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# Drive-by-Wireless Teleoperation with Network QoS Adaptation

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Abstract—This paper describes an adaptation scheme for driveby-wireless teleoperation of an electric vehicle. The performance variation due to the varying time delay and packet losses is investigated and catered for by using an adaptive gain scheduling as well as varying network load in the co-design framework. A support vector machine (SVM) predictor is proposed for network delay and packet loss prediction while, fuzzy based estimation and control is employed for QoS evaluation and corresponding reconfiguration for video packet rate and controller gain in order to ensure passivity and improved transparence.

Keywords-Networked teleoperation; co-design problem; driveby-wireless; supervised learning; QoS estimation

#### I. INTRODUCTION

In drive-by-wireless teleoperation, a remote vehicle is controlled with a wireless connection as opposed to traditional electrical, hydraulic and mechanical methods as presented in [1]. The control and video information is exchanged between the driver (master) and the vehicle (slave) bilaterally during teleoperation. Long distance teleoperation employs hybrid/heterogeneous communication network to transport command and feedback data between the operator and the slave system as direct control is not possible in scenarios where the mobile teleoperator (slave) is located in hard to reach or dangerous remote areas.

In addition to mobility, a wireless network eliminates hard connections between one or more control and sensor modules which results in simple design and lowered installation and maintenance costs. Moreover, for multi-vehicle case, a wireless network is more effective than point-to-point communication links as proposed in [2]. However, as per [3], wireless networks induce additional delays and information loss as they could be easily perturbed by the environmental effects and interference due to multipath effects or due to other communicating entities. [4] and [5] emphasize that the drive-by-wireless systems require multi-domain knowledge including communication networks, vehicle dynamics and bilateral teleoperation with force feedback for better haptic sensation.

In the literature, generally, bilateral teleoperation utilizes master-slave pair which communicates over a communication network. Despite its interesting features, bilateral teleoperation has some limitations and performance dependencies over several factors. The number of tasks they can perform as compared to human are also limited, since the dexterity of teleoperator is poorer Denis Genon-Catalot LCIS, Valence Denis.genon-catalot@iut-valence.fr

than the human dexterity as noted in [6]. This even worsens and sometimes destabilize with the added time delays. In addition to stability, bilateral teleoperator are supposed to provide sufficient transparency despite the presence of mechanical nonlinearities and communication imperfections as discussed in [7]. We consider only passivity based architecture for bilateral teleoperation of drive-by-wireless applications, which utilize energy concepts and impose the passivity requirement for each individual sub-system. However, this approach is too conservative, in the sense that it does not guarantee good performance under all operating conditions as argued in [8]. This justifies the intelligent adaptation of control gains with the operating conditions to maximize the performance and satisfy all control objectives.

In modeling a communication channel only time delay is considered during analysis and full knowledge of communication protocol with its flexibilities, limitations and QoS aspects are rarely addressed by the control engineers. However, it is interesting to investigate that even if the wave variables are exchanged between master and slave, giving a notion of importance to this information or using some network based tactics can improve the quality of tracking and performance in bilateral teleoperation for drive-by-wireless application. This requires a co-design approach applied to robotic systems as shown in [9] and [10].

#### II. CONTROLLER DESIGN FOR BILATERAL TELEOPERATION

The classical architecture for bilateral teleoperation, proposed by [11] was based on the scattering and passivity theory, which assures robustness against the network delays. This architecture neither guarantees the position tracking in stationary conditions nor force detection during the functioning of the system. In [12], the authors expanded the Anderson's work to guarantee stability under time varying delays but it produces significant transient oscillations.

In [13], the traditional configuration based on passivity is utilized and a position control loop is added on the master/slave side to track the position and force as shown in Fig. 1. In [14], a detail survey of techniques in bilateral teleoperation is presented. The single degree of freedom (DOF) master/slave dynamics with position control loop in standard notation are given as:

$$M_m x_m + B_m x_m = F_h + F_m \tag{1}$$

••

$$M_{s} x_{s} + B_{s1} x_{s} = F_{s} - F_{e}$$
(2)

