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ABSTRACT

We have experimentally obtained force – elongation, F(w), curves for the uniaxial extension/compression of single cylindrical bubbles and bubble clusters bounded by two horizontal walls at a variable separation w. We have studied the effect of the elongation rate on F(w) of cylindrical bubbles and the changes in F associated with instabilities and with topological transformations that occur during deformation of bubble clusters.

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1. Introduction

At low enough strains liquid foams deform elastically. The liquid films stretch or contract reversibly and the size of the Plateau borders (PB) changes but the topology is preserved, *i. e.* each bubble remains surrounded by the same bubbles [1, 2]. Elastic deformation of a foam is accompanied by liquid flow in the films and Plateau borders (and also in the PB quadruple junctions) and because flow is dissipative, the term viscoelastic is more appropriate for the foam deformation regime in which no

topological changes occur. Thus there are strain rate effects in foam deformation. One of the purposes of this paper is to report on experiments aimed at studying these rate effects in the uniaxial deformation of a cylindrical bubble confined by two parallel walls; we obtained force – displacement curves for various displacement rates. Recently, considerable attention has been given to the effects of viscous drag on the flow of foams [3-7]. Dissipative forces are associated with the flow of liquid in the films and Plateau borders and with the drag of wall Plateau borders as they slide along the confining walls as discussed in the early works of Bretherton [8], Schwartz and Princen [9] and Reinelt and Kraynik [10]. Our results may provide a good test for theories of foam rheology that incorporate viscous drag.

At higher strains topological changes occur in a foam, either locally, involving a small number of bubbles, or in avalanches which affect a large number of bubbles in succession [1, 11-13]. The topological changes give rise to discontinuities or jumps in the applied force, the amplitude of which depends on the number of elementary T1 topological changes in the avalanches. We report on foam deformation experiments in which we observed these features in many-bubble three-dimensional (3D) clusters.

Finally we also obtained force – displacement curves for the uniaxial compression of a 3D bubble cluster consisting of two equal bubbles one on top of the other (twin bubble). These exhibit a symmetry breaking transition with no change in topology followed by a topological change. This cluster was studied in detail by Bohn [14] and subsequently by Fortes *et al.* [15].

2. EXPERIMENTAL

We used a Wilhelmy balance to measure the force *F* required to deform 3D bubble clusters bounded by two horizontal walls, the separation *w* of which could be varied at a constant rate, $v = |\dot{w}|$. The Wilhelmy balance is commonly used for the measurement of the dynamic surface tension of liquids (*e.g.* [16]).

The bubble systems tested were a single cylindrical bubble, a twin bubble (two bubbles of the same volume, one on top of the other) and many-bubble clusters. The bubbles were bounded by a perspex plate at the top, suspended from the arm of the balance, and, in most cases, a liquid pool (the commercial detergent solution used in the preparation of the bubble clusters) at the bottom. The surface tension $\gamma_{\rm L}$ of the bulk liquid solution measured by the sessile drop method was $\gamma_{\rm L} = 35.0 \,\mathrm{mN}\,\mathrm{m}^{-1}$. Experiments with a horizontal plate replacing the pool were also made for single bubbles, but the stability of the bubbles was so poor that only very small variations in *w* could be achieved. The films contact the plates and the pool at approximately 90° and are free to slide on both of them.

The cylindrical bubble (Fig. 1(a)) was prepared from a hemispherical bubble formed on the top plate by blowing a volume V of air with a syringe into a small drop of the detergent solution sitting on the plate. The hemispherical bubble was then forced to contact the liquid pool (or plate) below producing a cylindrical bubble of volume V.

The preparation of a twin bubble required a special procedure (direct preparation from two bubbles did not work): three bubbles of the same volume, were blown with a syringe on the top plate to form a cluster which was then forced to contact the liquid pool, producing a layer with three sandwiched bubbles. By increasing the plate/pool separation one of the bubbles jumped to a second layer. Finally one of the two bubbles in the other layer was destroyed by means of a metal pin, thus forming the twin bubble configuration of Fig. 1(b) with a horizontal inter-bubble film.

