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# Infrared emission spectroscopy of CO<sub>2</sub> at high temperature. Part I: Experimental setup and source characterization

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## Abstract

An experimental setup is developed to analyze infrared emission of CO<sub>2</sub> plasmas at atmospheric pressure and temperatures up to 5000 K. A microwave discharge is used to produce the hot gas mixture and emission is recorded by a Fourier transform spectrometer with a spectral resolution between 0.01 and 0.1 cm<sup>-1</sup>. The plasma is confined inside quartz or sapphire tubes which perturb the measurements through refraction, reflection, absorption and emission. We present in this part the experimental setup, an analysis of tube effects, and the characterization of the plasma in terms of temperature and molar fraction distributions using CO emission in the overtone vibrational bands  $\Delta v=2$ . Analysis of the measurements of CO<sub>2</sub> emission in the 2.7  $\mu\text{m}$  and 4.3  $\mu\text{m}$  regions, and comparisons with calculations using different spectroscopic databases are given in the companion paper.

*Keywords:* FTIR emission spectroscopy, microwave plasma source,

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## 1. Introduction

The knowledge of very high temperature absorption and emission spectra of CO<sub>2</sub> remains a challenge for radiative transfer in applications such as combustion and planetary atmospheric entry. Simulations for heated CO<sub>2</sub>-N<sub>2</sub> mixtures at equilibrium have shown for instance that the IR emission of the CO<sub>2</sub> molecule remains predominant at temperatures as high as 4000 K [1].

Several experimental studies have been devoted to this molecule during the last fifty years. We describe in the following high temperature measurements and try to classify them according to the confinement of the absorbing or emitting gas in tight cells, flows inside heated cells or the use of combustion products.

Tight cells enable accurate measurements with well controlled temperature, pressure and mixture composition. The achievable temperatures are however limited to about 1000 K due to the soldering of the optical windows with the cell or the thermal tolerance of O-rings. Low spectral resolution absorption measurements with tight cells and grating spectrometers were undertaken for instance by Levi Di Leon and Taine [2] at temperatures up to 850 K. Diode laser absorption experiments enable very high spectral resolution but only cover limited spectral ranges. Rosenmann et al [3, 4] have performed such measurements in the 4.3  $\mu\text{m}$  region up to 800 K, and Michalcea et al [5] investigated the 2  $\mu\text{m}$  region in order to determine the most suitable absorption lines to be used as a diagnostic tool in combustion applications. André et al [6] have measured CO<sub>2</sub> absorption spectra in the range

3700–3750  $\text{cm}^{-1}$  using high resolution Fourier transform infrared (FTIR) spectroscopy and optical paths of about 2 m up to 700 K. Lower spectral resolution FTIR measurements were performed by Parker et al [7] around 12  $\mu\text{m}$  up to 800 K and by Medvecz et al [8] who measured absorption spectra of CO/CO<sub>2</sub>/N<sub>2</sub> mixtures up to 1250 K in the 4.3  $\mu\text{m}$  region. Phillips [9] has also performed FTIR measurements in the 4.3  $\mu\text{m}$  region up to 1000 K with 0.06  $\text{cm}^{-1}$  spectral resolution and has derived band model parameters from the experimental data.

Higher temperatures can be obtained using heated leaky cells inside furnaces and flowing gas mixtures. This technique enabled absorption measurements with grating spectrometers up to 1500 K in the 2.7 and 4.3  $\mu\text{m}$  regions at different pressures and optical paths [10, 11]. Such absorption cells were also used in Refs. [12, 13] in association with moderate resolution FTIR spectroscopy up to 1273 and 1373 K respectively.

In more recent studies, Modest and Bharadwaj [14] and Bharadwaj and Modest [15] developed a drop tube technique which enabled FTIR measurements at 4  $\text{cm}^{-1}$  spectral resolution up to 1550 K. They studied the 2, 2.7 and 4.3  $\mu\text{m}$  regions and compared their measurements with several spectroscopic data bases and statistical narrow-band data. The temperature gradients close to the tube end had apparently no significant effects.

Experiments through combustion products enable to reach higher temperatures but are also affected by uncertainties resulting from the partial knowledge of temperature and composition distributions, and boundary effects. Different authors have attempted to produce quasi two dimensional flames to reduce boundary layer effects [16, 17].

Pioneering studies were conducted by Ferriso and Ferriso et al [18, 19] who used a supersonic kerosene-oxygen burner at stoichiometric composition, and a Foelsch-type nozzle to avoid shock waves and to produce a quasi uniform cone at the exit of the divergent. The mixture temperature was measured by the emission/absorption technique and the composition was calculated at chemical equilibrium. Absorption spectra were recorded at  $4\text{ cm}^{-1}$  spectral resolution in the  $4.3\text{ }\mu\text{m}$  region for temperatures up to 3000 K. A similar study was conducted by Coppalle and Vervich [20] who measured low spectral resolution absorption spectra of a methane-oxygen flame at temperatures up to 2900 K in the  $4.3\text{ }\mu\text{m}$ . Diode laser absorption measurements of a  $\text{C}_2\text{H}_4$ -air flame have been carried out by Webber et al [21] in the  $2\text{ }\mu\text{m}$  region. Selected spectral lines were used in this last study to measure the temperature and CO,  $\text{CO}_2$  and  $\text{H}_2\text{O}$  molar fractions.

The aim of the present study is to measure emission spectra from gases produced by a microwave discharge which enables to reach temperatures as high as 6000 K. Particular attention is given to  $\text{CO}_2$  emission in the  $2.7$  and  $4.3\text{ }\mu\text{m}$  regions at temperatures never reached before and at high to medium spectral resolution. The microwave discharge through a  $\text{CO}_2$  flow at atmospheric pressure produces a mixture close to local thermodynamic equilibrium (LTE) containing mainly  $\text{CO}_2$ , CO,  $\text{O}_2$ ,  $\text{C}_2$  and atomic O species. The emission of CO in the ground electronic state in the range  $3800\text{-}4400\text{ cm}^{-1}$  allows accurate determination of the radial temperature distribution in the hot parts of the plasma. Local  $\text{CO}_2$  emission coefficients or line of sight integrated emission intensities can thus be determined and compared to predictions from spectroscopic databases to study their validity at elevated

temperatures. We present in this part the experimental setup (section 2) and analyze the effects of confinement tubes on plasma emission spectra (section 3). The plasma characterization using CO emission is then presented in section 4.

## 2. Experimental setup

[Figure 1 about here.]

The experimental setup shown on Fig. 1 is aimed at producing and analyzing stable plasma flows at high temperature, atmospheric pressure and local thermodynamic equilibrium for different gas mixtures. It is composed of a microwave plasma torch (MPT) which is coupled to an IR Fourier transform spectrometer.

Two different MPT systems were used. The first one (3 kW maximum power) has been originally designed by LITMAS company and the second one (6 kW) by SAIREM company. For both systems, microwaves are generated by a magnetron at 2.45 GHz frequency, pass through an isolator, and then a wave-guide. A triple-head impedance tuner, positioned between the isolator and the plasma cavity, allows to match the impedance in order to decrease the amount of reflected power to less than 1% of the forwarded power. Adjustment of this tuner is necessary from one experiment to the other as the impedance of the plasma cavity changes with the plasma operating conditions.

The plasma cavity, designed for the purpose of this study, is composed of a WR 340-type aluminum rectangular waveguide, hollowed across its axis to hold a vertical confinement tube of 45 mm outer diameter and 2.5 mm wall

thickness. The position of the tube within the plasma cavity was calculated so that the electric field of the microwaves is maximum at the center of the tube without plasma. The tangential injection of the gas at the bottom of the cavity produces a swirled gas flow which stabilizes the plasma in the tube center and avoids tube overheating. The plasma produced at atmospheric pressure by this type of devices was analyzed in a previous work using visible and UV emission spectroscopy, and the medium was shown to be very close to thermal and chemical local equilibrium, at least in the central region of the plasma [22, 23]. The first attempt to measure CO<sub>2</sub> emission in the 2.7 μm region is also described in Ref. [23] where the optical path was not under vacuum.

