Estimation of thermo-hydrodynamic parameters in energy production systems using non-stationary signal processing

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Outline

- Motivations and Application context
- Physical considerations
- Signal processing framework
- Results
- Conclusion

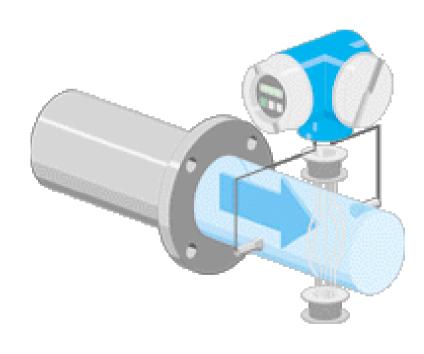
Estimation of hydraulic parameters of fluid flows (water or gas)

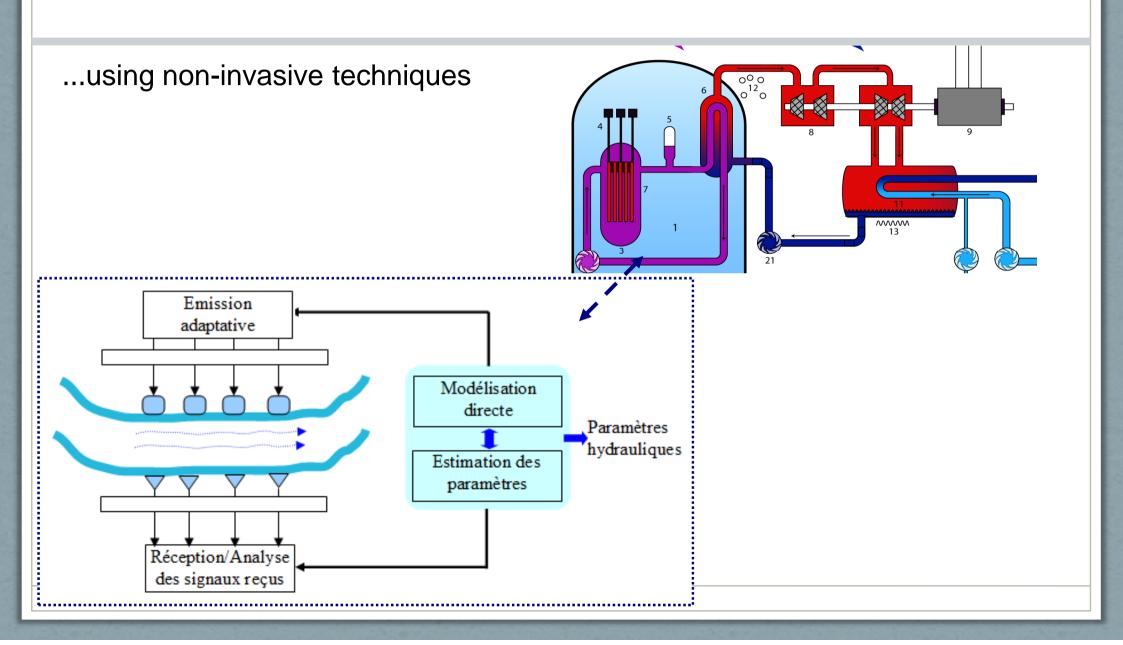




Current solution – mostly intrusive







Difficulties in terms of signal processing

- Complex propagation environments... No water in the cylinder **Transmitted** pulses Rx Tx Water + Steel effects!