Many-bubble clusters were prepared by blowing 10 to 20 bubbles of nearly the same volume, around 30 mm^3 , in a pile on the plate. The cluster was then forced to contact the pool originating a multilayer cluster bounded by the pool surface and the plate above (Fig. 1(c)).

Insert Figure 1

In all experiments the top plate was suspended from the arm of the balance and the (vertical) force was set to zero (F = 0) before forming the bubble cluster. The separation w was then increased or decreased at a constant rate $v = |\dot{w}|$ thus causing uniaxial deformation of the cluster. The velocities available were (in mm min⁻¹): 1, 5, 10, 20 and 30. The applied force F was recorded every second (for any velocity), from which F(w) was derived. All data refers to a bubble or cluster bounded by a liquid pool at the bottom.

3. RESULTS AND DISCUSSION

3.1. Single cylindrical bubble

Under static conditions (v = 0) the force F on the plate is

$$F_0 = F(v=0) = \pi R \gamma_0 \tag{1}$$

where *R* is the radius of the bubble cross-section and γ_0 is the (static) film tension, both being assumed as uniform along the bubble. The force F_0 is the sum of a force $2\pi R \gamma_0$ due to the contractile tendency of the film and an opposite force $\pi R \gamma_0$ that results from the pressure difference γ_0/R across the film, acting on the area πR^2 . Since the bubble volume $V = \pi R^2 w$, we can write equation (1) as

$$\frac{F_0}{\gamma_0 V^{1/3}} = \pi^{1/2} \left(\frac{w}{V^{1/3}}\right)^{-1/2} \qquad . \tag{2}$$

This equation can also be derived from $F_0 = \frac{dE}{dw}$ where *E* is the bubble surface energy given by $E = 2\pi R w \gamma_0 = 2(\pi V)^{1/2} \gamma_0 w^{1/2}$. We measured the static force F_0 for bubbles of two volumes *V* (2 and 4 cm³) at various *w* for each volume. Figure 2 shows plots of $\frac{F_0}{V^{1/3}}$ as a function of $\left(\frac{w}{V^{1/3}}\right)^{-1/2}$ for the two bubble volumes. The two plots coincide and lead to $\gamma_0 = 73.1 \text{ mN m}^{-1}$. This is, as expected, about twice the bulk liquid surface tension γ_1 .

Insert Figure 2

Figures 3(a) and 3(b) show experimental force – displacement, or F(w) curves for cylindrical bubbles of volumes $V = 2 \text{ cm}^3$ and $V = 4 \text{ cm}^3$ deformed at three of the five deformation rates v available. The curves were obtained with different bubbles of the same volume. The curves of Figs. 3(a) and 3(b) are drawn by connecting the (F, w)points read off the balance. The force F is always tensile and decreases with increasing w. At fixed w, the force increases with increasing deformation rate v, both in elongation and in compression, the force increment for a given change in v being nearly independent of w.

We found that the F(w) curves in elongation-compression coincide. The sliding velocity $v_{\text{slid}} = \left| \frac{\mathrm{d}R}{\mathrm{d}t} \right|$ of the Plateau borders and liquid meniscus relates to the deformation velocity $v = \left| \frac{\mathrm{d}w}{\mathrm{d}t} \right|$ by

$$v_{\rm slid} = \left(\frac{V}{4\pi w^3}\right)^{1/2} v \tag{3}$$

since $V = \pi R^2 w$ is constant. For the same V, v and w the absolute value of the sliding velocity is the same. Thus, we expect reversibility of the F(w) curve for a given v. It should be noted that irreversibility in foam deformation is due to topological neighbour switching events as in the work of Jiang et al. [12] on 2D foams. These events are absent in the deformation of a single bubble.

