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## Generating nanoliter to femtoliter microdroplets with ease

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In this letter, we present a simply constructed and easy-to-use fluidic device that generates arrayed aqueous phase microdroplets in oil of controlled size with volumes ranging from nanoliter to femtoliter without surfactant. This can be applicable with a range of materials, allowing production and storage of monodisperse microdroplets. We illustrate the potential of our methodology in the field of nanoparticle generation © 2011 American Institute of Physics. [doi:10.1063/1.3560453]

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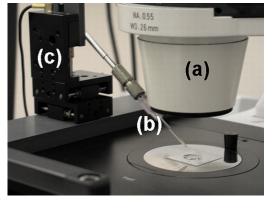
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Producing microdroplets, droplets in the micrometer 13 14 range, is of interest in many fields, including biology, bio-15 medical applications, drug discovery, chemical synthesis, 16 and particle synthesis (for photonics materials, drug deliv-17 ery). In the literature, different approaches to microdroplet 18 generation are presented, from the classical emulsion-based 19 method or bulk method<sup>2</sup> to the more recent droplet 20 microfluidics.<sup>3</sup> To date, a significant problem encountered 21 when forming droplets via bulk methods, the top-down ap-22 proach, is the wide microdroplet size distribution that typi-23 cally results. <sup>4</sup> This is remedied by emulsification at the indi-24 vidual droplet level, the bottom-up approach, based on the 25 ability of microfluidics devices to generate, control, and 26 handle microdroplets. One of the limitations of these ap-27 proaches is that necessitate the use of surfactant to achieve 28 well-defined structures (droplets) and to avoid droplet coa-29 lescence during storage. These surfactants affect chemical 30 composition and fluid interface properties. Another limitation 31 of microfluidics is that it is impossible to produce an ordered 32 pattern for channel sizes below 100 nm, because of wetting 33 properties. <sup>5</sup> Conversely, the classical emulsion-based method **34** can generate droplets in the nanometer range. Microfluidics 35 experiments are often referred to as "high-throughput droplet **36** generation." However, lower-throughput experiments, from 37 generation of a single droplet to dozens of droplets, using 38 nozzles or pipette have also been developed: for instance, **39** levitation of a single droplet, <sup>7</sup> isolated droplets held by a **40** micropipette<sup>8</sup> or nanoscale pipetting.<sup>9</sup> Note that some authors **41** describe a nozzle-free acoustic ejector<sup>10,11</sup> which has limita-42 tions due to possible liquid evaporation. All these technolo-43 gies are efficient but require a complex setup.

In this letter, we present a simply constructed and easy45 to-use fluidic device that generates arrayed aqueous phase
46 microdroplets in oil. Up to thousands of microdroplets are
47 generated with volumes ranging from nanoliter to femtoli48 ters, without surfactant. The device enables the entire volume
49 range to be attained in the course of one experiment. All
50 experiments are performed on an 18 mm diameter coverslip
51 treated in a way to obtain an hydrophobic surface to avoid
52 microdroplet spreading and coalescence, which can be ther53 mostatted, under an optical microscope (Zeiss Axio Observer
54 D1). Glass coverslip are spin coated at 4000 rpm for 1 min

<sup>(</sup>SPIN 150, SPS) with 4%-950 K PMMA (All Resist ARP 55 679.04) annealed 10 min at 170 °C. The coverslip is covered 56 with approximately 100  $\mu$ l of paraffin oil (Hampton Re- 57 search HR3-421, refractive index=1.467). The micrometer 58 sized droplets of water solution are generated on the cover- 59 slip by a microinjector (Femtojet, Eppendorf) used for the 60 injection of liquids in the volume range from femtoliters to 61 microliters. A home-made micromanipulator consisting of 3 62 miniature translation stages (piezo electric, MS30 Mechon- 63 ics) allows displacement of the injector (capillary holder) in 64 X, Y, and Z with a displacement of 18 mm in the three 65 directions by steps of 16 nm. A glass capillary (the micropi- 66 pette) with an internal diameter of 0.5  $\mu$ m (Femtotip Eppen- 67 dorf) is used. The whole setup is shown in Fig. 1. Here the 68 solution is 2.71 M NaCl aqueous solution, half the solubility 69 of NaCl in water at 20 °C. 12 Our first experiments with dif- 70 ferent solution compositions show the importance of interfa-71 cial tension between phases and viscosities of phases for the 72 control of the microdroplet sizes; however, the mechanism of 73 microdroplet generation is independent of the solution com- 74 position, as pointed out by Tabeling et al. 13 in the case of 75 microfluidics. Note that, here, we succeeded in generating 76 microdroplets with many aqueous phases tested. 14 By con- 77 trolling the speed displacement of the micropipette (in con-78 tact with the surface) and injection pressure we control the 79 droplet size. In Fig. 2(a) we show an array of monodisperse 15 80 water droplets of mean size 11.8  $\mu$ m  $\pm$  0.6  $\mu$ m. When the 81 speed displacement of the micropipette is varied from 1 to 82