The line of sight integrated emission spectra are recorded in the IR range using a high resolution Fourier transform infrared spectrometer (DA8, BOMEM company). The spectrometer is equipped with a CaF<sub>2</sub> beam splitter and a liquid nitrogen cooled InSb detector which allow measurements in the near and mid-infrared parts of the spectrum (above 1800 cm<sup>-1</sup>) at a resolution as high as 4.10<sup>-3</sup> cm<sup>-1</sup>. The spectrometer is under vacuum to prevent absorption by CO<sub>2</sub> and H<sub>2</sub>O in ambient air, and the optical path between the MPT and the spectrometer is also under vacuum as shown in Fig. 1. A nitrogen purged cavity is placed around the confinement tube in order to avoid residual absorption outside the tube. This last cavity is made of a refractory material which can operate at high temperature and do not perturb microwave propagation. The spectrometer optical axis is at a height  $h$  above the exit of the waveguide; studying the plasma at different horizontal sections defined by the height  $h$  allows us to explore different tem-

perature profiles and temperature levels since the plasma is cooled down by heat transfer phenomena as  $h$  increases.

The emission spectra are calibrated using the emission of a blackbody radiation source (Landcal company R1200P) at about 900 K with  $\pm 3$  K uncertainty. The spatial resolution in the radial direction is determined by the diameter of the pinhole placed in front of the InSb detector (0.5 mm) and from the CaF<sub>2</sub> collection lens magnification factor (0.25). This leads to a spatial resolution of about 2 mm. The emission spectra are recorded at different radial positions by moving the microwave plasma torch with a step of 0.5 mm.

The procedure to extract local emission coefficients from line of sight integrated emission intensities, when the medium can be assumed to be optically thin, is based on the classical Abel inversion. The axisymmetry of the calibrated spectra has been checked and a spatial Butterworth-based filter is applied to the intensity curves for each wavenumber. Details on data processing are given in Appendix A. This leads to local absolute emission coefficients (in  $\text{W}\cdot\text{m}^{-3}\cdot\text{sr}^{-1}\cdot(\text{cm}^{-1})^{-1}$ ) in the optically thin regions.

### **3. Refraction, reflection, absorption and emission by the tube**

Plasma confinement inside a quartz or sapphire tube is necessary for the stability of the flow and to avoid diffusion and convection mixing with the outer gaseous medium. However, the tube affects direct measurement of the intensity emitted by the plasma through refraction, reflection, absorption and emission phenomena. The measured temperature on the external wall of the tube reaches 800 K and its own emission is not negligible. The aim of this



section is to analyze these effects and to determine an accurate procedure for measurement correction when possible. We assume in the following that the plasma and the tube are perfectly axisymmetric and that tube interfaces are smooth so that refraction and reflection can be described by Fresnel's equations. The tube has an internal diameter  $R_1=20$  mm and an external one  $R_2=22.5$  mm.

### 3.1. Refraction effects

We denote by  $y$  the distance between the optical axis of the spectrometer and the line parallel to this axis and crossing the tube center (see Fig. 2), and by  $y'$  the distance between the tube axis (point  $O$ ) and the optical path inside the tube that is conjugated with the spectrometer axis through the tube.

[Figure 2 about here.]

Elementary geometrical calculations, using Fresnel's equations, are reported in Appendix B and lead simply to  $y' = y$ . This important result shows that refraction by quartz or sapphire tubes leads to a deviation of the optical axis but that the optical path associated to the spectrometer axis is not affected by this phenomenon as long as the system can be considered as axisymmetric. Thus, there is no correction to perform in Abel inversion due to refraction. The tube acts however as a slightly divergent lens but this effect, which could affect the spatial resolution of the measurements is neglected in the following.

### 3.2. Tube reflection, absorption and emission effects

#### 3.2.1. Optical properties of quartz and sapphire

We have measured the transmissivity curves of half-tubes made of quartz and sapphire at room temperature, and the emission curves of the tubes in the plasma operating conditions, just after the extinction of the plasma after each experiment. The last measurements were done at  $4 \text{ cm}^{-1}$  spectral resolution to enable fast recording of the spectra before a significant decrease of tube temperature. Examples of these measurements are shown on Fig. 3 for transmission and on Fig. 4 for emission. On this last figure, plasma emission is also presented for comparison. Figure 3 shows also the theoretical normal transmittance, accounting for reflection, but not for absorption, as computed from

$$T_\sigma = \frac{1 - \rho_\sigma(\theta = 0)}{1 + \rho_\sigma(\theta = 0)}, \quad \text{and} \quad \rho_\sigma(\theta = 0) = \left( \frac{n_\sigma - 1}{n_\sigma + 1} \right)^2, \quad (1)$$

where  $\rho_\sigma(\theta = 0)$  is the interface normal relectivity, and from the values of the real part of the refractive index  $n_\sigma$ , calculated from the Sellmeier-type dispersion relation

$$n_\lambda^2 - 1 = \frac{B_1 \lambda^2}{\lambda^2 - C_1} + \frac{B_2 \lambda^2}{\lambda^2 - C_2} + \frac{B_3 \lambda^2}{\lambda^2 - C_3}, \quad (2)$$

with the constants given in Table C.1.

Figure 3 shows first a good agreement between theoretical and measured transmittances in the transparency regions of quartz and sapphire. It shows also that absorption by the tubes occurs below  $3700 \text{ cm}^{-1}$  for quartz and  $2500 \text{ cm}^{-1}$  for sapphire. This is in agreement with the spectra of the absorption index that may be found in Refs. [24] and [25] for instance, and with

the present tube emission measurements shown on Fig. 4. Thus, the effects of tube reflection, absorption and emission must be taken into account to correct plasma emission measurements.

[Table 1 about here.]

[Figure 3 about here.]

[Figure 4 about here.]

Moreover, it is well known that sapphire absorption coefficient increases with temperature (see e.g. Ref. [25]). We have thus measured the absorption spectrum of the whole sapphire tube just after plasma extinction, using a globar as emission source, and extracted from this measurement, and from the theoretical values of the refractive index, the transmissivity of a half-tube. The result shown on Fig. 5 indicates clearly the strong variation of tube transmissivity with tube temperature. Half-tube transmissivity in the operating conditions will be considered for the analysis of the  $4.3 \mu\text{m}$   $\text{CO}_2$  region.

[Figure 5 about here.]

### *3.2.2. Relation between measured intensity, tube emitted intensity, and plasma emitted intensity*

In order to establish the relation between these different intensities, we assume a perfectly axisymmetric geometry, which yields, in association with Fresnel's equations, remarkable symmetry properties for multiple reflection

phenomena. Calculation details are given in Appendix C and the general result, accounting for both components of radiation polarization, is

$$I^{tr} = a I_p^e + b I_t^e, \quad (3)$$

where  $I^{tr}$  is the measured intensity,  $I_p^e$  and  $I_t^e$  are the intensities emitted by the plasma column and the tube column, and the constants  $a$  and  $b$  are given by:

$$a = \frac{\tau_t(1 - \rho_t)(1 - \rho_p)}{1 - \tau_p[\rho_p + \rho_t\tau_t^2(1 - \rho_p)^2]}, \quad b = \frac{(1 - \rho_t)[1 - \tau_p\rho_p + \tau_t\tau_p(1 - \rho_p)^2]}{1 - \tau_p[\rho_p + \rho_t\tau_t^2(1 - \rho_p)^2]}, \quad (4)$$

with the notations given in Appendix C.

Different scenarios can occur depending on the spectral region and the nature of the confinement tube. If the plasma is optically thin ( $\tau_p \simeq 1$ ), which is the case for CO<sub>2</sub> emission in the 2.7  $\mu\text{m}$  region and for CO overtone bands characterized by  $\Delta v=2$ , and if the tube can be assumed to be transparent ( $\tau_t \simeq 1$ ,  $I_t^e \simeq 0$ ,  $\rho \neq 0$ ), Eqs. 3 and 4 reduce to:

$$I^{tr} = \frac{(1 - \rho_t)}{1 - \rho_t(1 - \rho_p)} I_p^e. \quad (5)$$

The measured intensity  $I^{tr}$  is then equal, to the second order in the reflectivity  $\rho_t$  or  $\rho_p$ , to the intensity emitted by the plasma column. This is easily explained by the fact that the losses by reflection at the tube interfaces are compensated by the intensity emitted by plasma columns symmetrical to the considered column, and reflected by the tube towards the detector. Figure 6 shows that for  $\tau_p \simeq 1$  and  $\tau_t \simeq 1$ , the factor  $a = \frac{1}{2}(a_{\parallel} + a_{\perp})$  remains very close to 1 and the difference is smaller than 0.005 for  $y < 19$  mm. This is the reason why the calibration of the intensity with a blackbody source is done without tube.

