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Optimization of gene delivery to HEK293T cells by microporation using a central composite design methodology

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Abstract

Microporation is an efficient method for delivering plasmid DNA molecules into cultured cells. Herein, we present the optimization of gene delivery by microporation using a Central Composite Design methodology. It was given relevance not only to the transfection efficiency but also to the cell recovery. Different amounts of DNA (1 and 3 g) mainly affected cell viabilities and cell recoveries, which decrease from 93 % to 76 % and from 47 % to 25 % respectively, when higher DNA quantity is used. With this work we suggest an easy methodology to improve transfection of mammalian cells underlining the feasibility to achieve 60% of gene delivery efficiencies whilst recovering 50 % of cells, with 90 % of viability.

Keywords

Cell recovery; Central Composite Design; Gene delivery; Microporation; Plasmid DNA.

Introduction

Gene electrotransfer has been a powerful tool to transfer DNA molecules into a large variety of prokaryotic and eukaryotic cells. However, there are still some problems urging to be solved such as low cell viabilities and low transfection efficiencies especially when using low DNA amounts. Most of published data has been obtained from conventional electroporation that usually relies on the use of high electrode surfaces areas requiring minimum volumes of 50 l. Novel devices with different layouts have been recently developed and tested with several cell lines for diverse applications (see recent review (Lee et al. 2009)). Our study comprises the use of a microcapillary system with an electrode surface area of 0.33 mm² and 10 l chamber for cell suspension microporation (Kim et al. 2008). In most published work, transfection efficiency and cell viabilities are the only considered output values for electroporation optimization, which we consider that may mislead the process efficiency. In fact, high cell viabilities may be obtained even when few cells are recovered after being submitted to electric voltages. To our best knowledge few authors have published results regarding cell recovery and yield of transfection after electroporation of mammalian cells (Aluigi et al. 2006; Ferreira et al. 2008).

In this work a Central Composite Design (CCD) methodology was used as a valuable tool to assess the effect of several independent factors on HEK293T gene delivery efficiency by microporation. These cells are able to replicate appropriated plasmids (Wurm et al. 2003) and have been used in basic research and for production of virus and recombinant proteins (Pham et al. 2006). Moreover, microporation is a recent available and promising technology of gene transfer and taking into account the conditions that gave rise to higher percentages of cells expressing a reporter protein we have evaluated not only cellular viability but also cell recovery and transfection yield which constitutes new data regarding this methodology. Taken together, our results will certainly be very useful in gene delivery applications to mammalian cells.

Materials and methods

Plasmid construction and purification

The plasmid pcDNA3.1 (Invitrogen, La Jolla, CA) encoding *green fluorescent protein* (GFP) reporter gene was constructed using standard cloning methods. This plasmid has a SV40 ori, therefore able to replicate in mammalian cell lines that stably and constitutively expresses the SV40 large T antigen such as HEK293T. In brief, the reporter gene was digested from the plasmid pEGFP (BD Biosciences Clontech, Mountain View, CA) using restriction enzymes Hind III and Apa I and further cloned into pcDNA3.1. The construct (5,7 kb) was produced in *E. coli* and further purified using the Endotoxin-free (EF) Plasmid DNA Purification, NucleoBond[®] Xtra Midi EF (Macherey-Nagel, Düren, Germany) and resuspended in EF-water at 1 g/ l.

Cell culture and microporation

Human Embryonic Kidney (HEK) 293T cells (ATCC-LGC Nr: CRL-11268; Middlesex, UK) were grown in adherence in T_{75} flasks with Dulbecco's Modified Eagle Medium (DMEM) high glucose (4.5 g/l), 10% fetal bovine serum (FBS), 1% penicillin/streptomycin (100 µg/ml) (Gibco, Invitrogen, La Jolla, CA) and were maintained at 37 °C and 5% CO₂-humidified atmosphere.