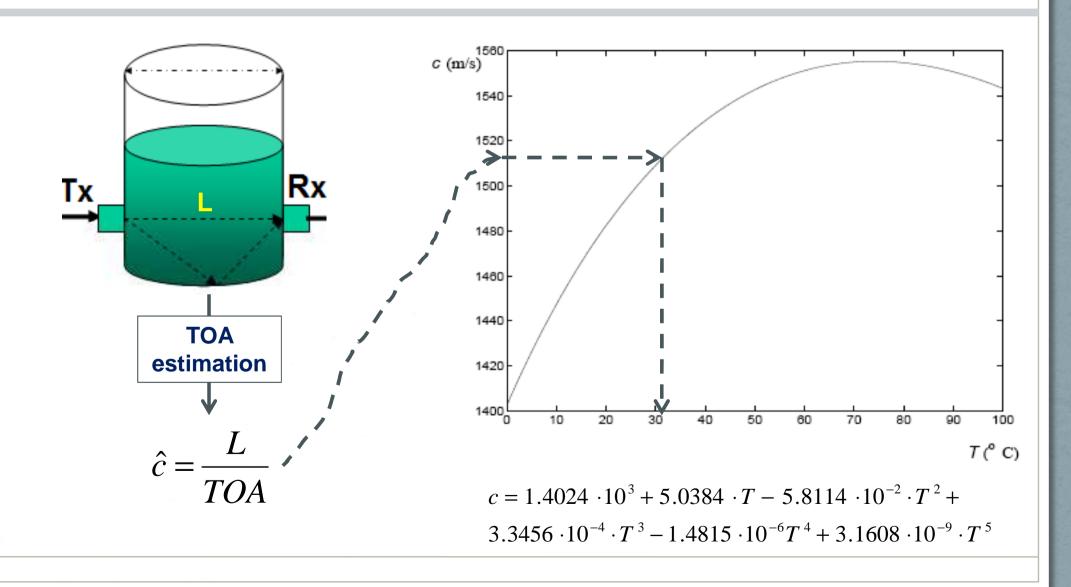
- Connection between signal and physical parameters!

Steel effects!

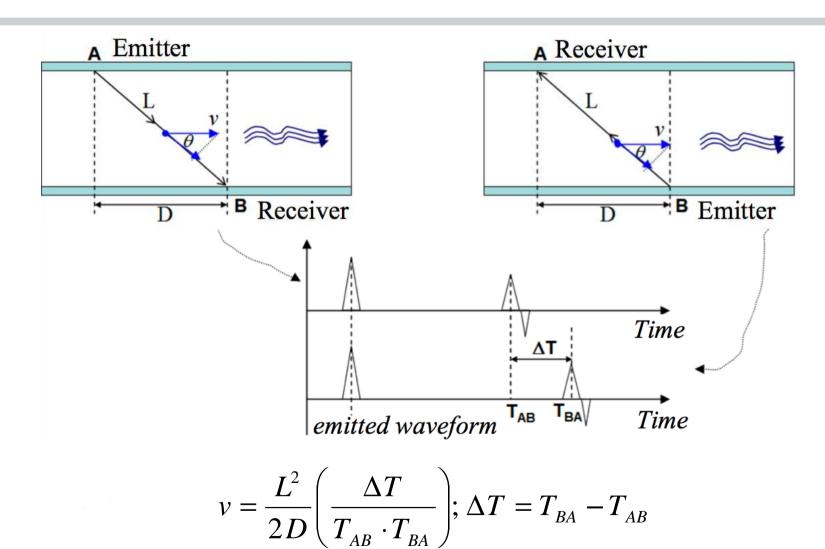
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Measuring temperature



Measuring flow rate

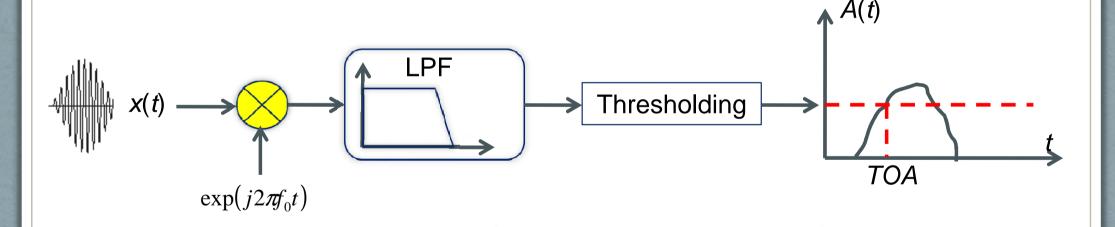


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Main topic: Estimation of TOAs (Time of Arrivals)

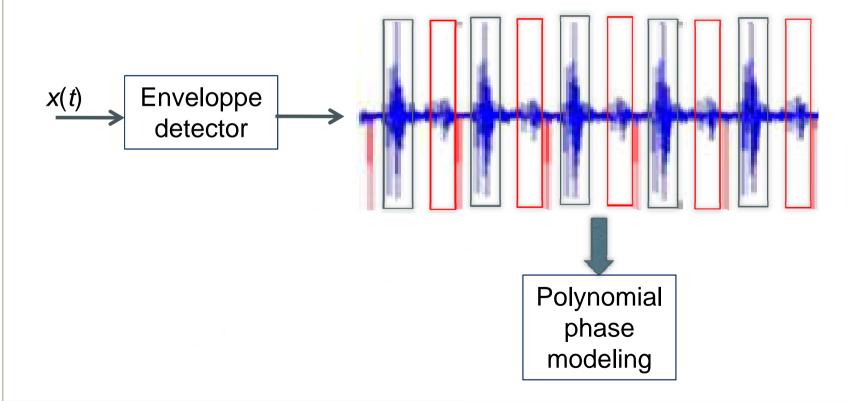
One common method (Enveloppe detector)



