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Effect of temperature and time on properties of Spark Plasma Sintered NiCuZn: Co ferrite

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Spark Plasma Sintering is a powerful method to produce fine grain dense ferrite at low temperature. However, the process, usually conducted in neutral atmosphere in a carbon die, yields carbon surface deposition and reduction of Fe^{3+} into Fe^{2+} . It's shown that subsequent annealing in air can remove carbon and, under some conditions, produce complete oxidation of Fe^{2+} ions. Regular values of the resistivity and permittivity (resp. 1 M Ω m, 13 ϵ_0) are recovered for most samples annealed not higher than 750°C. Relatively high value of the permeability (up to 240) and high merit factor ($\mu_s \times f_r > 5$ GHz) have been achieved.

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Keywords: Spark Plasma Sintering, Spinel ferrite, Grain size, Complex real permittivity, Complex initial permeability

I. INTRODUCTION:

The latest research in power electronics have focused on the miniaturization of electronic boards in particular by reducing the size of active components. Today, there is a tremendous demand of passive components reduction, particularly magnetic ones usually based on spinel ferrite. These ferrites attracted a lot of attention because of their magnetic behavior and their applications in power electronics devices for from the radio frequency (300 kHz to 3 MHz) to microwave (3 MHz to 20 GHz). The NiZn ferrite possesses a relative high initial permeability up to several hundred MHz, and a high resistivity, but the conventional sintering temperature is too high for co-sintering with silver or copper conductors (Sintering temperature at 1250°C). However, if copper is substituted in a proportion of 0.1-0.2, the conventional sintering temperature is decreased down to 950°C¹. This study will focus on studying the effect of temperature and sintering time using the Spark Plasma Sintering process² on structural, dielectric and magnetic properties of NiCuZn ferrite doped with cobalt.

II. EXPERIMENTAL:

Powders of basic oxides Fe_2O_3 , NiO, CuO and ZnO and Co_2O_3 were used for the preparation of NiCuZn ferrite using the standard technique of ceramics: jar mixture of precursor oxides, adding Co_2O_3 – in order to decreased the magneto-crystalline anisotropy constant –, calcination at 760°C for two hours and grinding by attrition for 30 min. The molar ratio was adjusted to achieve the following composition: $Ni_{0.195}Cu_{0.2}Zn_{0.599}Co_{0.006}Fe_2O_4$.

This composition was checked after sintering by SEM-EDS which confirms this composition within the accuracy of the method (Co was not detected). The sintering was carried out at different temperatures to determine the optimum properties at low sintering temperature. To investigate the structural and dielectric properties different pellets $\varnothing 8$ have been produced by SPS between 650 and 800°C in steps of 50°C under a uni-axial pressure of 50 MPa, in neutral atmosphere (Argon) with a heating rate of 160°Cmin⁻¹ followed by a plateau of 0 to 15 min and cooling 160°Cmin⁻¹. After sintering, the two faces of each sample were polished to remove graphite pollution from the pistons. For each sample, a second was made under the same conditions but with additional treatment at 500°C under air in order to burn residual carbon and reoxyde the surface. The crystal structure of the different sintered samples was studied by X-ray diffraction using a PANalytical X'Pert PRO MPD diffractometer, with cobalt source. The area swept in this study is between 20° and 80° in steps of 0.001°. The relative density was calculated as the ratio of the experimental density measured by Archimedes method and the theoretical density deduced from lattice parameter. To determine the crystallite size, the spectra were refined by the Rietveld method using the software Maud⁴. The electrical resistivity was measured using a multimeter by the four points method. The dielectric permittivity and complex initial permeability as a function of frequency (between 100 kHz and 500 MHz) have been determined by impedance spectroscopy (HP 4195 B). To make the measurements of dielectric properties before and after annealing, we have deposited a gold layer about 100 nm by Sputtering. The permeability measurements were performed in coaxial cell, with ring samples ($\varnothing_{ext} = 8$ mm, $\varnothing_{int} = 4$ mm and h = 3 mm).