For an optically thin plasma ( $\tau_p \simeq 1$ ) but a partially absorbing tube ( $\tau_t \neq 1$ ) as for the quartz tube near  $3700 \text{ cm}^{-1}$ , Figure 6 shows that the factor  $a$  is very close to  $\tau_t$  (differences limited to 2% for  $y < 18 \text{ mm}$ ) and a simple division of the measured intensity by the half-tube transmissivity yields an accurate correction. When the plasma can no longer be considered as optically thin (case of  $\text{CO}_2$  in the  $4.3 \text{ }\mu\text{m}$  region), reflections by the tube are not compensated by other internal reflections and Fig. 6 shows that, for  $\tau_p=0.1$  for instance, the error introduced by the simple division of  $I^{tr}$  by  $\tau_t$  leads to an underestimation of the plasma intensity by about 13% at  $y=0$ . Measurements of  $\text{CO}_2$  emission in the  $4.3 \text{ }\mu\text{m}$  region should then be corrected to account for self-absorption. But as the plasma spectral optical thickness is not determined experimentally, this phenomenon will introduce an important source of uncertainty in this spectral region.

[Figure 6 about here.]

Finally, Fig. 4 and Eqs. 3 and 4 show that emission from the tube should be subtracted from the measured intensity to adjust the signal background. This simple subtraction is rigorous when the plasma is optically thin ( $\tau_p \simeq 1$ ) since the measured tube emission is the same with and without plasma, as long as this measurement is carried out very quickly after plasma extinction. A further correction is required again in the  $4.3 \text{ }\mu\text{m}$  region where the plasma is not optically thin. Figure 4 shows however that sapphire emission remains small in comparison with the maximum level of  $\text{CO}_2$  emission.

To summarize the above analysis of tube effects, we have shown that refraction effects can be neglected in data processing and put forward the following corrections concerning reflection, emission and absorption:

- When the plasma is optically relatively thin ( $2.7 \mu\text{m}$  region and CO emission in the range  $3800 < \sigma < 4400 \text{ cm}^{-1}$ ), reflections of the plasma emitted intensity are compensated by other internal reflections and the intensity calibration must be carried out without tube.
- In the same spectral regions, no further corrections are required for sapphire tubes, while the measured intensity should be divided by the half-tube measured transmissivity  $\tau_t$  for quartz tubes.
- tube emission is systematically subtracted from the measured intensity.

The main source of uncertainty due to the confinement tubes results from reflection effects and high plasma optical thickness in the  $4.3 \mu\text{m}$  region. These phenomena may lead to an underestimation of the measured plasma intensity by about 15%.

#### 4. Source characterization

At a given height  $h$  above the exit of the microwave cavity, the temperature profile  $T(r, h)$  was determined from CO emission in the  $4000\text{--}4400 \text{ cm}^{-1}$  region. As shown on Fig. 7, CO overtone bands corresponding to  $\Delta v = v' - v'' = 2$  are well isolated and the emission signal obviously contains significant contributions from hot bands, up to  $v' = 8$  or  $9$ , which insures a good sensitivity to the temperature. After calibration and Abel inversion, several techniques can be used to extract the temperature from the local emission spectrum (see e.g. [17]). The Boltzmann method, or the ratio of two selected line intensities is very sensitive to the background continuum, to line overlapping, and to line shapes and broadening parameters. We use

here a least square adjustment between normalized theoretical spectra and experimental ones to determine the local temperature. In order to avoid the knowledge of CO partial pressure, the measured local emission spectrum, deduced from Abel inversion, is normalized by dividing it by its maximum value, and then compared to normalized theoretical spectra calculated at different temperatures. Comparisons of the absolute levels of the spectra are used afterwards to check the chemical equilibrium hypothesis.

[Figure 7 about here.]

Theoretical line by line calculations of CO spectra, carried out with  $0.01 \text{ cm}^{-1}$  spectral resolution, are based on line intensities calculated by Chackerian and Tipping [26] and line positions deduced from the Dunham coefficients given in Ref. [27]. Collisional line broadening coefficients are taken from Ref. [28] for different collision partners. The simple harmonic oscillator (with  $w=2143.27 \text{ cm}^{-1}$ ) and rigid rotor model is used for the calculation of the internal partition sum of CO, and is found in very good agreement with direct summation calculations (see e.g. [29, 30]) with differences less than 3% for temperatures up to 7000 K. We have also checked that line positions and intensities agree well (typically within less than  $0.003 \text{ cm}^{-1}$  for positions and 2% for intensities) with the HITRAN data [31] for the cold lines belonging to this last data base, and with HITEMP data [32] with the same accuracy.

In order to avoid important differences between theoretical and experimental spectra resulting from different line shapes and from FTIR apparatus function, both spectra are convolved with a triangular function of  $0.8 \text{ cm}^{-1}$  spectral resolution at the triangle base before the least square adjustment.

Examples of measured and theoretical CO overtone spectra, calculated at the temperature yielding the least square difference, are shown in Fig. 8 for a height above the plasma cavity  $h=6$  mm and for different radii. The plasma is confined in a quartz tube in this example. The agreement is very good in the central regions with differences limited to a few percents of the maximum signal. At the center of the plasma, the measured temperature is about 5475 K and band heads up to  $v'=8$  are clearly identified. Higher differences are observed in the outer regions of the plasma where CO emission becomes weak. However, the difference between calculated and measured normalized emission coefficients do not present a spectral structure, correlated with the emission coefficient itself, which indicates that the medium is very close to local thermodynamic equilibrium with a single temperature Boltzmann distribution of vibrational and rotational CO levels.

[Figure 8 about here.]

In order to check chemical equilibrium, we compare in the following the absolute levels of the measured and calculated emission coefficients. The latter require however the knowledge of CO molar fraction. Assuming local chemical and thermodynamic equilibrium at the measured temperature, the local composition of the medium is computed by solving the law of mass action for dissociation (Guldberg-Waage equation) and for ionization (Saha equation) reactions, together with electrical neutrality, the perfect gas law and the total conservation of the nuclei [1, 29]. The retained chemical species for CO<sub>2</sub> plasmas are CO<sub>2</sub>, CO, O<sub>2</sub>, C<sub>2</sub>, C, O, C<sup>+</sup>, O<sup>+</sup>, CO<sup>+</sup> and e<sup>-</sup>. Figure 9 shows the computed composition in the temperature range of interest. CO



molar fraction becomes less than 0.01 for  $T < 1600$  K and CO emission is expected to be very low on the periphery of the plasma.

[Figure 9 about here.]

Comparisons between absolute levels of local emission coefficients are given in Fig. 10 for the same experiment as in Fig.8. Here again, a good agreement is observed in the central region of the plasma indicating the reliability of temperature measurement and of chemical equilibrium assumption. For  $r=10$  and  $r=15$  mm, the calculated emission level is smaller than the experimental one with typical differences of about 15% and 30% respectively. As displayed in Fig.9, CO molar fraction is very sensitive to the temperature in the 2000–2500 K range. If we assume chemical equilibrium and use the absolute emission spectrum to adjust the local temperature, we find for instance 2567 K instead of 2525 K for  $r=10$  mm and 2150 K instead of 2075 K for  $r=15$  mm. The spectral structure of the residual in this last adjustment becomes however more pronounced. So, a plausible explanation of the differences observed on the borders of the plasma is a departure from chemical equilibrium. CO concentration is however very small in these regions and does not affect significantly  $\text{CO}_2$  concentration. Indeed, the experimental CO emission spectrum is about one hundred times smaller at  $r=15$  mm than at the plasma center.

[Figure 10 about here.]

Figure 11 displays typical temperature profiles determined from the normalized and from the absolute CO emission spectra with a confinement tube in

quartz and at the height  $h=6$  mm. At this height, the very high temperature narrow central region shown in the figure is confirmed visually by the high luminosity of this region in the visible range. As CO concentration becomes too small on the boundaries ( $r > 15$  mm), its emission signal becomes very weak and unusable to determine the temperature. The temperature profile is thus extrapolated in these regions by using the last reliable measurement point using CO spectra and wall temperature. The latter has been measured at the external tube wall by a contact K-type thermocouple and was found in the range  $800 \pm 50$  K for the heights  $h$  considered here. Two types of extrapolations were assumed, a simple linear one, and a smooth one preserving the temperature derivative at the last measurement points. These extrapolations are also shown on Fig. 11. The uncertainty on the temperature profile, especially in the borders of the plasma, will constitute the most important source of uncertainties in this experimental study and will be accounted for when comparing experimental and theoretical CO<sub>2</sub> spectra.

[Figure 11 about here.]

