrated for cellulose-polymer interfaces. Herein the engineering of interfacial toughness at cellulose-polymer interfaces has been demonstrated and may be extended to other polymer systems. The demonstration is of great significance for cellulose biocomposite materials, since the laminate can be viewed as a model for fiber/matrix and nanofiber/matrix interfaces. Furthermore, we anticipate a highly durable interface bond in moist environments due to the grafted molecules and the corresponding physical entanglements in the interphase region.

CONCLUSION

In the present work, grafting impenetrable cellulose fiber surfaces with polymer chains was demonstrated as a tool for tailoring the interfacial adhesion in a bilayer laminate due to the formation of physical entanglements between chains in the matrix and on the surface. A grafting-from approach was utilized to covalently graft the MFC-films with PCL to different target DPs (MFC-PCL), controlled by the addition of a free initiator.

Characterization of the ungrafted PCL and PCL-grafted MFC films showed an increase in the molecular weight, and the graft layer thickness, with higher target DP. The MFC-PCL films were hot-pressed together with thin PCL-films to form bilayer laminates, which thereafter was subjected to peel tests in order to investigate the effect of graft length on the interfacial adhesion in the bilayer laminate. The peel test revealed a significant impact of the graft length on the interfacial adhesion, and an increase in the molecular weight of the PCL grafts required a gradually increase in the peeling energy for a delamination of the

bilayer laminate. Thus, the formation of entanglements across the immiscible cellulose/PCL interface promotes plastic shear yielding in the bulk polymer layer and therefore dramatically enhances interfacial toughness of the immiscible interface studied.

Acknowledgement. Swedish Agency for Innovation Systems (VINNOVA) and Swedish Center for Biomimetic Fiber Engineering (BIOMIME) are thanked for financial support.

M. Ankerfors at Innventia AB, Sweden, is thanked for providing the MFC.

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Table Caption

Table 1. Characterization of ungrafted PCL formed during ROP of -CL, contact angle of the PCL grafted MFC-films, and results from the peel test of the bilayer laminate.

Scheme Caption

Scheme 1. ROP of -CL from the MFC-film surface using benzyl alcohol as free initiator.

Figure Captions

Figure 1. FTIR spectra of blank MFC-film and MFC-films grafted with different target DP of PCL.

Figure 2. AFM images of reference MFC-film (A), MFC-PCL150 (B), MFC-PCL600 (C). The images are $1.5x1.5~\mu m^2$.

Figure 3. Interfacial peeling energy (toughness) of bilayer laminates prepared by joining MFC-PCL film with a PCL film.

Table 1.

Sample		SEC	NMR	CA	Peel test ^e	Peel test ^e
	Theo.MW ^a	Mn (PDI) ^b	Mn (conv) ^c	CA (std) ^d	Displacement ^f	Peeling
	(g/mol)	(g/mol)	(g/mol, %)	(°)	(mm)	energy (std) (J/m²)
	(DP _{theo})	(DP _{SEC})	(DP _{NMR})			(J/III)
MFC-film	-	-	-	67 (±2)	15.0	14.9 (4.2)
MFC-PCL75	8700	7900 (1.2)	6700 (91)	91 (±1)	17,5	15,3 (4.4)
	(75)	(69)	(59)			
MFC-PCL150	17200	10000 (1.2)	7750 (93)	93 (±2)	20.0	41.7 (11.6)
	(150)	(88)	(68)			
MFC-PCL300	34300	12200 (1.3)	9700 (91)	94 (±1)	20.0	52.8 (11.8)
	(300)	(107)	(85)			
MFC-PCL600	68500	22200 (1.4)	17400 (94)	105 (±3)	20.0	64.9 (21.2)
	(600)	(195)	(150)			
PCL-film	-	-) -	84 (±1)	-	

a) Theoretical molecular weight (MW) and degree of polymerization (DP_{theo}) was calculated by [M]/[I]_{free},. b) Mn = number average molecular weight; PDI = polydispersity index as determined by size exclusion chromatography, and degree of polymerization DP_{sec} . c) Mn = number average molecular; conv = monomer conversion, degree of polymerization DP_{NMR} calculated from ¹H NMR spectroscopy. d) water contact angle with standard deviation in brackets. e) results from the peel test of the bilayer laminates prepared from the PCL grafted MFC films and neat PCL films. f) The instrument set-up allowed for a maximum displacement of 20 mm.

