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# GPS measurements of near-field deformation along the southern Dead Sea Fault System

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[1] Analysis of short-term deformation along the southern part of Dead Sea Fault (DSF) provides a systematic view of kinematics this part of the continental transform. The southern DSF consists of two principal segments: the Wadi Araba and Jordan Valley faults. In addition to other regional continuous GPS data, this study uses new data from 25 survey sites and 4 continuous GPS stations in Jordan for improved near-field observations. Resulting velocities are reported with 1- $\sigma$  uncertainties ranging from 0.4–1.0 mm/yr. Application of elastic dislocation models yields estimates of slip rates for Wadi Araba and Jordan Valley faults are  $4.9 \pm 0.4$  mm/yr and  $4.7 \pm 0.4$  mm/yr, respectively. Modeling also suggests different depths of effective fault locking with  $15 \pm 5$  km and  $8 \pm 5$  km for the Wadi Araba and Jordan Valley faults, respectively. These slip rates are generally consistent with the upper end of the range of slip rates estimated from late Quaternary geology. Spatial variations in effective fault locking generally correspond with a heterogeneous mantle lithosphere. A similar observation can be observed along the southern San Andreas Fault, and this may reflect the influence of heterogeneity in the uppermost mantle on crustal faulting processes.

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## 1. Introduction

[2] The Dead Sea Fault (DSF) is the left-lateral, continental transform bounding the northwestern Arabian plate and the Sinai plate in the eastern

Mediterranean region. Compared with other continental transforms, the relatively simple structure of DSF is appealing for elucidating fundamental insight on the kinematics of large strike-slip faults. Additionally, documenting strain accumulation is

also important for assessing the regional earthquake hazard.

[3] Regional plate models for the eastern Mediterranean region provide first-order constraints on rates of fault slip associated with plate boundaries. Although plate motion is a fundamental constraint for fault slip, slip rates predicted by such models are dependent upon the assumed fault geometries of the corresponding plate boundaries. Furthermore, such models are generally insufficient for directly assessing spatial variations in fault kinematics that may reflect more localized aspects of continental deformation.

[4] Neotectonic slip rate estimates, on the other hand, provide direct observations of fault kinematics. However, direct comparisons of neotectonic slip rates can often be complicated by epistemic uncertainties specific to each study site. In contrast to ad hoc comparison of point measurements corresponding with geologic (i.e., neotectonic) estimates of slip rate, near-field geodetic networks permit assessing spatial kinematic variations from a self-consistent perspective. More specifically, measurement and model-based assumptions will be identical and systematic, so that spatial variability may be more confidently assessed.

[5] This study assesses the kinematics of the southern DSF using new, high-precision Global Positioning System (GPS) measurements. These results complement other recent studies of near-field deformation along the northern DSF [Alchalbi *et al.*, 2010] and central DSF [Gomez *et al.*, 2007], and they build upon previous studies of near-field deformation that were limited only to parts of the southern DSF [e.g., Wdowinski *et al.*, 2004; Le Beon *et al.*, 2008]. Kinematic modeling of GPS velocities suggests along-strike variations in patterns of strain accumulation that correspond with seismogenic fault segmentation and lithospheric properties. Similar patterns are also observed along the southern San Andreas Fault, and these may reflect the influence of a heterogeneous mantle lid on crustal faulting processes.

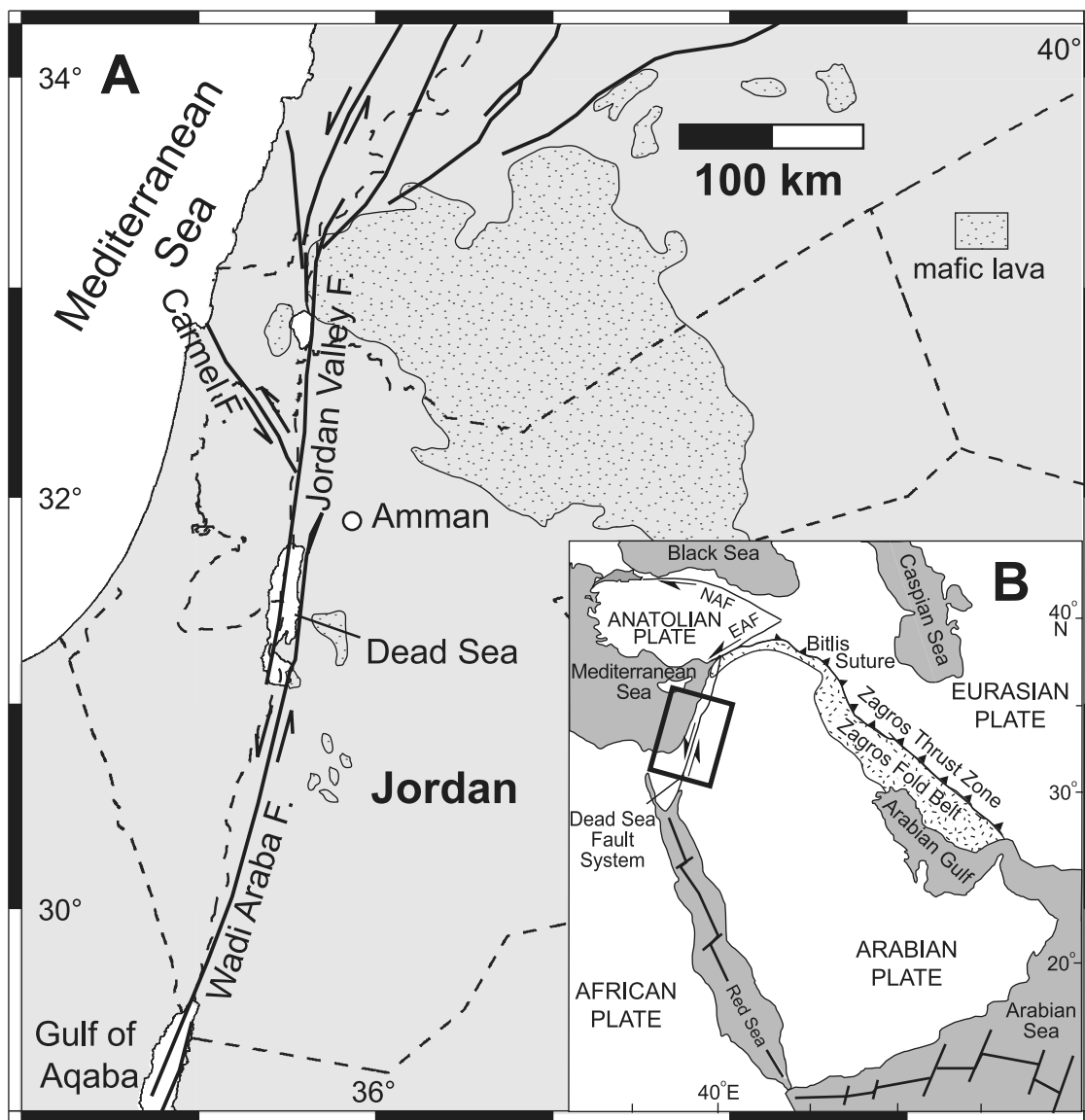
## 2. Active Tectonic Setting

[6] The N-S striking Dead Sea Fault (DSF) spans nearly 900 km, linking proto-oceanic spreading in the Red Sea with continental escape tectonics of the Anatolian plate. The DSF accommodates the left-lateral motion of Arabian plate relative to the Sinai plate as they converge with Eurasia and Anatolia and consists of three main sections (Figure 1):

(1) A southern section spanning from the Gulf of Aqaba through the Jordan Valley, (2) A NNE-SSW striking restraining bend through the Mount Lebanon and Anti Lebanon ranges, and (3) A northern section tracing along the Syrian Coastal Mountains until it intersects the East Anatolian Fault in southern Turkey. The southern section of the DSF, the focus of this study, is approximately 350 km in length and consists of two major segments: The Wadi Araba Fault (WAF) and the Jordan Valley Fault (JVF), which bound the Dead Sea pull-apart basin.

[7] Total left-lateral slip of 105 km is observed along the southern DSF [Freund *et al.*, 1970]. Left-lateral slip along the southern DSF initiated around 17–18 Ma [Garfunkel and Ben-Avraham, 2001] and accrued 60 km of displacement during a first phase of motion [e.g., Bartov *et al.*, 1980, Freund *et al.*, 1970]. A second phase of movement started during the late Miocene or early Pliocene [Quennell, 1984] and appears to correspond with the onset of oceanic spreading in the Red Sea [e.g., Hempton, 1987]. Total displacements on the southern and northern sections of the DSF during this episode are 45 km and 20–25 km, respectively [Freund *et al.*, 1970; Quennell, 1984]; the difference may be accommodated by up to 20 km of shortening of the Palmyride fold belt [e.g., Chaimov *et al.*, 1990]. Some studies suggest that, during the late Cenozoic, the DSF may have developed a regional trans-tensional component of motion (i.e., a “leaky” transform) which is thought to be partly responsible for the opening of the Dead Sea basin [Garfunkel, 1981; Freund *et al.*, 1970]. Despite this transtension, crustal thickness varies smoothly across the southern DSF and may connect to a lower crustal detachment [Weber *et al.*, 2009]. Modest seismic activity also suggests that the NW-SE striking Carmel Fault (Figure 1) may transfer some motion off of the main structure of the DSF [e.g., Hofstetter *et al.*, 1996].

