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Stability of the columnar and smectic phases of length-bidisperse parallel hard cylinders

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7 **Stability of the columnar and smectic phases of length-bidisperse**
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10 **parallel hard cylinders**
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Abstract

The effect of length-bidispersity on the stability of nematic, smectic and columnar phases of rod-like particles is studied in the perfect alignment limit using the Onsager's second virial theory. The rod-like particles are modeled as hard cylinders of equal diameters (D) but different lengths ($L_1 \neq L_2$). Three different smectic structures are observed: (i) the conventional smectic (S_1) phase, where both components accommodate in the same layer; (ii) the microsegregated smectic (S_2) phase, which can be considered as an alternation of fluid layers rich in short and long rods, respectively; and (iii) two layers of short rods accommodate inside one layer of long rods, which gives the third smectic (S_3) structure. Due to the inefficient packing of the short and long rods into a layered structure along the symmetry axes of the rods, the smectic phase is destabilized with respect to nematic and columnar phases upon mixing the short and long components. With decreasing length ratio ($l = L_2 / L_1$) the smectic phase is destabilized with respect to the nematic phase at compositions rich in short rods and two forms of smectic phases, namely S_1 and S_2 , take place in alternation. The alternation of the structure is the consequence of the minimization of the number of overlapping layers of the short rods with one long rod. In mixtures rich in long rods, the short and long rods are in the same layer up to $l=0.39$, while the short rods can accommodate into the interstitial region of long rods for $l<0.39$ and the system forms a S_2 phase. The S_3 phase is observed in the range $0.57<l<0.39$ and is due to the efficient packing of two layers of short rods inside one smectic layer of long rods. Our theoretical predictions for the three smectic structures are in close agreement with the smectic phase behaviour of a binary mixture of short and long helical polysilanes (Okashi et al., *Macromolecules* **42**, 3443 (2009)). It seems reasonable that the helical polysilanes can be considered as an ideal system for testing the hard-body theories. Finally, it is interesting that the stabilization process of the columnar phase with respect to the smectic ordering with decreasing length ratio turns over at $l=0.3$.

1 Introduction

Liquids and colloidal suspensions consisting of linear particles display an extremely interesting phase behaviour that becomes even more pronounced as we proceed from monodisperse systems to mixtures. In addition to the nematic, smectic and solid structures encountered in the pure substances, fractionation and demixing transitions [1-7], microsegregated smectic as well as columnar phases may occur in mixtures [8-18]. Frenkel [19] was the first to point out that an entropy-driven columnar phase transition is possible even in monodisperse systems, although only for disc-shaped particles such as cut spheres, while elongated particles such as spherocylinders and cylinders display only isotropic, nematic and smectic (and crystalline) phases [20-22]. Further insight into the stability of the nematic, smectic and solid phases in systems of identical parallel cylinders was provided by Mori and Kimura [23] and Xu et al. [24]. Microsegregation of different rods in the smectic phase was first reported by Koda and Kimura [12] who applied the second virial approximation to parallel cylinders. Following this line of research, Koda et al. investigated mixtures of parallel rods and spheres, both by Monte Carlo simulation and by basic density functional theory [14-15]. Further studies of rod-sphere systems followed by Dogic et al. [16], Cinacchi et al. [6] and Vesely [18]. The first account of a suppression of the smectic phase is due to Sluckin, who studied a length-polydisperse mixture of hard rods [8]. Evidence of the importance of the columnar phase was then explored by several simulation and theoretical studies [9-11,13,25-28]. In a sequence of extensive simulation studies, Stroobants [9,10] demonstrated the presence of a columnar phase in mixtures of long and short rods. Sear and Jackson [13] applied second virial theory and bifurcation analysis to parallel bidisperse cylinders, demonstrating the possibility of a nematic-columnar transition masking the smectic phase. Both MC simulation and theoretical methods were used by van Roij et al. [3, 26] to

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3 investigate the demixing of short and long rods in the isotropic and nematic phases, as well as
4 the smectic and columnar bifurcations. Cui and Chen [11] and Bohle et al. [25] applied
5 bifurcation analysis and Landau theory to study the ordered phases of bi- and polydisperse
6 rods, while Bates and Frenkel used semigrand MC simulation, again demonstrating the
7 presence – and possible dominance – of a columnar phase [27]. In the recent FMT study of
8 Martínez-Ratón and Cuesta [28] the dominance of the columnar phase is confirmed above a
9 threshold value of the polydispersity in a system of parallel cylinders.
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20 Several rod-like colloidal dispersions have been prepared to examine by experiment
21 the effect of hard body interactions in the stabilization of the liquid crystalline mesophases.
22 Well-known examples are polydisperse mineral liquid crystals [29-30], the mixture of
23 colloidal spheres and TMV viruses [31], the binary mixture of thin and thick fd viruses [5]
24 and solutions of single walled carbon nanotubes [32-34]. A common feature of the mineral
25 rods and the carbon nanotubes is that they are polydisperse mainly with respect to length. To
26 give a theoretical explanation for the phase behaviour of polydisperse rods, it is customary to
27 use continuous distribution functions such the Shultz-Flory distribution in Onsager and
28 related theories [35-36]. Instead of using continuous distribution functions one may consider
29 the system as a binary mixture of short and long rods, which leads to qualitatively correct
30 results for the phase transitions. For instance, the isotropic-nematic-nematic three phase
31 coexistence of a dispersion of sterically stabilized rodlike boehmite particles can be explained
32 by Onsager theory of short and long rods [30].
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50 In a foregoing study we have investigated mixtures of hard elongated particles with
51 equal length but differing diameters [37]. As a natural continuation of our previous work, the
52 present work is devoted to mixtures of parallel cylinders having equal diameters but different
53 lengths. The experimental motivation of our work is the very recent study of the smectic
54 phase in binary mixtures of short and long helical polysilanes [38]. The main feature of the
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3 polysilanes is that excluded volume interactions are dominant, electrostatic and the van der
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5 Waals interactions are weak, and almost monodisperse solutions can be prepared. Due to
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7 these advantageous properties the polysilanes can be considered as an ideal playground for
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9 testing the Onsager and other density-functional theories. Okoshi et al. [38] have focused on
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11 determining the possible smectic structures of binary mixtures of polysilanes using x-ray
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13 scattering and atomic force microscopy. In addition to the conventional and the
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15 microsegregated smectic phases, a new finely structured smectic phase was discovered. We
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17 make an attempt to find this new smectic structure in our present study. Another reason of our
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19 work is that the relative stability of the columnar, smectic and nematic phases in various
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21 regions of parameter space has not yet been studied thoroughly in MC simulation and
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23 theoretical studies. It is clear that the columnar phase is an important though somewhat
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25 elusive feature in the interplay of ordered phases in mixtures of elongated particles. A
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27 nematic-columnar transition may preempt the formation of a smectic phase, and
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29 microsegregation may be delayed by the formation of well-mixed columnar structures. At
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31 high densities, even the transition to a solid is sometimes preceded by the formation of a
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33 columnar phase of larger entropy. It is the purpose of this study to investigate the relative
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35 stabilities of the ordered and demixed states of bidisperse parallel cylinder systems, using a
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37 method that provides higher accuracy and reliability than the bare bifurcation approaches.
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2 Model system and Onsager theory for smectic and columnar phases

We consider the binary mixture of parallel hard cylinders, where both components have equal diameters ($D = D_1 = D_2$) while their lengths are different ($L_1 \neq L_2$). Restricting ourselves only to nematic, smectic and columnar phases, it is useful to decompose the positional vector of the cylinders (\vec{r}) as a sum of mutually perpendicular vectors \vec{r}_\perp and \vec{r}_\parallel . We use $\vec{r}_\perp = (x, y, 0)$ for the description of the columnar phase, while $\vec{r}_\parallel = (0, 0, z)$ is for the smectic one, the long axes of the cylinders being orientated along the z -axis. In this way the columnar phase is a two-dimensional solid in the x - y plane, while the smectic is a one-dimensional solid along the z axis. The corresponding local columnar and smectic densities for binary mixtures are $\rho_i(\vec{r}_\perp)$ and $\rho_i(\vec{r}_\parallel)$ ($i=1,2$), respectively. The ideal Helmholtz free energy density of $N = N_1 + N_2$ particles in a vessel of volume V for the binary mixture can be written for the columnar phase as

$$\frac{\beta F_{id}}{V} = \frac{1}{A} \sum_{i=1}^2 \int d\vec{r}_\perp \rho_i(\vec{r}_\perp) \{ \ln(\Lambda_i^3 \rho_i(\vec{r}_\perp)) - 1 \}, \quad (1a)$$

where $\beta = \frac{1}{k_B T}$ (T being the temperature and k_B the Boltzmann constant), $\rho_i = N_i / V$ is the local number density of component i ($i=1,2$), Λ_i^3 is the de Broglie volume of each component, including the translational and rotational contributions to the kinetic energy, and $A = \frac{\sqrt{3}}{2} a^2$ is the area of the hexagonal unit cell. In the smectic phase the ideal contribution of the free energy is simpler and can be written as a one-dimensional integral as follows

$$\frac{\beta F_{id}}{V} = \frac{1}{a} \sum_{i=1}^2 \int_0^a dz \rho_i(z) \{ \ln(\Lambda_i^3 \rho_i(z)) - 1 \}, \quad (1b)$$

where a is now the smectic period.

The residual contribution of the Helmholtz free energy is approximated by the second virial contribution in the virial series [39,40]

$$\beta F_{res} = -\frac{1}{2} \sum_{i,j=1}^2 \int d\vec{r}_1 \rho_i(\vec{r}_1) \int d\vec{r}_2 \rho_j(\vec{r}_2) f_M^{ij}(\vec{r}_{12}), \quad (2)$$

where the Mayer function (f_M^{ij}) of the hard cylinders can be written as a product of Heaviside functions of columnar and smectic variables,

$$f_M^{ij}(\vec{r}) = -\theta(D - r_{\perp}) \theta(L_{ij} - |z|), \quad (3)$$

with $r_{\perp} = |\vec{r}_{\perp}|$ and $L_{ij} = \frac{L_i + L_j}{2}$. Substituting Eq. (3) into Eq. (2) only the z spatial variable can be integrated out for the columnar phase, and x and y for the smectic order. The resulting residual free energy densities for the columnar and the smectic phases are

$$\frac{\beta F_{res}}{V} = \frac{1}{A} \sum_{i,j=1}^2 L_{ij} \int_A d\vec{r}_{\perp 1} \rho_i(\vec{r}_{\perp 1}) \int d\vec{r}_{\perp 2} \rho_j(\vec{r}_{\perp 2}) \theta(D - r_{\perp 12}), \quad (4a)$$

$$\frac{\beta F_{res}}{V} = \frac{1}{2a} \sum_{i,j=1}^2 D^2 \pi \int_0^a dz_1 \rho_i(z_1) \int dz_2 \rho_j(z_2) \theta(L_{ij} - |z_{12}|). \quad (4b)$$

The sum of the corresponding equations of Eq. (1) and Eq. (4) constitutes our total Helmholtz free energy density. The equilibrium structure of the binary mixture is determined by that density profile which minimizes the free energy of the system. In this work we use the method of Fourier parametrization for both columnar and smectic ordering. Instead of the local number densities, we parametrize the positional distribution functions given by the ratio of local and mean number densities, i.e. $f_i(\vec{r}) = \rho_i(\vec{r}) / \rho_i$ ($i=1,2$).