0.1 mm s<sup>-1</sup>, the droplet size varies from 12 to 31  $\mu$ m [Fig. 83

FIG. 1. (Color online) Image of the whole experimental setup, (a) microscope, (b) glass capillary, and (c) XYZ miniature translation stages.

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FIG. 2. (Color online) (a) Image of droplets generated with P=5000 Pa and v=1 mm s<sup>-1</sup>, (b) Image of droplets generated with P=4000 Pa and v varying from 0.1 (first line) to 1 mm s<sup>-1</sup> (last line) by 0.1 mm s<sup>-1</sup> step, and (c) Image of droplets generated with v=1 mm s<sup>-1</sup> and P varying from 5000 Pa (first line) to 1500 Pa (last line) by 500 Pa step. All images are at the same magnification: 1 pixel=0.5625  $\mu$ m. (enhanced online) [URL: http://dx.doi.org/10.1063/1.3560453.1]

84 2(b), see video]. Furthermore, when the injection pressure is 85 varied from 1500 to 6000 Pa, the droplet size varies from 8.5 86 to 14  $\mu$ m [Fig. 2(c)]. Mean diameter variations as a function 87 of distance between droplets, speed displacement, and injec-88 tion pressure are plotted in Fig. 3.

We analyze the micropipette velocity v influences on 90 experimental results in the frame of a simple model. The 91 distance d between droplets is as follows:

$$92 d = v \times t, (1)$$

**93** where *t* the time interval between successive droplet forma**94** tions. The volume *V* of the droplet is as follows:

$$95 V = n \times t. (2)$$

**96** where  $\eta$  is the flow rate from the micropipette. From Eqs. (1) **97** and (2) we deduce that

$$V = \frac{\eta \times d}{v}.$$
 (3)

99 Assuming a spherical shape for the droplet with a diameter 100 D, thus

$$V = \frac{\pi}{6} \times D^3 \tag{4}$$

102 leads to the following:

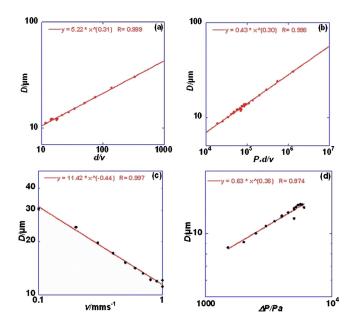


FIG. 3. (Color online) Droplet diameter vs (a) distance between droplets over speed displacements at  $\Delta P$ =4000 Pa, (b) distance between droplets with  $\Delta P$  varying between 1500 and 6000 Pa, (a) and (b) v varying between 0.1 and 1 mm s<sup>-1</sup>, (c) speed displacements at injection pressure of 5000 Pa and, (d) injection pressures at speed displacement of 1 mm s<sup>-1</sup>.

$$D = \left(\frac{6 \times \eta}{\pi}\right)^{1/3} \times \left(\frac{d}{v}\right)^{1/3} \tag{5a}$$

in a first approximation, ignoring dynamic factors, we as- 104 sume proportionality between flow rate and injection pres- 105 sure  $\Delta P$  106

$$D = A \times \left(\frac{\Delta P \times d}{v}\right)^{1/3},\tag{5b}$$

where A is a constant. Figure 3(a), a plot of D vs d/v at 108  $\Delta P$ =4000 Pa, gives  $D \propto (d/v)^{0.31}$  and Fig. 3(b), a plot of D 109 vs  $\Delta P \times d/v$ , gives  $D \propto (\Delta P \times d/v)^{0.30}$  showing a very good 110 experimental agreement with Eqs. (5a) and (5b).