[8] In addition to transform motion, late Cenozoic mafic volcanic activity has occurred in the Arabian plate adjacent to the DSF. Cenozoic volcanism occurs in three regions [e.g., Barberi *et al.*, 1980]: (1) Within the Dead Sea/Jordan Valley rift zone, (2) Along the eastern margin of the rift, and (3) in the Harrat Al Sham in northern and eastern Jordan [e.g., Ilani *et al.*, 2001; Garfunkel, 1989; Camp and Roobol, 1989]. Mafic volcanism initiated around 13 Ma and shows geochemical signatures of a mixed asthenospheric and lithospheric source [Shaw *et al.*, 2003].



**Figure 1.** (a) Regional tectonic map of the Dead Sea Fault System. (b) Inset shows the broader setting of the Arabian plate.

[9] Seismological analyses of the mantle lithosphere beneath the southern Dead Sea Fault suggest differences in the nature of the mantle lid between the Wadi Araba and Jordan Valley. Pn velocity tomography [Al-Lazki *et al.*, 2004], Pg Attenuation [Bao *et al.*, 2011], and Sn attenuation [Al-Damegh *et al.*, 2004] are consistent in suggesting normal, but thin, lithosphere beneath the Wadi Araba versus highly attenuating and slower mantle lithosphere beneath the Jordan Valley (as well as northern Jordan, and southwestern Syria). The Wadi Araba region was also studied by Laske *et al.* [2008] using surface wave analysis to estimate a thin mantle lid (80-km thickness) of normal S wave velocity. At lower spatial resolution, Chang

and Van der Lee [2011] document the restricted nature of the mantle S wave anomaly and suggest it as evidence of a plume beneath NW Arabia.

[10] Historical records document the strong earthquake potential of the southern DSF, despite a general seismic quiescence during the past century [e.g., Ambraseys *et al.*, 1994]. Aside from a large earthquake in the Gulf of Aqaba in 1995 ( $M \sim 7.4$ ), the southern DSF has not experienced large, surface-rupturing earthquakes along the WAF and JVF since 1458 AD and 1033 AD, respectively [e.g., Klinger *et al.*, 2000b; Ferry *et al.*, 2011]. On the other hand, recent moderate earthquakes, such as the 2004 ( $M \sim 5.3$ ) earthquake near the northern



end of the Dead Sea basin [Al-Tarazi *et al.*, 2006; Lazar *et al.*, 2006] attest to the present-day activity of the transform, and paleoseismic studies suggest return periods of large earthquakes average  $\sim 1,100$  years over the past 14 k.y. [e.g., Ferry *et al.*, 2011], although temporal clustering of earthquakes over longer time periods may also occur [e.g., Marco *et al.*, 1996]. Distributions of historical macroseismic observations also suggest general seismogenic segmentation between the Jordan Valley and the Wadi Araba for the largest earthquakes [e.g., Ferry *et al.*, 2011]. The boundary between these segments is generally interpreted to correspond with the Dead Sea basin.

[11] Plate tectonic models predict present-day left-lateral slip rates of 4–8 mm/yr along the DSF [e.g., Reilinger *et al.*, 2006; McClusky *et al.*, 2003; Joffe and Garfunkel, 1987; DeMets *et al.*, 1994; Westaway, 1994]. However, such fault kinematic predictions are dependent upon the assumed geometry and assume no permanent deformation off of the main faults comprising plate boundaries. Geological estimates of rates for the Wadi Araba Fault during late Pleistocene to Holocene range 2–6 mm/yr [e.g., Le Beon *et al.*, 2010; Makovsky *et al.*, 2008; Niemi *et al.*, 2001; Klinger *et al.*, 2000a; Ginat *et al.*, 1998]. In the Jordan Valley, offset Late Quaternary offset Gullies suggest a slip rate to about 4.7–5.1 mm/yr [Ferry *et al.*, 2007].

[12] Regional, continuous GPS data and elastic dislocation models have been used to propose slip rates of  $3.3 \pm 4$  mm/yr [Wdowinski *et al.*, 2004; Mahmoud *et al.*, 2005] along the southern DSF. However, data for these studies was almost exclusively confined to observations from the Sinai plate. Along the Wadi Araba Fault, detailed near-field GPS measurements and 1-D elastic dislocation models suggest a slip rate of  $4.9 \pm 1.4$  mm/yr [Le Beon *et al.*, 2008]. This work improves upon these geodesy-based kinematic parameters sufficient to assess spatial variations along the entire southern DSF.

### 3. GPS Measurements

[13] The GPS network used in this study was established in Jordan in 2005 and consists of 29 Survey-Mode sites and four continuous GPS station, as well as other regional continuous GPS stations with publicly available data. Survey-mode GPS sites consist of 10 cm steel pins cemented into bedrock. Most of these sites have been observed annually between 2005 and 2010 (Table 1). GPS

antenna were set up using fixed-height antenna masts, and sites were observed for a minimum of 24 h during each survey campaign using Trimble R7 dual-frequency GPS receivers with Trimble Zephyr geodetic antennae. Continuous GPS stations in Jordan used in this study have time series spanning 2–5 years (Table 1).

#### 3.1. Data Processing

[14] Raw GPS data were processed following a standard, two-step procedure using the GAMIT/GLOBK software [Herring *et al.*, 1997; Dong *et al.*, 1998; King and Bock, 1998]. In the first step, loosely constrained estimates of station coordinates, orbital and Earth orientation parameters, and atmospheric zenith delays were determined from raw GPS observables using GAMIT. Data from the Jordanian GPS network were analyzed along with raw GPS data from other continuously operating GPS (CGPS) stations in the region. Data from survey campaigns were subdivided into 8–10 h epochs (typically at 2400 UTC), so that multiple, loosely constrained solutions were available for each site during each given campaign. In addition to the times of the four survey campaigns in Jordan, CGPS data, when available, were also analyzed monthly between 2005 and 2009; a summary of the CGPS stations and their observations epochs is provided in Table 1.

[15] Subsequently, a global Kalman filter (GLOBK) was applied to the loosely constrained solutions and their associated covariance matrices in order to estimate a self-consistent set of station coordinates and velocities. As part of this second step, the data were combined with loosely constrained solutions for stations from the International GNSS Service (IGS) processed and distributed by MIT. A six-parameter Helmert transformation was estimated by minimizing the horizontal velocities of 134 globally distributed IGS stations with respect to the 2005 realization of the International Terrestrial Reference Frame (ITRF2005). The WRMS of the residual velocities for the IGS stations into ITRF 2005 was 0.7 mm/yr. During this process, obvious outliers in the continuous and campaign time series for regional sites were identified and removed; data from individual survey campaigns were then amalgamated into single epochs for final velocity estimation.

[16] Accurate characterization of the uncertainties in the velocities is critical to avoid over interpretation of the small tectonic signal associated with the DSF. It is well regarded that the formal, standard