Finally, we have compared the measured CO intensities (in absolute levels and without Abel inversion) to the calculated intensities obtained by solving the radiative transfer equation along a ray at different distances  $y$  from the plasma axis. The results are plotted in Fig. 12 using both temperature profiles deduced from normalized and absolute CO emission coefficient. The intensities are plotted on Fig. 12 for the central chord ( $y=0$ ) and for  $y=5$  and  $y=10$  mm. They are not sensitive to temperature extrapolation since CO concentration vanishes at the periphery. A good agreement is obtained

between these intensities with, as may be expected, a better agreement for the external chords when the temperature profile deduced from absolute levels of CO emission coefficient is used.

[Figure 12 about here.]

## 5. Summary

An original setup was developed to measure IR emission spectra of gas mixtures at temperatures up to 6000 K. It includes a microwave discharge in a flowing gas, CO<sub>2</sub> in the present study, and a high resolution FTIR spectrometer under vacuum.

The optical effects due to the confinement of the gas mixture inside quartz or sapphire tubes were discussed in detail. The analysis and tube transmittance measurements showed that refraction effects may be neglected and that reflection on smooth tube surfaces and absorption by the tube can be accurately taken into account in the spectral regions where the gas mixture is optically thin. Significant uncertainties remain however when the medium is optically thick like for CO<sub>2</sub> in the 4.3  $\mu\text{m}$  region.

For CO<sub>2</sub> plasma, the temperature radial distribution was determined from CO emission in the 4000–4400  $\text{cm}^{-1}$  spectral range. A least square adjustment between normalized calculated and Abel inverted experimental emission coefficients yielded accurate determination in the central regions of the mixture. In the same regions, the absolute levels of CO local emission confirmed that the atmospheric plasma is at local chemical and thermodynamic equilibrium. However, due to very low CO concentration in the relatively cold

outer regions, the temperature profile had to be extrapolated in these regions. The uncertainties resulting from this extrapolation will be accounted for in the comparisons between theoretical and experimental CO<sub>2</sub> emission spectra presented in the companion paper.

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## Appendix A. Data processing and Abel inversion

We briefly describe in this appendix the data processing algorithm that enables to transform line of sight integrated intensities of CO overtone emission to local emission coefficients through Abel inversion. This procedure was first developed in Ref. [33] where more details may be found .

If the plasma can be considered as axisymmetric and optically thin for a given wavenumber  $\sigma$ , the measured intensity  $I_\sigma(y)$  at a distance  $y$  from the plasma center is given by:

$$I_\sigma(y) = 2 \int_y^{R_p} J_\sigma(r) \frac{r dr}{\sqrt{r^2 - y^2}} \quad (\text{A.1})$$

where  $J_\sigma(r)$  is the local emission coefficient (in  $W.m^{-3}.sr^{-1}.(cm^{-1})^{-1}$ ) at radius  $r$  and  $R_p$  is the plasma total radius. The emission coefficient is retrieved by the Abel inversion formula:

$$J_\sigma(r) = -\frac{1}{\pi} \int_r^{R_p} \frac{dI_\sigma(y)}{dy} \frac{dy}{\sqrt{y^2 - r^2}}. \quad (\text{A.2})$$

In practice, measurements are carried out with a spatial step  $\Delta y = 0.5$  cm on both sides of the plasma center. The signal is then made symmetrical by finding the local extremum corresponding to the plasma center and by averaging the values at equal distances from this center. A Butterworth filter is then applied to eliminate experimental noise, especially at the plasma borders. The transfer function of this filter is given by:

$$|H(\omega)|^2 = \frac{1}{1 + (\frac{\omega}{\omega_c})^{2n}}, \quad (\text{A.3})$$

where the cutoff frequency  $\omega_c$  was taken equal to 0.4 and the filter order  $n$  was fixed to 2. The axisymmetric and filtered signal was then Abel-inverted

for each wavenumber using a cubic spline method. A local third order polynomial is used to extrapolate the signal between each couple of adjacent measurement points using the continuity of the polynomials and of their derivatives. Abel inversion reduces then to the calculations of integrals of the form:

$$Q_k(\alpha, \beta) = \int_{\alpha}^{\beta} \frac{y^k}{\sqrt{y^2 - \alpha^2}} dy, \quad k \leq 2, \quad 0 \leq \alpha \leq \beta \leq R_p \quad (\text{A.4})$$

These integrals have the analytical expressions:

$$\left\{ \begin{array}{l} Q_0(\alpha, \beta) = \ln \left( \frac{\beta}{\alpha} + \sqrt{\left(\frac{\beta}{\alpha}\right)^2 - 1} \right) \\ Q_1(\alpha, \beta) = \sqrt{\beta^2 - \alpha^2} \\ Q_2(\alpha, \beta) = \frac{\alpha^2}{2} Q_0(\alpha, \beta) + \frac{\beta}{2} Q_1(\alpha, \beta) \end{array} \right. \quad (\text{A.5})$$

## Appendix B. Refraction effects

The different angles  $\theta_1$  to  $\theta_4$ , involved in the following are defined in Fig. 2. If we assume that the indices of refraction of the plasma and of the outer medium are equal to 1, and denote by  $n$  the refraction index of the tube we have

$$\sin\theta_3 = \frac{y}{R_2}; \quad \sin\theta'_2 = \frac{\sin\theta_3}{n} = \frac{y}{nR_2}. \quad (\text{B.1})$$

The distance  $AB$  between the points of the optical path intersecting the tube interfaces can be deduced from

$$R_1^2 = R_2^2 + AB^2 - 2R_2 \times AB \times \cos\theta'_2, \quad (\text{B.2})$$

and then the angle  $\theta_2$  from

$$R_2^2 = R_1^2 + AB^2 + 2R_1 \times AB \times \cos\theta_2. \quad (\text{B.3})$$

Finally, the distance  $y'$  is given by

$$\frac{y'}{R_1} = \sin\theta_4 = n \sin\theta_2. \quad (\text{B.4})$$

Using the trigonometric relation  $\sin^2\theta + \cos^2\theta = 1$  for the angles  $\theta_2$  et  $\theta'_2$ , we find respectively

$$\left(\frac{y'}{nR_1}\right)^2 + \left(\frac{R_2^2 - R_1^2 - AB^2}{2R_1AB}\right)^2 = 1, \quad (\text{B.5})$$

$$\left(\frac{y}{nR_2}\right)^2 + \left(\frac{R_2^2 - R_1^2 + AB^2}{2R_2AB}\right)^2 = 1. \quad (\text{B.6})$$

The combination of these two relations leads to  $y' = y$ .

### **Appendix C. Relation between the measured intensity and the intensities emitted by the plasma and by the tube**

We adopt the following notations (see also Figure 2) and omit subscripts to indicate parallel and perpendicular polarizations which are understood throughout the following notations and relations:

- $I^{tr}$ : Intensity transmitted to the detector (measured quantity),
- $I_p^e$ : Intensity emitted by a plasma column at the distance  $y$  from the center (quantity to be compared to theoretical data),
- $I_t^e$ : Intensity emitted by a tube column. As the tube is relatively optically thin, this intensity is assumed to be the same for tube emission in the inward and outward directions,

- $I_{int}^i$ : Incident intensity on the internal tube interface,
- $I_{ext}^i$ : Incident intensity on the external tube interface
- $I_{int}^l$ : Intensity leaving the internal tube interface,
- $I_{ext}^l$ : Intensity leaving the external tube interface,
- $\rho_p$  : Specular reflectivity at tube interface for radiation propagating from the plasma to the tube,
- $\rho_t$  : Specular reflectivity at tube interface for radiation propagating from the tube to the outer medium,
- $\tau_t$  : Transmissivity of the tube (not accounting for reflections),
- $\tau_p$  : Transmissivity of the plasma column.

The two reflectivities  $\rho_p$  and  $\rho_t$  are calculated, for each polarization, from the general expressions related to radiation travelling from medium  $i$  with real refractive index  $n_i$  to medium  $t$  with index  $n_t$ , and neglecting the imaginary part of the index in comparison with its real part:

$$\rho_{\parallel} = \left( \frac{n_i \cos\theta_t - n_t \cos\theta_i}{n_i \cos\theta_t + n_t \cos\theta_i} \right)^2, \quad \rho_{\perp} = \left( \frac{n_i \cos\theta_i - n_t \cos\theta_t}{n_i \cos\theta_i + n_t \cos\theta_t} \right)^2. \quad (\text{C.1})$$

The different angles used in this expression are calculated from the expressions given in Appendix B for each distance  $y$  to the plasma axis. The axisymmetry of the problem and Eq. C.1 show that  $\rho_p$ , for instance, is also equal to the specular reflectivity at tube interface for radiation propagating from the tube to the plasma, which is required to express  $I_{int}^l$ .