Scheme 1.

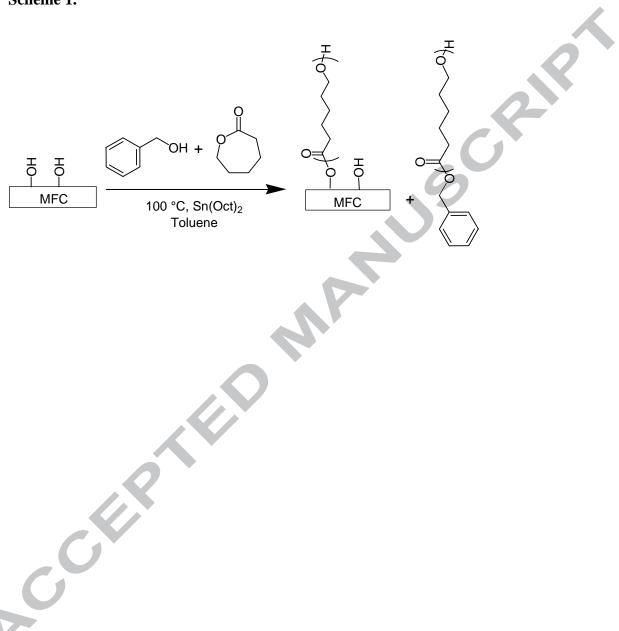


Figure 1.

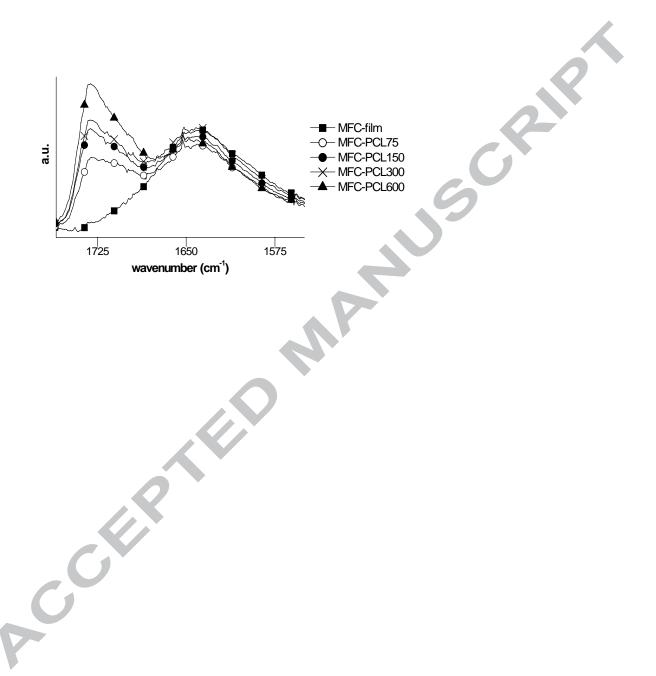
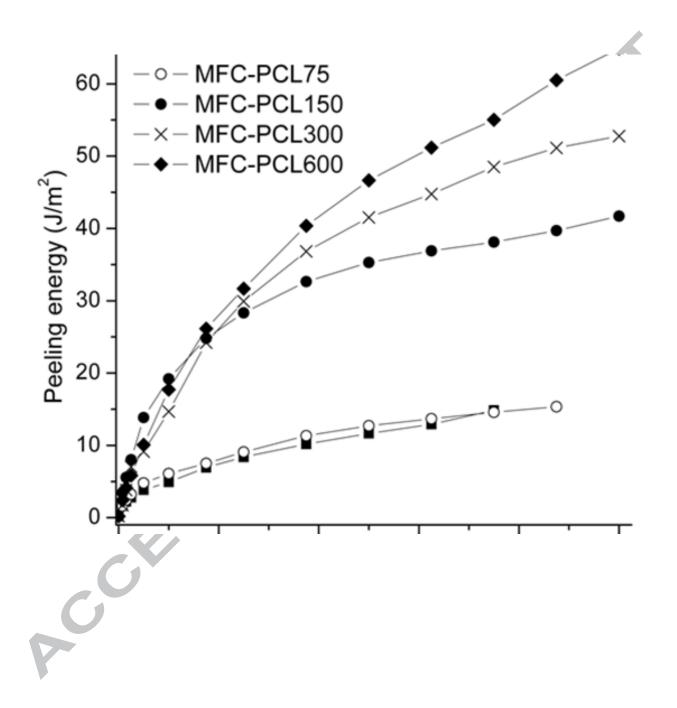


Figure 2.