where  $x_m$  is the velocity of the master,  $F_h$  and  $F_m$  constitute the control couple applied to the motors at the master/slave,  $M_m$ ,  $M_s$  are the inertias,  $B_m$ ,  $B_{s1}$  are the viscous frictions of master and slave,  $F_h$ ,  $F_e$  are the reaction couple from the operator and the environment and  $x_m$ ,  $x_s$  are the respective positions.  $F_{feed} = K(x_m(t-T)-x_s)$  and  $F_{back} = K(x_s(t-T)-x_m)$  are the position controllers for the slave and master loop respectively. We utilize the scattering transformation to assure the passivity of the system in the presence of constant time delays so that the characteristics that describe the channel are similar to those of a transmission line without losses. The transformation used in Anderson and Spong (1989) is as under:

$$U_{m} = \frac{1}{\sqrt{2b}} (F_{m} + b \dot{x}_{m}), \quad V_{m} = \frac{1}{\sqrt{2b}} (F_{m} - b \dot{x}_{m}) \quad (3)$$
$$U_{s} = \frac{1}{\sqrt{2b}} (F_{s} + b \dot{x}_{sd}), \quad V_{s} = \frac{1}{\sqrt{2b}} (F_{s} - b \dot{x}_{sd}) \quad (4)$$

The scattering variables  $(u_m, u_s, v_m, v_s)$  are transmitted across the delay line instead of the original velocities and forces. The transient error is dependent on delay while in the steady state position tracking  $e(t) = x_m(0)-x_s(0)$  is dependent on the initial position difference even when there is no packet loss. However, with packet losses, the performance of the control loop deteriorates even more. The position tracking error is defined as  $e = x_m(t-T)-x_s(t)$ , where  $x_m(t-T)$  is the delayed master position received on the slave side. For the stability analysis, it is assumed that the human operator and the environment model are passive systems, bounded by known functions of the master and slave velocities. All signals are assumed to belong to the extended  $l_{2e}$  space and  $x_m, x_s=0$  for t < 0.

#### III. STABILITY AND PERFORMANCE IN PASSIVE BILATERAL TELEOPERATION

The stability of the position controller is proposed with a Lyapunov function which puts the condition proven in Chopra et al. (2004) that:

$$\mathbf{K}_{\text{pass}} \prec \sqrt{\frac{b_m b_{s1}}{\tau^2}} \tag{5}$$

Where  $K_{pass}$  is the gain limit which should not be exceeded in order to respect the passivity.

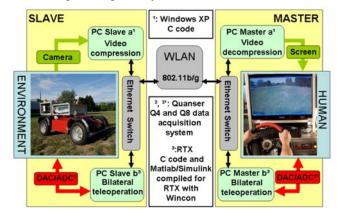


Figure 1. NeCS-Car Embedded System and Communication Architecture.

Using Barbalat's lemma it was shown that the tracking error can be rewritten in (6) as found in [5]:

$$\mathbf{e} = \mathbf{x}_{\mathrm{m}}(\mathbf{t}) - \mathbf{x}_{\mathrm{s}}(\mathbf{t}) - \int_{\mathbf{t}-T} \mathbf{x}_{m}(\tau) d\tau \qquad (6)$$

It is important to note that the stability of this architecture is proven by taking into account a fixed delay assumption. However, the simulation results prove that the system is stable under limited packet losses, whereas the tracking performance is degraded with increasing packet losses. The transparency objective performance metric requires that the impedance perceived by the human and the environment impedance must be equal as shown in [19], i.e.  $Z_h = Z$ . In addition, the position and force at the master interface and the slave are ideally required to be equal. However, it depends on the similarity between master and slave devices, gain adjustments and delays introduced by the network. The stiffness decreases with the increased delay and packet loss rate. The mechanical impedance Zt is the transmitted impedance of the slave as seen by the human operator i.e. Z. In most cases this impedance can be sufficiently well approximated by an LTI system and hence can be formulated as the transfer function shown above. Thus, with increased delay and packet losses, environment impedance Ze decreases and affects the transparence.

#### IV. NECS-CAR EXPERIMENTAL SETUP

The NeCS-Car is a dedicated platform for teleoperation funded by the Networked Control System (NeCS) team at the Control System department of GIPSA-lab. A remote operator can drive the car via a hybrid (Ethernet + WLAN) networked communication by observing the video and force feedback.

#### A. Hardware

The overall system architecture is shown in Fig. 1. The embedded PC hosts 2 operating systems, each having their own network card and can be considered as 2 separate PCs for video and control system. For communication between controller, image processor and IP video cameras, Ethernet is used as the embedded network which is connected with a 100 Mbps switch linking the Slave with the Master via WLAN router.