**Table 1.** Velocities for GPS Sites Shown in Figure 2<sup>a</sup>

| Site   | Longitude | Latitude | Ve<br>(ITRF) | Vn<br>(ITRF) | Ve<br>(Ar) | Vn<br>(Ar) | Sig. E | Sig. N | Corr.  | First<br>(Date) | Last<br>(Date) | Span<br>(yr) |
|--|-----------|----------|--------------|--------------|------------|------------|--------|--------|--------|-----------------|----------------|--------------|
| <i>Jordan</i>                                  |           |          |              |              |            |            |        |        |        |                 |                |              |
| AQBA   | 35.018    | 29.528   | 21.86        | 19.72        | -1.43      | -1.58      | 0.68   | 0.68   | -0.021 | 2005.6          | 2010.5         | 4.9          |
| ASGF   | 37.648    | 32.333   | 23.10        | 22.33        | 0.43       | -0.14      | 0.61   | 0.62   | 0.006  | 2005.6          | 2010.5         | 4.9          |
| BISH   | 36.818    | 32.156   | 21.91        | 20.96        | -0.73      | -1.15      | 0.57   | 0.57   | 0.003  | 2005.6          | 2010.5         | 4.9          |
| DANA   | 35.580    | 30.698   | 24.68        | 20.49        | 1.17       | -1.07      | 0.75   | 0.71   | 0.000  | 2006.5          | 2010.5         | 4.0          |
| DASK   | 35.691    | 32.501   | 21.71        | 20.84        | -0.43      | -0.76      | 0.67   | 0.68   | 0.005  | 2005.6          | 2010.5         | 4.9          |
| DBUS   | 35.659    | 30.897   | 23.10        | 20.30        | -0.27      | -1.29      | 1.25   | 1.24   | -0.011 | 2008.5          | 2010.5         | 2.0          |
| DRAA   | 35.572    | 31.249   | 21.53        | 20.39        | -1.05      | -1.16      | 0.62   | 0.62   | 0.007  | 2005.6          | 2010.5         | 4.9          |
| FIFA   | 35.456    | 30.907   | 21.24        | 19.56        | -2.08      | -1.94      | 1.03   | 1.06   | -0.068 | 2007.5          | 2010.5         | 3.0          |
| HUG1   | 36.189    | 32.107   | 21.51        | 21.83        | -1.04      | 0.00       | 0.66   | 0.67   | -0.022 | 2005.5          | 2010.5         | 5.0          |
| HUGS <sup>b</sup>                              | 36.189    | 32.101   | 22.26        | 21.45        | -0.29      | -0.38      | 0.45   | 0.45   | 0.000  | 2005.5          | 2011.0         | 5.5          |
| JAFR   | 36.368    | 30.680   | 23.40        | 21.65        | -0.27      | -0.26      | 0.67   | 0.67   | 0.006  | 2005.6          | 2010.5         | 4.9          |
| JASH   | 35.915    | 32.294   | 21.59        | 22.19        | -0.76      | 0.49       | 0.61   | 0.62   | 0.012  | 2005.6          | 2010.5         | 4.9          |
| JUST <sup>b</sup>                              | 35.987    | 32.493   | 21.41        | 21.03        | -0.80      | -0.71      | 0.70   | 0.69   | -0.001 | 2008.4          | 2011.0         | 2.5          |
| MUD2   | 35.632    | 32.158   | 23.04        | 19.92        | 0.65       | -1.66      | 0.67   | 0.66   | 0.009  | 2005.6          | 2010.5         | 4.9          |
| MUTA <sup>b</sup>                              | 35.718    | 31.095   | 21.90        | 20.56        | -1.33      | -1.06      | 0.56   | 0.56   | -0.001 | 2007.2          | 2011.0         | 3.7          |
| NAML   | 35.403    | 30.469   | 23.53        | 21.61        | -0.12      | 0.13       | 1.20   | 1.21   | -0.024 | 2008.5          | 2010.5         | 2.0          |
| NAQB   | 35.433    | 30.086   | 22.28        | 20.73        | -1.67      | -0.76      | 1.84   | 1.89   | 0.087  | 2008.5          | 2010.5         | 2.0          |
| NEBO   | 35.739    | 31.766   | 20.53        | 21.55        | -1.19      | -0.08      | 0.94   | 0.92   | 0.021  | 2005.6          | 2010.5         | 4.9          |
| PANO   | 35.602    | 31.644   | 21.72        | 19.27        | -1.07      | -2.29      | 1.24   | 1.25   | -0.026 | 2008.5          | 2010.5         | 2.0          |
| PETA <sup>b</sup>                              | 35.469    | 30.327   | 22.51        | 19.78        | -1.26      | -1.73      | 0.67   | 0.67   | -0.002 | 2008.2          | 2011.0         | 2.8          |
| PETH   | 35.455    | 30.265   | 23.20        | 20.54        | -0.62      | -0.96      | 1.22   | 1.20   | -0.009 | 2005.6          | 2007.5         | 1.9          |
| QIRA   | 35.403    | 30.621   | 21.55        | 18.74        | -1.98      | -2.73      | 1.03   | 1.00   | -0.052 | 2007.5          | 2010.5         | 3.0          |
| QURA   | 35.340    | 29.810   | 23.07        | 20.00        | -1.07      | -1.45      | 0.59   | 0.59   | 0.001  | 2005.6          | 2010.5         | 4.9          |
| RAMA   | 35.151    | 29.907   | 22.52        | 18.60        | -1.51      | -2.76      | 0.83   | 0.82   | -0.009 | 2007.5          | 2010.5         | 3.0          |
| RSAS   | 35.922    | 31.514   | 23.13        | 20.02        | 0.18       | -1.69      | 0.66   | 0.64   | -0.010 | 2005.6          | 2010.5         | 4.9          |
| RUMM   | 35.426    | 29.630   | 23.87        | 20.31        | -0.42      | -1.18      | 0.83   | 0.81   | 0.004  | 2007.5          | 2010.5         | 3.0          |
| SAFI   | 35.514    | 31.078   | 23.29        | 19.77        | 0.09       | -1.75      | 1.21   | 1.22   | -0.010 | 2008.5          | 2010.5         | 2.0          |
| TUBA   | 36.562    | 31.319   | 22.47        | 21.59        | -0.76      | -0.40      | 0.63   | 0.63   | 0.004  | 2005.6          | 2010.5         | 4.9          |
| WADR   | 35.359    | 30.176   | 23.08        | 19.70        | -0.78      | -1.76      | 1.22   | 1.20   | -0.005 | 2008.5          | 2010.5         | 2.0          |
| <i>Southern Lebanon and Syria Survey Sites</i> |           |          |              |              |            |            |        |        |        |                 |                |              |
| ANJR   | 35.922    | 33.740   | 17.83        | 20.98        | -1.02      | -2.09      | 0.53   | 0.54   | -0.024 | 2002.4          | 2007.8         | 5.4          |
| HZRT   | 35.880    | 33.859   | 17.49        | 21.21        | -1.26      | -1.84      | 0.52   | 0.51   | -0.013 | 2002.4          | 2007.8         | 5.4          |
| JZIN   | 35.579    | 33.545   | 17.72        | 19.74        | -1.21      | -3.17      | 0.58   | 0.59   | -0.001 | 2002.4          | 2007.8         | 5.4          |
| JIYE   | 35.401    | 33.641   | 17.24        | 19.11        | -1.57      | -3.72      | 0.66   | 0.66   | -0.022 | 2002.4          | 2007.8         | 5.4          |
| KBDD   | 38.437    | 33.571   | 20.26        | 25.18        | 0.71       | 0.96       | 0.46   | 0.45   | -0.010 | 2001.1          | 2008.7         | 7.6          |
| MCHK   | 35.761    | 33.516   | 17.88        | 20.97        | -1.11      | -2.03      | 0.49   | 0.49   | -0.004 | 2002.4          | 2007.8         | 5.4          |
| RBDA   | 35.162    | 33.149   | 18.49        | 18.45        | -0.65      | -4.27      | 0.74   | 0.76   | 0.025  | 2002.4          | 2007.8         | 5.4          |
| RSHD   | 36.913    | 32.702   | 20.42        | 24.15        | 0.55       | 0.62       | 0.44   | 0.43   | -0.009 | 2001.1          | 2008.7         | 7.6          |
| TFEL   | 36.235    | 33.860   | 17.47        | 22.15        | -1.36      | -1.07      | 0.53   | 0.53   | -0.010 | 2002.4          | 2007.8         | 5.4          |
| <i>Other Regional Sites</i>                    |           |          |              |              |            |            |        |        |        |                 |                |              |
| ANKR <sup>b</sup>                              | 32.758    | 39.887   | -0.80        | 9.96         | -16.37     | -10.29     | 0.28   | 0.28   | -0.004 | 2000.9          | 2011.0         | 6.0          |
| AREL <sup>b</sup>                              | 35.209    | 32.102   | 20.84        | 18.00        | -1.52      | -3.39      | 0.57   | 0.57   | -0.002 | 2005.2          | 2008.6         | 3.4          |
| BAHR <sup>b</sup>                              | 50.608    | 26.209   | 29.89        | 26.98        | 0.20       | -0.52      | 0.32   | 0.31   | -0.002 | 2000.9          | 2008.6         | 3.6          |
| BSHM <sup>b</sup>                              | 35.023    | 32.779   | 22.21        | 17.57        | 0.42       | -3.73      | 0.32   | 0.32   | 0.000  | 2000.9          | 2011.0         | 6.0          |
| CSAR <sup>b</sup>                              | 34.890    | 32.488   | 20.58        | 17.43        | -1.41      | -3.81      | 0.41   | 0.41   | -0.001 | 2004.4          | 2011.0         | 6.0          |
| DRAG <sup>b</sup>                              | 35.392    | 31.593   | 21.55        | 17.73        | -1.23      | -3.74      | 0.32   | 0.32   | 0.000  | 2000.9          | 2011.0         | 6.0          |
| DSEA <sup>b</sup>                              | 35.369    | 31.037   | 22.62        | 19.00        | -0.58      | -2.46      | 0.45   | 0.45   | -0.001 | 2005.2          | 2011.0         | 5.8          |
| ELAT <sup>b</sup>                              | 34.921    | 29.509   | 24.36        | 18.33        | 0.07       | -2.93      | 0.33   | 0.33   | -0.002 | 2001.1          | 2011.0         | 6.0          |
| ELRO <sup>b</sup>                              | 35.771    | 33.182   | 21.59        | 19.93        | -0.04      | -1.71      | 0.33   | 0.33   | 0.000  | 2000.9          | 2010.6         | 5.6          |
| GILB <sup>b</sup>                              | 35.416    | 32.479   | 20.84        | 18.14        | -1.26      | -3.34      | 0.33   | 0.33   | 0.000  | 2000.9          | 2011.0         | 6.0          |
| JSLM <sup>b</sup>                              | 35.202    | 31.771   | 21.45        | 17.17        | -1.16      | -4.22      | 0.37   | 0.37   | 0.002  | 2002.3          | 2011.0         | 6.0          |
| KABR <sup>b</sup>                              | 35.145    | 33.023   | 20.51        | 17.67        | -1.12      | -3.69      | 0.33   | 0.32   | 0.000  | 2000.9          | 2011.0         | 6.0          |
| KATZ <sup>b</sup>                              | 35.688    | 32.995   | 21.31        | 19.86        | -0.45      | -1.74      | 0.33   | 0.33   | -0.002 | 2000.9          | 2011.0         | 6.0          |
| LAUG <sup>b</sup>                              | 35.674    | 34.115   | 19.70        | 18.92        | -1.18      | -2.67      | 0.39   | 0.39   | 0.000  | 2002.8          | 2010.7         | 5.7          |
| LHAV <sup>b</sup>                              | 34.866    | 31.378   | 21.43        | 16.40        | -1.42      | -4.83      | 0.37   | 0.37   | -0.001 | 2001.1          | 2008.9         | 3.9          |
| MERS <sup>b</sup>                              | 34.256    | 36.566   | 12.49        | 14.23        | -6.13      | -6.72      | 0.35   | 0.35   | 0.000  | 2002.4          | 2011.0         | 6.0          |
| NICO <sup>b</sup>                              | 33.396    | 35.141   | 18.31        | 13.20        | -1.28      | -7.35      | 0.32   | 0.32   | 0.000  | 2000.9          | 2011.0         | 6.0          |
| NRIF <sup>b</sup>                              | 35.036    | 30.038   | 22.30        | 18.12        | -1.61      | -3.19      | 0.44   | 0.44   | -0.001 | 2005.2          | 2011.0         | 5.8          |