Sub-confluent cells were harvested and washed with DPBS. Cells were resuspended in a sacarose based buffer (SB-PBS: 250 mM Sacarose and 1 mM MgCl₂ in DPBS) or in the Resuspension Buffer (RB – provided by the equipment manufacturer) at a density of $\sim 2 \times 10^5$ cells/10 l and incubated with plasmid DNA on ice. Microporation was accomplished within 20 min. maximum using a Microporator (MP-100) purchased from Digital Bio Technology (Seoul, South Korea) according to manufacturer's instructions. The ratio between cells and DNA ranged 7 10^4 -20 10^4 cells/g and DNA amount is referred when appropriated. Afterwards cells were added to 100 1 of pre-warmed medium without antibiotics and equally divided into 2 wells of a 24-well culture

plates containing culture medium under the same conditions. Cells were incubated at 37 °C in a 5% CO_2 -humidified atmosphere, harvested after 24 hours using DPBS and analyzed.

Transfection efficiency, Cell Viability, Cell Recovery and Yield

Transfection efficiency was measured by flow cytometry using FACSCalibur equipment (BD Biosciences, San Jose, CA) and reported as percentage of GFP positive cells (GFP⁺ cells). A laser excitation wavelength of 488 nm was used and experiments were conducted in 137 mM NaCl, 2.8 mM KCl solution as the sheath fluid. Results considered statistically representative had minimum 1000 events gated. Data were analyzed by CellQuest software (BD Biosciences, San Jose, CA).

The percentage of viable cells was estimated by trypan blue exclusion method. For each micro-electroporated sample (m), Cell Recovery (CR) was determined using the equation:

$$CR(\%)_m = \frac{CA_m}{CA_c} \times 100$$
(Eq.1)

where CA is the number of cells alive and c is the non-electroporated control. The yield of transfection (*Y*) was calculated using the following equation:

$$Y(\%)_m = \frac{GFP \oplus \times CA_m}{CT_c}$$
(Eq.2)

where *CT* is the number of total cells.

Experimental Design

Factorial designs are generally used to evaluate the effects of multiple independent factors and their degree of interaction. In this work we used a CCD to optimize gene delivery to HEK293T cells, using a microporation technology. The response (dependent variable) was the percentage of GFP^+ cells measured by flow cytometry. Accordingly, we evaluated the effects and interaction of four independent variables: electric pulse (X_1) , pulse width (X_2) , number of pulses (X_3) and DNA amount (X_4) . Using a face centred star points design, three coded levels (low (-1); central (0) and high (+1)) were chosen according to previously obtained results (data not shown). The coded values of independent variables are given in Table 1. **(Table1)**

This CCD design was used with the assistance of STATISTICA software (StatSoft, Tulsa, OK, USA) which has allowed estimation of a full quadratic model with the general description: $N = 2^{k \cdot p} + 2k + C_0$, where N is the number of experiments, *k* is the number of independent variables (*k* = 4), *p* the fractionalization number (in a full design, *p* = 0) and *C*₀ is the number of central points (*C*₀ = 4), required for curvature estimation (Barker 1985). Accordingly, a total of 28 (2⁴⁻⁰+2 4+4) different combinations (including four replicates of the central point each sighed the coded value 0) were chosen according to a CCD configuration for four independent variables.

Results and Discussion

The majority of reported studies regarding optimization of gene delivery efficiency to primary or established cell lines involve changing one variable while maintaining other formulation variables constant. Such time- and labor-consuming strategy may be ineffective because fails to consider potential interactions between variables. Alternatively, a statistical approach such as Central Composite Design involves a minimum number of experiments for a large number of factors. Additionally, Response Surface Methodology determines the optimum level of each factor by building a mathematical model. In the literature there are only few studies using the referred methodology aiming at optimizing non-viral gene delivery vectors and methodologies. The first reported study regarding this topic aimed to demonstrate the utility of Central Composite Design in modeling responses such as vector size, zeta potential and transfection efficiency of several non-viral gene delivery vectors (Birchall et al. 2001). Similarly other authors have verified the effect of several parameters and their interaction on physical stability of polyplexes (Gazori et al. 2009; Zhong et al. 2007). Regarding electroporation, and to our knowledge there is no reported study aiming at multivariate optimizing procedure for *in vitro* gene delivery in mammalian cells.

