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Giant coercivity of dense nanostructured spark plasma sintered barium hexaferrite

F. Mazaleyrat, A. Pasko, A. Bartok, M. LoBue



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F. Mazaleyrat, A. Pasko, A. Bartok, M. LoBue Giant H_C of SPS Ba-ferrite — MMM 2010 Atlanta

Introduction

- Features of current hard magnets
- RE subtitutions in hexaferrites
- Nanostructured hexaferrites

2 Synthesis of Ba nano-ferrite

- Sol-gel
- Thermal treatment

3 Results

- X ray diffraction
- electronic microscopy
- Magnetic properties

Conclusion



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Features of current hard magnets RE subtitutions in hexaferrites Nanostructured hexaferrites

SmCo Magnets

- High coercivity; high Curie point
- Medium remanence; high cost



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NdFeB

- High coercivity; high remanence;
- Low Curie point; medium price.



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Hexaferrite

- Medium coercivity; low remanence
- Positive thermal coefficient of coercivity; low cost



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Features of current hard magnets RE subtitutions in hexaferrites Nanostructured hexaferrites

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Image: A mathematical states and a mathem

La and Co substitution in Sr ferrite

Composition

 $Sr_{1-x}La_xFe_{12-y}Co_yO_{19}$

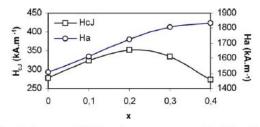


Fig. 1. Anisotropy field H_a and intrinsic coercivity H_{cJ} of $Sr_{1-x}La_x$ $Fe_{12-x}Co_xO_{19}$ ferrite magnets measured at room temperature.



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Néel or Stoner-Wohlfarth model

- perfectly oriented isotropic magnet $\mu_0 H_C = \frac{2K}{J_S} = \mu_0 H_K = 1.7 \text{ T}$
- isotropic magnet $\mu_0 H_C = 0.48 \mu_0 H_K = 0.85~{\rm T}$ and $J_R = J_S/2 = 0.25~{\rm T}$



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Problem

- works not badly loose nano-powders $\mu_0 H_C \gtrsim 0.55~{
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- sintering yields grain growth \Rightarrow nucleation field $\mu_0 H_C = \mu_0 H_N = 4\mu_0 \frac{\sqrt{AK}}{J_5 D} \approx 0.25 \text{ T}$



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Solution

Use spark plasma sintering to densify without grain growth



Sol-gel Thermal treatment

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Sol-gel Thermal treatment

sol-gel citrate precursor method

starting material

- High purity iron(III) nitrate + barium hydroxide;
- citric acid \rightarrow molar ratio of citrate to metal ions 2:1.;



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Iron hydroxide preparation

- Iron(III) nitrate dissolved in water, precipitated with ammonia \rightarrow iron(III) hydroxide
- filtering and washing



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Sol-gel

- iron(III) hydroxide dissolved in citric acid at 60-70°C
- barium hydroxide additon
- chelation of metal ions at pH6



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Sol-gel Thermal treatment

Compound formation



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Sol-gel Thermal treatment

Compound formation

• evaporation $(80-90^{\circ}C) + drying (150-170^{\circ}C)$



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Sol-gel Thermal treatment

Compound formation

- evaporation (80-90°C) + drying (150-170°C)
- elimination of organic matter at 450°C for 2 hours in air



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- calcination in air at different temperatures between 700 and 1000°C



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Sol-gel Thermal treatment

Compound formation

- evaporation (80-90°C) + drying (150-170°C)
- elimination of organic matter at 450°C for 2 hours in air
- \bullet calcination in air at different temperatures between 700 and 1000°C
- choice of optimal treatment for smaller grain size fully formed compound \Rightarrow 900°C/1 h

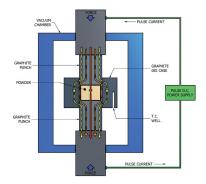


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Sol-gel Thermal treatment

Spark Plasma Sintering

- Heating rate 160 Kmin⁻¹
- Temperature 800°C
- Duration 0 to 20 min
- Cooling rate 160 Kmin⁻¹
- Pressure 50 MPa



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X ray diffraction electronic microscopy Magnetic properties

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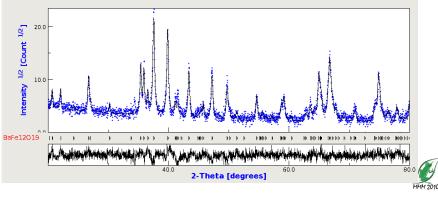