In the columnar phase the Fourier representation of $f_i(\vec{r}_{\perp})$ is given by

$$f_i(\vec{r}_{\perp}) = \sum_{n_1 n_2} f_{i, n_1 n_2} \cos(n_1 \vec{q}_1 \cdot \vec{r}_{\perp} + n_2 \vec{q}_2 \cdot \vec{r}_{\perp}), \quad (5)$$

where f_{i,n_1n_2} is the Fourier coefficient of component i , n_1 and n_2 are integer numbers, and \vec{q}_1, \vec{q}_2 are reciprocal lattice vectors. The reciprocal lattice vectors of the hexagonal phase can be obtained by the orthogonality relation between the unit and reciprocal vectors. These vectors are $\vec{q}_1 = \left(q, -\frac{q}{\sqrt{3}}, 0 \right)$ and $\vec{q}_2 = \left(0, \frac{2q}{\sqrt{3}}, 0 \right)$, where $q = \frac{2\pi}{a}$. The simple form of Eq. (5) is due to the inversion symmetry of the columnar phase: $f_i(\vec{r}_\perp) = f_i(-\vec{r}_\perp)$. Inserting Eq. (5) into Eq. (4a) and using the orthogonality relations of the cosine and sine functions one obtains that

$$\frac{\beta F_{res}}{V} = 4D^2 \sum_{i,j,n_1n_2} L_{ij} \rho_i \rho_j f_{i,n_1n_2} f_{j,n_1n_2} \Gamma_{n_1n_2}(qD), \quad (6)$$

where $\Gamma_{n_1n_2}(qD) = \int_0^1 dx j_0 \left((2n_2 - n_1) \sqrt{\frac{1-x^2}{3}} qD \right) \sqrt{1-x^2} \cos(n_1 q D x)$ and $j_0(x) = \sin(x)/x$.

$\Gamma_{n_1n_2}(qD)$ can be calculated analytically in some special cases, for example $\Gamma_{00} = \frac{\pi}{4}$, $\Gamma_{2n,n} = \frac{\pi}{2} \frac{J_1(nqD)}{nqD}$. The ideal contribution of the free energy Eq. (1a) cannot be simplified further by the substitution of Eq. (5), but it becomes now a function of the Fourier coefficients. Since the total free energy density, which is the sum of Eqs. (1a) and (6), depends on the Fourier components and the wave number q , the equilibrium columnar structure can be determined by the following set of equations

$$\frac{\partial \left(\frac{\beta F}{V} \right)}{\partial f_{i,n_1n_2}} = 0, \quad \frac{\partial \left(\frac{\beta F}{V} \right)}{\partial q} = 0, \quad (7)$$

where $i = 1, 2$ and $-n \leq n_1 \leq n$, $-n \leq n_2 \leq n$. The normalization constraints of the number

densities $\frac{1}{A} \int d\vec{r}_\perp \rho_i(\vec{r}_\perp) = \rho_i$ determine the values of the zeroth order Fourier coefficients; the

results $f_{1,00} = 1$ and $f_{2,00} = 1$ hold for nematic and columnar phases, too. In the nematic phase

all Fourier components are zero except $f_{1,00}$ and $f_{2,00}$, while $f_{1,n_1n_2} \neq 0$ and $f_{2,n_1n_2} \neq 0$ in the columnar phase. The Fourier coefficients decay rapidly with increasing n_1 and n_2 . In our calculations it has been more than sufficient to cut the series at the 6th shell, i.e. $n=6$, which guarantees that $|f_{i,m}| < \varepsilon$, with $\varepsilon = 10^{-4}$.

To include the possible in-phase and out-of-phase ordering of the short and long rods in the smectic phase we use the following Fourier ansatz for the long and short rods

$$f_1(z) = \sum_{i=0}^m f_{1,i} \cos(iqz), \quad (8a)$$

$$f_2(z) = \sum_{i=0}^m f_{2,i} \cos(iqz - i\varphi_0), \quad (8b)$$

where the phase shift φ_0 is zero for in-phase order, while it is π for out-of-phase order (microsegregation). We consider the Fourier components ($f_{1,i}$ and $f_{2,i}$), wave number ($q = \frac{2\pi}{a}$) and the phase shift (φ_0) as free variables of the smectic phase. Using Eqs. (8a-8b)

in Eq. (4b) we can derive the residual free energy density in terms of our free variables

$$\frac{\beta F_{res}}{V} = \frac{1}{2} \sum_{i,j=1}^2 \rho_i \rho_j V_{exc}^{ij} + \frac{1}{2} D^2 \pi \times \left\{ \rho_1^2 \sum_{i=1}^m f_{1,i}^2 \frac{\sin(iqL_1)}{iq} + 2\rho_1 \rho_2 \sum_{i=1}^m f_{1,i} f_{2,i} \frac{\sin\left(iq\left(\frac{L_1 + L_2}{2}\right)\right)}{iq} \cos(i\varphi_0) + \rho_2^2 \sum_{i=1}^m f_{2,i}^2 \frac{\sin(iqL_2)}{iq} \right\}, \quad (9)$$

where V_{exc}^{ij} denotes the excluded volume between a particle of component i and another particle of component j . It can be shown easily that $V_{exc}^{ij} = \frac{\pi}{4} (D_i + D_j)^2 (L_i + L_j)$. As for the columnar phase, the ideal contribution of the free energy Eq. (1b) cannot be simplified further by the help of Eq. (8) and we determine it numerically. The free energy of the smectic phase,

which is the sum of Eq. (1b) and Eq. (9), is minimized with respect to the free variables to obtain the equilibrium structure and the free energy of the smectic phase. The minimization yields the following set of equations

$$\frac{\partial \left(\frac{\beta F}{V} \right)}{\partial f_{i,j}} = 0, \quad \frac{\partial \left(\frac{\beta F}{V} \right)}{\partial q} = 0, \quad \frac{\partial \left(\frac{\beta F}{V} \right)}{\partial \varphi_0} = 0, \quad (10)$$

where $i=1,2$ and $j=1,\dots,m$. From the normalization condition of the number densities

$\frac{1}{a} \int_0^a dz \rho_i(z) = \rho_i$ it is trivial to prove that $f_{1,0} = 1$ and $f_{2,0} = 1$. The value of m is set such that

the order of magnitude of $f_{i,m}$ cannot be more than 10^{-4} . In our calculations the maximum value of m has not exceeded 16 even at very high pressures.

In summary, Eq. (7) determines the free energy of the columnar phase, while Eq. (10) is for the smectic phase. For the case of vanishing Fourier coefficients both the columnar free energy (sum of Eqs. (1a) and (6)) and the smectic free energy [sum of Eqs. (1b) and (9)] reproduces the free energy of the nematic phase.

Having obtained the free energy of the nematic, smectic and columnar phases we can determine the pressure and chemical potentials from the standard thermodynamic equations as follows

$$\beta \mu_i = \frac{\partial \left(\frac{\beta F}{V} \right)}{\partial \rho_i}, \quad \beta P = -\frac{\beta F}{V} + \sum_{i=1}^2 \rho_i \frac{\partial \left(\frac{\beta F}{V} \right)}{\partial \rho_i} \quad (i=1, 2) \quad (11)$$

These equations are used to determine the phase boundary between two coexisting phases

α_1 and α_2 from the conditions of the phase coexistence $\beta \mu_i^{\alpha_1} = \beta \mu_i^{\alpha_2}$ ($i=1,2$) and

$\beta P^{\alpha_1} = \beta P^{\alpha_2}$. In the following section we search for possible phase transitions between the

same types of phases, such as nematic-nematic and smectic-smectic demixing transitions, and

we examine the possibility of nematic-smectic, nematic-columnar and smectic-columnar

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3 phase transitions. The extent of the fractionation and the structure of the stable phases are
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5 studied in detail.
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10 **3 Results and discussion**

11 **3.1 Phase behaviour of monodisperse hard cylinders**

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13 The phase behaviour of parallel cylinders has been studied thoroughly several times by
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15 Monte Carlo simulation methods [15,21,41] and Onsager type theories [23,24,39-40,42].
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17 More recently a sophisticated density-functional theory, the Fundamental-Measure theory
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19 (FMT), has been applied also to this system [22,43]. Mulder [39] has shown that Onsager's
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21 second virial theory is capable to describe the nematic-smectic A (N-S) phase transition of
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23 parallel hard cylinders. It was proved that the N-S phase transition is of second order and that
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25 the transition density (scaled with particle volume) is independent of the length-to-breadth
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27 ratio (L/D). The results of Onsager theory for the transition properties are presented in Fig. 1.
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29 The distance between neighbouring layers at the N-S transition is about $1.39 L$. Regarding the
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31 columnar (C) phase we are only aware of some bifurcation analysis studies of the nematic-
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33 columnar phase transition based on Onsager theory [13,40]. It was found that, within this
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35 theory, the nematic phase becomes unstable with respect to columnar density modulation well
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37 above the N-S phase transition, which means that the N-C phase transition cannot take place.
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39 Capitán et al. [22] proposed a FMT approximation for the system of parallel cylinders,
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41 obtaining the complete phase diagram. The C phase was found always to be metastable, the
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43 sequence of stable phases being N-S-K (crystal phase).
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53 Even though the C phase is probably preempted by the K phase in the monodisperse
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55 fluid, we expect that this phase will be stabilized in the bidisperse system. Consequently, in
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57 what follows we discuss the formation of the columnar phase in the monodisperse fluid with a
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59 view to obtaining the limits of phase stability in the phase diagrams of the mixture. We
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3 proceed beyond the bifurcation analysis of Onsager theory by obtaining the full numerical
4 solutions of the columnar equations [see Eq. (7)] for Fourier coefficients and wave number in
5 the monodisperse case at a given packing fraction ($\eta = \rho v_0$, where v_0 is the volume of the
6 cylinder). Two columnar solutions are detected in the packing fraction range of $0.83 < \eta$
7 < 0.945 : one solution is a weakly ordered columnar phase, while the other corresponds to a
8 strongly ordered columnar structure. The weakly ordered columnar phase has a larger lattice
9 constant (a) than the strongly ordered one. In accordance with the bifurcation analysis the
10 weakly ordered columnar phase is less ordered with increasing density and becomes nematic
11 at the N-C bifurcation packing fraction ($\eta_{bif} \approx 0.945$), while the strongly ordered columnar
12 phase exists at the N-C bifurcation and becomes more ordered with increasing packing
13 fraction. The two columnar solutions at $\eta = 0.9$ are depicted in Fig. 2, while the equations of
14 state of the nematic and columnar branches are shown in Fig. 3. Note that the nematic and
15 columnar curves of Fig. 3 resemble the equation of state of a typical first-order phase
16 transition [44]. Because of the presence of a van der Waals-like loop in the equation of state
17 the nematic-columnar phase transition would be first order, provided it existed as a stable
18 phase transition. The calculated coexisting nematic and columnar packing fractions are 0.814
19 and 0.888, respectively. These values are above the N-S transition packing fraction, so the
20 nematic-columnar phase transition is unstable. It is worth noting that the columnar solution
21 exists much below the nematic-columnar bifurcation packing fraction.