**Table 1.** (continued)

| Site   | Longitude | Latitude | Ve<br>(ITRF) | Vn<br>(ITRF) | Ve<br>(Ar) | Vn<br>(Ar) | Sig. E | Sig. N | Corr.  | First<br>(Date) | Last<br>(Date) | Span<br>(yr) |
|--|-----------|----------|--------------|--------------|------------|------------|--------|--------|--------|-----------------|----------------|--------------|
| NSSP <sup>b</sup>  | 44.503    | 40.226   | 27.58        | 14.86        | 9.28       | -10.42     | 0.33   | 0.33   | 0.000  | 2001.1          | 2010.5         | 5.5          |
| RAMO <sup>b</sup>  | 34.763    | 30.598   | 26.54        | 20.36        | -0.36      | -3.71      | 0.78   | 0.76   | -0.001 | 2000.9          | 2011.0         | 6.0          |
| SLOM <sup>b</sup>  | 34.284    | 31.228   | 24.49        | 14.64        | 1.64       | -6.33      | 0.51   | 0.50   | -0.001 | 2004.7          | 2011.0         | 6.0          |
| TELA <sup>b</sup>  | 34.781    | 32.068   | 21.92        | 17.29        | -0.38      | -3.90      | 0.33   | 0.33   | -0.001 | 2000.9          | 2011.0         | 6.0          |
| TRAB <sup>b</sup>  | 39.776    | 40.995   | 24.37        | 10.99        | 7.98       | -12.38     | 0.38   | 0.38   | 0.000  | 2000.9          | 2007.9         | 2.9          |
| UDMC <sup>b</sup>  | 36.285    | 33.510   | 21.12        | 21.01        | -0.36      | -0.86      | 0.35   | 0.35   | 0.000  | 2002.3          | 2010.9         | 5.9          |
| YRCM <sup>b</sup>  | 34.928    | 30.992   | 21.53        | 17.07        | -1.63      | -4.19      | 0.48   | 0.48   | -0.002 | 2005.5          | 2010.5         | 5.0          |
| ZECK <sup>b</sup>  | 41.565    | 43.788   | 24.35        | 9.09         | 9.71       | -15.02     | 0.32   | 0.32   | 0.000  | 2000.9          | 2011.0         | 6.0          |
| <i>Le Beon et al. (Rotated Into Reference Frame of This Study)</i> |           |          |              |              |            |            |        |        |        |                 |                |              |
| ABK0   | 35.270    | 30.280   |              |              | 0.23       | -1.71      | 1.10   | 1.18   | 0.012  |                 |                |              |
| AYN0   | 35.780    | 30.960   |              |              | -0.31      | 0.02       | 1.10   | 1.10   | 0.035  |                 |                |              |
| BUR0   | 35.640    | 30.980   |              |              | -1.41      | 1.91       | 1.22   | 1.28   | 0.021  |                 |                |              |
| JEM0   | 35.080    | 29.750   |              |              | -0.73      | 0.78       | 1.10   | 1.23   | -0.006 |                 |                |              |
| JFR0   | 36.190    | 30.260   |              |              | -0.06      | 0.14       | 1.14   | 1.16   | 0.092  |                 |                |              |
| MAN0   | 35.680    | 30.170   |              |              | -0.26      | 0.51       | 1.11   | 1.18   | 0.051  |                 |                |              |
| QUL0   | 35.510    | 30.310   |              |              | 0.83       | -1.00      | 1.05   | 1.12   | 0.036  |                 |                |              |
| ROM0   | 35.310    | 29.700   |              |              | 1.17       | -0.61      | 1.10   | 1.24   | 0.020  |                 |                |              |
| SAF0   | 35.520    | 31.080   |              |              | -0.52      | -1.40      | 1.10   | 1.10   | 0.019  |                 |                |              |
| SUL0   | 35.440    | 30.440   |              |              | -0.88      | 0.10       | 1.16   | 1.20   | 0.023  |                 |                |              |
| BOR0   | 34.610    | 30.510   |              |              | -0.69      | -3.85      | 1.08   | 1.12   | -0.042 |                 |                |              |
| DIM0   | 35.080    | 31.030   |              |              | -0.22      | -5.02      | 1.07   | 1.08   | -0.002 |                 |                |              |
| MAP0   | 34.970    | 30.320   |              |              | -1.67      | -2.43      | 1.04   | 1.12   | -0.015 |                 |                |              |
| MNH0   | 35.130    | 30.290   |              |              | 0.23       | -3.62      | 1.09   | 1.16   | 0.000  |                 |                |              |
| SAG0   | 34.860    | 29.780   |              |              | -0.23      | -3.13      | 1.09   | 1.22   | -0.031 |                 |                |              |
| TAM0   | 35.300    | 30.950   |              |              | 0.49       | -4.11      | 1.07   | 1.08   | 0.010  |                 |                |              |
| TIM0   | 34.960    | 29.780   |              |              | 0.47       | -2.93      | 1.08   | 1.22   | -0.020 |                 |                |              |

<sup>a</sup>Velocities are presented in ITRF2005 and Arabia-fixed reference frames.

<sup>b</sup>Denotes continuous GPS station.

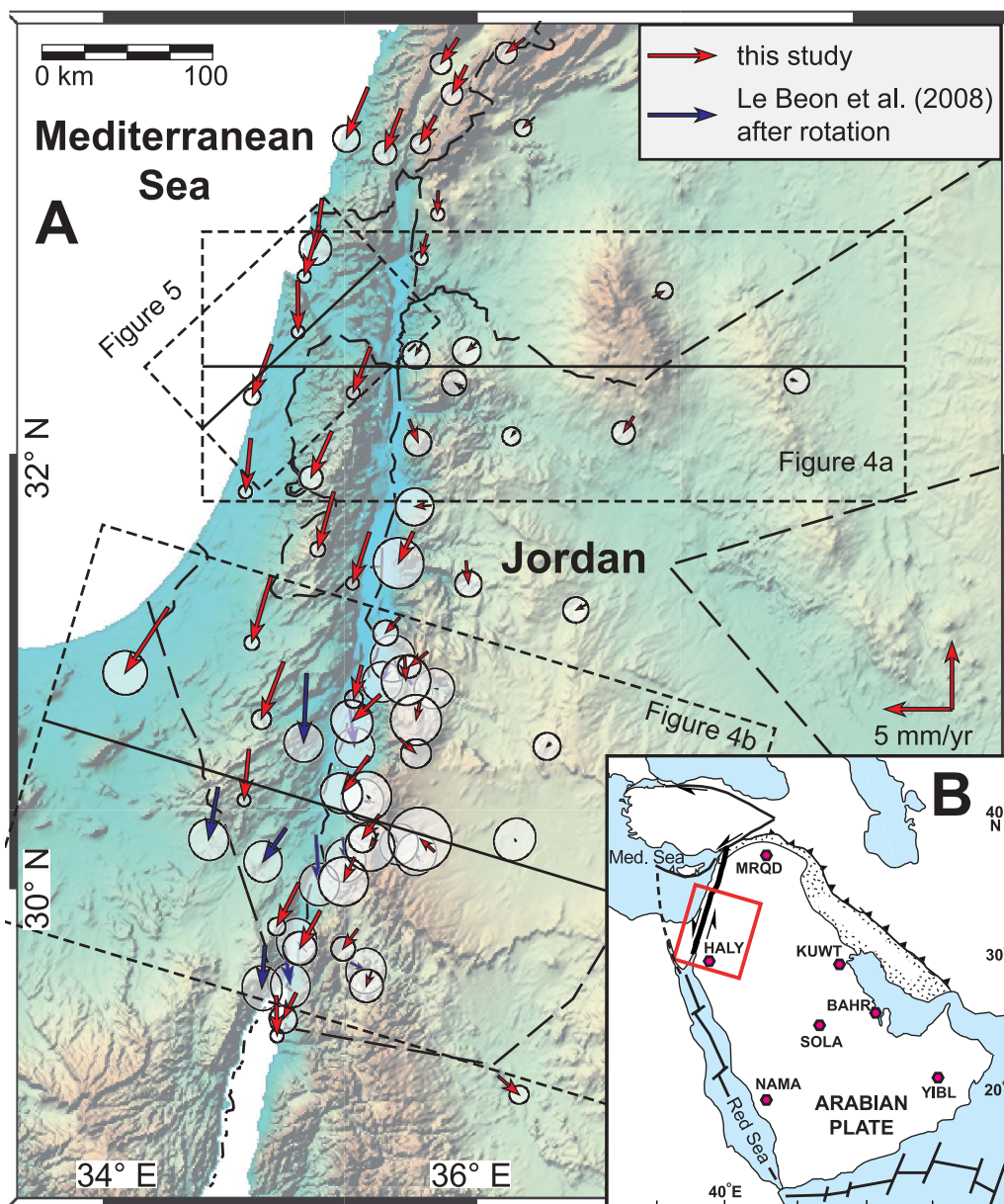
error of the GPS solution underestimates the true uncertainty in the GPS velocities [e.g., Zhang *et al.*, 1997; McClusky *et al.*, 2000]. Detailed studies of CGPS data indicate that the noise in GPS time series may be characterized by colored noise that varies from fractal white noise to random walk [Zhang *et al.*, 1997; Mao *et al.*, 1999]. However, by estimating relative velocities (i.e., defining “local” plate reference frames), we implicitly remove the common mode component of the noise within the region [McClusky *et al.*, 2000]. The remaining noise error in GPS observations accounts for factors such as monument stability and setup errors. In GPS processing with GLOBK, noise is modeled as a time-dependent, random walk error in the velocity estimation. In our study, we applied a random walk noise of 1.3 mm/sqrt(yr), which represents the average of random walk noise estimated for CGPS sites in the eastern Mediterranean region by Reilinger *et al.* [2006]. We believe this is justified owing to the use of extremely stable, fixed-height antenna masts during the all of the survey campaigns.