With these notations, one can write the expressions of each intensity and



for each polarization:

$$I^{tr} = (1 - \rho_t)I_{ext}^i \quad (C.2)$$

$$I_{ext}^i = (1 - \rho_p)\tau_t I_{int}^i + I_t^e \quad (C.3)$$

$$I_{int}^i = \tau_p I_{int}^l + I_p^e \quad (C.4)$$

$$I_{int}^l = (1 - \rho_p)\tau_t I_{ext}^l + (1 - \rho_p)I_t^e + \rho_p I_{int}^i \quad (C.5)$$

$$I_{ext}^l = \rho_t I_{ext}^i. \quad (C.6)$$

Equation C.2 means that the measured intensity  $I^{tr}$  is simply equal to the incident intensity on the outer tube interface multiplied by the interface transmission factor  $(1 - \rho_t)$ . In Eq. C.3, the incident intensity on the outer tube interface  $I_{ext}^i$  is written as the sum of the incident intensity on the inner tube interface, multiplied by a transmission factor, and the intensity emitted by the tube. Equation C.4 reflects the fact that the incident intensity on the inner tube interface is equal to the intensity leaving the inner interface, multiplied by plasma column transmissivity, plus the intensity emitted by this plasma column. In Eq. C.5, the intensity leaving the inner interface is expressed as the sum of three terms, a directly reflected intensity on this interface, a transmitted intensity coming from tube emission, and the transmitted part of the intensity leaving the outer interface. Finally, since no significant radiation comes from outside, the intensity leaving the outer interface is simply expressed in Eq. C.6 as the reflected part of the incident intensity on the same interface.

The solution of this system leads to the expression of  $I^{tr}$ :

$$I^{tr} = a I_p^e + b I_t^e, \quad (C.7)$$

with

$$a = \frac{\tau_t(1 - \rho_t)(1 - \rho_p)}{1 - \tau_p[\rho_p + \rho_t\tau_t^2(1 - \rho_p)^2]}, \quad b = \frac{(1 - \rho_t)[1 - \tau_p\rho_p + \tau_t\tau_p(1 - \rho_p)^2]}{1 - \tau_p[\rho_p + \rho_t\tau_t^2(1 - \rho_p)^2]}. \quad (\text{C.8})$$

$I^{tr}$  appears then to be a linear combination of the intensities emitted by the plasma and by the confinement tube with the constants  $a$  and  $b$  depending on the different reflectivities and transmissivities. Equations C.7 and C.8 are in fact written for each polarization:

$$I_{\parallel}^{tr} = a_{\parallel} I_{\parallel p}^e + b_{\parallel} I_{\parallel t}^e, \quad (\text{C.9})$$

$$I_{\perp}^{tr} = a_{\perp} I_{\perp p}^e + b_{\perp} I_{\perp t}^e, \quad (\text{C.10})$$

where the coefficients  $a_{\parallel}$ ,  $b_{\parallel}$ ,  $a_{\perp}$  and  $b_{\perp}$  are calculated from Eqs. C.8 with reflectivities  $\rho_p$  and  $\rho_t$  depending on the polarization state according to Eqs. C.1. As the emission by the plasma and the tube are not polarized ( $I_{\parallel p}^e = I_{\perp p}^e = \frac{1}{2}I_p^e$  and  $I_{\parallel t}^e = I_{\perp t}^e = \frac{1}{2}I_t^e$ ), the total transmitted intensity is given by:

$$I^{tr} = I_{\parallel}^{tr} + I_{\perp}^{tr} = \frac{1}{2}(a_{\parallel} + a_{\perp})I_p^e + \frac{1}{2}(b_{\parallel} + b_{\perp})I_t^e. \quad (\text{C.11})$$

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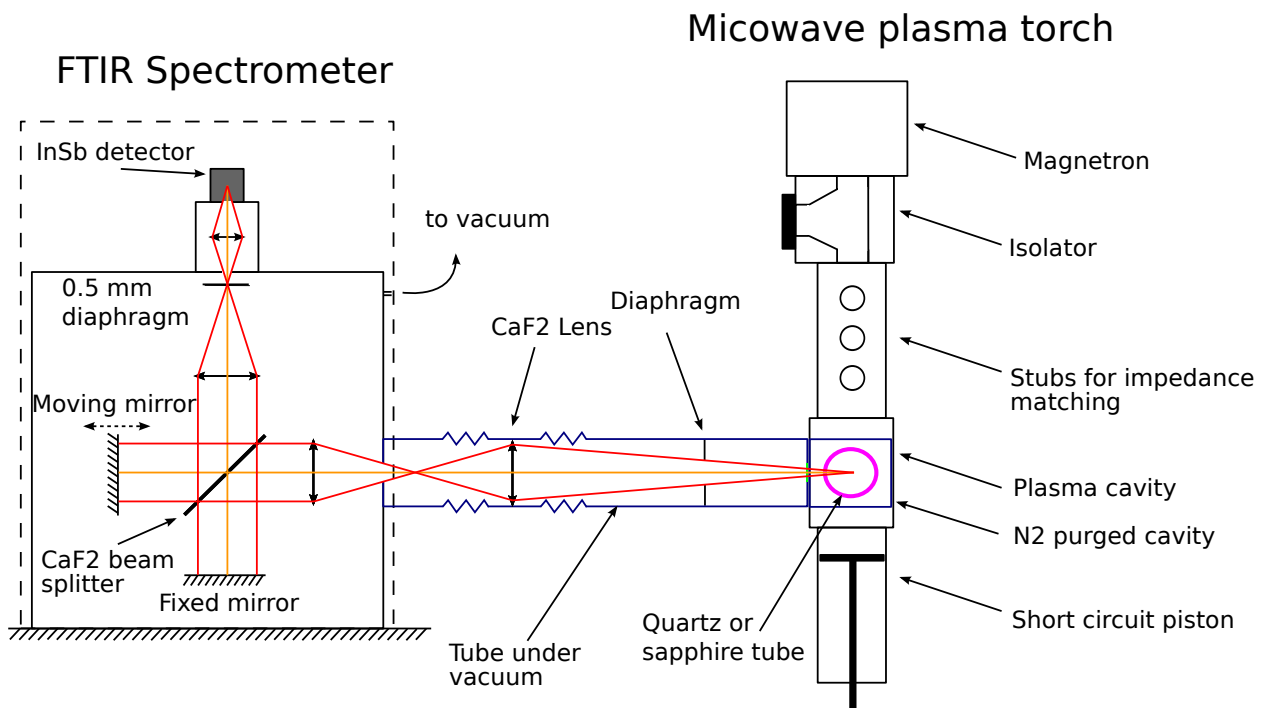


Figure 1: Experimental setup.