BUT, in our case, f_0 must follow the Doppler effect (induced by the flow)

Main topic: Estimation of TOAs (Time of Arrivals)

- Classical detection and Polynomial Phase Modelling



High-Order Ambiguity Function (HAF) = Fourier transform of high-order instantaneous moment

$$HIM_{s}^{(1)}(t) = s(t)$$
 $HIM_{s}^{(2)}(t) = s(t) \cdot s^{*}(t - \tau)$
 $HIM_{s}^{(K)}(t) = HIM_{s}^{(K-1)}(t) \cdot HIM_{s}^{(K-1)^{*}}(t - \tau)$

Main property: the k^{th} order HAF of a k^{th} order polynomial phase signal (PPS) is a spectral peak, corresponding to the k^{th} order polynomial coeeficient

$$HIM_{s}^{(K)}(t) = \underbrace{A^{2^{K-1}} \exp j(\tilde{\omega}_{K} \cdot t + \tilde{\phi}_{K})}_{\text{Sinusoid}} \longrightarrow \underbrace{HAF_{\kappa}[s; \alpha, \tau] = A^{2^{K-1}} e^{j\tilde{\phi}} \delta(\alpha - \tilde{\omega})}_{\text{Hadisoid}}$$

$$\tilde{\omega}_{k} = k! \tau^{k-1} a_{k} \qquad \tilde{\phi}_{k} = (k-1)! \tau^{k-1} a_{k-1} - 0.5k! (k-1) \tau^{k} a_{k}$$

• Classical estimation procedure

Polynomial coefficient estimation Phase Compensation
$$s(t) \longrightarrow \hat{a}_K = \frac{1}{K!\tau^{K-1}} \underset{\alpha}{\operatorname{arg max}} |HAF_K[y;\alpha,\tau] \longrightarrow s(t) \leftarrow s(t) \cdot \exp\left(-j2\pi\hat{a}_K t^k\right) \longrightarrow \{\hat{a}_m\}_{m=\overline{0,K}}$$

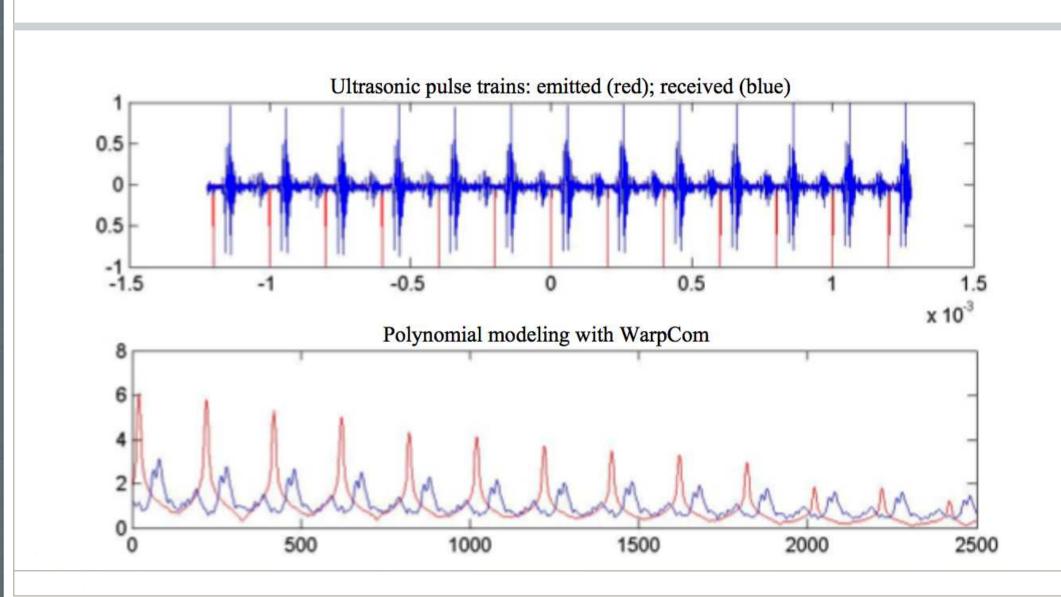
• New estimation procedure – reduce the error propagation effect (WarpCom)

$$t \xrightarrow{\mathbf{U}} t_{w}^{(K)} = \left(\frac{t}{\hat{a}_{K}}\right)^{1/K}$$