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The next issue is the stability of the smectic phase with respect to columnar order. Our
smectic and columnar free energy calculations indicate that the smectic phase becomes
unstable with respect to columnar structure at unphysically high densities with an
accompanying first order smectic-columnar phase transition. The coexistence packing
fractions of Onsager theory (see Fig. 1) are unphysical because they are above the close
packing limit of the cylinders. This discrepancy of Onsager theory is due to the fact that it is a

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3 virial theory truncated at the second term. The inclusion of higher order virial terms [23] or
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5 multiplying the residual free energy (Eq. (2)) by a $1/(1-\eta)$ term [8, 13] shifts the transition
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7 densities into the physically acceptable packing fraction range, but they do not change the
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9 phase diagram qualitatively. For the sake of simplicity we do not change the theory.
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11 Regarding the solid phase, we have not made an attempt to calculate the free energy and the
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13 pressure, as the focus of our study is the stability of smectic with respect to columnar ordering
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15 in binary mixtures. Moreover the solid phase is destabilized in the mixture of short and long
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17 rods, because the short rods impose shorter period than the long rods along the symmetry axes
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19 of the rods. For these reasons, we refrain ourselves from comparing our results with those
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21 from the more accurate FMT approximation [22,43].
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3.2 Phase behaviour of length-bidisperse hard cylinders

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31 Since the smectic A phase is the first in the rank which destroys the nematic order in
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33 the monodisperse system of hard cylinders, it is reasonable to examine first the stability of the
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35 nematic phase with respect to a smectic A modulation in the mixture of short and long
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37 cylinders. The simplest method to locate the borders of the nematic and smectic regimes is the
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39 nematic-smectic bifurcation analysis. In our formalism this is equivalent to finding the lowest
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41 density at which Eq. (10) still has nonzero solutions for the Fourier coefficients of the
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43 positional distribution functions. In this regard the composition ($x_i = N_i / N$) and the length
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45 ratio of the system ($l = L_2 / L_1$) are free parameters in the calculations. The bifurcation
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47 analysis of Koda and Kimura [12] shows that the nematic phase can be destabilized either by
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49 a monolayered smectic phase (S_1) or by a bilayered or microsegregated smectic one (S_2). The
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51 length-bidispersity always destabilizes the smectic order with respect to the nematic phase
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53 because the characteristic smectic periods of the short and long rods do not fit. For example,
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55 in a short-rod-rich smectic phase the added long rods cannot accommodate into the layer
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3 structure of the short rods, but they have to occupy more than one layer. Depending on the
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5 length of the long rod the number of occupied layers can start from one and go up to infinity.
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7 To minimize the excluded volume between short and long rods the long rods occupy the
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9 optimum position in the layer. With monolayered or bilayered stacking it is possible to reduce
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11 the number of layers overlapping with a long rod by one. For example, a long rod which
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13 occupies n layers in monolayered structure, can interact with only $n-1$ in a bilayered smectic
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15 structure. The resulting stable phase is the bilayered structure, because there is an entropy
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17 gain from the more efficient packing. The opposite situation can also happen that the stable
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19 monolayered structure has occupation number $n-1$, while the metastable bilayered structure
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21 has n . Koda and Kimura [12] have derived analytical equations for the structure of the smectic
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23 phase at the nematic-smectic bifurcation in the limit of pure phases ($x_1 \rightarrow 0$ and $x_1 \rightarrow 1$).

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25 The regions of S_1 and S_2 phases alternate according to

$$(2i-1)a_{NS} - L_2 \leq L_1 \leq 2ia_{NS} - L_2, \quad (12a)$$

$$0 \leq L_1 \leq a_{NS} - L_2 \text{ and } 2ia_{NS} - L_2 \leq L_1 \leq (2i+1)a_{NS} - L_2, \quad (12b)$$

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27 ($i=1,2,3,\dots$) where the first equation gives the interval of L_2 for a stable S_1 structure, while the
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29 second one is for the S_2 . a_{NS} is the smectic period at the nematic-smectic bifurcation of the
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31 pure phase of component 2, which equals $1.39L_2$. In Fig. 4 we present the results of
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33 bifurcation analysis for the structure, the packing fraction and the period of the smectic phase
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35 as a function of composition and length ratio. We can see from Fig. 4a that our results follow
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37 the prediction of Eq. (12), but it also gives further information about the stability of smectic
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39 structures for intermediate compositions. In accordance with Eq. (12) we find S_2 - S_1 - S_2 - S_1
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41 sequences for $0.2 < l < 1$ in the short-rod-rich regions, while systems with a majority of long
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43 rods show only the S_2 - S_1 change. Figures 4b and 4c demonstrate the commensuration problem
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45 of the particles' lengths. Both the bifurcation packing fraction and the smectic period have
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47 abnormal behaviour at intermediate values of length ratio and composition. The packing
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3 fraction goes up to unphysical ranges in the vicinity of an equimolar mixture, while the
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5 smectic period shows increasing discontinuity with decreasing length ratios. The results
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7 clearly show the suppression of the smectic phase and the possible predominance of stable
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9 columnar structures, because the columnar phase does not suffer from the commensuration
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11 problems.
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15 A more detailed insight is provided by the positional distribution functions
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17 $f_i(z) = \rho_i(z)/\rho_i$ of the possible smectic phases. Numerical solution of Eq. (10) results in
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19 three qualitatively different smectic structures: a monolayered (Figs. 5a) and a bilayered
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21 structure (Fig. 5b), and a two-in-one-layer ordering (Fig. 5c). We can see that the long rods
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23 are more ordered than the short ones in all three cases. This is due to the fact that the long
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25 rods constitute the majority species and they contribute with a higher excluded volume cost
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27 than the short ones. The shorter rods can move out more freely from the center of the layer
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29 without increasing the excluded volume cost. The conventional smectic phase (S_1) is mainly
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31 stable in weakly length-bidisperse systems ($l > 0.6$), but it can also take place in the strongly
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33 bidisperse case. In the special case of $L_2 < 0.39 L_1$, the short rods can accommodate in the
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35 interstitial region and the short rods are squeezed out from the layer of the long rods to make
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37 the packing of the short and long rods more efficient. The resulting bilayered smectic
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39 structure is shown in Fig. 5b. The two-in-one smectic ordering (S_3) is the most interesting
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41 (Fig. 5c), because it has not been predicted theoretically before. The first experimental
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43 evidence for the existence of a S_3 smectic structure is reported in the very recent study of
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45 Okashi et al [38]. It is found that the two-layer accommodation is possible in the length ratio
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47 interval of $0.34 < l < 0.59$. Note that the length ratio of Fig. 5c is located inside this interval. The
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49 existence of the S_3 structure is due to commensuration, because two layers of shorts rods can
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51 fit into one layer of long rods. Finally Fig. 5. proves that our model and the experimental
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3 system are in close relationship because the smectic structures of the binary mixture of short
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5 and long polysilanes are those shown in Fig. 5.
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8 We have monitored how the structural change takes place in the smectic phase by
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10 changing the length ratio at a given pressure. We have chosen two compositions ($x=0.01$ and
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12 0.99) very close to the monodisperse limits to avoid the stability problem of the smectic
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14 phase. Figure 6 demonstrates that S_1 and S_2 structures transform into each other continuously.
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16 In the long-rod-rich phase (Fig. 6a) the short rods go into the interstitial region with
17
18 decreasing length ratio. At around $l=0.3$ the short rods form a nematic phase because they can
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20 stay everywhere with equal probability. This is an interesting structural behaviour because the
21
22 long rods are in the smectic phase irrespectively of the value of the length ratio. In the short-
23
24 rod-rich smectic phase we observe the same structural S_1 - S_2 change in the distribution of long
25
26 rods (see Fig. 6b). The only difference is that the period of the smectic phase is now shorter.
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28 To locate the border of S_1 - S_2 (S_2 - S_1) smectic transformations we have used the condition
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30 $f_2(z)=1$ ($f_1(z)=1$) in the solution of Eq. (10). The S_3 phase can only appear in long rod rich
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32 phases in the vicinity of $l=0.5$. In this region of length ratio the stable phases are the S_1 and S_3
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34 structures. Since the transformation of the positional distribution function of the short rods
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36 from S_1 to S_3 is continuous, the second derivative of f_2 must be zero with respect to z at $z=0$
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38 and this helps to locate the border of S_1 - S_3 structural change. For this reason we have used the
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$$\text{condition } \left. \frac{d^2 f_2}{dz^2} \right|_{z=0} = 0 \text{ to search for the } S_1\text{-}S_3 \text{ transformation.}$$

51 With the help of the nematic, smectic and columnar free energies we are in a position
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53 to construct the phase diagram of the system of short and long rods. Solving the phase
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55 equilibrium conditions we obtain the densities and compositions of the coexisting phases.
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57 The resulting phase diagrams are presented in the pressure-composition plane for the most
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59 important length ratios in Fig. 7. In the first system the lengths of the components are not far
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3 from each other. Mixing the short and long rods does not result in a substantial change in the
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5 nematic-smectic A second order phase transition. Owing to the difference in the lengths only
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7 weak destabilization of the smectic phase can be seen with respect to the nematic one.
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9 Interestingly, the smectic-columnar biphasic region moves into the direction of lower pressure
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11 by adding short (long) rods to the system of long (short) rods. This means that, contrary to the
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13 smectic phase, the columnar phase becomes more stable with decreasing length ratio. We can
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15 also observe weak fractionation between the coexisting phases. At around $x=0.4$ the
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17 coexisting smectic and columnar phases have the same composition, i.e. an azeotropic point
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19 bounds the stability region of the columnar phase. We can expect that the upper bound of the
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21 nematic and the lower bound of the columnar phase meet at lower length ratio. This happens
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23 slightly above $l=0.6$. We can see that a first order nematic-columnar phase transition takes
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25 place at $l=0.6$ in a narrow composition and pressure range. The nematic-columnar phase
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27 transition is terminated by a critical endpoint where it meets the N-S critical line. At this point
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29 the critical phase coexists with the columnar phase. Interestingly, a pressure-induced S_1 - S_2
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31 structural change takes place on the short-rod-rich side. This is due to the fact that the smectic
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33 layers get closer to each other with increasing pressure and the long rods enter into the two
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35 neighbouring layers. By moving into the interstitial region the long rods interact with only
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37 two layers; the packing entropy gain gives rise to the structural change in the smectic phase.
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39 In accordance with our results the system of short and long polysilanes shows only S_1
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41 ordering both in short and long rod rich phases in the range of $0.59 < l < 1$ [38]. At $l=0.5$ the
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43 smectic phase is microsegregated on the short rod side in accordance with Eq. (12), the
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45 nematic-columnar phase coexistence region widens, and a small region where the nematic-
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47 smectic phase transition is of first order (with a corresponding three phase point) is detected
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49 close to a composition of 50%. In addition a S_3 smectic structure occurs in a finite range of
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51 composition, which is rich in long rods. The interesting lower pressure border of the S_3
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3 structure shows that the density of the short rods must exceed a minimum value to produce
4 double layering. At the lower length ratio of $l=0.4$ we obtained the same phase diagram as for
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8 $l=0.5$, except for the S_1 - S_2 change and for the fact that the nematic-smectic phase transition is
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10 of second order. We can also observe that the fractionation of the N-C phase transition
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12 gradually increases with decreasing length ratio. The phase behaviour of the experimental
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14 system resembles closely the phase behaviour of the hard cylinder mixture, because the S_3
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16 (S_2) structure is stable at compositions rich in long (short) rods in the region of $0.34 < l < 0.59$
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18 and the short rod rich smectic phase is microsegregated [38]. The phase diagram of $l=0.3$
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20 shows that a S_2 - S_1 structural change takes place upon compression. In this case the short rods
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22 can accommodate in the interstitial region, but the compression moves the layers closer to
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24 each other and the short rods penetrate into the two layers. To avoid the double penetration
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26 the short rods move inside the layer and the system forms a monolayered smectic phase. Note
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28 that no S_3 ordering takes place at $l=0.3$, which agrees with the experimental observations [38].
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31 Another interesting result is that the lower boundary of the columnar phase starts to move up,
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33 i.e. the columnar phase destabilizes due to the efficient S_2 stacking. In addition the N-C phase
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35 boundary becomes very wide. At the lowest value of length ratio ($l=0.15$), we can clearly see
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37 the destabilization effect of the S_2 stacking on the columnar phase. The stability region of the
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39 smectic phase is very wide, while that of columnar moves up and becomes very narrow. The
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41 very short and the long rods do not want to form columns, but they segregate very strongly at
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43 high pressures: the short-rod-rich nematic phase is in coexistence with a microsegregated
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45 smectic phase. We have also examined the possibility of a nematic-nematic demixing
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47 transition, but it is always located in the biphasic region of the N- S_2 phase boundary. Our
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49 attempts to find a stable N-N phase transition at very low length ratios has not been
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51 successful, because the N- S_2 transition becomes wider and moves down into the direction of
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53 lower pressure.
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3 In summary, the occurrence of a stable columnar phase in the intermediate length ratio
4 range is the result of the subtle interplay between translational, packing and mixing entropies.
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6 The short and long rods cannot accommodate together into the stacks of layers without high
7 packing entropy loss. In addition the demixing of the smectic phase into phases rich in short
8 and long rods is accompanied by high mixing entropy cost. The existence of two-in-one
9 smectic (S_3) ordering in the vicinity of $l=0.5$ is due to the efficient packing of the short rods in
10 the smectic layers of the long rods.
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22 3 Conclusions