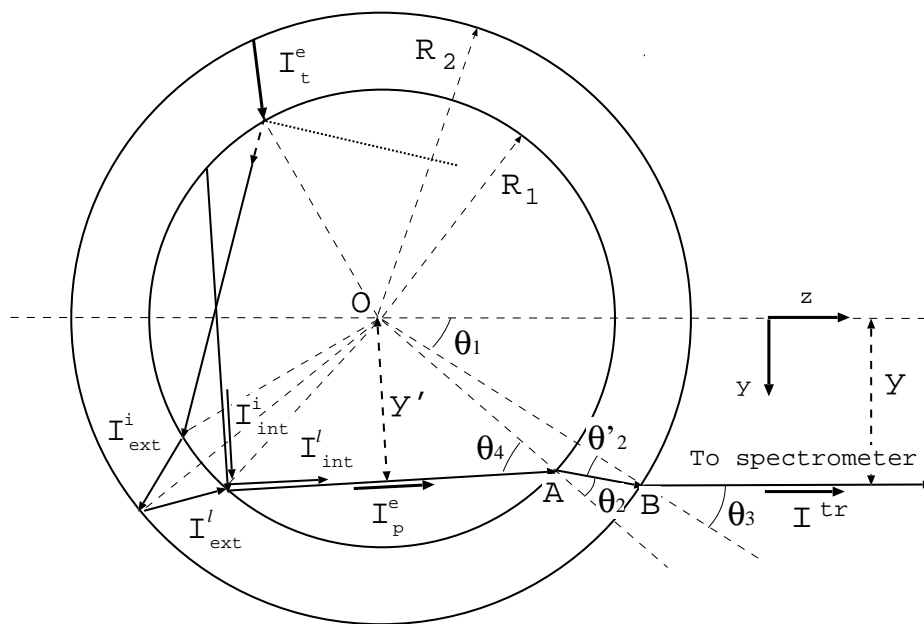


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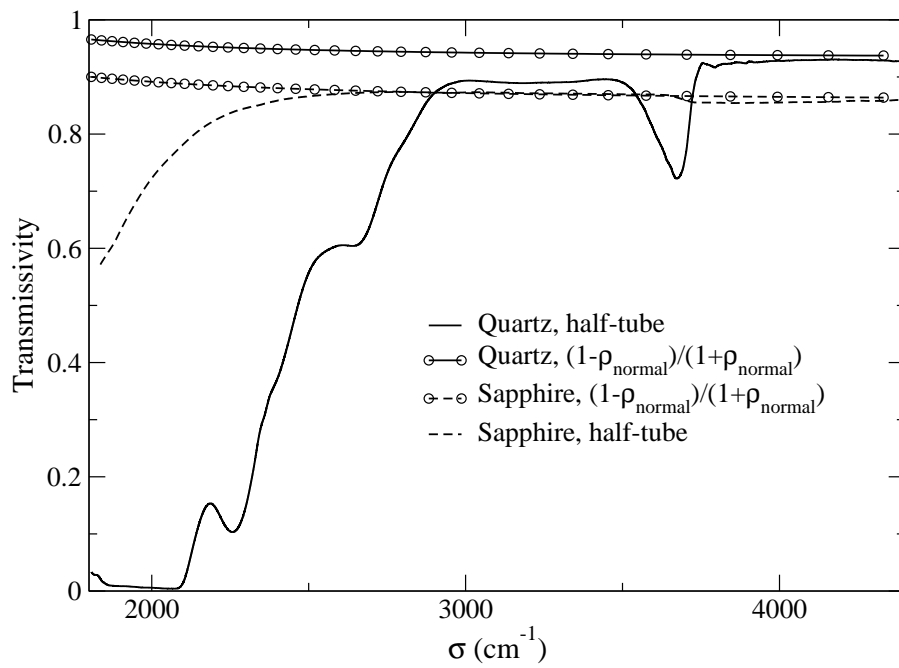


Figure 3: Measured and calculated transmissivities of quartz and sapphire half-tubes (2.5 mm width, room temperature). The calculations only take into account reflections at the interfaces while the measurements include also absorption effects.

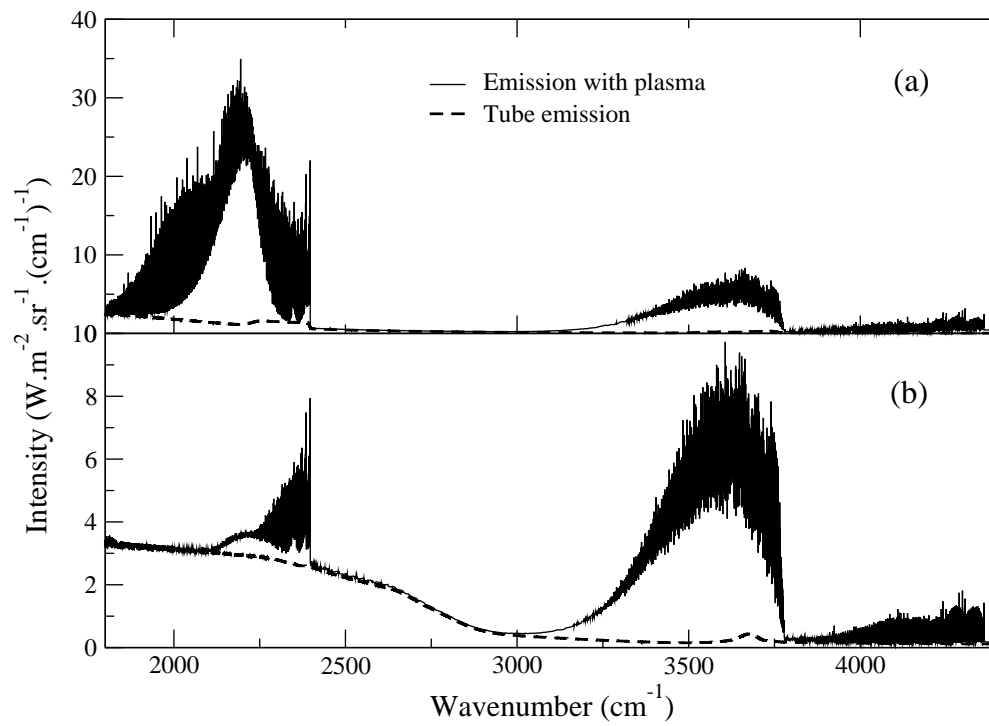


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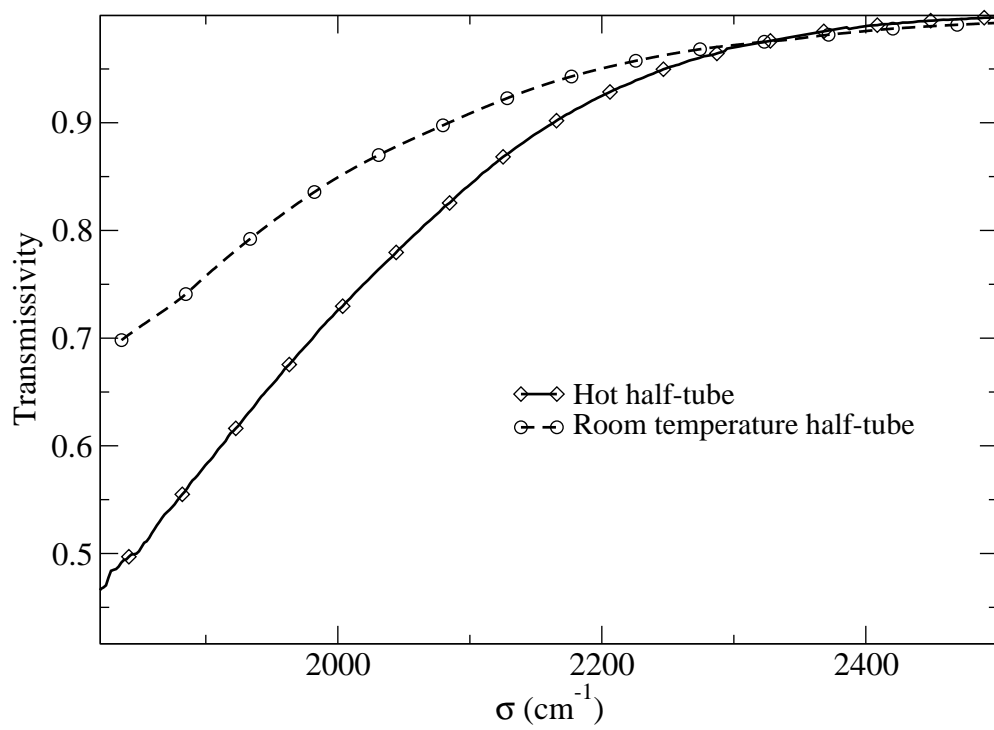


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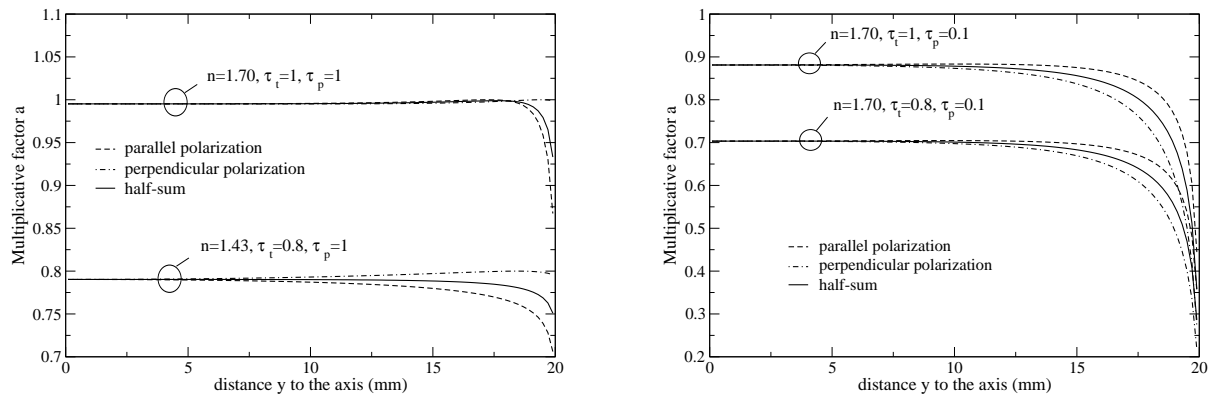