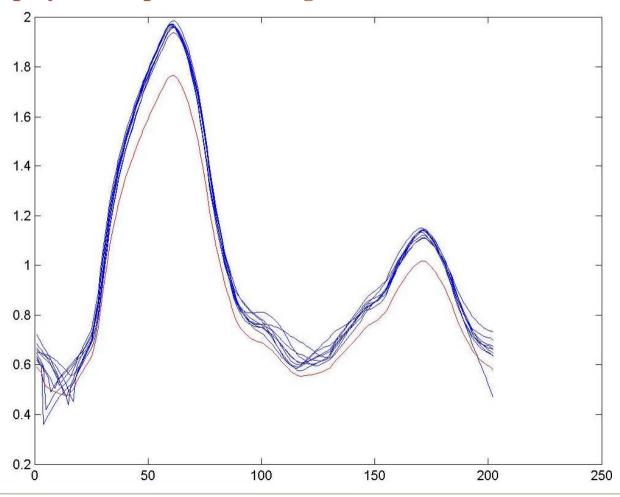
Polynomial coefficient estimation

Phase coefficient

$$\hat{a}_{K} = \frac{1}{K!\tau^{K-1}} \underset{\alpha}{\operatorname{argmax}} | mlHAFW_{K}[s;\alpha,\tau] | \longrightarrow S \longleftarrow U_{S} \longrightarrow \{\hat{a}_{m}\}_{m=0,K}$$



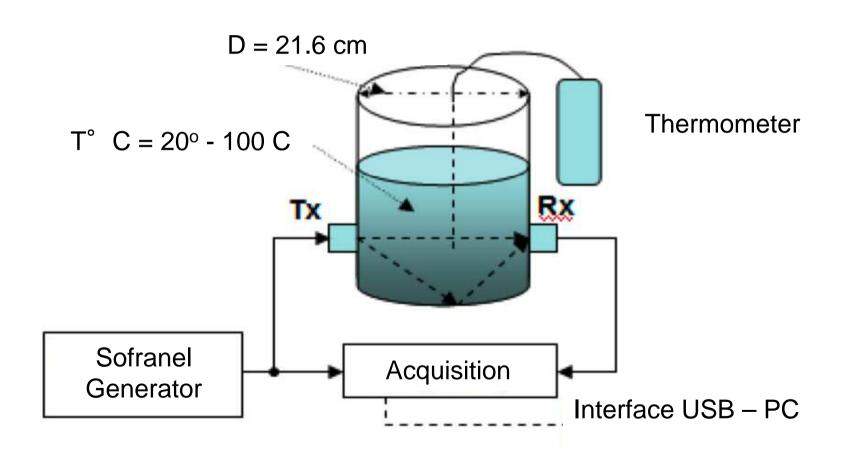
• Warping-based polynomial phase modeling



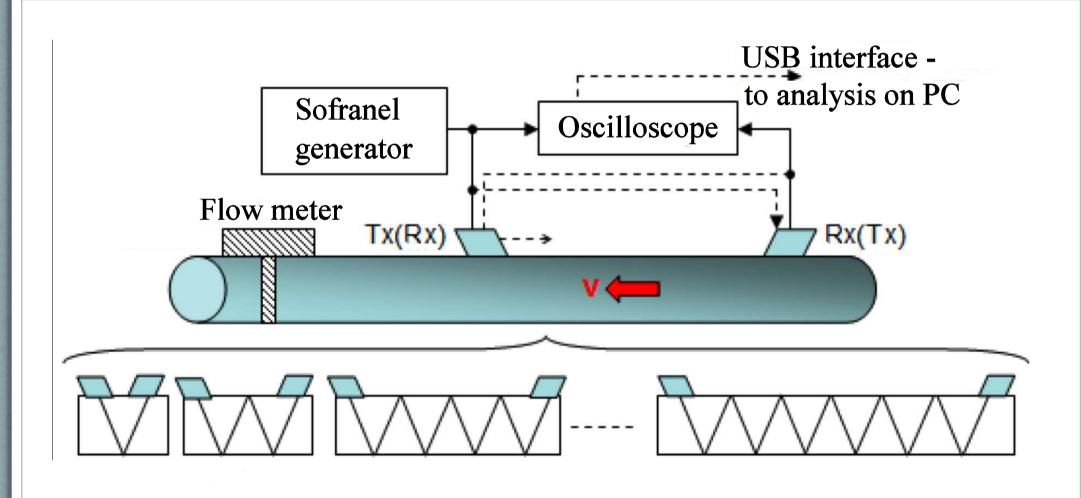
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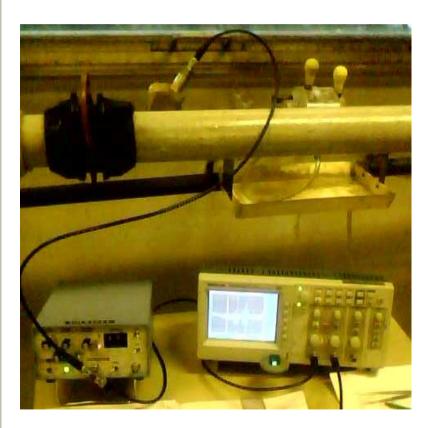
Experimental setup for measuring temperature