[17] After stabilizing the reference frame, the site velocities were resolved to an Arabia-fixed reference frame, which facilitates assessing the local

deformation. The reference frame was defined by minimizing the motion of 6 GPS sites distributed around Arabia (Figure 2, inset); the WRMS of the residual velocities used to define the Arabian plate is 0.8 mm/yr. GPS velocities (in ITRF2000-NNR and Arabia-fixed reference frames) for the sites around the southern DSF are provided in Table 2. We estimate ITRF2005 Euler pole for the Arabian plate is  $48.790 \pm 0.9^\circ \text{N} / 5.133 \pm 1.9^\circ \text{W} / 0.481 \pm 0.019^\circ / \text{Myr}$ . This compares with results of Reilinger *et al.* [2006]. However, the error reported here is larger because Reilinger *et al.* analyzed longer time series for the regional CGPS sites, whereas our study primarily analyzed data during the time periods of GPS survey campaigns in Jordan (2005–2010).

### 3.2. Results: Velocity Field

[18] As shown in Figure 2, the velocity field depicts the overall, left-lateral shear along the southern DSF. The overall orientations of velocity vectors are coherent, and the velocity magnitudes demonstrate a gradual decrease toward the DSF. This pattern is consistent with a locked fault that accumulates elastic strain.



**Figure 2.** (a) GPS velocities along the southern Dead Sea Fault System. Velocities are shown in an Arabian-fixed reference frame. In addition to velocities from this analysis, velocity vectors reported by *Le Beon et al.* [2008] across the Wadi Araba Fault have been rotated into our reference frame and included for completeness. (b) Map depicting location of GPS sites used to define the Arabian plate reference frame.

[19] To construct a more complete view of near-field deformation, we have also incorporated GPS velocities reported by *Le Beon et al.* [2008] spanning the Wadi Araba. Prior to combining these velocities with results from our analysis, a rotational transformation was estimated that minimized the residual misfit of GPS velocities for 11 sites that are common to *Le Beon et al.* and this study (Figure 3); the RMS fit was 0.6 mm/yr, much less than the  $1\text{-}\sigma$  uncertainties reported by *Le Beon*

et al. This transformation was applied to velocities reported by *Le Beon et al.*, before incorporating into our analysis; adding these velocities produces a more spatially complete coverage of the southern DSF.

[20] Because transform motion primarily involves strike-slip, an initial assessment of fault kinematics can be made by analyzing GPS velocities along profiles across the fault (Figure 4). Two profiles are examined that cross the WAF and the JVF,



**Table 2.** Kinematic Results From Block Models for the Southern Dead Sea Fault<sup>a</sup>

|                            | Locking Depth (km) | Slip Rate (mm/yr) |
|----------------------------|--------------------|-------------------|
| <i>Jordan Valley Fault</i> |                    |                   |
| Minimum                    | 4                  | 4.4               |
| Maximum                    | 13                 | 5.2               |
| Preferred                  | 8                  | 4.7               |
| <i>Wadi Araba Fault</i>    |                    |                   |
| Minimum                    | 10                 | 4.6               |
| Maximum                    | 24                 | 5.3               |
| Preferred                  | 15                 | 4.9               |

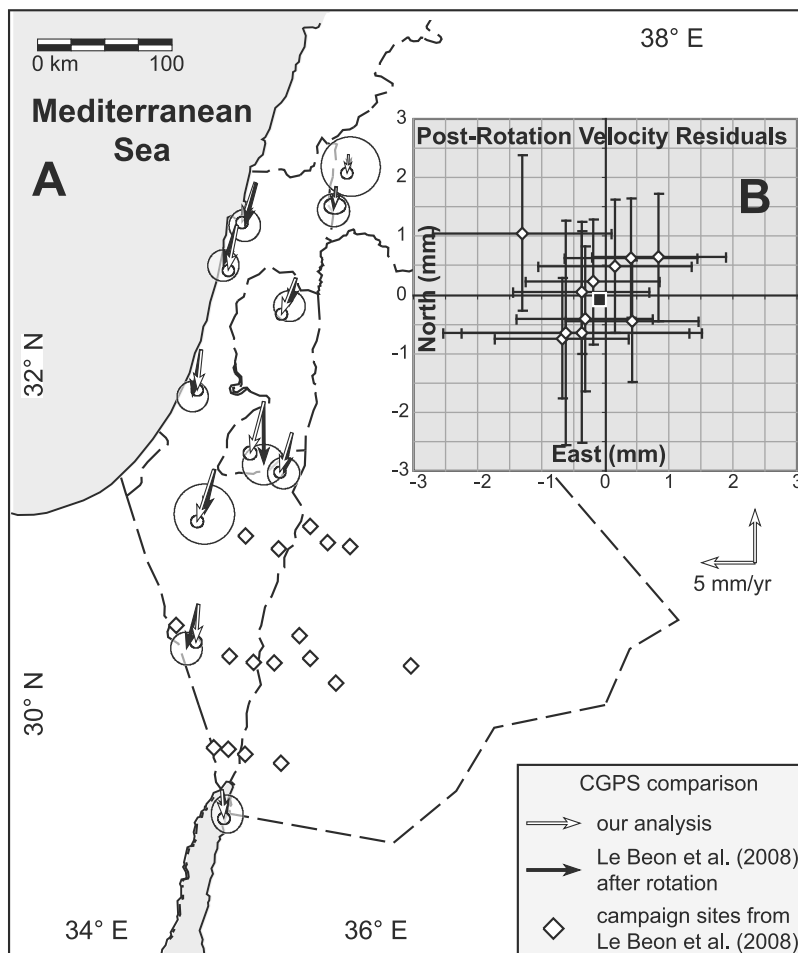
<sup>a</sup>Minima and Maxima are based on the probable (1-sigma) confidence region (Figure 6) estimated after modeling 500 iterations of the block model allowing for Gaussian noise of site velocities. Preferred parameters correspond to the minimum WRMS from noise analysis; asymmetry of probability distribution is skewed toward shallower locking depths.

respectively. The profiles in Figure 4 decompose the GPS velocities into motions parallel and perpendicular to the DSF.

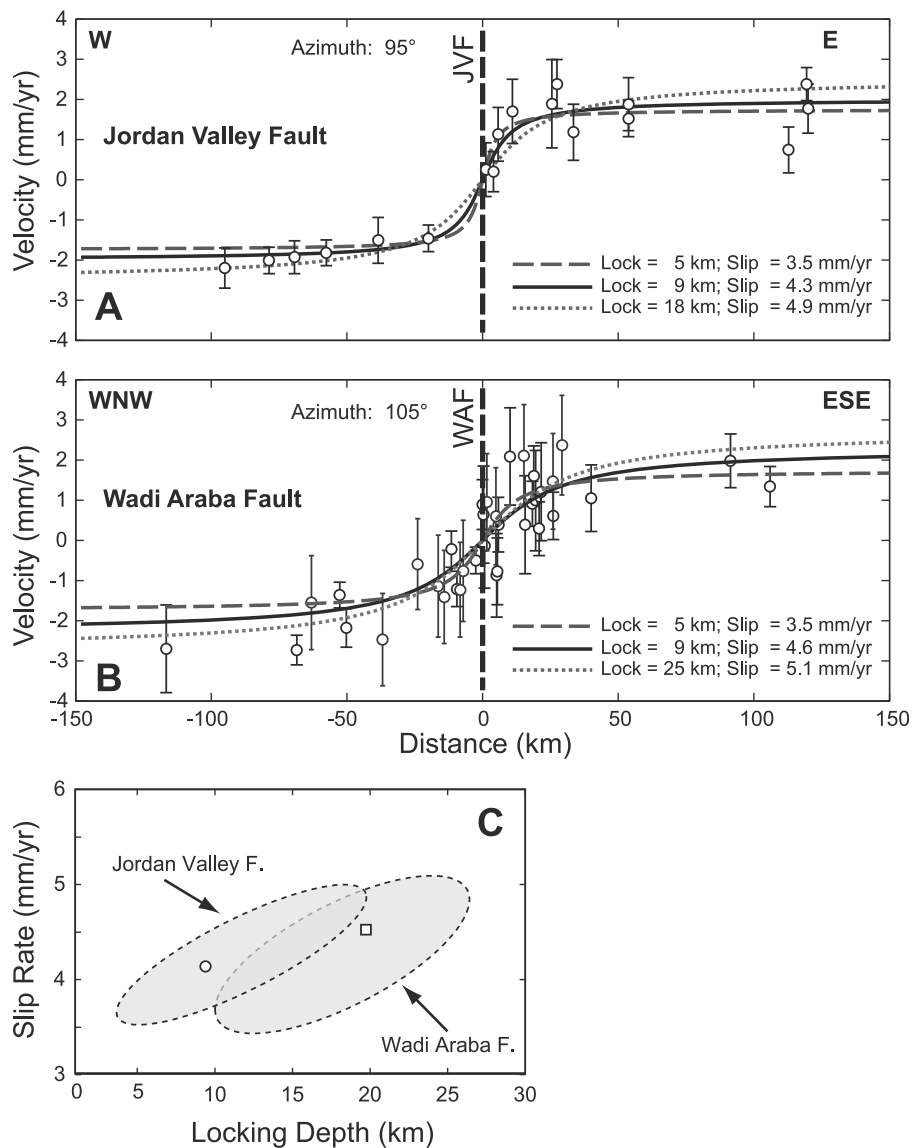
[21] In both profiles, the velocities parallel to the transform show a progressive increase in southward velocity from east to west; this pattern is generally consistent with basic models of elastic strain accumulation for strike-slip faults and will be explored further below. GPS velocities perpendicular to the DSF do not depict statistically significant motions indicative of either transtension or transpression.