Insert Figure 3

When the liquid pool at the bottom was replaced by a perspex plate, the measured force for the same V, w and v, was slightly larger i. e., drag forces are larger with a liquid pool. This is probably due to the replacement of a Plateau border at the bottom by a liquid meniscus, which increases the film thickness and the size of the Plateau border at the plate. Note that for v = 0 the (static) force is the same for the platepool and plate-plate boundaries.

We also carried out tests in which the deformation rate v was suddenly changed during deformation of a cylindrical bubble. Examples of the resulting F(w) curves are in Fig. 3(c) for rate reductions from v = 30 and 10 mm min^{-1} to $v = 1 \text{ mm min}^{-1}$ in the Page 7 of 26

elongation of a bubble with $V = 2 \text{ cm}^3$. A transient is observed following the velocity change, analogous to the transient at the onset of deformation (change from v = 0 to a non-zero v) which can be detected in the curves of Figs. 3(a) and (b).

In Figs. 4(a) and 4(b) we show the experimental data (excluding the transient in force) obtained for bubbles of $V = 2 \text{ cm}^3$ and $V = 4 \text{ cm}^3$, respectively, deformed at various elongation rates, in the form of a plot of $\frac{F}{\pi R \gamma_0} = \frac{F}{F_0}$ as a function of $\frac{w}{V^{1/3}}$. The radius *R* is obtained from $V = \pi R^2 w$. The horizontal segments on the left of Figs. 4(a) and 4(b) are for the average $\frac{F}{\pi R \gamma_0}$ for each elongation rate. We used these average values to determine the exponent *n* in the relation between the excess force per unit circumferential length and the elongation velocity

$$\frac{F - F_0}{2\pi R \gamma_0} = \left(\frac{v}{v^*}\right)^n \tag{4}$$

where v^* is a constant velocity. The log – log plots of Fig. 4(c) give for the best fit exponent n = 1.02 for both volumes (straight lines in Fig. 4(c)) and the constant $v^* = 36.3 \,\mathrm{mm \, s^{-1}}$ for $V = 2 \,\mathrm{cm^3}$ and $v^* = 22.2 \,\mathrm{m \, s^{-1}}$ for $V = 4 \,\mathrm{cm^3}$.

Insert Figure 4

Bretherton [8] predicted a power law relation with exponent n = 2/3 between the sliding friction force F_{slid} per unit length of a PB and the sliding velocity v_{slid} (both parallel to the plate): $F_{slid} \propto v_{slid}^n$. This is close to the exponent *n* obtained in experiments by Cantat *et al.* [3] on foam sliding on a plate. In our experiments sliding is induced by a vertical excess force $(F - F_0)$ and the velocity *v* is vertical. The sliding velocity v_{slid} relates to *v* by equation (3), but the relation between F_{slid} and the excess force $(F - F_0)/2\pi R$ is not known. Besides, the mechanism of dissipation in our experiments is not exclusively sliding of the PB at the top plate. It is therefore not surprising that we obtain an exponent $n \cong 1$ in equation (4), which deviates from that predicted by Bretherton [8].

3.2. Twin bubble

At large separations, w, of the confining walls the inter-bubble circular film in a twin bubble is horizontal (Fig. 1(b)) and joins the curved films at 120° under equilibrium. As w decreases to a critical w_0^* for which F = 0, a buckling instability arises at which the inter-bubble film starts tilting; its tilt relative to the confining walls increases as w is further decreased until at w_1^* the inter-bubble film touches the confining walls and a topological transition occurs whereby the film further rotates to a configuration with two vertical cylindrical bubbles contacting at a vertical planar film (see Fig. 1(b)) which we term the vertical twin bubble. This buckling instability, under static conditions, was analysed in detail by Bohn [14], who found $w_0^* = 0.886V^{1/3}$ and $w_1^* = 0.767V^{1/3}$ for a twin bubble with V the volume of each bubble. Bohn also found that during the (static) buckling transition, *i.e.* for w between w_0^* and w_1^* , the force F = 0. For $w < w_1^*$, the vertical twin bubble forms and the force under static conditions is given by

$$F = \lambda V^{1/2} \gamma_0 w^{-1/2} \qquad \qquad \lambda = \left(\frac{8\pi}{3} + \sqrt{3}\right)^{1/2} \cong 3.1796 \qquad (5)$$

which can be derived along the same lines as equation (2), noting that the radius of the curved films, R', relates to the cross-sectional area A of each bubble by $R' = \frac{2}{\lambda} A^{1/2}$ (angles of 120° at film junctions).