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X ray diffraction electronic microscopy Magnetic properties

Refinement of XRD spectra

- M phase Ba hexaferrite is formed after calcination
- example: sample SPS0 (0 min)



Computation made using Rieveld based MAUD software Computation made using Rieveld based MAUD software Computed and Compute

X ray diffraction electronic microscopy Magnetic properties

Quantitative results of XRD analysis

| Sample | Sintering | Lattice constants | | | Cr. size | Density |
|---------------|---------------|-------------------|---------------|----------------------|---------------|---------|
| Ref. | time (min) | <i>a</i> (nm) | <i>c</i> (nm) | v (nm ³) | <i>D</i> (nm) | (%) |
| Lit* | single cryst. | 0.5892 | 2.3183 | 0.6970 | - | 100 |
| Com^\dagger | coarse grain | 0.5893 | 2.3201 | 0.6977 | >1000 | >95 |
| CP | as calcinated | 0.5895 | 2.3219 | 0.6987 | 60 | - |
| SPS0 | 0 | 0.5888 | 2.3238 | 0.6976 | 70 | 76 |
| SPS5 | 5 | 0.5890 | 2.3237 | 0.6981 | 84 | 94 |
| SPS13 | 13 | 0.5886 | 2.3222 | 0.6967 | 74 | 88 |
| SPS20 | 20 | 0.5889 | 2.3226 | 0.6976 | 77 | 86 |

* litterature values from data base



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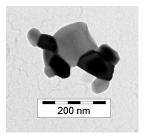


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X ray diffraction electronic microscopy Magnetic properties

TEM — Calcinated powder

Particles are nearly equiax with size matching XRD analysis with relatively large distribution (50-200 nm)



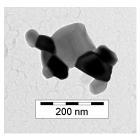
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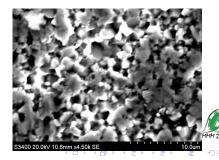
TEM — Calcinated powder

Particles are nearly equiax with size matching XRD analysis with relatively large distribution (50-200 nm)



SEM — Sintered

The material is composed of 1μ m nano-grains with several 100 nm pores



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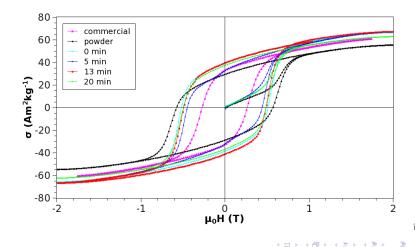
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X ray diffraction electronic microscopy Magnetic properties

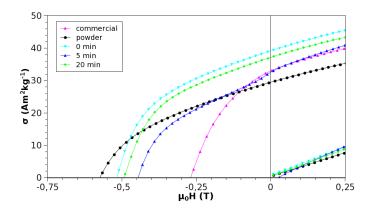
Hysteresis loops





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The role of grain size homogeneity



The double-phase behavior of sample SPS5 is due to the presence of big particles



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Correlation coercivity/structure

Grain size

No clear correlation is found with the grain size, due its small change and accuracy



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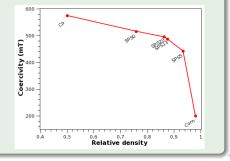
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Density

Density seems to play the leading role through exchange at interface and internal demagnetization. For the powder (CP) d is arbitrarily set to 0.5

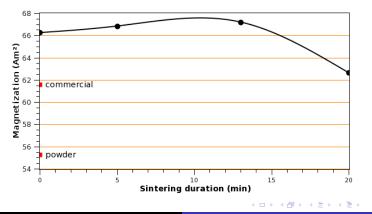


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Saturation magnetization

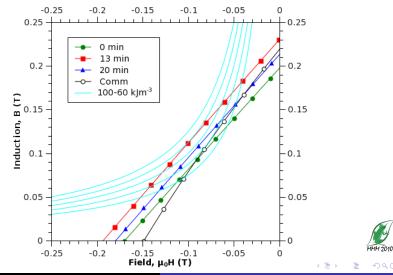
- sintering presumably changes Fe^{3+} positions in the different sites $\Rightarrow M_S \nearrow$ (lattice parameter $c \nearrow$)
- 2 reduction of Fe³⁺ into Fe²⁺ \Rightarrow *M*_S \searrow



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Functional properties



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Conclusion and prospects

Conclusion



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Conclusion and prospects

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SPS combines very fine grain size and high density



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- Evolution of saturation magnetization has to be cleared-up
- Anisotropic magnets have to be produced



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Problem

Orientation of nano-particles is difficult



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Thank you for your attention!