#### B. Communication

Some time critical data is exchanged between master and slave because this 200 Kg vehicle can be driven up to a maximum speed of 10 m/s on uneven ground. The control data (speed, position, brake, etc) is sent over UDP. The packet size for control information is 83 bytes (125 bytes with header) of data sent with a sampling rate of 1000 Hz (1 Mbps). About 20% of the traffic sent over UDP is lost. For video data, both TCP/IP or UDP/IP protocol and different compression algorithms can be tested. IP camera with MPEG-4 compression can also be connected to the slave Ethernet switch to generate traffic perturbations (data rate of 3.1 Mbps over TCP/IP measured while driving) over the network. For control data reconstruction due to packet loss, our approach is similar to [18] where scattering transform energy is exchanged to continuously monitor the passivity condition in order to choose between the hold last value (HLS) and zeroing. In this way, passivity of the communication block is conserved. NeCS-Car parameters used are as follows:  $M_m = 0.0284 \text{ N.m}^2 / \text{rd}$ ,  $M_{s1} = 3.25 \text{ N.m}^2 / \text{rd}$ ,  $B_m = 0.0817 \text{ N.m.s/rd}$ ,  $B_{s1} = 5.6833 \text{ N.m.s/rd}$ . The sampling time  $T_s = 0.001s$ .

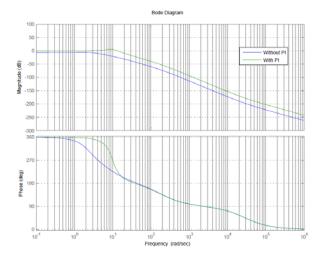


Figure 2. Bode plot with and without PI Controller.

A PI controller is used to improve the reversibility with  $K_p = 10$ and  $T_i = 0.2$ . The improvement in response is witnessed by the bode plot where larger bandwidth is available due to higher cutoff frequency with PI controller as shown in Fig. 2.

#### V. ANALYSIS OF TRANSPARENCE IN DRIVE BY WIRELESS APPLICATIONS

Transparence refers to the good feeling of the task felt by the operator. Ideally, the operator feeling to sense the ground and environment should be the same as if he/she is directly interacting at the teleoperator site. This concept is difficult to model and defined as a mathematical formulation for quantitative performance measure. However, there are several approaches in the literature today e.g. in [29], [30] and [31]. The classical approach takes into account the impedance matching between the master and the slave [31]. In [32], an extended transparence condition is defined based on trackability and immersivity.

In most cases, the H-matrix is used to describe the transparence which relates the output variables slave velocity  $(V_s)$  and reflected force  $(F_h)$  with the input variables reflected force  $(F_e)$  and master velocity  $(V_m)$ , as:

$$H = \begin{bmatrix} h_{11} & h_{12} \\ h_{21} & h_{22} \end{bmatrix}$$
(7)

Where,  $h_{11} = \frac{F_h}{V_m}\Big|_{F_e=0}$  is the master impedance  $Z_m$ ,  $h_{21} = \frac{V_s}{V_m}\Big|_{F_e=0}$  is the velocity gain (G<sub>v</sub>) from master to slave,  $h_{12} = \frac{F_h}{F_e}\Big|_{V_m=0}$  is the force Gain (G<sub>F</sub>) and  $h_{22} = \frac{V_s}{F_e}\Big|_{V_m=0}$  is the slave admittance (Y<sub>s</sub>).

For optimal transparence,  $G_F=G_v=1$  which result in  $V_m = V_s$ and  $F_h = F_e$ . Also, it is required that  $Z_m=0$  and finally the slave should be unaffected by the external forces ( $Y_s=0$ ). However, these ideal requirements are rarely satisfied due to the sensor and actuator non-linearities and hardware limitations.

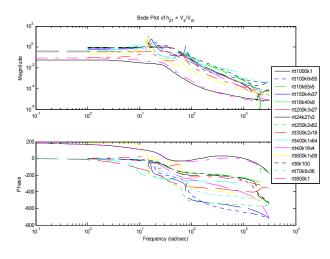
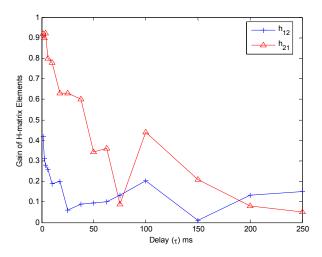
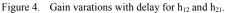


Figure 3. Bode plot of  $h_{21}$  with variation in delay.