In Fig. 5 we show an experimental force – displacement curve for a twin bubble $(V = 1 \text{ cm}^3)$ compressed at 5 mm min⁻¹. The F(w) plot has two main branches (full lines): the small F (large w) branch refers to the twin bubble, while the large F (small w) branch refers to the vertical twin bubble. For the twin bubble dF/dw > 0 and the force reaches F = 0 at $w_0^* \cong 0.8V^{1/3}$ (Fig. 5) in good agreement with the value predicted by Bohn [14] for the static twin bubble referred to above. While the planar inter-bubble film rotates to reach the confining horizontal walls, the force remains at zero (Fig. 1(b))

and w changes from w_0^* to w_1^* . On further decreasing w, the force rises from zero to 2.6 mN (dashed line in Fig. 5) and the vertical twin bubble forms (Fig. 1(b)). The duration of this topological transition is about 6s. The force F on the confining walls, under static conditions is given by equation (5). For $w = w_1^*$, equation (5) gives F close to the experimental value 2.6 mN. Following this jump, the force increases with decreasing w (in the low w branch). We found that $F \propto w^{-1/2}$ in this branch, as for static deformation (equation (5)).

Insert Figure 5

3.3. Many-bubble cluster

Figure 6 shows force – time data points for a fairly monodisperse 3D cluster with 10 bubbles (bubble volume V around 30 mm³), confined by a plate and a pool surface, deformed in successive elongation – compression cycles, with the applied force F varying over a 4 mN range. The displacement rate in this test was $v = 5 \text{ mm min}^{-1}$. Similar curves were obtained with other many-bubble clusters but we did not study the effect of v. The dF/dt > 0 regions of the curve correspond to compression ($\dot{w} < 0$) and those with dF/dt < 0 to elongation ($\dot{w} > 0$). The curve of Fig. 6 resembles those obtained in simulations of two-dimensional bubble clusters in [1].

Insert Figure 6

The force – time F(t) data of Fig. 6 show sudden force changes ΔF associated with topological transitions. These occur when there is a decrease (in compression) or increase (in elongation) in the number of layers in the cluster (from 1 to 3 layers) due to bubble rearrangements (isolated or in avalanches). Between the jumps the foam deforms elastically. For example, at large F (typically small w) there are relatively large intervals of w with no jumps in F, which are associated with pure elastic deformation of the one-layer cluster [11], with F varying approximately linearly with $w^{-1/2}$, as for a single cylindrical bubble. The average slope |dF/dw| of these regions is around

 0.9 mN mm^{-1} . It is worth noting that under extension the bubble monolayer survives past the force (at A in Fig. 6) where it first appears in compression (at A'). The fact that the first peak in *F* occurs at larger *F* than the other two, is probably due to bursting of a few bubbles at the cluster free surface.

The discontinuities in *F* at lower *F*'s are due to neighbour switching topological changes, which alter the number of bubble layers and the number of bubbles in each layer. Most values of ΔF associated with topological changes are around 0.1mN $(\Delta F/\gamma_0 V^{1/3} \cong 0.5)$, but a few are much larger (up to 0.9mN), probably associated with avalanches of topological transitions. The number of topological transitions when *w* changes by $\Delta w = 8.3 \text{ mm} (\Delta t \cong 100 \text{ s})$ is between 3 and 6. The variation of *w* per topological change is thus 1.4 - 2.8 mm, close to the average bubble diameter.