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TABLE I. Initial permeability, relaxation frequency and merit factor of SPS ferrite toroids

Time	Sintering at 650°C			Sintering at 700°C			Sintering at 750°C			Sintering at 800°C		
	5 min	10 min	15 min	5 min	10 min	15 min	5 min	10 min	15 min	5 min	10 min	15 min
μ_i	17,3	17.4	17.4	34	39	52	126	156	178	152	213	242
f_r (MHz)	169	169	170	131	115	89	37	32	27	33	24	22
$\mu_i \times f_r$ (GHz)	2.92	2.94	2.96	4.45	4.48	4.62	4.66	4.99	4.80	5.02	5.11	5.32

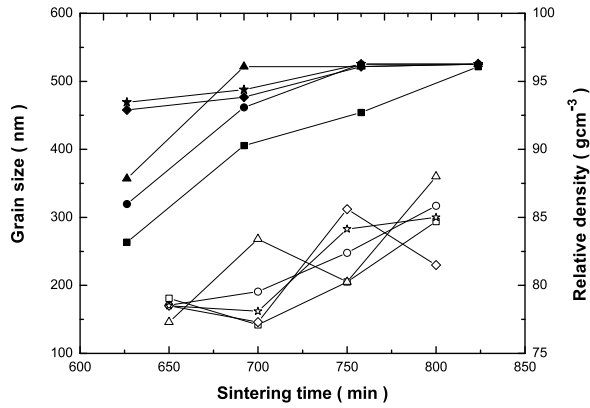


FIG. 1. Grain size and Relative density as a function of temperature and time of sintering: Square (0 min), Circle (1 min), Up Triangle (5 min), Diamond (10 min) and Star (15 min).

III. RESULTS AND DISCUSSION:

A. Structural properties:

X-ray diffraction patterns taken from the powder after calcination shows all peaks characteristic of the spinel phase and no trace of parasitic phase or basic oxides. Refinement of the spectra using an inverse spinel type ferrite structure confirms this conclusion and yields a grain size of 100 nm. For sintered samples, no difference is visible –the lattice parameter is always 841.7 pm– except the crystallite size (Fig.1) which increases with sintering temperature. It is noticeable that the sintering time has little influence on this parameter. In contrast the relative density strongly depends on annealing step duration (see in set Fig.1). The strongest density (95%) can be achieved even at 700° C if the temperature is maintained at least 5 min.

B. Dielectric properties:

The electrical resistivity and complex permittivity were measured before and after burning in air to clarify the effect of carbon on ferrite. Figure 2 shows the resistivity versus sintering time for different sintering temperatures before and after burn. The large increase of re-

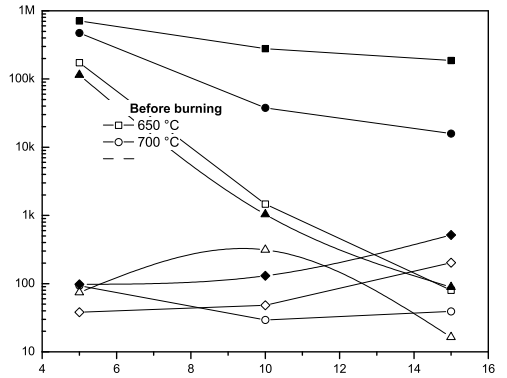


FIG. 2. Electric resistivity as a function of sintering time for different temperatures before and after burning

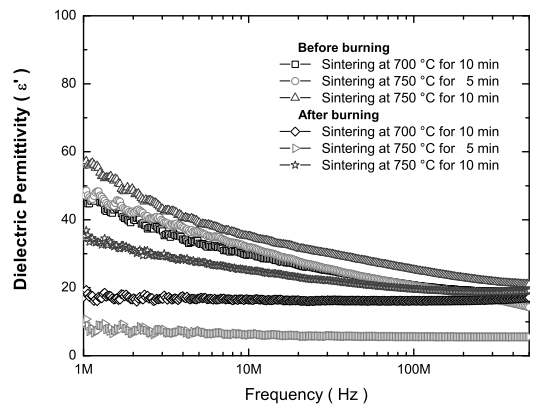


FIG. 3. Complex Permittivity as a function of frequency of sintering at 700 (top box) and 750° C (bottom box) before and after burning.