In Fig. 3, variation of gain and phase with frequency is shown. As delay increases, the cutoff frequency decreases so as the stability margins. This fact is more visible from Fig.4, 5, 6 and 7.





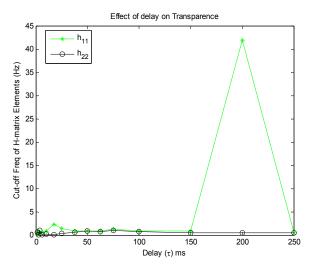


Figure 5. Variation in cut-off frequency of  $h_{11}$  and  $h_{22}$  with delay.

As noted in Fig. 4, as delay increases both  $h_{12}$  and  $h_{21}$  magnitude decreases showing a deteriorated response. From Fig.5,  $h_{11}$  is shown to have increasing magnitude with increasing delay. While for  $h_{22}$ , the gain decreases with delay. The cut-off frequency is shown in Fig. 6 and 7. The overall impression can be obtained in general for having a decreasing trend. Thus, it can be deduced that cutoff frequency decreases with delay.

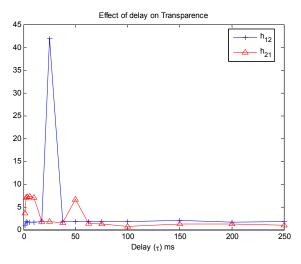


Figure 6. Variation in cut-off frequency of h<sub>12</sub> and h<sub>21</sub> with delay.

#### VI. CO-DESIGN FOR DRIVE-BY-WIRELESS APPLICATION

The network conditions are important to take into account for successful teleoperation of a remote vehicle. The co-adaptation of control with QoS requires a co-design approach. Wireless network OoS is evaluated in several applications e.g. for topology control, intelligent routing and handover from one cell to another in mobile telephony. The intelligent decision is required when a mobile user needs to change current cell to perform handover. In many scenarios, artificial intelligence (AI) techniques are used for the case of heterogeneous network (vertical handover) or homogenous network (horizontal handover) to choose between the base stations, based on QoS performance parameters as in [25] and for congestion estimation in sensor networks as in [22] and [23]. In [26], a neural network based feedback scheduler is proposed for networked control systems with flexible workload. Fuzzy approach is found to be used in wireless networks for intelligent admission control, bandwidth control, scheduling and policing as shown in [27]. Networked control systems (NCS) also utilize AI techniques for scheduling, integrated design, diagnosis and reconfiguration in the presence of faults e.g. [20] presents fuzzy bandwidth scheduling to manage the quality of control (QoC) and requirement of bandwidth (RoB) in NCS. In our proposition of the co-design approach, the complete architecture is shown in Fig. 8.

#### A. Delay and Packet loss Prediction

The first block of the co-design architecture comprises of delay and extracting the packet loss information from it. The support vector machine (SVM) is a popular method for chaotic time series forecasting as in [21]. Support Vector Machine (SVM) has the property to transform a training vector into a high dimensional

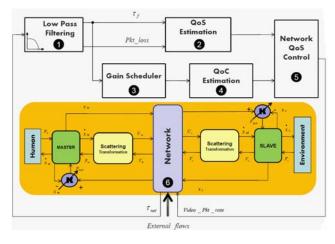


Figure 7. Co-adaptation strategy for bilateral Teleoperation.

(theoretically infinite) dimensional space by the function. SVM finds a linear separating hyper plane with the maximal margin in this higher dimensional space. In [17], a new use of SVM as a prediction tool is proposed. In this work, the idea has been modified to an adaptive (one sample ahead) prediction tool, for an online implementation.

#### B. Prediction quality and performance

There are several hyper-parameters of SVM learning machine module that need to be arbitrary chosen in order to ensure the best possible quality and performance of prediction. These parameters are:

- Kernel type For the kernel type, RBF (Radial Basis Function) is preferred since other studies as [16], [24] and [15] have shown that it is the most suitable one for the prediction problem.
- c Cost parameter, is a tradeoff between model flatness against tolerance of deviations larger than epsilon in optimization formulation.
- ε Epsilon parameter which determines the zone of insensitivity of cost function, ε=0.1 is found sufficient for our case.
- κ MSE check horizon Since the proposed module constantly adapts it selves to current network conditions, it is necessary to choose an appropriate horizon of past samples which will be used to calculate current MSE error.
- α MSE (Mean Square Error) check threshold Past samples determined by MSE check horizon are compared with the same (in terms of time) predicted samples and the SVM model is retrained if MSE is bigger than the MSE check threshold.
- λ Training horizon is the number of past samples used to train the SVM model.
- µ Error threshold for SVM training is chosen as 2 ms for our
   case which corresponds to the sampling rate of 1 ms.