4. SUMMARY

We have reported on experiments conducted with a Wilhelmy balance aimed at obtaining force – displacement F(w) curves of foams under uniaxial deformation. We studied the effect of the deformation rate on the F(w) curves for a single cylindrical bubble and attempted to fit the data to a power law relating force and deformation rate. We have also studied the effect on F(w) of topological transitions and symmetry breaking instabilities that occur during the deformation of foam clusters. These lead to discontinuities in the force F or in dF/dw, separating regions of continuous elastic deformation.

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Figure captions

Figure 1 – Side views of: (a) Single cylindrical bubble; (b) Twin-bubble: "horizontal" (initial configuration), buckled and "vertical" configurations; (c) Many-bubble cluster with three layers of bubbles. The Plateau borders and the liquid menisci are not shown.

Figure 2 – The measured reduced static force $\frac{F_0}{V^{1/3}}$ for cylindrical bubbles of volume $V = 2 \text{ cm}^3$ (\blacklozenge) and $V = 4 \text{ cm}^3$ (\blacksquare) as a function of $\left(\frac{w}{V^{1/3}}\right)^{-1/2}$; w is the height of the bubble.

Figure 3 – Force (*F*) – bubble height (*w*) curves obtained in tensile tests at different elongation rates: (—) 30 mm min⁻¹, (---) 10 mm min⁻¹, and (…) 1 mm min⁻¹ for cylindrical bubbles of volume: (a) $V = 2 \text{ cm}^3$ and (b) $V = 4 \text{ cm}^3$. (c) F(w)curves with sudden deformation rate change undertaken at w = 12 mm for bubbles with $V = 2 \text{ cm}^3$; the initial rates were: (—) 30 mm min⁻¹ and (---) 10 mm min⁻¹; the final rate was 1 mm min⁻¹ in both cases. In (a), (b) and (c) the curves are fits to the experimental points, which are shown (squares) only for $v = 30 \text{ mm min}^{-1}$ in (a).

Figure 4 – The reduced force $\frac{F}{\pi R \gamma_0} = \frac{F}{F_0}$ to deform a cylindrical bubble of radius Rand volume $V = \pi R^2 w$, as a function of $\frac{w}{V^{1/3}}$ for the various elongation rates used: (\Box) 30 mm min⁻¹, (\diamond) 20 mm min⁻¹, (\blacktriangle) 10 mm min⁻¹, (\blacksquare) 5 mm min⁻¹ and (\diamond) 1 mm min⁻¹. w is the bubble height and γ_0 is the static film tension. The horizontal segments indicate the average values for each v. Bubble volumes: (a) $V = 2 \text{ cm}^3$ and (b) $V = 4 \text{ cm}^3$. (c) Log – log plot of the force increment $\frac{F - F_0}{2\pi R \gamma_0}$ required to deform a cylindrical bubble at an elongation rate v, for the two bubble volumes: $(\spadesuit)V = 2 \text{ cm}^3$ and $(\blacksquare)V = 4 \text{ cm}^3$. F_0 is the static force for v = 0.

- Figure 5 Force (F) cluster height (w) curve obtained in a compression test of a twin bubble cluster $(V = 1000 \text{ mm}^3)$ at a compression $v = 5 \text{ mmmin}^{-1}$, starting at w = 16 mm. Buckling occurs in the narrow interval where F = 0. The force jump from F = 0 to F = 2.6 mN (dashed line), is associated with the topological change at the end of buckling to a vertical twin bubble (see Fig. 1(b)). Experimental points are not shown. The insert shows a zoom of the curve region around F = 0.
- Figure 6 Force (F) time (t) data points obtained in extension compression cycles of a fairly monodisperse three-dimensional 10-bubble cluster (average bubble volume $\cong 30 \text{ mm}^3$). The top, smoother regions correspond to elastic deformation of a single layer of bubbles. Subsequently bubbles jump to build a second layer (starting at A) and then a third layer (at B) in extension and viceversa in compression.

