#### 4. Modeling of GPS Velocities

[22] In this study, quantitative kinematic analysis of these GPS velocities is accomplished using elastic dislocation models. Elastic dislocation models are commonly applied to geodetic data (including GPS) in order to relate point velocities and/or strains to fault kinematic parameters including slip rate and depth of fault locking. As an example of further utility, *Devès et al.* [2011] applied elastic dislocations to explain long-term deformation and first-



**Figure 3.** (a) Comparison of GPS velocities for common sites (continuous GPS stations) with results of *Le Beon et al.* [2008]. Velocities of *Le Beon et al.* (white arrows) are shown after rotation. (b) Scatterplot of residual velocities for common sites after transformation to our reference frame. The mean residual of the fit is 0.4 mm/yr.



**Figure 4.** Profiles of strike-parallel GPS velocities across (a) the Jordan Valley and (b) Wadi Araba. For each profile, 1-D elastic dislocation models (discussed in the text) are shown for a range of slip rates and locking depths. Heavy, dashed line denotes the location of the DSF along each profile. See Figure 2 for location. (c) 2-sigma confidence limits on slip rates and locking depths estimated from Monte Carlo simulation of the noise level in the data. Although there is a suggestion of different fault locking depths for the two fault segments, such a distinction is not robust from these 1-D models.

order topography along the southern Dead Sea Fault. Although topography was their primary constraint, Dèves et al. demonstrated overall consistency with previous GPS results [Le Beon et al., 2008]. Hence, improved fault kinematic parameters may help refine models of long-term deformation, too.

[23] In this study, a two-step modeling approach is used: (1) Initially, 1-D profile models are applied separately to the Wadi Araba and Jordan Valley faults to assess kinematic consistency. (2) Subse-

quently, 2-D elastic block models are applied to address regional tectonic questions and more robustly estimate kinematic parameters. Results from the 1-D models provide justification for the geometry that must be assumed in the 2-D models.

[24] The locking depths modeled here are more properly considered as ‘effective’ locking depths, as the actual variation of slip with depth is more likely gradual, rather than abrupt. However, geodetic measurements cannot unambiguously resolve the depth distribution of slip [e.g., Savage, 2006].

However, the effective locking depth can be considered as a description of the degree to which a crustal fault accumulates earthquake moment [e.g., *Smith-Konter et al.*, 2011].

#### 4.1. 1-D Elastic Dislocation Models and Consistency of Wadi Araba and Jordan Valley Faults

[25] A preliminary estimate of the slip rates may be provided by applying 1-dimensional (i.e., profile) elastic dislocation models using the analytical function presented by *Savage and Burford* [1973]. Although very simplified, this approach permits comparing independent models for the Wadi Araba and Jordan Valley faults (in block modeling discussed below, they are implicitly linked).

[26] In this 1-D analysis, theoretical station velocity relative to the fault ( $v$ ) is maintained by fitting GPS data to a locked fault model depth ( $D$ ) as a function of long-term slip rate ( $b$ ) and horizontal distance ( $x$ ) from fault:

$$v = (b/\pi) \tan^{-1}(x/D) \quad (1)$$

The long-term slip rate,  $b$ , corresponds with the loading of the locked, upper portion of the fault by stable sliding in the lower crust.

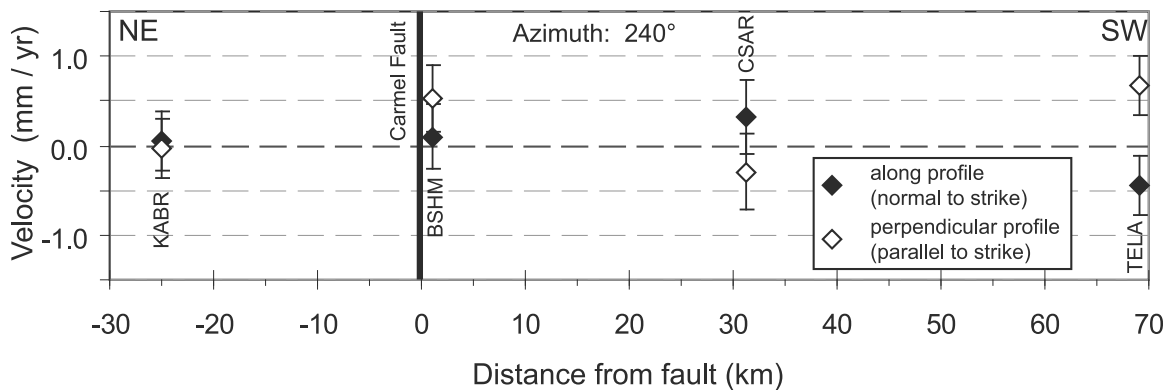
[27] Best fit 1-D models were estimated using a grid search inversion. The inverse modeling solved for three parameters: slip rate, locking depth, and a constant that minimizes velocity at the fault. The constant term changes the reference frame to that of the fault (rather than one plate or the other), as required by the analytical solution in equation (1). Uncertainties for 1-D model parameters were estimated using a ‘Monte Carlo’ simulation of assumed, Gaussian noise in the velocity data [e.g., *Gomez et al.*, 2007]; the inversion was repeated allowing velocities to vary with a normal probability based on the standard deviation reported by GLOBK. In total, 1,000 iterations were performed for each profile, and the probable (1-sigma) uncertainty was estimated from the scatter the resulting parameters.

[28] As shown in Figure 4, the Jordan Valley and Wadi Araba profiles are statistically similar, with fault slip rates and locking depths ranging from 4.5–5.1 mm/yr. Initial estimates of locking depths are 5–18 km for the Jordan Valley Fault and 10–25 km for the Wadi Araba Fault. Preferred estimates of 1-D model slip rates and locking depths are based on the minimum WRMS from the inversions: 4.2 mm/yr at 9 km for the JVF, and 4.5 at 19 km for

the WAF. The main implication of this initial analysis is that slip rates of the JVF and WAF are statistically similar, although locking depths may vary. For the tectonics of the Dead Sea basin, this implies that slip across the step-over is generally conserved between its two bounding faults. Therefore, extension within the basin is primarily a result of the displacement gradient resulting from the transfer of slip from the WAF to the JVF.

[29] From these profiles, there does not appear to be a significant transfer of slip from the DSF to the Carmel Fault at the present time. This is also suggested from the velocities of continuous GPS sites in a profile spanning the Carmel Fault (Figure 5), which show no statistically significant changes in motion perpendicular to the fault, nor along strike. The continuous GPS stations spanning the Carmel Fault have velocity uncertainties less than 0.5 mm/yr (1 sigma) (Figure 5). Our results reaffirm and refine earlier interpretations of the Carmel Fault from GPS [*Wdowinski et al.*, 2004; *Le Beon et al.*, 2008] and InSAR analyses [*Nof et al.*, 2007] and further reduce the uncertainty and maximum slip rate constraint. Our results disagree with recent interpretations of 4.5 mm/yr of right-lateral displacement by *Reinking et al.* [2011] based on short occupation (typically less than 6 h), survey-mode GPS data. However, we believe the CGPS results are more reliable than the survey-mode results of *Reinking et al.* [2011], owing to survey epochs of longer duration (typically 24-h) and greater number (in this study, weekly observations spanning 6+ years). Hence, we interpret that the Carmel Fault slips at a rate less than 0.5 mm/yr, at most.