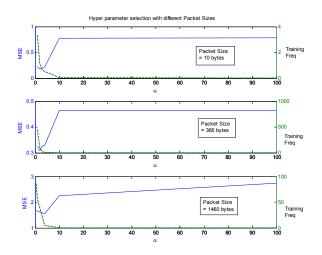


Figure 8. Fuzzy Packet rate surface

In Fig. 9, a selection of key hyper parameters for different packet sizes is shown. Thus, MSE and training frequency are plotted against MSE threshold ( $\alpha$ ). When large values of ' $\alpha$ ' are allowed, it means that the MSE may go higher and the training frequency will be lower and vice versa. As seen from the Fig. 9, for different packet sizes (10 bytes, 366 bytes and 1460 bytes), the optimum MSE threshold is quite close which means that SVM prediction can be used for variable packet sizes.

#### VII. QUALITY OF SERVICE ESTIMATION

The second block is the QoS module to estimate QoS from delay and packet loss. The QoS is defined as the necessary network resources made available for a particular application, so it is dependent on the application requirements. In literature, several criterions are available for QoS estimation e.g. by evaluating the received signal strength (RSS), signal to noise ratio (SNR), bit error rate (BER), available bandwidth, packet loss rate etc. Our approach is to use fuzzy inference for estimation of QoS. This will result in reconfiguring the network flows as well as the controller parameters in order to achieve appropriate gain values for position control, thus ensuring improved quality of control (QoC) in bilateral teleoperation.

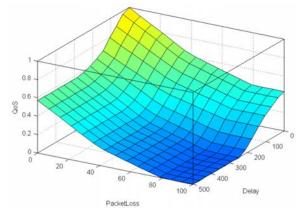


Figure 9. Fuzzy QoS surface

Fuzzy inference system operates with fuzzy sets (F), characterized by a membership function (x) which gives the degree of similarity of x to F. Thus, FIS is capable of approximating any continuous function with an arbitrary bound B as in [27]. In engineering, the most widely used are the rule-based FIS of Mamdani or Takagi Sugeno type. In this work, only triangular MFs are used in Sugeno FIS for delay (DL) and packet loss (PL) as the two inputs of QoS fuzzy inference block. The range of delay varies from 0 to 500 ms, for packet loss it is 0 to 100 and for QoS it is scaled between 0 and 1. The fuzzy rule base (reduced) for QoS estimation is shown in Table 1, where QoS has more weight for packet loss than delay. This is because of the fact that the information loss has a severe impact on transparence and stability as compared to delay.

TABLE I.	FUZZY RULE BASE INSIDE THE QOS ESTIMATOR WITH 2
	INPUTS

DL	PL	QoS	α
NE	LW	EX	1
NE	HH	GD	1
NE	VH	BD	1
SL	NE	EX	0.5
LG	NE	GD	0.5
VL	NE	BD	0.5
	NE NE NE SL LG	NE LW NE HH NE VH SL NE LG NE	NELWEXNEHHGDNEVHBDSLNEEXLGNEGD

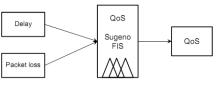


Figure 10. QoS Fuzzy Inference system (FIS)

As noted from above that the simple rules are chosen to ensure rapid decision and low computation for online use. The two input variables are given the states as none (NE), Small (SL), Large (LG) and Very Large (VL) for delay. Low (LW), High (HH), Very High (VH) for packet loss and the QoS output is marked with Excellent (EX), Good (GD) and Bad (BD) levels.

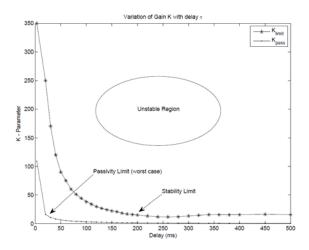


Figure 11. Variation in Controller Gain with delay

Fig. 9 shows the nonlinear surface representing the effect of delay and packet loss on QoS.