With our work we intended to show how the variables: electric pulse (X_1) , pulse width (X_2) , number of pulses (X_3) and DNA amount (X_4) affect gene delivery by microporation, and also inquire about their main interactions using a Central composite design (CCD). The number of GFP⁺ cells, obtained by flow cytometry analysis was the dependent variable and the results are shown on Table 2. When using an electric pulse of 1500V within 30ms and/or 3 pulses, the recovered cells were not enough for flow cytometry measurement due to high cell mortality and so we considered as zero in the CCD. (Table 2)

A second-order polynomial equation (Eq. 3) was used to express the GFP⁺ cells percentage as a function of four independent variables. The quadratic effect of Electric pulse (X_1^2) and DNA amount (X_4^2) have shown the most pronounced effects on the number of GFP⁺ cells.

 $GFP^{+} \text{ cells } (\%) = 36.1 + 2.8X_{1} - 3.1X_{2} - 1.8X_{3} + 2.7X_{4}^{\tilde{}} 25.7X_{1}^{2} - 9.0X_{2}^{\tilde{}} 4.4X_{3}^{2} + 9.6X_{4}^{\tilde{}} 6.3X_{1}X_{2} - 3.6X_{1}X_{3} + 1.6X_{1}X_{4} + 3.4X_{2}X_{3}^{\tilde{}} 1.7X_{2}X_{4} \quad (R^{2}=0.95)$ (Eq. 3)

For each parameter estimator a test of significance was performed. Parameters with less than 95% significance (*p*-values above 0.05) were discarded and pooled into the error term (residual error). Accordingly, in the previous equation the parameter linear relation of X_3 by X_4 was not considered (p = 0.56). The model was further validated by analysis of variance (ANOVA), using a methodology previously presented by others (Martins et al. 2009), for determining which of the factors significantly affect the response variables in study (GFP⁺ cells), using a Fisher's statistical test (*F*-test),. The results are shown on Table 3. (**Table 3**)

Data show that the model is statistically significant (for all the regression models, F-value > F-critical, *p*-value < 0.001) explaining 95 % (R^2 = 0.95) of the observed variance. There is no evidence of lack of fit at 95 % confidence level, as determined by the ratio MS(LF)/MS(PE) (for all

response variables, F-value (LF) < F-critical and p-value > 0.05), which means that the model explains the observed differences on the response variable. The relationships between independent and dependent variable can be easily visualized using RSM, where the obtained regression model was used to calculate the response surface for each response variable (Fig.1). (Figure 1) The effects of electric pulse and DNA amount on GFP⁺ cells percentage are visualized from a threedimensional plot and a contour plot (Fig. 1A). A saddle-shaped surface plot was obtained and two maximal points were observed: one at higher and other at lower DNA amount, using an electric pulse of ~1200 V. Conversely, when using two pulses and 2 g of DNA the highest percentage of GFP⁺ cells are obtained at electric pulse and pulse width ranging from 1200-1300 V and 20-24 ms respectively (Fig. 1B). A similar peak-shaped response surface was obtained when plotting electric pulse and number of pulses at 20 ms and using 2 g of DNA, and again a higher number of GFP⁺ cells was obtained with 1200 V (Fig.1C). Optimal experimental conditions were selected from the response surfaces plots and higher values of GFP⁺ cells (~60 %) were obtained with 1200-1300 V, 20 ms of pulse width either using 1 or 3 g of DNA. The number of pulses (1-3) did not greatly affect the number of GFP⁺ cells contrarily to some reported studies, although using different cell lines and electroporation equipments (Lin et al. 2009). It is well known that when cells are submitted to high electric pulses a major amount of DNA enter into the cells though concurrently an increase of cell death is observed (Ferreira et al. 2008). Several studies, using different cells, have shown that a way to circumvent this fact is by decreasing electric pulse and increasing the duration of pulse (pulse width) or within low voltages use more than one pulse (Cemazar et al. 2009). Higher transfection efficiency levels have also been obtained by increasing the DNA amount up to 60 g (corresponding to ~2 10⁴ cells/ g DNA) (Helledie et al. 2008) regardless lower DNA amounts are commonly employed. In fact, in our experiments with 3 g of DNA a similar ratio of cell/g DNA ($\sim 7 \ 10^4$) was used.