We take the analysis further by introducing the mecha-  $^{112}$  nism of drop formation through the Rayleigh-Plateau insta-  $^{113}$  bility as follows:  $^{16}$  the flow generated by the microinjector  $^{114}$  passes through the exit orifice and breaks up to form drops,  $^{115}$  assuming a cylindrical stream (a liquid jet breaks because the  $^{116}$  surface energy of a liquid sphere is smaller than that of a  $^{117}$  cylinder, while having the same volume). If we assume that  $^{118}$  the fluid flowing out of the micropipette is a cylinder of  $^{119}$  radius  $^{r}$  and length  $^{d}$  ( $^{d}$  is also the distance between drop-  $^{120}$  lets), the instability occurs for the following:

$$\frac{r}{d} = B,\tag{6}$$

where B is a constant (critical ratio in the Raleigh–Plateau 123 instability). V the volume of fluid flowing out of the pipette 124 during time t [Eq. (2)], is equal to the volume of the cylinder 125 at t, thus

$$V = \eta \times t = v \times t \times \pi \times r^2. \tag{7}$$

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Combining Eqs. (6), (7), and (1) gives the following:

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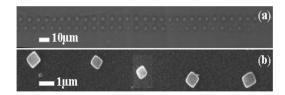


FIG. 4. (a) Array of droplets of NaCl solutions generated through the layer of liquid oil. The size of droplets is 3  $\mu$ m corresponding to an effective volume of 14 fl, and (b) SEM images of single crystals generated.

129 
$$D = (6 \times B^2)^{1/3} \times d$$
 (8)

**130** showing the linear dependence of D with d. Combining Eqs. **131** (6) and (7) gives the following:

$$132 d = \frac{1}{B} \sqrt{\frac{\eta}{\pi \times v}} = v \times t. (9)$$

133 Combining Eqs. (8) and (9) gives the following:

134

$$D = \left(\frac{6}{B \times \pi \times \sqrt{\pi}}\right)^{1/3} \times \sqrt{\frac{\eta}{v}} = C \times \sqrt{\frac{\Delta P}{v}}, \tag{10}$$

**135** where in a first approximation, ignoring dynamic factors, we **136** assume proportionality between flow rate and injection pres-**137** sure  $\Delta P$  via a constant C. Experimental results presented in **138** Figs. 3(c) and 3(d) give  $D \propto \Delta P^{0.36}/v^{0.44}$  in good agreement **139** with this model.

While such an analysis roughly describes for the rela-141 tionship of D and d with injection pressure  $\Delta P$  and velocity 142 v, there may be variations in the relationship, for various 143 reasons as follows:

- 144 (1) The fluid wets the substrate which changes the surface 145 energy balance. We observed this when the substrate 146 was changed.
- 147 (2) The fluid injected by the micropipette requires a threshold value of  $\Delta P$ , in function of its diameter.
- 149 (3) The quantity of fluid injected by the micropipette is
  150 dependent on the particular geometry of its apex. Wall
  151 thickness seems to influence the droplet size, for
  152 instance.

153 Figure 2 show droplets of diameters ranging from 32 to 154 8.5 μm corresponding to volume ranging from 321 to 15 pl 155 (assuming a spherical shape for the droplet). Further research 156 should determine the three-dimensional shape of the drop-157 lets; for instance, some authors have proposed a hemisphere 158 for microdroplets of 5 μm deposited on a glass coverslip. 159 Note that generating droplets of hundreds of microns, in the 160 nanoliter range, is easy with this setup. Conversely, in the 161 example presented below droplets of 3 μm are generated, 162 thus the femtoliter range is also attainable.

Finally, we illustrate the potential of our methodology in 164 the field of particle generation, where small volume systems

offer promising properties. <sup>17,18</sup> Figure 4(a) presents an array <sup>165</sup> of monodisperse droplets of 3  $\mu$ m containing NaCl 2.71M 166 solution. Droplets slowly evaporate until supersaturation is 167 established. A high supersaturation level is reached and a 168 single nucleation event occurs, always yielding one single 169 crystal of monodisperse size ( $740 \times 740 \times 370 \text{ nm}^3$ ) per 170 droplet [Fig. 4(b)], heights of crystals were measured by 171 AFM. However, applications fields are not restricted to this 172 field, as pointed out in the introduction.

In conclusion, we have developed a technique using a 174 commercial microinjector coupled with an X, Y, and Z mi- 175 cromanipulator which is applicable to a range of materials 176 and allows the production and storage of monodisperse mi- 177 crodroplets of aqueous phase in oil and without surfactant, 178 maintaining control over size. Moreover, because isolated 179 aqueous microdroplets are generated by micropipette, they 180 can be manipulated individually by micropipette. Finally, 181 this technology can be implemented in standard laboratory 182 environments.

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