#### A. Gain Scheduling

The third block in the co-design architecture is the gain scheduling. With increasing delay, the gain for the position control loop needs to be decreased in order to respect passivity and therefore stability. The gain is adapted from the relation between delay t and gain K as shown in Fig. 5. The outer curve  $K_{limit}$  shows the values of gain where stability is lost as experienced in real time. Next, the inner curve gives the limit imposed by the passivity condition. The practical values of K on the system which takes into account the worst case value of  $B_{sl}$  are taken as about 50% of the  $K_{pass}$ . Worst case damping values are used in the passivity criteria to make sure that the passivity is respected at all operating conditions.

The variation in passivity condition is dependent on the time delay and varying values of master and slave damping  $B_m$  and  $B_{s1}$  respectively.  $B_{s1}$  varies due to the nonlinearities e.g. backlash (0.2328 rad), dry friction etc in the Rack and Pinion Gearset (RPG) as well as due to wheels in contact with the environment. Whereas,  $B_{s1}$  has different values for different drivers. The worst case values for  $B_{s1}$  and  $B_m$  are estimated as 1.3123 N.m.s/rd (without wheels) and 0.0817 N.m.s/rd (free steering) respectively.

#### B. Quality of Control Estimation

The fourth block is used to estimate QoC and the tracking performance. It is a combined sum of position, velocity and force errors as follows:

$$QoC_{\varepsilon} = 1 - (Gqos_{F} * \varepsilon_{F}) + (Gqos_{x} * \varepsilon_{x}) + (Gqos_{v} * \varepsilon_{v})$$
(7)

where,  $Gqos_F$ ,  $Gqos_x$  and  $Gqos_v$  are arbitrary scaling weights for errors in force (F), position (x) and velocity (v) as per design objectives and for our experiments, they are taken as 0.001, 1 and 0.1 respectively to normalize the tracking errors as given in Eqs. (8), (9) and (10) below.

$$\varepsilon_{x} = x_{s} - x_{m} \qquad (8)$$
  

$$\varepsilon_{v} = v_{s} - v_{m} \qquad (9)$$
  

$$\varepsilon_{F} = F_{e} - \Gamma_{m} \qquad (10)$$

Where,  $\Gamma_m$  is the applied motor torque resulting from the input force/velocity at the master end.

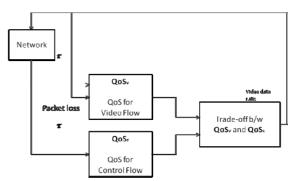


Figure 12. Variation in Controller Gain with delay

The simplified co-design architecture for implementation is shown in Fig. 12. The delay is taken as  $\tau_v = \tau_c + \tau_p$ , where  $\tau_v$  and  $\tau_c$  are the delays in video and control flows respectively.  $\tau_p$  is the fixed delay in the video flow due to processing except the communication delay on the network i.e. video acquisition, coding, packetization, reception of packets, decoding and video display. This is because  $\tau_c$  is easy to measure on the master station. The QoC function is a performance measure for the control and tracking performance as well as the time domain on-line transparence which is given in Eq. (7). The tradeoff between QoS<sub>v</sub> and QoS<sub>c</sub> is given as:

$$QoC = p * QoS_{\tau} * (1-p) * QoC_{\varepsilon}$$
(11)

where,

$$p = \frac{1}{1 + \left| X_{m}^{\bullet} \right|^{2}}$$

and  $|x_{-}|$  is the master's velocity. When  $\dot{x}_{m} \to 0$ ,  $QoS_{\tau}$  will have a unitary value while  $QoC_{\varepsilon}$  will approach to zero.  $QoS_{\tau}$  is the QoS of the control flow dominated by the delay, while  $QoC_{\varepsilon}$  is based on scaled control errors. This is important to consider because in the steady driving, when there is no control action applied from the driver, there is no need to evaluate QoC. Thus, the only parameter of interest will be QoS which is a direct function of delay. The time varying gain which is the output of controller block is normalized (K=K/100) and passed through a low pass filter  $G_k = \frac{1}{5s+1}$ , to avoid noisy

switching of the controller. The time constant of the controller has double frequency as compared to the highest frequency of the slave dynamics to avoid aliasing (Slave dynamic model pole  $p_s = -0.0907$  rad/s as compared to the controller filter pole  $p_k = 0.2$  rad/s).

#### C. Network QoS Control

The fifth block in the co-design architecture is the Fuzzy QoS management block. The input variables includes QoS, QoC and the distance between the Master/Slave stations, while the output is the video packet rate as shown in Fig. 8. All these I/O variables are ranged between 0 and 1 except the distance which is taken from 0 to 100 m.