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24 We have examined the phase behaviour of the binary mixture of short and long
25 parallel hard rods as a function of length ratio using Onsager's second virial theory. One- and
26 two-dimensional Fourier expansions have been applied to represent the smectic and columnar
27 phases, respectively. We have found that the stability regions of the nematic, smectic and
28 columnar phases are very sensitive to the length ratio. The nematic phase can be stabilized by
29 length bidispersity because either the short or the long rods do not fit into the 1D periodic
30 structure of the smectic phase rich in long rods or rich in short rods. This commensuration
31 problem is very strong in the vicinity of equimolar composition where the short components
32 are trying to create a 1D periodic structure with a short smectic period, while the long rods
33 prefer the formation of a smectic phase with long smectic period. A further consequence of
34 the commensuration problem is the stabilization of the columnar with respect to the smectic
35 phase at high pressures (densities). With decreasing length ratio the regime of smectic
36 stability shrinks, while those of the nematic and columnar phases become more extended. At
37 $l=0.6$ the nematic and columnar regions meet and a first-order nematic-columnar phase
38 transition is stabilized. The region of the nematic-columnar phase transition widens and it
39 becomes more fractionated with decreasing length ratio. However, below $l<0.4$ the tendency
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3 changes because the rods of the short component can fit into the interlayer region of the
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5 neighbouring layers and a microsegregated (bilayered) smectic phase may form. Due to the
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7 efficient packing of the bilayered smectic structure and the gain in the translational entropy,
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9 the region of the smectic phase widens, while the columnar phase is suppressed and shifted
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11 into the direction of higher pressures. Therefore the stability of the columnar phase is limited
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13 by lower and upper bounds in the length ratio. To stabilize the columnar phase the best
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15 systems are those where the long rods are 2-3 times longer than the short ones. No nematic-
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17 nematic and smectic-smectic demixing transitions are found, since the strong nematic-smectic
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19 and nematic-columnar fractionations preempt the demixing transitions. We have shown that
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21 our binary mixture of short and long rods and that made of real polysilane molecules have the
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23 same types of smectic phases. In addition, the smectic phases in systems rich in short and long
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25 rods show the same structural changes with decreasing length ratio. Qualitative tests between
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27 theory and experiment to check the stability of nematic and columnar phases are not possible
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29 at the moment, because the objective of the study of Okoshi et al. [38] has been only the
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31 smectic ordering.
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39 In conclusion our study shows that the phase diagram of the short and long rods
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41 system can be very complex due to commensuration effects of the particle lengths. It remains
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43 an open question whether the orientational entropy contributions change the topology of the
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45 phase diagrams in the nematic, smectic and columnar regimes. We hope that our work
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47 provides a useful guide for future experimental works on rod-like mixtures exhibiting
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49 spatially ordered mesophases such as the recently synthesized binary mixture of helical
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51 polysilanes [38].
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Figures

Figure 1. Phase sequences of the monodisperse system of parallel hard cylinders. The solid phase is not included in the model.

Figure 2. Positional distribution function of a weakly ordered (a) and a strongly ordered columnar (b) phase at $\eta=0.9$. The lattice constant of the columnar phase: (a) $a^* = 1.41$, (b) $a^* = 1.39$.

Figure 3. Columnar and nematic solutions in the pressure-packing fraction plane (reduced pressure: $P^* = \beta P v_0$, packing fraction: $\eta = \rho v_0$) for the pure system of parallel hard cylinders. Dashed line connecting the filled squares shows the coexisting nematic and columnar phases. Filled diamond symbol locates the nematic-columnar bifurcation point.

Figure 4. Nematic-smectic bifurcation of the binary mixture of short and long cylinders. a) Structure of the smectic phases in the length ratio-composition plane. $\sigma = 1$ means microsegregated (bilayered) smectic phase (S_2), while $\sigma = 0$ denotes monolayered smectic phase (S_1) b) Packing fraction (η) of nematic-smectic bifurcation in the length ratio-composition plane. c) Smectic period ($a^* = a/L_1$) in the length ratio-composition plane. x is the mole fraction of long rods.

Figure 5. Possible smectic phases of the binary mixture of short and long cylinders. a) Smectic phase where both components are in phase (S_1). b) Microsegregated smectic phase where the distributions of the components are out of phase (S_2). c) Smectic phase where the

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3 components are in phase and the short rods forms two layers inside the layer of long rods (S_3)
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5 For all cases the values of the mole fraction of long rods and the reduced pressure are 0.6 and
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7 4, respectively. The length ratios are 0.65 (a), 0.3 (b) and 0.5 (c).
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12 **Figure 6.** Structural change in the smectic phase as a function of length ratio in long rod rich
13 a) and short rod rich phases b). The composition is $x=0.99$ in a), while it is 0.01 in b). The
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15 value of the reduced pressure is 5 for all cases.
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22 **Figure 7.** Phase diagram of the binary mixture of short and long cylinders in pressure-
23 composition plane. The values of the length ratio ($l=L_2/L_1$): 0.65 (a), 0.6 (b), 0.5 (c), 0.4 (d),
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25 0.3 (e) and 0.15 (f). The horizontal short dashed lines connect either the nematic-smectic
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27 critical endpoint with the coexisting columnar phase or show the nematic-smectic-columnar
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29 three phase coexistences. In Fig. b) and e) the short dashed line connects also the terminal
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31 point of S_1 - S_2 structural change with the coexisting columnar phase. The border of S_1 - S_2 , S_2 -
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33 S_1 and S_1 - S_3 structural transformations are denoted as a dashed curve. The long dashed curve
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35 is the boundary of the unstable nematic-nematic demixing transition. We use the following
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37 notations: N-nematic, S_1 -monolayered smectic, S_2 -bilayered smectic, S_3 -two-in-one smectic
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39 and C-columnar phase. x is the mole fraction of long rods.
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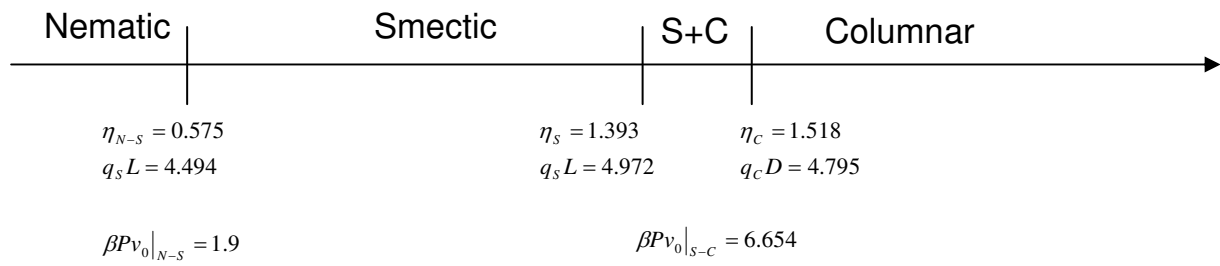


Figure 1.

For Peer Review Only

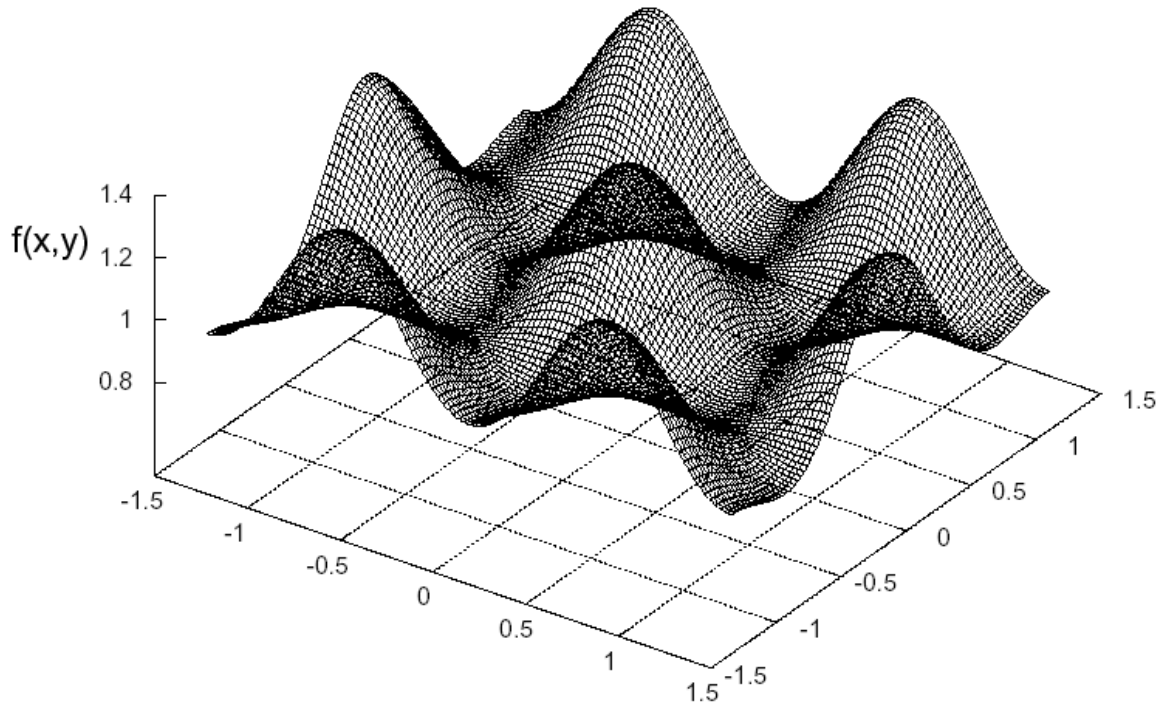


Figure 2 a)