Mn (PDI) be Mn (conv) bd (g/mol, %) (°) Displacemen peeling energy (std) (mm) (J/m²) MFC-film 67 (±2) 15.0 14.9 (4.2) MFC- PCL75 MFC- 17200 10000 (1.2) 7750 (93) 93 (±2) 20.0 41.7 (11.6) PCL150 MFC- PCL150 MFC- 68500 22200 (1.4) 17400 (94) 105 (±3) 20.0 64.9 (21.2) PCL-film 84 (±1)	Mn (PDI) b.c b.d (conv) b.d (conv	Mn (PDI) bc Mn (conv) CA (std) c Displacemen Peeling t g energy (std) (g/mol) (g/mol) (g/mol, %) (°) (mm) (J/m²) (J/m²)		MW ^a	SEC	NMR	Contact angle	Peel test ^f	Peel test ^f	
Column C	MFC- 17200 10000 (1.2) 7750 (93) 93 (±2) 20.0 41.7 (11.6) MFC- 34300 12200 (1.3) 9700 (91) 94 (±1) 20.0 52.8 (11.8) MFC- PCL300 MFC- 68500 22200 (1.4) 17400 (94) 105 (±3) 20.0 64.9 (21.2)	(g/mol) (g/mol) (g/mol) (g/mol, %) (°) (mm) (1/m²)			Mn (PDI) b,c	Mn (conv)		Displaceme	n Peeling	
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MFC- PCL300 12200 (1.3) 9700 (91) 94 (±1) 20.0 52.8 (11.8) MFC- PCL600 22200 (1.4) 17400 (94) 105 (±3) 20.0 64.9 (21.2)	MFC- PCL300 12200 (1.3) 9700 (91) 94 (±1) 20.0 52.8 (11.8) MFC- PCL600 22200 (1.4) 17400 (94) 105 (±3) 20.0 64.9 (21.2)	MFC-PCL300								
MFC- 34300 12200 (1.3) 9700 (91) 94 (±1) 20.0 52.8 (11.8) MFC- 68500 22200 (1.4) 17400 (94) 105 (±3) 20.0 64.9 (21.2)	MFC-PCL300 12200 (1.3) 9700 (91) 94 (±1) 20.0 52.8 (11.8) MFC-PCL600 22200 (1.4) 17400 (94) 105 (±3) 20.0 64.9 (21.2)	MFC-PCL300		8700	7900 (1.2)	6700 (91)	91 (±1)	17.5	15,3 (4.4)	
MFC- PCL300 12200 (1.3) 9700 (91) 94 (±1) 20.0 52.8 (11.8) MFC- PCL600 22200 (1.4) 17400 (94) 105 (±3) 20.0 64.9 (21.2)	MFC- PCL300 12200 (1.3) 9700 (91) 94 (±1) 20.0 52.8 (11.8) MFC- PCL600 22200 (1.4) 17400 (94) 105 (±3) 20.0 64.9 (21.2)	MFC-PCL300		17200	10000 (1.2)	7750 (93)	93 (±2)	20.0	41.7 (11.6)	
MFC- 68500 22200 (1.4) 17400 (94) 105 (±3) 20.0 64.9 (21.2)	MFC- PCL600 22200 (1.4) 17400 (94) 105 (±3) 20.0 64.9 (21.2)	MFC-PCL600	MFC-	34300	12200 (1.3)	9700 (91)	94 (±1)	20.0	52.8 (11.8)	
		PCL-film 84 (±1) -	MFC-	68500	22200 (1.4)	17400 (94)	105 (±3)	20.0	64.9 (21.2)	
- 04 (£1) -	CE-IIIII - -			+			84 (±1)			