sistivity after burn may be explained by 2 phenomenons. First, SPS in a graphite die produces carbon evaporation and deposition at the surface of the sample, that short circuits the ferrite. This carbon layer is visible on XRD spectrum when recorded on as-sintered samples. Burn under air easily burns the surface deposited carbon. Secondly, the evaporated carbon can react with ferrite and after this treatment, the resistivity recovers the

high value expected for NiZn ferrites, except for sample sintered at 800°C which are probably reduced in the bulk and cannot be reoxidised because the porosity is closed. To confirm the reduction of Fe^{3+} in to Fe^{2+} we investigated the dielectric properties of these ferrite in a frequency range between 1 MHz and 500 MHz at room temperature. Figure 3 shows the different spectra of complex permittivity for different plateau length and temperatures before and after burning (500°C). For samples sintered at (700°C) and burnt, the dielectric permittivity is constant – in agreement with literature – and the decrease as a function of frequency is no longer observed. This confirms the burn of carbon and re-oxidization of the surface. By opposition samples sintered at 750°C for 10 and 15 min still show after burning the decrease in $\epsilon'(f)$ probably because the porosity is closed (the relative density is larger than 96 %) so Fe^{2+} can't be oxidized back into Fe^{3+} in the bulk. The high permittivity at low frequency has been observed in CCTO and BTO ferroelectrics⁵⁻¹³. The Internal Barrier Layer Capacitor (IBLC) effect is related to the micro-structure, composed of (semi)conducting grains separated by insulating grain boundaries. The effective relative permittivity given by $\epsilon_{eff} = \epsilon_{gb}D/t$ depending on the grains size (D) and the average thickness of grain boundary (t).

C. Complex initial permeability:

Table 1 shows the values of initial permeability, relaxation frequency and merit factor for different samples sintered at 650, 700, 750 and 800°C. There is either an increase of complex permeability according to the sintering temperature and sintering duration. This increase is due to grain growth and porosity reduction^{14,15}. Compared to the permeability values obtained by A. Lucas¹⁶ for the same types of ferrites sintered at 935°C for 2 h (conventional sintering), we note that the initial permeability is much lower, between 20 and 250, compared to 560 for conventional method. This is due to a much smaller grain size and probably to the single domain structure of the particles. The complex permeability spectra depicted in fig. 3 are showing the typical Snoek features as the real parts converges at high frequency. It is remarked that all of them exhibits a marked resonance in the real part characteristic of materials having a good homogeneity in terms of grain size and composition.

Tables 1 shows that the real part of the initial permeability is roughly proportional to the relaxation frequency f_r , which confirms Snoek's law¹⁷. Although the permeability is lower than that of conventionally sintered materials, the merit factor $\mu_i \times f_r$ is finally very close (up to 5.32 compared to 5.8 GHz).

In conclusion, this study has shown that SPS is very efficient for NiCuZn ferrite processing. These dense and well crystallized samples exhibits very fine grain size. The dielectric and magnetic properties can be controlled

by sintering temperature and time, keeping a high value

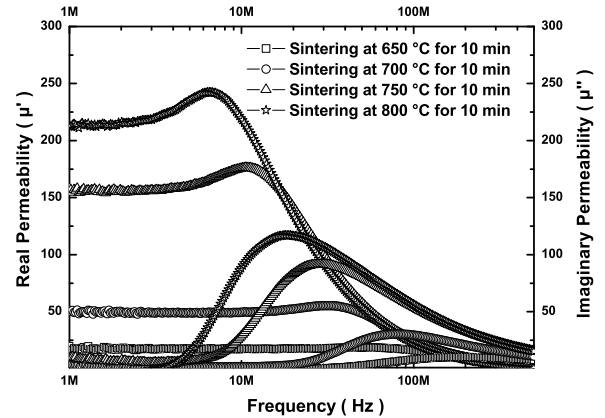


FIG. 4. Real and imaginary parts of the permeability for selected samples

of the merit factor. Samples annealed at 750°C for 5 min shows a good compromise in term of permeability, relaxation frequency (f_r) and resistivity when submitted to re-oxidation treatment. Higher permeability can be obtained but only at the price of larger dielectric loss. Hence, SPS should be used for the fabrication of NiCuZn ferrite based integrated magnetic component using LTCC process.

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