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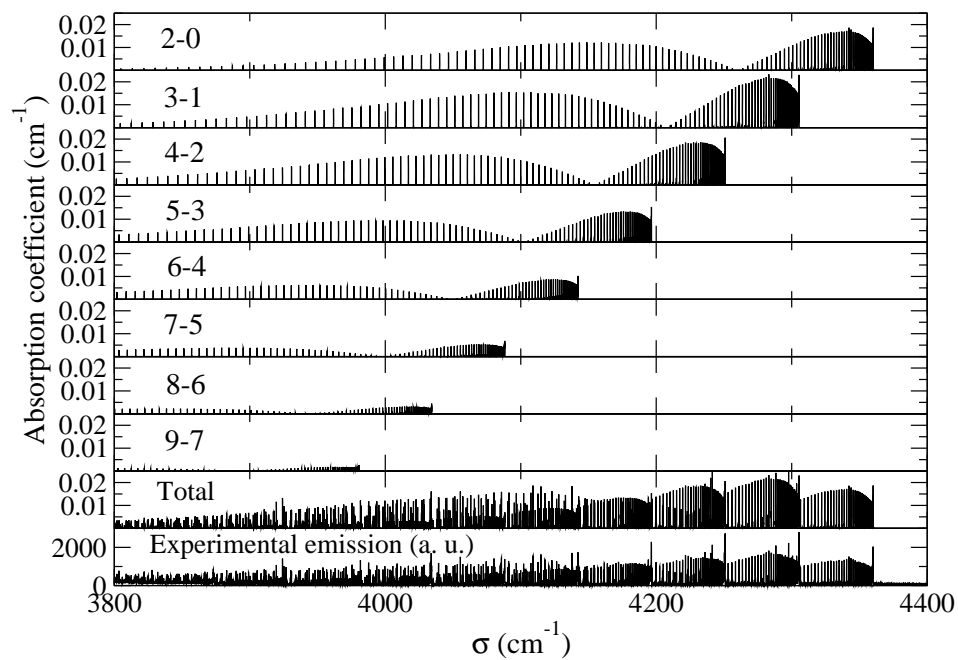


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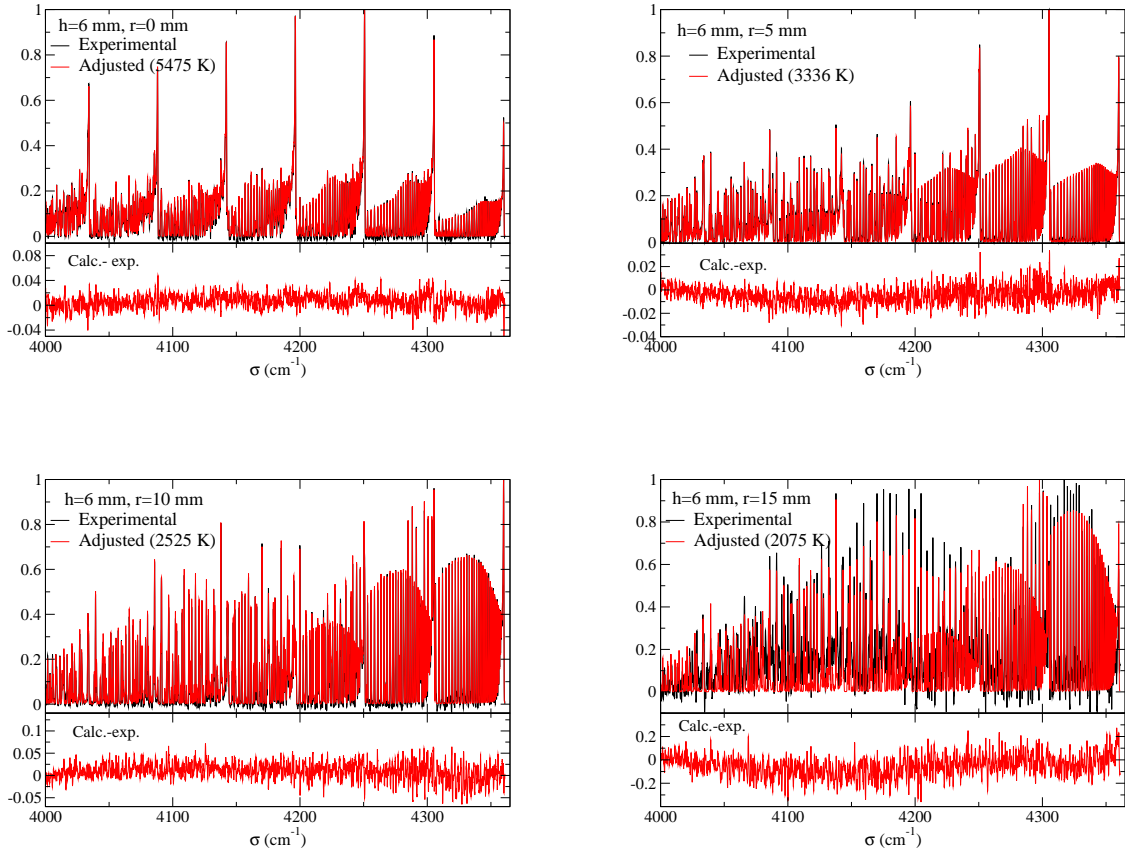


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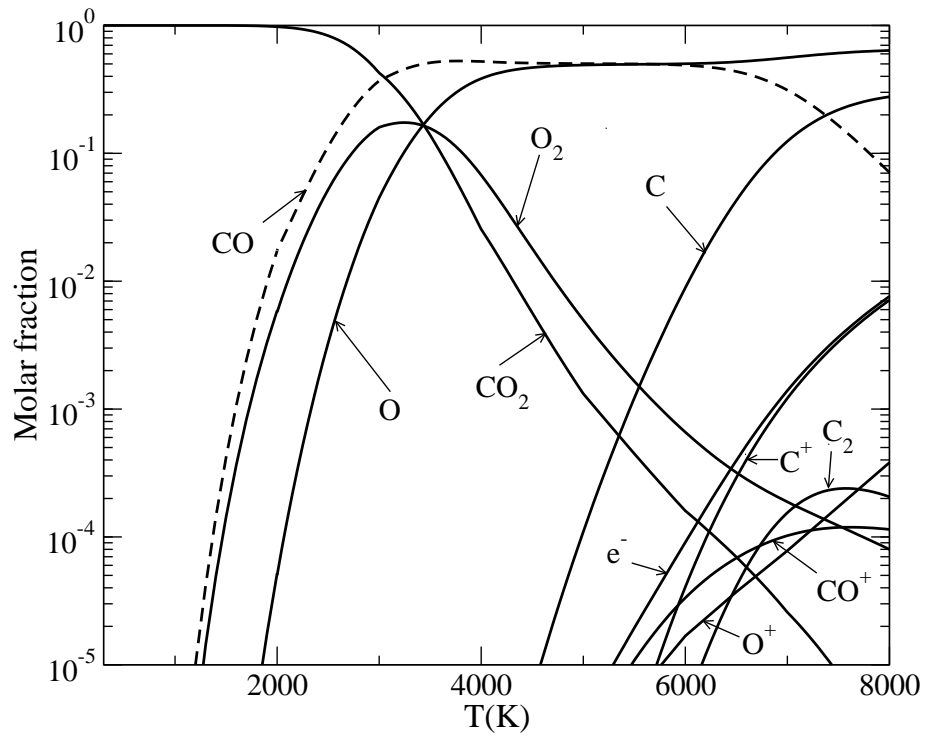


Figure 9: Chemical composition (molar fractions) of  $\text{CO}_2$  plasma at equilibrium and at 1 atm.