[30] These 1-D models provide preliminary kinematic parameters. The uncertainties are relatively large, but comparable to those reported from similar models by *Le Beon et al.* [2008]. On the other hand, such models are limited in that they are incapable of accounting for oblique plate motion, which is important for testing the hypothesis of a “leaky” transform along the southern DSF. These 1-D models are analyzed independently of on another. The confidence limits on locking depths and slip rates shown in Figure 4c are large and demonstrate considerable overlap, although optimal solutions suggest different depths of fault locking, the distinction is not robust from the 1-D models, alone. However, since they are part of the same plate boundary, fault slip rates must be consistent and compatible with plate motion, and this provides additional constraints that may reduce parameter uncertainties.



**Figure 5.** Profile of velocities perpendicular and parallel to the Carmel Fault. The four continuous GPS stations shown were selected owing to their similar (and maximum) distance away from the main Dead Sea Fault in order to minimize differences in velocities resulting from locking and elastic strains associated with the main transform. See Figure 2 for location.

## 4.2. 2-D Elastic Block Modeling

[31] A more geometrically appropriate elastic model (and more robust estimate of the fault slip rate) involves 2-D blocks bounded by faults of finite lengths, rather than 1-D profiles across faults of infinite length. This modeling follows the methodology of *Meade and Loveless* [2009] and considers the spatial variations in the velocity field due to fault geometry and the effect of block rotations that are not accounted for in 1-D models. In this approach, an optimal fit between plate motion, fault slip, and GPS velocities is determined using a linearized least squares inverse method. Once again, the motivation is that rigid plate motion can provide an additional constraint to reduce uncertainties in the modeled fault parameters.

[32] In this block model, far-field velocities within Arabia are used (the same ones used in the Arabian-plate definition). Sites in Lebanon [*Gomez et al.*, 2007] were included, as well. GPS near-field, survey-sites from Syria were not used in the modeling, owing to concerns of internal deformation of both northern Arabia and the northern Sinai plates [*Alchalbi et al.*, 2010]. Data were weighted based on the velocity uncertainties and spatial density of survey sites. The block model for the southern DSF is a relatively simple, vertical fault that steps leftward at the Dead Sea basin (Figure 5). Owing to the statistical similarity of slip rates in the 1-D models (above), the fault geometry was approximated with a step-over at the Dead Sea basin, and the Carmel fault was not included.

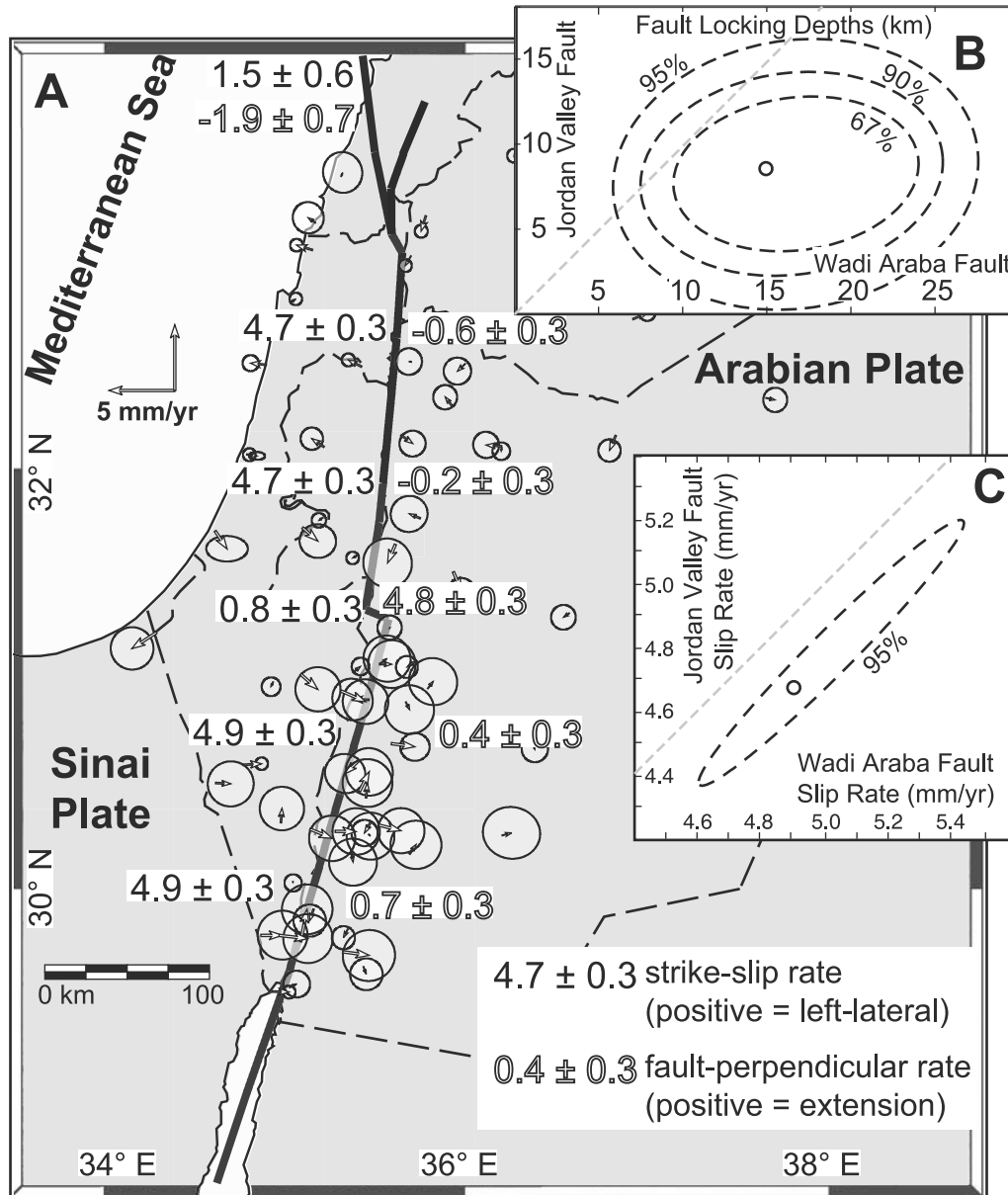
[33] Our analysis estimated locking depth by with multiple runs of the block modeling code; for each run, locking depth was varied by 1 km increments

between 1 km and 35 km, and the optimal combination of locking depths and slip rates were determined based on minimizing the weighted RMS of the residual, near-field velocities. In order to quantify uncertainties for the model parameters, these models were run with Gaussian noise added to each velocity. Based on the scatter of the optimal parameters for more than 2,000 model iterations, confidence limits (ellipses on scatterplots) were estimated for locking depths (Figure 6b) and slip rates (Figure 6c). Kinematic parameters predicted by the block model for the Wadi Araba and Jordan Valley faults are shown in Table 2.

[34] The confidence limits on effective locking depths (Figure 6b) suggest different locking depths for the two main branches of the southern DSF. This is demonstrated by the confidence regions, which are generally located outside the region of equal locking depth (dashed gray line in Figure 6b). As shown in Figure 6b, the distinction is generally supported at the 90% confidence level, although the 95% confidence ellipse does not completely exclude the possibility. Hence, at the 90% confidence level, the effective locking depth on the JVF is shallower than the effective locking depth on the WAF; the robustness of this distinction is derived from the plate motion constraint in the block modeling method.

[35] The 95% confidence ellipse for slip rates in Figure 6c demonstrates high covariance between the Wadi Araba and Jordan Valley faults. This is reflects the fact that both slip rates linked through their mutual dependency on the Arabia-Sinai Euler pole. Owing to the Euler pole's position relative to the southern DSF, predicted slip rates are slightly lower on the Jordan Valley Fault than along the





**Figure 6.** (a) Block model for the southern Dead Sea Fault System showing best fit velocities from the 2-D analysis. (b) Confidence limits on effective depth of fault locking for the Jordan Valley and Wadi Araba faults from block model analysis incorporating noise. Confidence ellipses for 67%, 90%, and 95% are shown. Dashed, gray line denotes equal locking depths. Much of the confidence region is outside of the range of equal fault locking depths. (c) 95% confidence limits on range of fault slip rates for the two fault segments, based on the block model. The strong covariance between the two faults reflects the fact that both faults are linked through their mutual dependency on plate motion. Dashed gray line denotes equal slip rate values.

Wadi Araba Fault. The slip rate magnitudes are slightly greater than, but statistically similar to, slip rates predicted by the regional block model of *Reilinger et al.* [2006] (based primarily on far-field GPS with an assumed locking depth). However, we believe that kinematic modeling of the new results (which include solving for locking depth) is more

robust with regard to the DSF owing to the inclusion of near-field data.

[36] On a final note, in the best fitting block model, there are no statistically significant residual velocities (i.e., misfit) that require adding another block boundary (i.e., the Carmel Fault). This does not necessarily discount present-day activity of the

Carmel Fault; in fact, infrequent seismicity suggests some degree of activity [e.g., Hofstetter et al., 1996]. However, the implication is that deformation associated with it is smaller than the detection threshold of GPS, and there is no measurable strain accumulating.