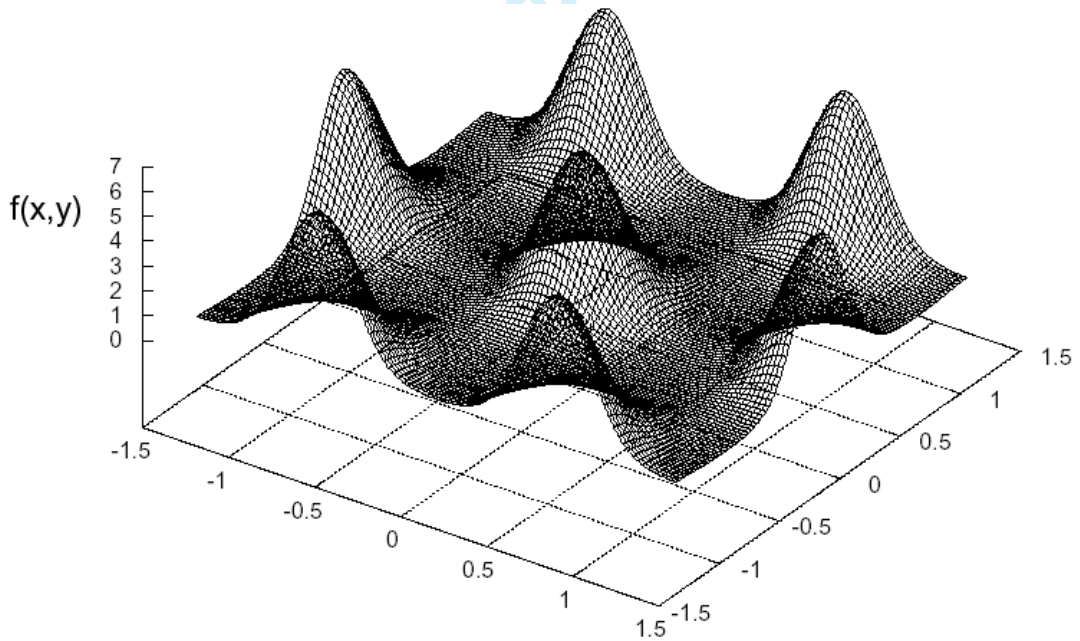


Figure 2 b)

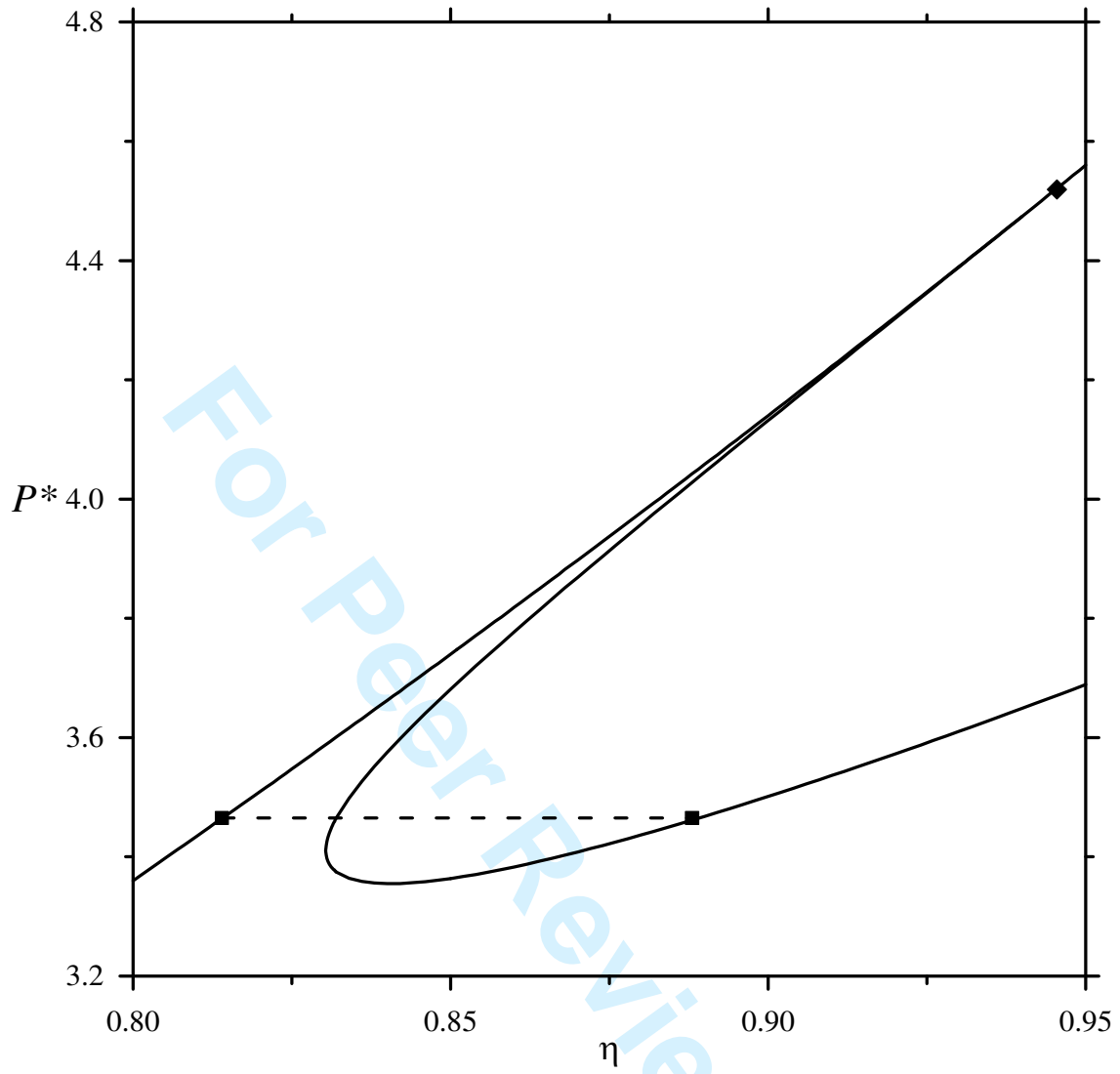


Figure 3.

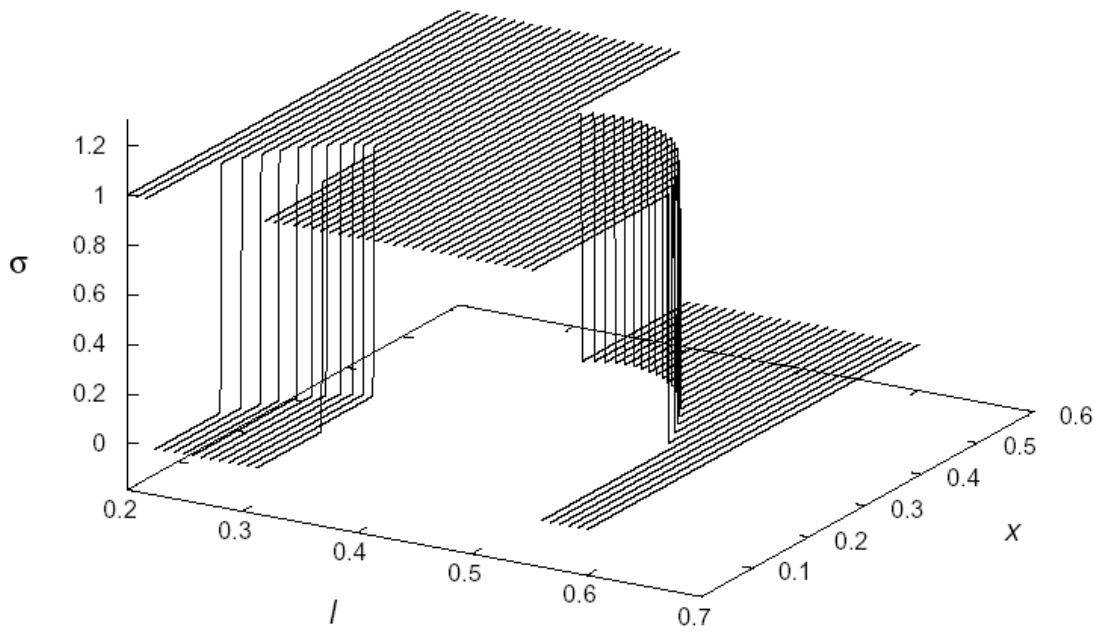


Figure 4 a)

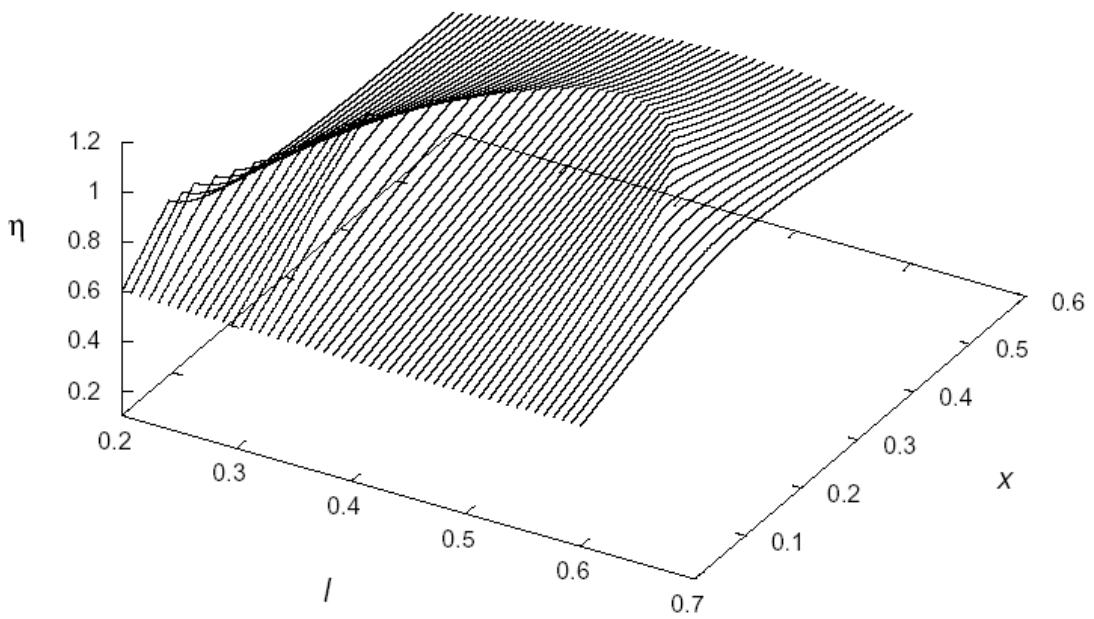


Figure 4 b)