We further compared two different microporation buffers using different DNA amounts with the purpose of evaluating respective cellular viabilities, cell recoveries and overall yield. In this study we took advantage from the information retrieved from the previously shown CCD experiment and fixed the following microporation conditions: 1250 V, 20 ms and 1 pulse. One buffer was supplied by the equipment kit (RB - with unknown formulation) and the other was prepared in the laboratory with the formulation: 250 mM Sacarose, 1 mM MgCl₂ and 10 mM Tris.HCl in DPBS (SB-PBS). The data shown in Figure 2 were obtained from three independent experiments. (Figure 2) Using the equation model obtained by the experimental design (Eq.3) the predicted values for GFP+ cells when using SB-PBS under the referred conditions (in coded level: $X_1 = 0.165$; $X_2 = 0$; $X_3 = 1$) are 40 % for 1 g DNA ($X_4 = 1$) and 46 % for 3 g DNA ($X_4 = 1$). In fact, from figure 2A the obtained values were respectively 55% and 63%, slightly higher than the predicted values, though as predicted both had similar values. On the other hand, when using RB the DNA amount is crucial. Lower amount of DNA displays higher number of GFP⁺ cells (Fig 2B). As depicted from Fig. 2 the buffer prepared in the laboratory (SB-PBS) displayed higher cellular viabilities, and most importantly higher cellular recoveries and higher yields. Common to both buffers, as expected, is the fact that lower DNA amounts give rise to higher cell viabilities and recoveries which is mainly reflected in higher yield. Cellular viability using SB-PBS ranged from 70-90 % while with RB it achieved a maximum of 60 % using a lower DNA amount. Cell recoveries and transfection yields obtained with RB were lower than 20 % whereas with SB-PBS a maximum recovery of 50 % and 30 % yield were obtained. These results suggest that RB of unknown composition might have a higher conductivity than SB-PBS. In fact, previous reports have shown that the percentage of surviving cells increases with the decreasing medium conductivity (Ferreira et al. 2008) suggesting that electroporation buffer is other parameter that might be considered on electrotransfer optimization protocols. Even though each electroporation equipment has a specific buffer suggested by the supplier, some authors have recently reported promising results of gene delivery efficiencies using accessible buffers of known

composition (Ferreira et al. 2008; Kang et al. 2009). Actually, in one experiment transfection efficiency obtained with RB was slightly higher than those obtained with SB-PBS because 78 % of GFP^+ cells were obtained using 1 g of DNA. Contrarily, increasing DNA amount led to a clear reduction of transfection efficiency. This fact is in fair agreement with manufacturer instructions which suggests the use of 0.5 g of DNA per $1.5 \, 10^5$ cells. It was recently reported that electroporation of cells in a capillary system gave rise to an enhancement of transfection rate and cell viability when compared to the cuvette system (Kim et al. 2008). In the conventional electroporation, using a cuvette, the reported cellular viabilities are generally below 70 % and most importantly the cell recoveries are rarely mentioned, with the exception of few studies with primary cells (Aluigi et al. 2006; Ferreira et al. 2008). In this work we achieved cell viabilities up to 90 % and cell recoveries near 50 %. Overall we were able to obtain a yield of transfection of 30 %.