## 5. Discussion and Tectonic Implications

### 5.1. Regional Tectonics

[37] The block model from this study incorporates both far-field constraints and near-field constraints. The Euler pole describing the relative motion of the Arabian and Sinai plates is  $34.51 \pm 3.2^\circ\text{N}$ ,  $31.25 \pm 4.5^\circ\text{E}$ ,  $0.52 \pm 0.045^\circ/\text{yr}$ . We prefer block-model based estimates to other recent estimates of Arabia-Sinai Euler poles based on geologic slip rates [e.g., Klinger et al., 2000a; Le Beon et al., 2010] or 1-D dislocation models [e.g., Le Beon et al., 2008; Wdowinski et al., 2004]; such models are predicated on the assumption that all plate motion is parallel to the transform and, therefore, the southern DSF traces the arc of a great circle about the Euler Pole. In contrast, 2-D models permit plate motion both parallel and orthogonal to boundaries and provide more robust estimation of an Euler pole. In general, far-field locations should provide sufficient control of plate motion, barring internal deformation. Although located slightly farther north and east of the pole of Reilinger et al. [2006], the poles overlap considerably within the uncertainties.

[38] The block model also permits revisiting the “leaky” transform hypothesis for the DSF. Some transform-orthogonal extension is suggested for the Wadi Araba section of the DSF, but the best fitting block models suggest no transtension along the Jordan Valley. The small amount of opening along the Wadi Araba Fault (6–17% of the strike-slip rate) is similar to the relative magnitudes of opening and strike-slip used by Devès et al. [2011] to model first-order topography along the southern DSF, and by Smit et al. [2010] who applied analog modeling to approximate overall basin structure. This suggests that GPS-derived kinematics may reflect the long-term, late Cenozoic behavior of the Dead Sea Fault. This is further supported by recent studies suggest that the Dead Sea basin may have evolved primarily by increasing strike-slip displacement [Garfunkel and Ben-Avraham, 2001]. Hence, the leaky (i.e., transtensional) nature of the southern DSF appears to be relatively confined to the Wadi Araba Fault.

[39] Late Quaternary estimates of slip rates published during the past decade vary between 2–6 mm/yr [e.g., Le Beon et al., 2010; Makovsky et al., 2008; Ferry et al., 2007; Niemi et al., 2001; Klinger et al., 2000a]. The slip rates based on elastic modeling of our GPS results are generally consistent with the upper range of these neotectonic estimates. This suggests that the elastic model approximations are probably sufficient to model the GPS velocities along the DSF. Furthermore, if modified, visco-elastic models [e.g., Savage and Prescott, 1978] are considered, the congruence of slip rate estimates based on elastic models and geologic estimates implies that the lower crustal viscous relaxation time is greater than the  $\sim 1,100$  year average recurrence period for the southern DSF. A long relaxation time suggests the possibility of a relatively high viscosity lower crust, which may be consistent with lower crustal seismicity [e.g., Shamir, 2006; Aldersons et al., 2003]. The lower crust may be sufficiently viscous that shear remains confined to a relatively narrow zone. Integrated geophysical observations of the southern DSF [Weber et al., 2009] suggest that the transform cuts through the mantle lithosphere as a narrow, subvertical zone. That observation, along with the congruence of elastic models and neotectonic slip rates, are consistent with a ‘Deep-Slip’ model for interseismic strain accumulation, in which crustal faults are loaded by slip in the lower crust and mantle lithosphere [Scholz, 2002].

### 5.2. Fault Segmentation and Lithospheric Heterogeneity

[40] As noted above, the block model suggests along-strike variation in the effective locking depth along the southern Dead Sea Fault. Although effective locking depth is not necessarily the true depth of fault locking within the crust (the abrupt transition from locking to slipping is not generally realistic), it nonetheless represents the total rate of elastic strain and moment accumulation along a fault. Apparent variations in effective locking depth along the southern DSF may exemplify different seismogenic character of the two major segments. These locking depths also approximate two concentrations in crustal seismicity located by Shamir [2006] at 10 and 16 km, respectively. Further, differences in seismic behavior between the WAF and JVF are suggested by assessment of the magnitude-frequency scaling by Al-Homoud [2003], who reported b-values of 0.89 and 0.77 for the JVF and WAF, respectively, although confidence limits are not reported from that study.



[41] These apparent seismogenic variations correspond with aforementioned variations in lithospheric structure beneath the DSF. As suggested by studies of regional seismic wave velocities and attenuation [Bao *et al.*, 2011; Al-Lazki *et al.*, 2004; Al-Damegh *et al.*, 2004], the uppermost mantle (i.e., the mantle lithosphere) beneath the JVF and Dead Sea basin may be warmer and/or thinner than the mantle lithosphere beneath the WAF. Additionally, variations in long-term lithospheric strength may also correspond with segmentation of the southern DSF. For example, Götze *et al.* [2007] documented variations in long-term, flexural rigidity (effective elastic thickness) along the southern DSF consistent with inferred seismogenic segmentation. Those authors found weaker elastic lithosphere around the Dead Sea (and areas northward) compared with the Wadi Araba region. Hence, shallower depths of fault locking appear to be associated with warmer mantle lithosphere along the southern DSF.

[42] For comparison with another continental transform, spatial variations in effective locking depth have also been documented along the southern San Andreas Fault, where a systematic analysis of effective locking depths as been recently published by Smith-Konter *et al.* [2011]. An overall trend of decreasing locking depth is observed from the southern San Andreas and San Jacinto faults (locking depths of 16–21 km depth) southward toward the Salton Trough where fault locking is 10–12 km, and shallower, still for the Imperial Valley Fault with 3–9 km locking depths. Although the uncertainties for individual fault segments may be relatively large (e.g., along the San Andreas Fault near Palm Springs), the general southward decrease in effective locking depth appears to be robust. Furthermore, this pattern of locking depth variability is consistent with results from other studies applying block models to analyze interseismic strain in southern California [e.g., Loveless and Meade, 2011; Meade and Hager, 2005], as well as recent modeling spatial variability of elastic rigidity based on geodetic data [Chéry *et al.*, 2011].

[43] Similar to the DSF, the shallower depths of effective fault locking depths are generally associated with regions of anomalously slow and attenuating mantle lithosphere (i.e., warm and/or thin upper mantle) [e.g., Buehler and Shearer, 2010; Hearn, 1996; Lawrence and Prieto, 2011]. Seismic tomography of P wave and S wave velocities as shallow a 60 km indicate a thinned mantle lid and  $V_p/V_s$  ratios suggest partial melt at these depths beneath the shallowest locking depths in the Salton

Trough [Schmandt and Humphreys, 2010]. In the case of the southern San Andreas Fault, warmer upper mantle (and thinner lithosphere) is related to proto-oceanic rifting at the northern end of the Gulf of California [e.g., Lachenbruch *et al.*, 1985].

[44] The examples of the Dead Sea Fault and San Andreas Fault suggest that thermal structure of the upper most mantle may, in part, influence faulting locking in the upper crust. Thermomechanical models have been applied to relate seismicity to lithospheric structure and thermal state [e.g., Miller and Furlong, 1988], and depths of seismicity are often linked to fault locking depths [e.g., Smith-Konter *et al.*, 2011]. In simplified models of crustal strength, the depth of fault locking may generally correspond with the transition from brittle to ductile failure [e.g., Scholz, 2002; Sibson, 1982]. However, a direct link between lithospheric structure and effective fault locking depth has not been explored, likely due, in part, to broad ranges on the uncertainties in fault locking depths. We suggest that, with improved resolution of effective fault locking depths, such as those reported herein, such a link may be assessed. As discussed by Miller and Furlong [1988], spatial variations in seismic behavior can be controlled by thermal state, regional stress magnitude, strain rate, and lithology. The southern DSF is a long-lived (18+ m.y.), lithospheric structure that cuts the entire crust [e.g., Weber *et al.*, 2009]; for such “mature” faults, the primary factor influencing seismicity is generally the thermal state of the lithosphere [e.g., Miller and Furlong, 1988]. The thermal structure of the upper mantle beneath the DSF, as imaged seismologically, is consistent with this.

[45] First-order segmentation of the southern DSF corresponds with the Dead Sea basin, a feature that developed with the Middle Miocene initiation of the transform [Garfunkel and Ben-Avraham, 2001; Ben-Avraham *et al.*, 2008]. Therefore, segmentation of the southern DSF predates the upper mantle thermal anomaly and is more probably due to factors such as inherited crustal structure [e.g., Weber *et al.*, 2009], rather than a result of the thermal anomaly. Superposition of the present thermal structure, perhaps by a mantle plume onto this segmented transform results in segments with different seismogenic characteristics, as expressed by variation in fault moment accumulation.

## 6. Conclusions

[46] New GPS measurements from Jordan, combined with other regional data, provide a compre-

hensive view of present-day, near-field deformation associated with the southern Dead Sea Fault (DSF). The results demonstrate that slip rates of 4.4–5.2 mm/yr are conserved between the Wadi Araba and Jordan Valley faults across the Dead Sea basin. Additionally, the GPS velocities suggest minimal extension perpendicular to the transform (i.e., transtension) and suggest that the Carmel Fault does not transfer significant plate motion from the DSF.

[47] The model-derived slip rates are generally consistent with the upper end of recently reported estimates based on offset, Late Quaternary landforms. This consistency of short-term and long-term slip rate estimates suggests that the slip rate has not varied over time. Similarity of GPS-based and long-term slip rates may further suggest that the lower crust has a relatively high viscosity, if modified visco-elastic models of faulting are considered.

[48] Elastic block modeling of GPS velocities suggests along-strike variations in effective fault locking depth along the DSF that correspond with heterogeneity in the mantle lid. Although other factors may be at work, the correlation with uppermost mantle seismic anomalies suggests that, in the case of the southern DSF, first-order variations in seismic moment accumulation may be influenced by the thermal state of the uppermost mantle.

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