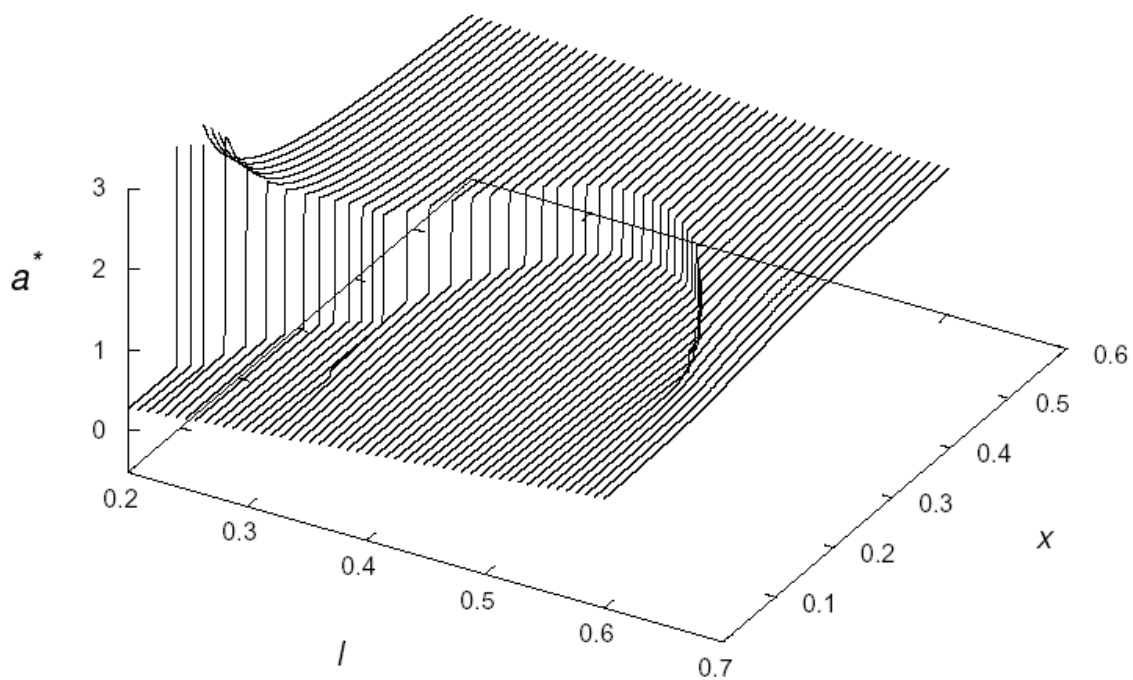


Figure 4 c)

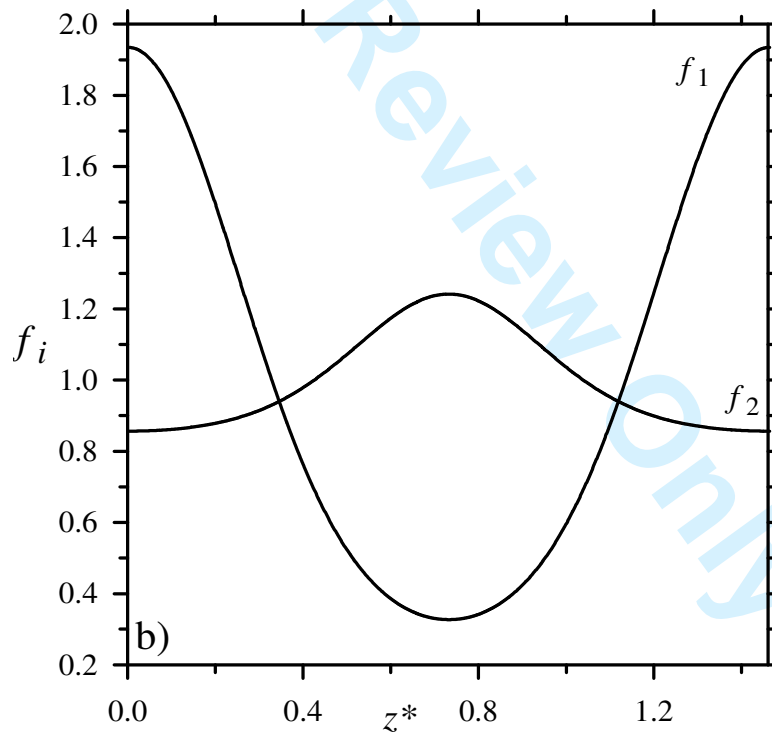
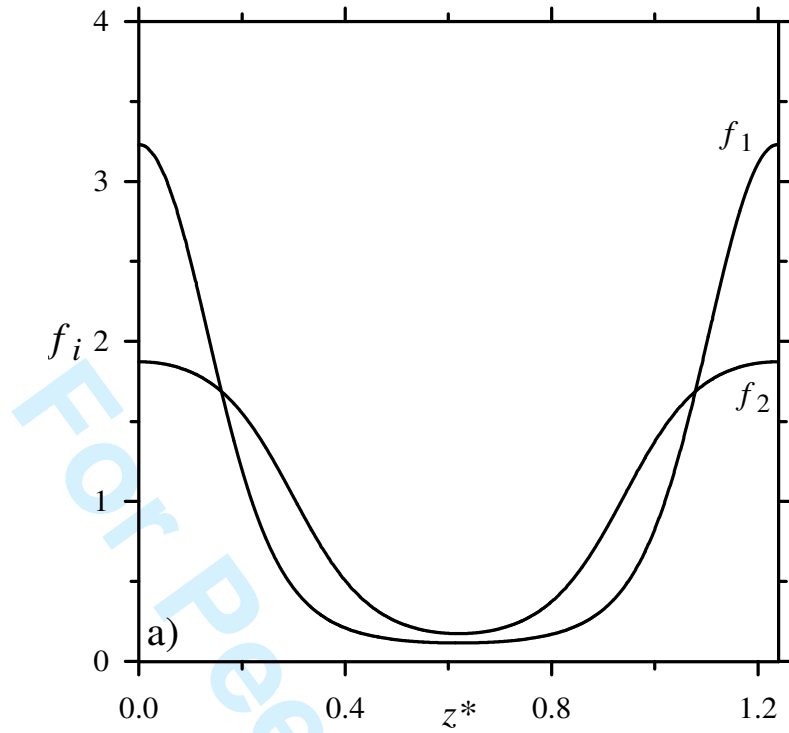
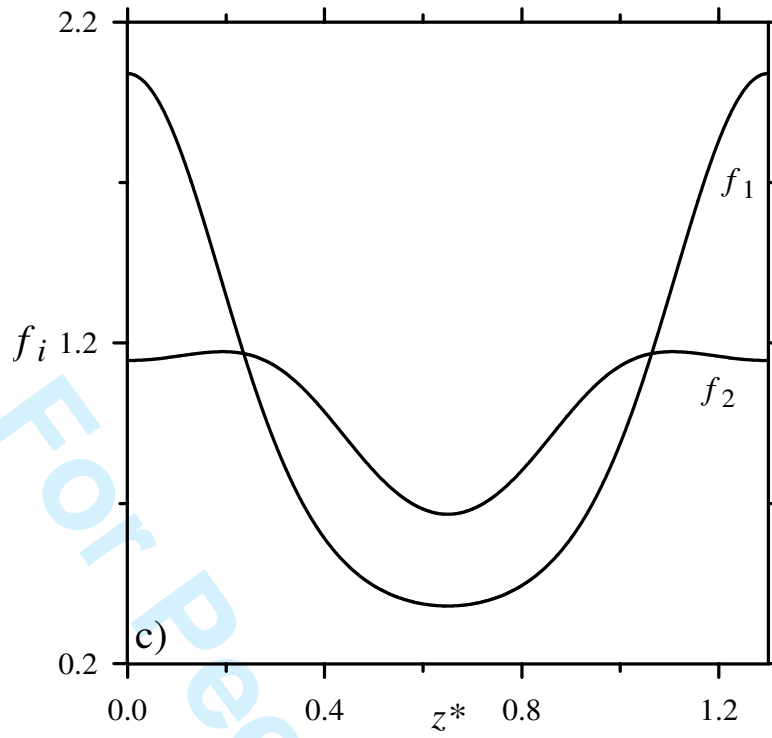


Figure 5 a) and b)



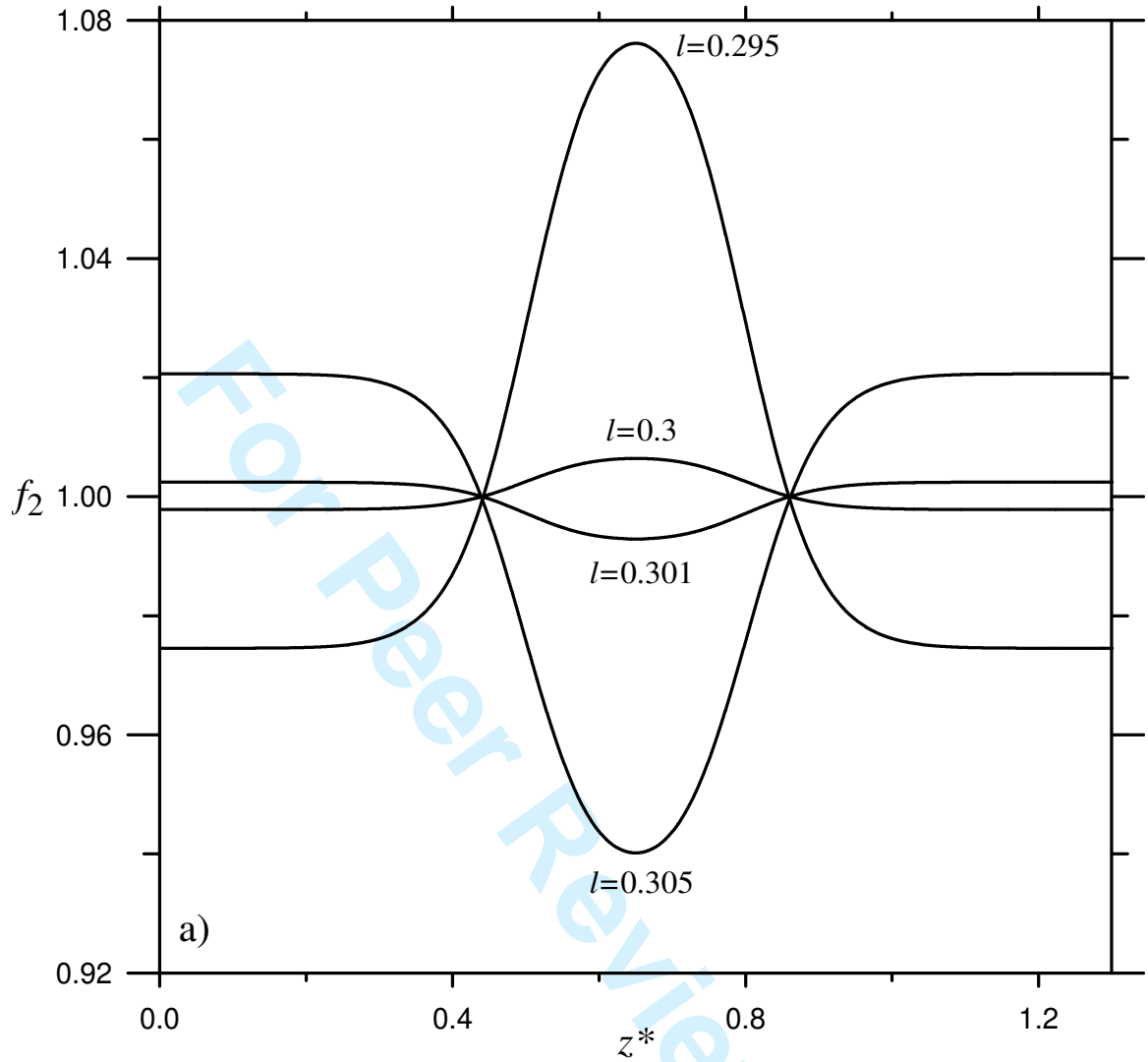


Figure 6 a)