Experimental setup for measuring flow rate



Experimental setup for measuring flow rate

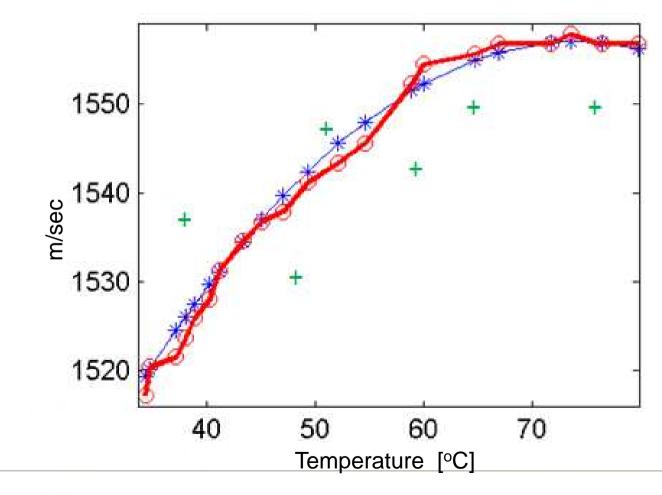




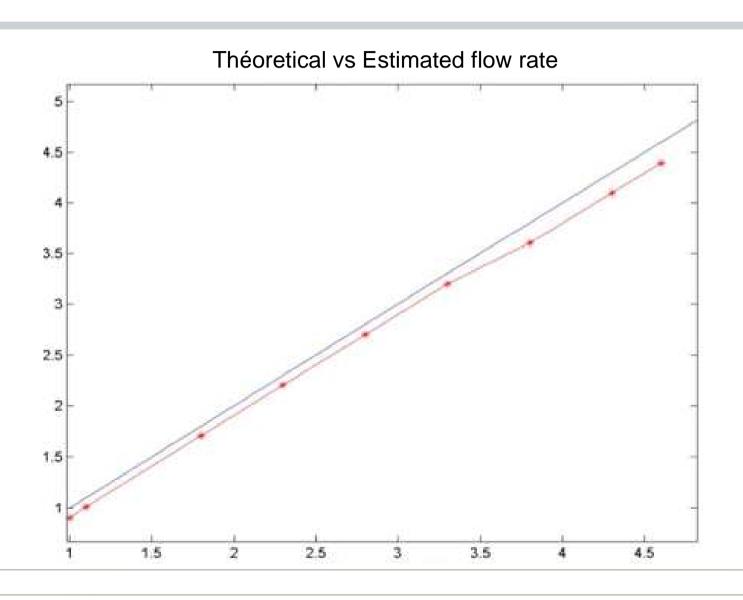
Results: Temperature

Ultrasound velocity:

Theoretical (*), Estimated by Enveloppe Detector (+), Estimated by Phase Modeling (o)



Results: Flow rate



Conclusion

Physics of ultrasound propagation + non-stationary signal processing =>

good estimation of the time of arrival =>
good estimation of the hydraulic parameters (temperature, flow rate)

FUTURE WORKS

Wide – bande signals and Matching Filtering

But need to model accurately the effects of the propagation...

NEED FOR MORE ADVANCED SIGNAL PROCESING!