We further evaluated the ability of microporated cells expressing GFP to form colonies under antibiotic selection. The plasmid used in this study had a resistance to Zeocine which was added to the cell culture (250 g/ml) two days after microporation. After ten days, all non-transfected cells were dead and the first colonies were expanded maintaining around 95 % of cells continuously expressing GFP. HEK293T cells can be used either for recombinant protein production or as a model to study a specific cellular feature or disease. For both applications gene delivery might be essential and in this study we presented an approach to optimize gene delivery to these cells.

Conclusions

In conclusion, this work illustrates the feasibility of microporation for the efficient delivery of plasmids into mammalian cells, using an easy to prepare buffer, whilst maintaining cell viability concurrently with high cell recoveries. Moreover, the usefulness of CCD for gene delivery optimization was demonstrated. This approach might be successfully applied to other transfection

protocols for evaluating interactions between factors involved on transfection efficiency, therefore contributing to a faster monitoring and optimization.

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Indon	Coded levels			
Independent Variables		-1	0	+1
X_1	Electric pulse (V)	900	1200	1500
\mathbf{X}_2	Pulse width (ms)	10	20	30
X ₃	Pulse number	1	2	3
X_4	DNA amount (g)	1	2	3

 Table 1 Uncoded and coded levels of the independent variables.

		U		0	1	
Run _	Independent variables				Dependent variable	
	X_1^{*}	${X_2}^*$	X_3^*	X_4^*	GFP ⁺ cells (%)	
1	-1	-1	-1	-1	0.4	
2	1	-1	-1	1	26.1	
3	-1	1	-1	-1	2.2	
4	1	1	-1	-1	0.0	
5	-1	-1	1	-1	0.9	
6	1	-1	1	-1	0.0	
7	-1	1	1	-1	10.3	
8	1	1	1	-1	0.0	
9	-1	-1	-1	1	0.5	
10	1	-1	-1	1	35.2	
11	-1	1	-1	1	4.2	
12	1	1	-1	1	0.0	
13	-1	-1	1	1	1.9	
14	1	-1	1	1	17.4	
15	-1	1	1	1	8.3	
16	1	1	1	1	0.0	
17	-1	0	0	0	9.2	
18	1	0	0	0	10.1	
19	0	-1	0	0	25.0	
20	0	1	0	0	27.6	
21	0	0	-1	0	32.6	
22	0	0	1	0	29.3	
23	0	0	0	-1	34.7	
24	0	0	0	1	55.1	
25	0	0	0	0	38.6	
26	0	0	0	0	39.2	
27	0	0	0	0	35.0	
28	0	0	0	0	37.0	

Table 2 Experimental results of the dependent variable (GFP⁺ cells (%)) after microporation ofHEK293T using a CCD design setup.

*Uncoded levels of independent variables (X_1 =electric pulse; X_2 =pulse width; X_3 =pulse number; X_4 =DNA amount) are presented in Table 1.

			-			-
Source	SS	df	MS	F-value	F-critical	p-value
Regression	7167	13	551	23	3	< 0.001
Residual	335	14	24			
Lack of fit						
(LF)	323	11	29	8	9	0.06
Pure Error						
(PE)	12	3	4			
Total	7501	27				

Table 3 ANOVA for the reduced quadratic model (Eq. 3) that predicts the response variable GFP^+ cells, as a function of the independent variables after microporation.

Fig. 1 Predicted response surface plots relating the percentage of GFP^+ cells with two independent variables while the other two are fixed. The fixed variables were: 2 pulses and 20 ms of pulse width (A); 2 µg of DNA and 2 pulses (B) and 20 ms of pulse width and 2 µg of DNA (C). The 2-D and 3-D figures are predicted by the quadratic model equation (Eq. 3).

Fig. 2 Effect of microporation buffers SB-PBS (A) and RB (B) on gene delivery to HEK293T cells with different amounts of plasmid DNA (1 g in black and 3 g in white) at 1250 V, 20 ms and 1 pulse. The number of GFP^+ cells, cell viability, cell recovery and yield of transfection were obtained from three independent experiments (mean standard deviation).