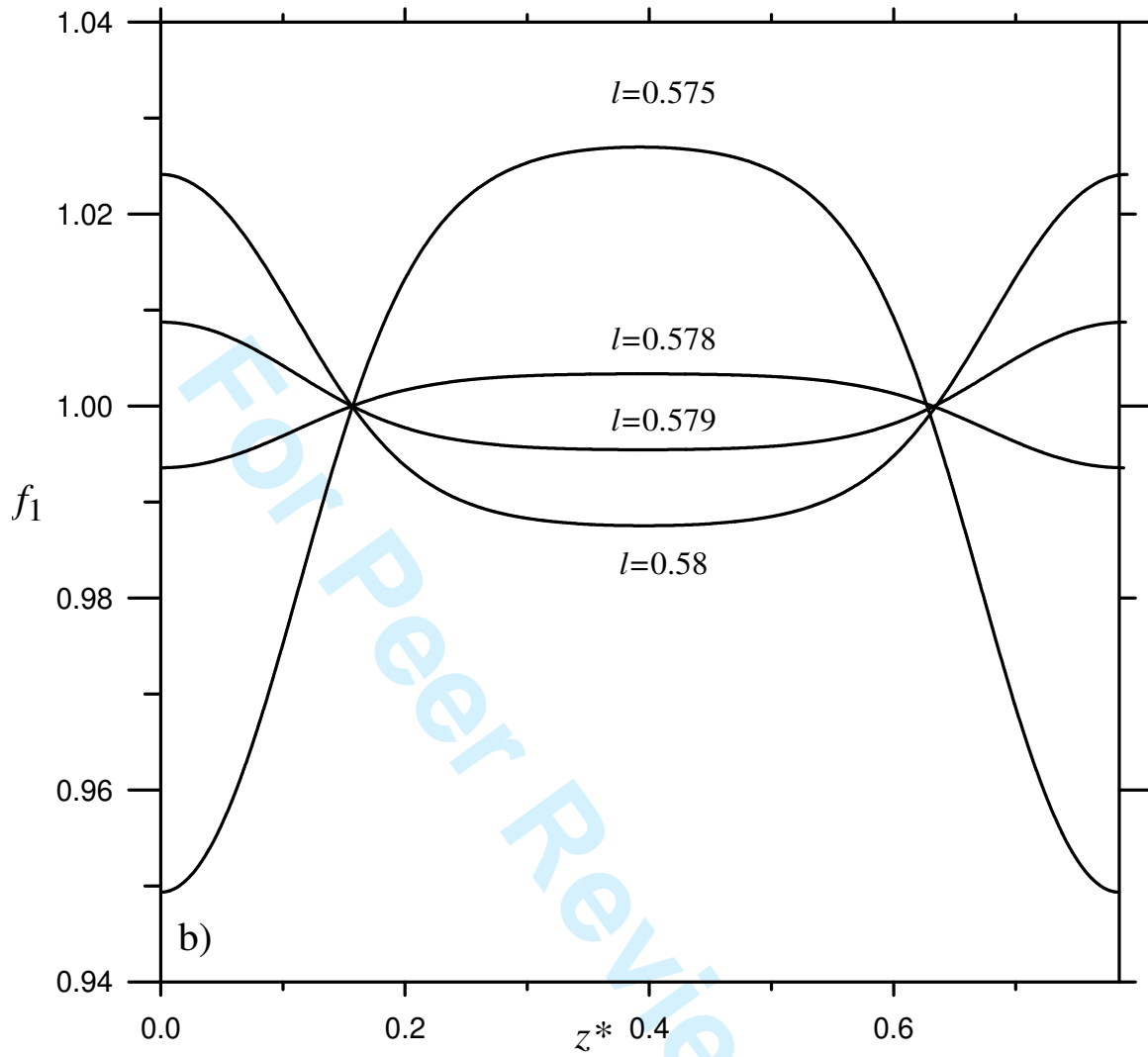


Figure 6 b)

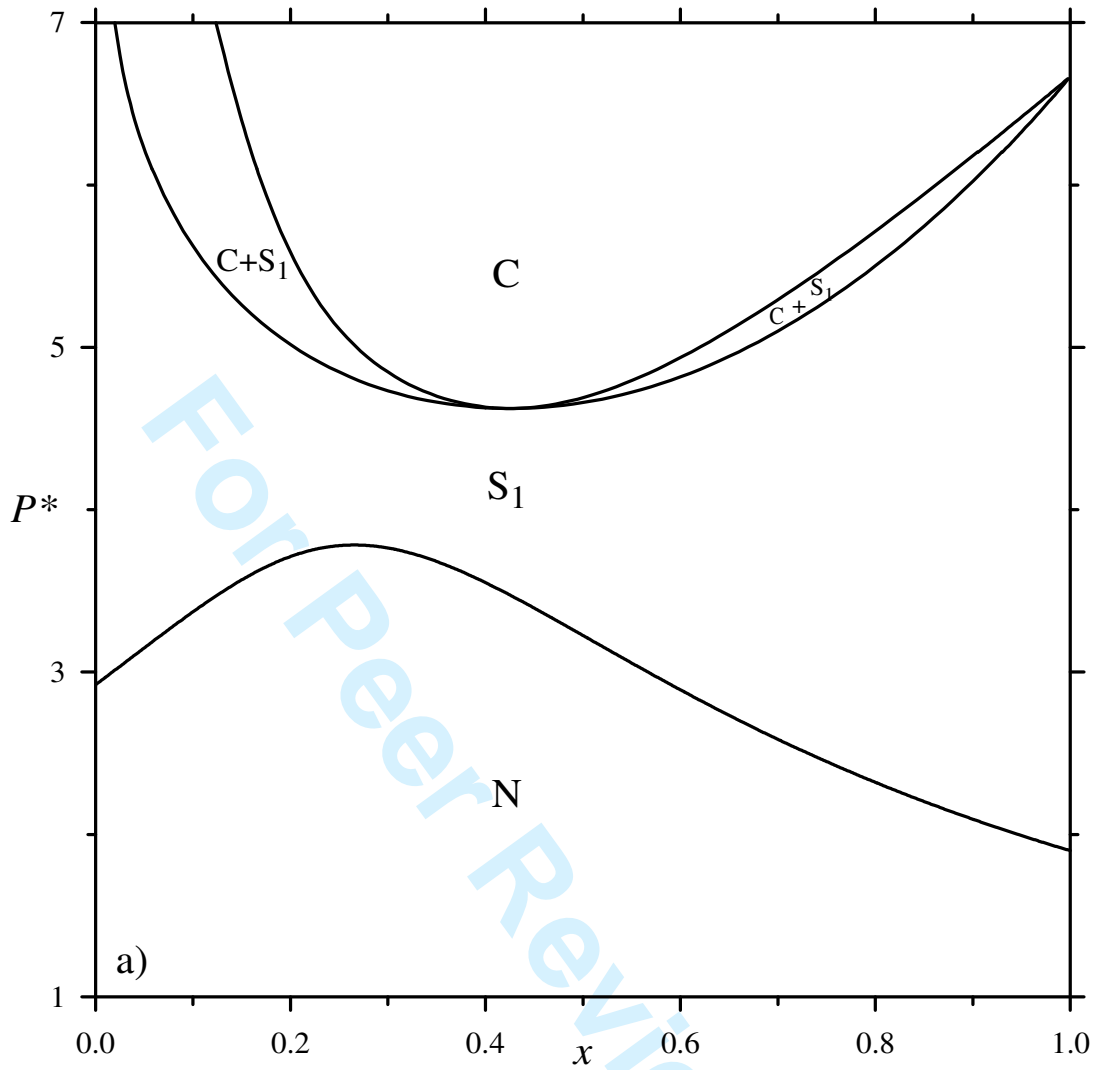
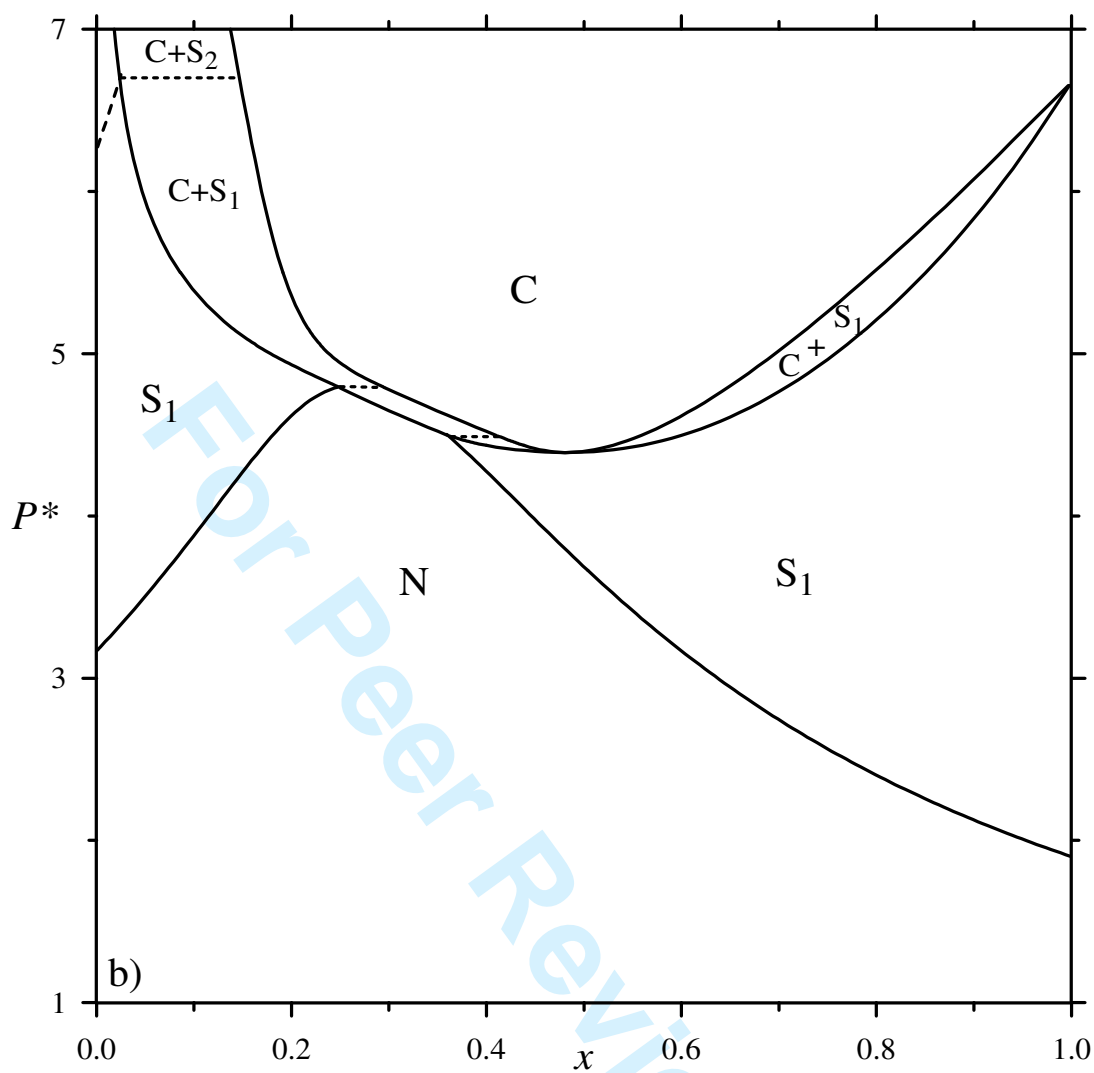


Figure 7 a)