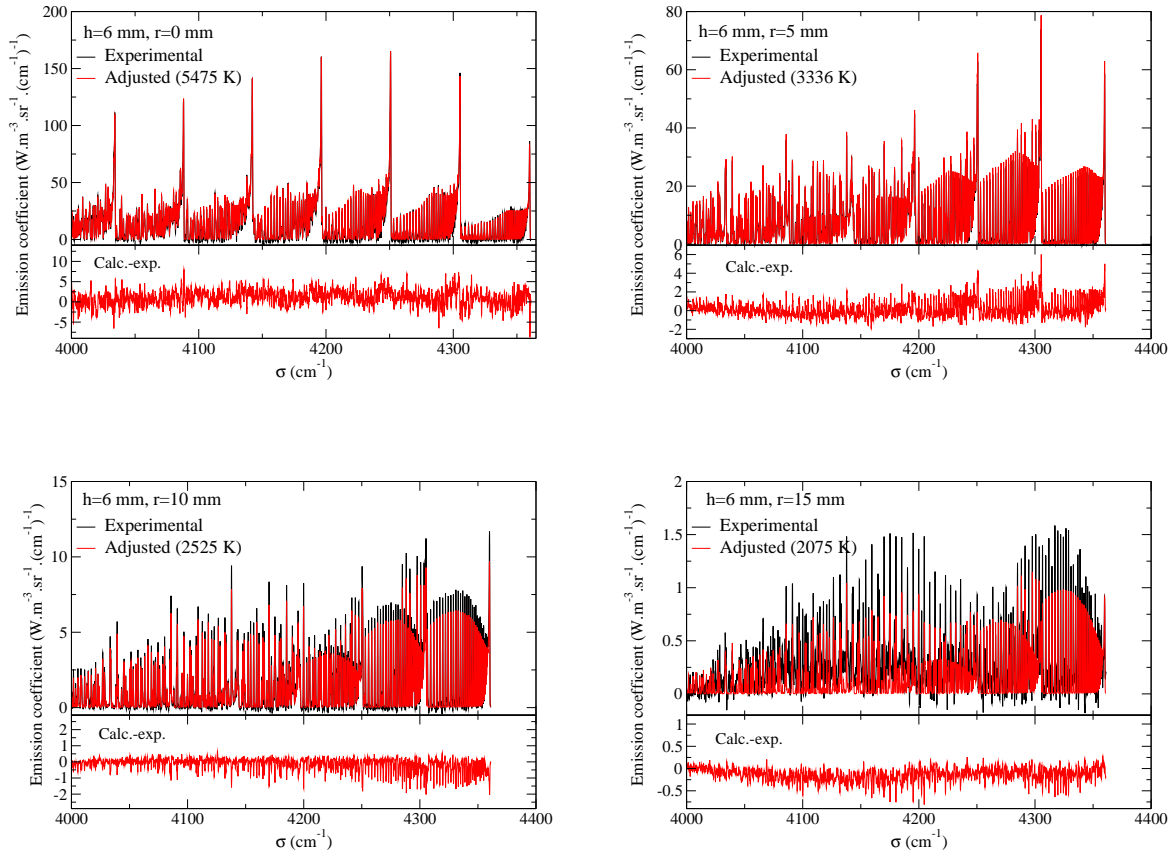


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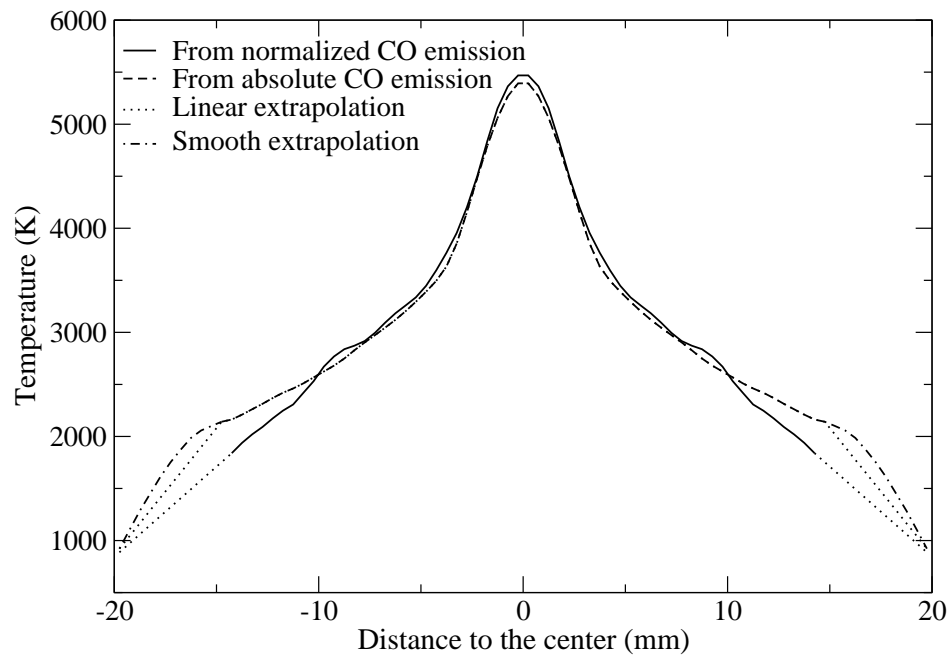


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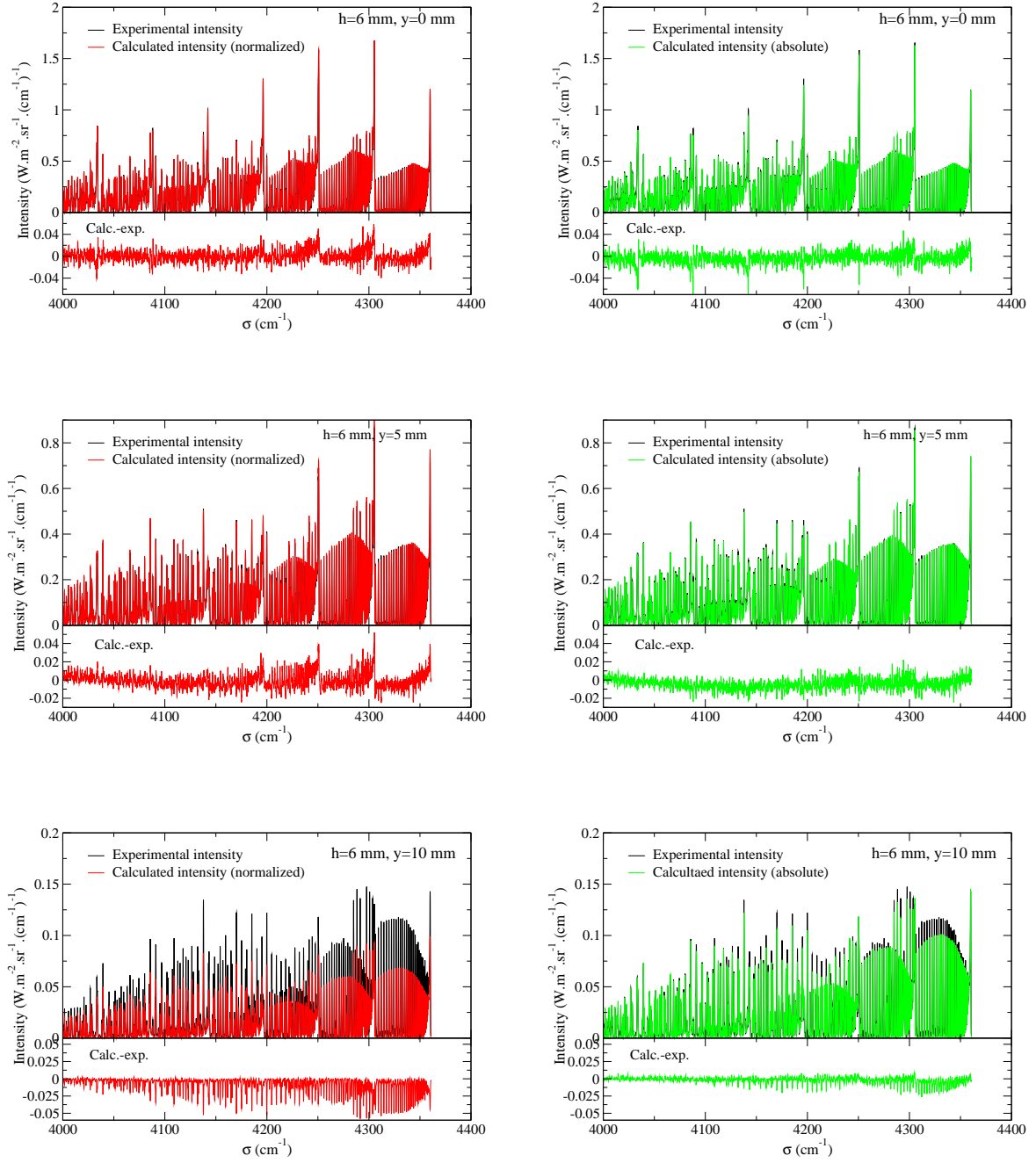


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	B <sub>1</sub>	B <sub>2</sub>	B <sub>3</sub>	C <sub>1</sub>	C <sub>2</sub>	C <sub>3</sub>
Quartz	0.69617	0.40794	0.89748	0.0046792	0.013512	97.934
Saphir	1.024	1.058	5.281	0.003776	0.01225	321.4

Table C.1: Constants for the dispersion relation, Eq. 2 where the wavelength  $\lambda$  is in  $\mu\text{m}$ . The data for quartz and sapphire are from Ref. [34] and [35] respectively and are widely adopted in the literature (see e.g. [36]).