To control the delay experienced in the control loop, the video traffic can be varied. This variation can be performed in the steps of 10 packets=sec to vary from 10 packets (121 kbps) to 1000 packets (12.1 Mbps). The non-linear relation between delay and video traffic with the maximum bound is shown in Fig. 8, which is used in the simulation. This delay curve is just used as a reference for simulating the e ect of video rate on delay; otherwise, it depends on environment type and time of experimentation. The maximum video rate does not exceeds the (one-way) delay of 250 ms. Delay exceeding 500 ms is considered as the communication failure and as a result the NeCS-Car safety loop stops the car immediately.

As shown in Table 3, the input variables are marked with none (NE), Good (GD), Bad (BD), Average (AV) and Very Large (VL). While, the output has levels such as High (HH), Low (LW), Medium (MD) for packet rate. The packet rate FIS surface is shown in Fig. 13. It can be noted that the role of distance is limited in decision as given by a single rule which states that when the slave is farther than d, packet rate just can't be made better as the link capacity is limited. This is because the distance measure (GPS or estimated) has large errors as compared to WLAN range and vehicle speed, therefore not suitable for online QoS management. Knowing that the QoC is the actual objective of our design, all QoC rules have double weight in the decision.

 
 TABLE II.
 MSE check threshold versus quality and performance of SVM prediction (packet size 1460 bytes, trace length 10000 samples)

c	ε	α	к	λ	Quality (MSE)	Quality (NMSE)	Performance (% trainings per sample)
1	0.1	0.5	16	100	1.6837	0.8147	86.32
1	0.1	1	16	100	1.6602	0.8033	56.69
1	0.1	4	16	100	1.5512	0.7506	5.08
1	0.1	10	16	100	2.2586	1.0929	0.32
1	0.1	100	16	100	2.7448	1.3281	0.01

#### D. Network Block

The sixth block in the architecture is the network architecture and the chosen protocol. In recent technologies, QoS classes are available to be mapped on flows and ports for guaranteed bandwidth and delay characteristics e.g. 802.11e, 802.1p/q, 802.16 etc.

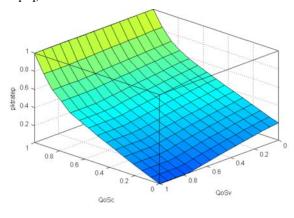


Figure 13. Fuzzy Packet rate surface

In addition, whether the network is wired or wireless also affects the performance. In wireless networks, interference and multipath phenomenon is troublesome.

 TABLE III.
 FUZZY RULE BASE INSIDE THE PR CONTROLLER

	OoC	Distance	PR	Α
QoS				1
	-			1
NE	BD	NE	LW	1
NE	AV	NE	MD	1
GD	NE	NE	HH	0.5
BD	NE	NE	LW	0.5
AV	NE	NE	MD	0.5
NE	NE	VL	LW	1
	GD BD AV	NE BD NE AV GD NE BD NE AV NE	NEBDNENEAVNEGDNENEBDNENEAVNENE	NEBDNELWNEAVNEMDGDNENEHHBDNENELWAVNENEMD

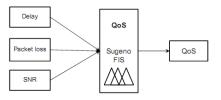


Figure 14. Fuzzy Inference system (FIS) for Packet rate generation

Dual band routers offer redundant frequency channels and two different SSIDs to switch networks in case of degraded QoS over one. External flows are simulated to vary network load and observe performance changes.

#### E. Co-Adaptation with QoS

The co-design architecture is implemented on NeCS-Car for real time performance. Fig. 15 shows the comparison of adaptation of video data rate with variations in delay and packet losses with the case where fixed video data rate  $(\phi_{fix} = 10Mbps)$  is sent over the network. This test is performed in the static conditions and inside the lab. At 55 sec and 105 sec, two external video flows of  $(\phi_{ext1} = \phi_{ext2} = 3Mbps)$  over TCP/IP are added to simulate the network perturbations. This results in low QoS, due to increased delay and packet loss detected by the QoS module. Thus, the QoS controller generates the respective gain K and video packet rate fn for the bilateral teleoperation. The result proves the corresponding decrease in video rate and improvement in QoC as shown in Fig. 16. It can be noted that in case of fixed data rate, the external perturbations would result in very low gain for position controller and poor tracking performance. The improved performance in QoC is obtained at the cost of deterioration in video quality due to decreased video data rate. However, this degradation is not annoying for the operator (up to a limit defined by human perception) as seen in the quality of video context.