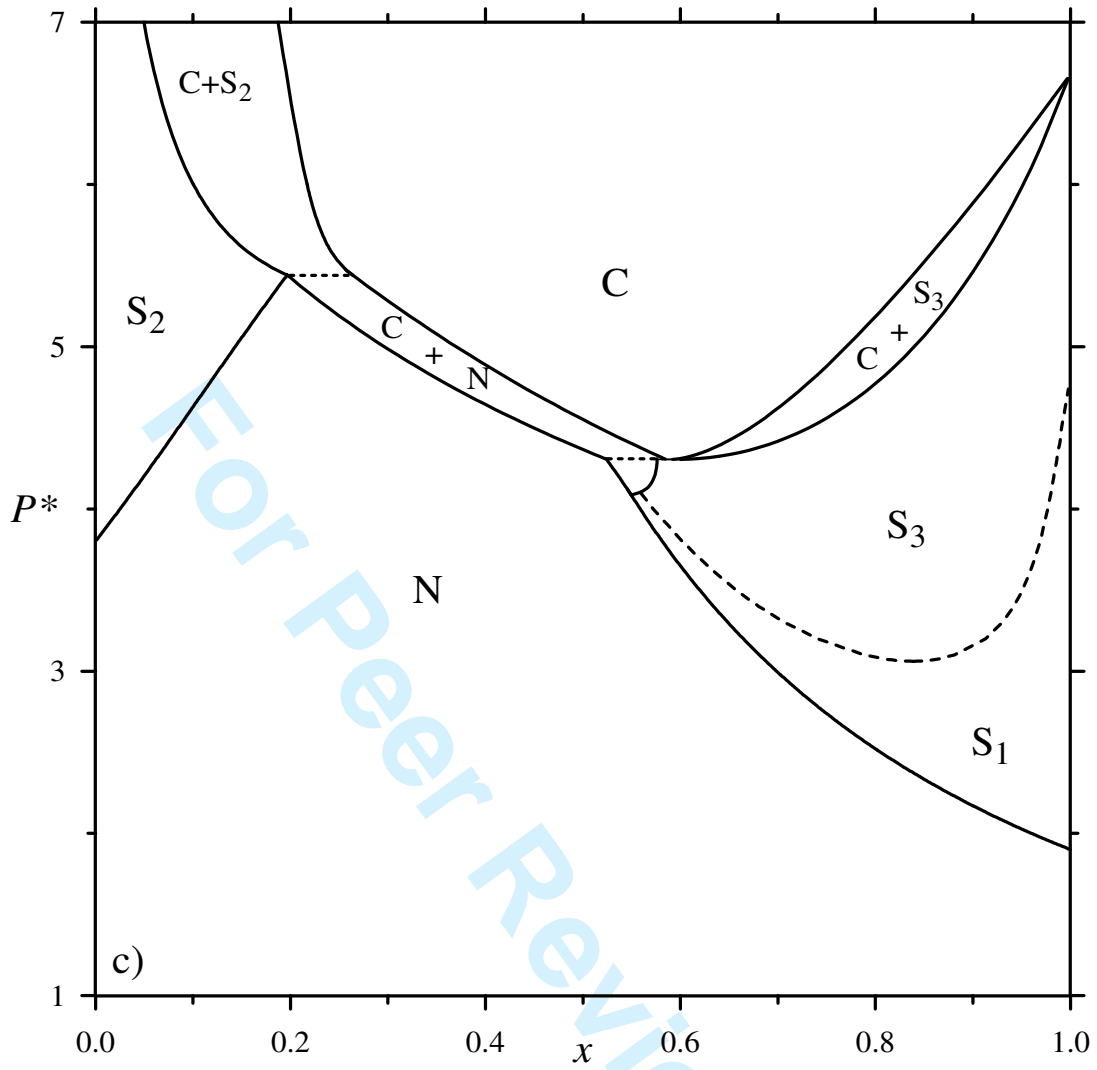


Figure 7 c)

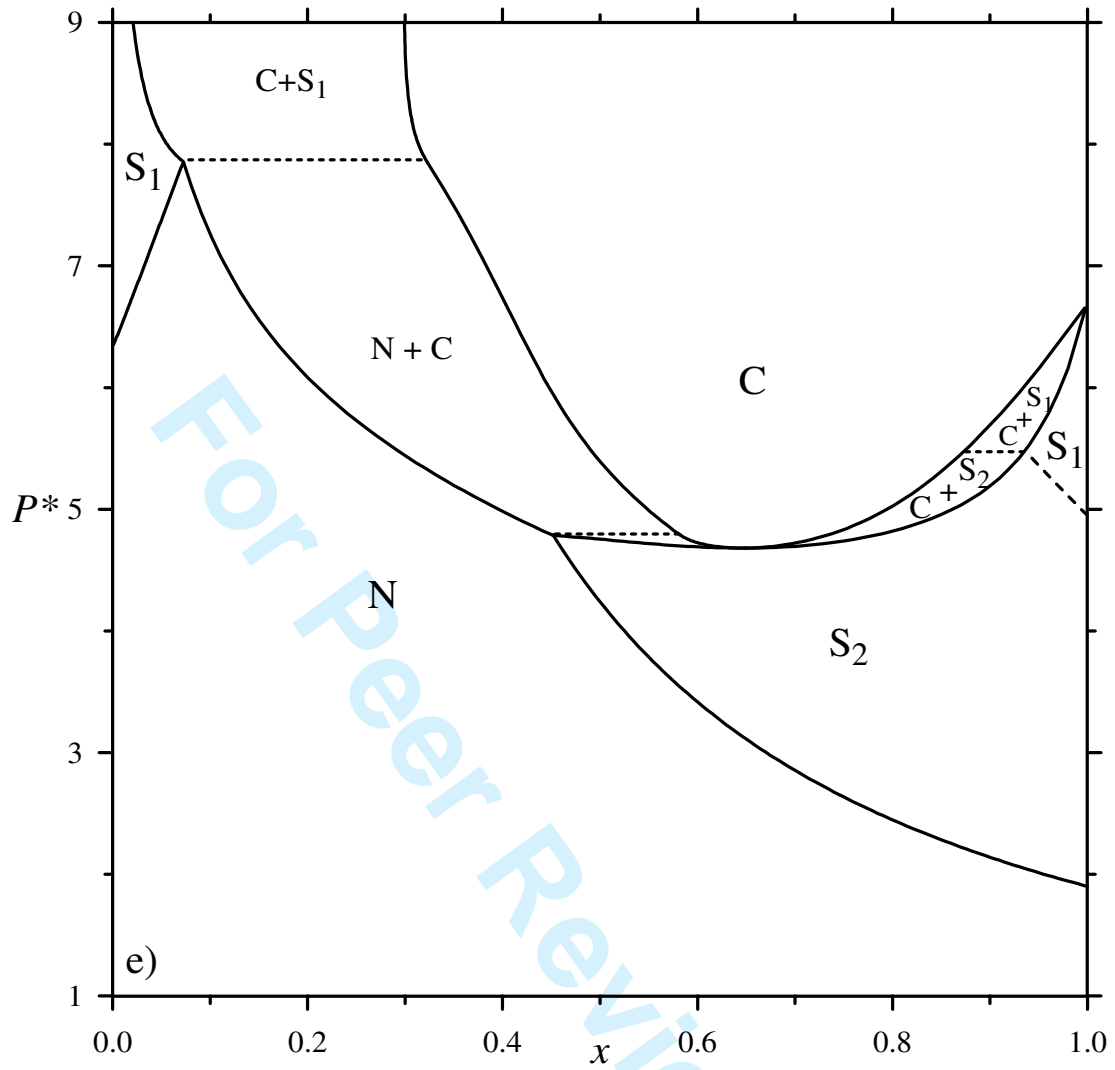


Figure 7 e)

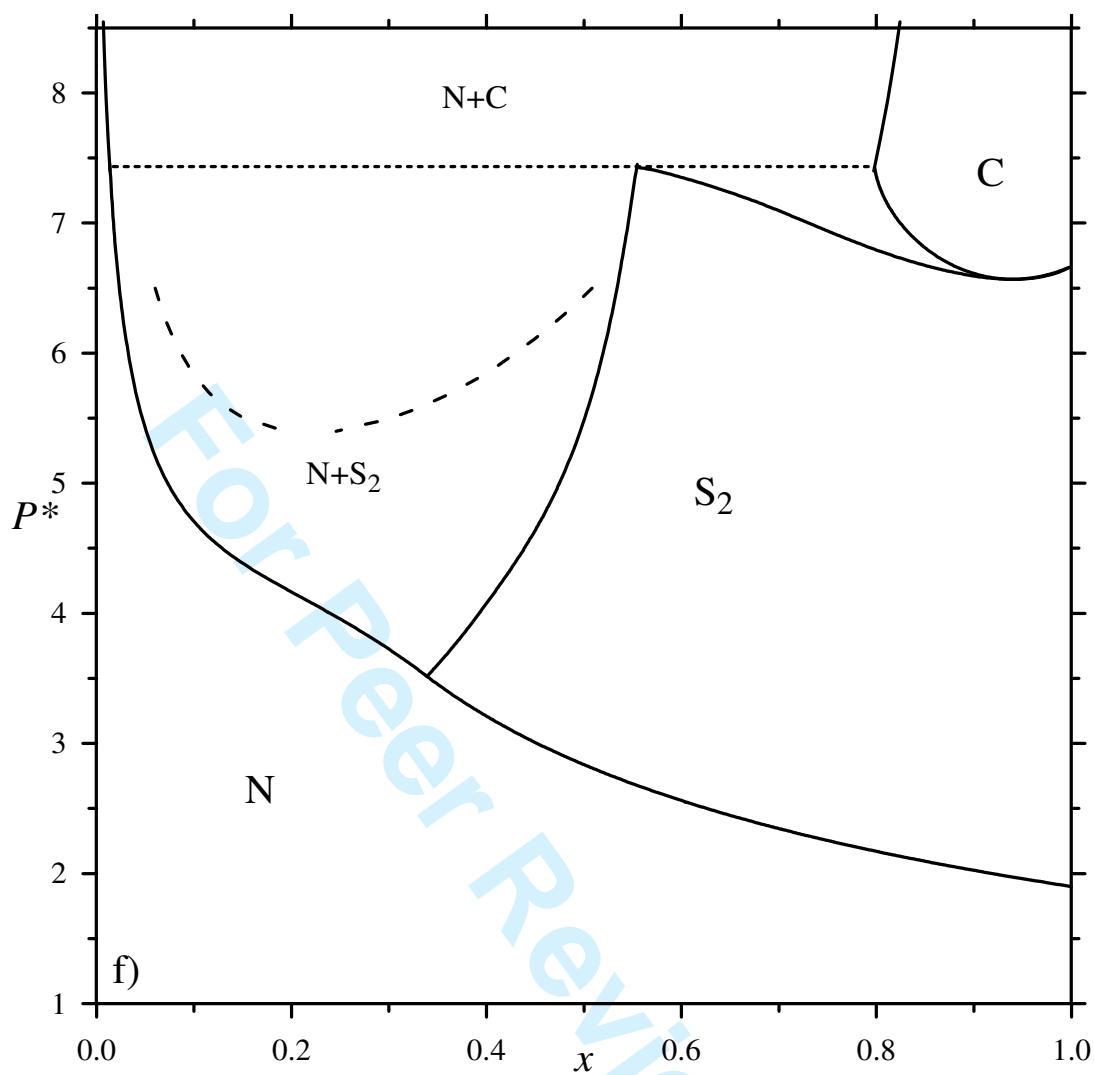


Figure 7 f)