In the second part, we carried out dynamic testing in a ushaped path, where the vehicle comes back towards the master after around 60 sec as shown in Fig.17. As can be noted, the distance between the master and slave increases, due to the decreasing QoS<sub>c</sub> and increasing delay and packet losses, the change in video data rate (above the nominal data rate) reduces to zero at 50 sec. At this time the return path started and the network QoS starts improving again. While the rising time constant for the data rate is quite larger as compared to the decreasing time constant, the video rate mounts guite slowly, offering lowest possible delay for the control flow. Due to poor network conditions, the vehicle stopped at 100 sec as the delay rises instantly and the safety loop comes into action to stop the car. A v-shaped trend in the video rate can be noted which exactly reflects the NeCS-Car movement away from the base station and towards it when QoS is improved which results in higher video rate. The position, velocity and force errors are presented in the sub-figure which corresponds to the QoS as reflected from the packet loss curve.

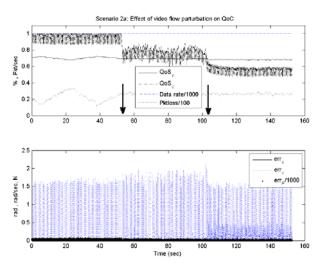


Figure 15. Effect of video flow purturbation (static case).

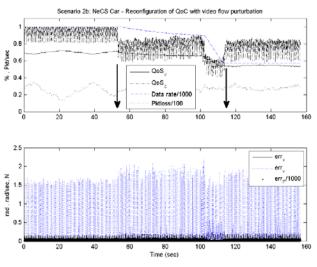


Figure 16. Reconfiguration of video load as per QoS and QoC

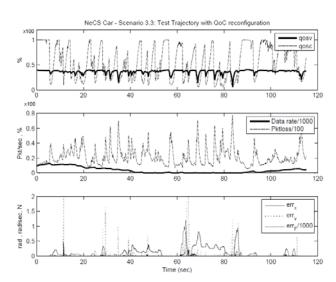


Figure 17. Video Load Management (Dynamic Case)

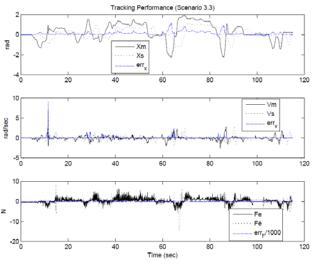


Figure 18. Tracking performance with QoS management.

Fig. 18 shows the tracking performance for the dynamic scenario. It can be seen that the control errors are notable at around 60 sec when a sudden drop in QoS was experienced due to the farthest distance between the master and slave. At most of other times the tracking performance is good as the master position is faithfully followed by the slave.

#### F. Effect of video packet rate on image information

The video is transmitted at 25 fps with varying image information in bits per pixel which affects directly the video data rate per frame sent over network.

In Fig. 19(a), original image is shown. Whereas, in Fig. 19(b), 1000 pk/s video data is sent which corresponds to 12 Mbps over the network. In the subsequent Fig. 19(c), (d) and (e), the information per frame is decreased further up to 500, 200 and 90 pk/s resulting in data rates of 6, 2.4 and 1.08 Mbps respectively.

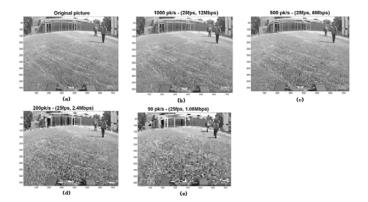


Figure 19. Fuzzy Packet rate surface

The results shows that even with minimum bandwidth, the remote driver is able to differentiate between the obstacles in order to avoid it. Thus, varying wireless network load strategy in case of lowered QoS can be effectively applied to drive-bywireless applications.

#### VIII. CONCLUSION

This paper presents a co-design approach to cater for the effect of degradation of network QoS on the control performance in bilateral teleoperation of drive-by-wireless applications. A fuzzy logic controller is used to manage the video flows (which as a result effects the network delay and its variation), in order to guarantee the stability by respecting the passivity criteria. The video rate adaptation is found to improve the tracking performance. However, more analysis will be worked out on the aspect of transparence in the future work. An extension is also possible by considering internet for teleoperation of drive-by-wireless application.

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